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RESEARCH MEMORANDUM

THE HYDRODYNAMIC FORCE CHARACTERISTICS OF STREAMLINE
BODIES OF REVOLUTION HAVING FINENESS RATIOS OF 6,
9, AND 12 WITH AND WITHOUT CHINE STRIPS

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SUMMARY

Hydrodynamic force characteristics, as determined by general tank tests, are given for three streamline bodies of revolution equipped with chine strips and having fineness ratios of 6, 9, and 12, respectively. In addition, these force characteristics are given for the same bodies with the chine strips removed and, to a limited extent, for the same bodies with the tail cones removed.

Hydrodynamic resistance, pitching moment, wetted length, and height of the model above the water surface are tabulated for a range of trim, load, and speed. In order to facilitate analysis, the curves are plotted using hydrodynamic coefficients which generally group along single curves for all speed-load combinations.

INTRODUCTION

The usefulness of hydro-skis as a means of obtaining high-speed, water-based airplanes with a minimum of compromise to their aerodynamic performance was presented in reference 1. In that investigation, the hydro-skis were incorporated in a streamline fuselage because such a fuselage offers aerodynamic and structural advantages. It was demonstrated in reference 2 that the hydrodynamic performance of this configuration was influenced to a large degree by the hydrodynamic characteristics of the fuselage. The hydrodynamic performance of this fuselage equipped with hydro-skis was greatly improved by the addition of narrow longitudinal strips on the lower rear portion of the fuselage. Other investigations (refs. 3 to 7) also indicate that simple modifications to streamline fuselages greatly improve their usefulness as fuselages of water-based airplanes. These investigations indicate that full-length, narrow strips located port and starboard of the lower profile line would be generally the most desirable configuration.

The primary purpose of this paper is to provide general hydrodynamic force data on streamline bodies of revolution of fineness ratios 6, 9, and 12 with and without chine strips. Since the data obtained may prove useful in the design of hydrodynamic bodies other than fuselages for ski-equipped seaplanes, the scope of the investigation was extended to speeds beyond the current ski-emergence speeds of such aircraft. Tests were made on three models having the same nondimensional offsets and the same volume but differing in fineness ratio. Corresponding tests were also made on the models with the strips removed. In addition, limited tests were made on the models equipped with chine strips but with a small portion of the aft end removed to simulate a fuselage with jet exhaust. Values of resistance, trimming moment, wetted length, and height of the model above the water surface are presented for a wide range of trim, load, and speed.

SYMBOLS

C_{D_Q} drag coefficient based on volume of fuselage,

$$\frac{R}{\frac{1}{2}\rho Q^2/3V^2} = \frac{2C_{R_Q}}{(C_{V_Q})^2}$$

C_{D_Δ} drag coefficient based on load,

$$\frac{R}{\frac{1}{2}\rho(\Delta/w)^2/3V^2} = \frac{2C_{R_Q}}{(C_{\Delta_Q})^{2/3}(C_{V_Q})^2}$$

C_{L_Q} lift coefficient based on volume of fuselage,

$$\frac{\Delta}{\frac{1}{2}\rho Q^2/3V^2} = \frac{2C_{\Delta_Q}}{(C_{V_Q})^2}$$

C_{M_Q} trimming-moment coefficient based on volume of fuselage,

$$\frac{M}{wQ^{4/3}}$$

C_{R_Q} resistance coefficient based on volume of fuselage

$$R/wQ = 0.0467R$$

C_{V_Q} speed coefficient based on volume of fuselage,

$$\frac{V}{\sqrt{gQ^{1/3}}} = 0.211V$$

$C_{V\Delta}$

speed coefficient based on load,

$$\sqrt{\frac{V}{g\left(\frac{\Delta}{w}\right)^{1/3}}} = \frac{C_{VQ}}{\left(C_{\Delta Q}\right)^{1/6}}$$

 $C_{\Delta Q}$

load coefficient based on volume of fuselage,

$$\frac{\Delta}{wQ} = 0.0467\Delta$$

D

maximum diameter of fuselage, ft

g

acceleration of gravity, 32.15 ft/sec²

h

height of center-line midpoint (as located on model with tail cone) above free-water surface, ft

L

length of model, ft

l

wetted length measured from aft end of the model to intersection of heavy-spray line with lower profile line, ft

M

trimming moment about center-line midpoint (as located on model with tail cone), lb-ft (14.9 C_{M_Q})

n

fineness ratio of fuselage, L/D

Q

volume of basic models, 0.338 cu ft

R

resistance, lb

V

speed, ft/sec

w

density of water, 63.3 lb/cu ft

x

distance from center of pressure to aft end of fuselage, ft

 Δ

load on water, lb

ρ

mass density of water, 1.97 slugs/cu ft

τ

angle of trim of center line, deg

DESCRIPTION OF MODELS

The three models tested were streamline bodies of revolution of fineness ratios 6, 9, and 12. The nondimensional offsets presented in table I were identical for all models and are the same as those for the family of fuselages tested in reference 8. For all three models, the centroid of the volume was $0.46L$ from the nose, the volume Q was 0.338 cubic foot. For the offsets in table I the ratio of the volume of a model to the volume of the cylinder formed by its length and maximum diameter is 0.591 regardless of size or fineness ratio.

Pertinent dimensions and characteristics of the models are compared in figure 1. Narrow, full-length chine strips were located 45° from the lower profile line. In order to simulate a fuselage with jet exhaust, the aft ends were made removable aft of the station where the cross-sectional area of the fuselages were 0.073 square foot. The volume of these removable cones was 0.001, 0.002, and 0.003 cubic foot for fineness ratios 6, 9, and 12, respectively. Transverse lines, 1 inch apart, were painted on the underside of each model for measuring wetted length (fig. 2).

APPARATUS AND PROCEDURE

Tests were conducted with the small model towing gear of Langley tank no. 2 (fig. 3). A V-shaped wind screen, 3 feet wide with an included angle of 90° and extending to within less than an inch from the water surface, was placed directly in front of the model. High-speed runs made with the models just above the water surface showed that the screen reduced aerodynamic forces to a negligible value.

The models with chine strips were tested at fixed trims of 0° , 4° , 8° , 12° , 16° , and 20° at constant speeds and loads. The load-speed range for these tests is shown in figure 4. Tests were also made on the models with the chine strips removed but were restricted to low speeds because of excessive forces and spray. Additional tests were made on the models with chine strips but with the tail cones removed. These tests were limited to a trim of 8° and load coefficients of 0.2 and 0.4.

Measurements were made of resistance, trimming moment, wetted length, and height of the center-line midpoint above the free-water surface. Resistance was measured by a strain-gage dynamometer, which indicated the horizontal force on the towing staff. Trimming moment was measured by a strain-gage dynamometer, which indicated the moment about the midpoint of the center line of the model. In the case of the model with the tail cone removed, the center-line midpoint was the same distance from the

nose as that for the model of the same fineness ratio with the tail cone attached. Center of pressure, as calculated from the measured forces and moments, is the point where the resultant of the hydrodynamic forces intersected the center line.

Wetted length was determined from underwater photographs, as illustrated in figure 2. It was measured along the center line from the aft end of the model to the station at which the heavy-spray line intersected the lower profile line.

The measurements are believed to be accurate within the following limits:

Load, lb	±0.1
Resistance, lb	±0.1
Trimming moment, lb-ft	±0.3
Wetted length, ft	±0.02
Height, ft	±0.01
Trim, deg	±0.1
Speed, fps	±0.2

RESULTS AND DISCUSSION

The data for the models of fineness ratios 6, 9, and 12, with chine strips, are given in tables II, III, and IV and are plotted in figures 5 and 6, 7 and 8, and 9 and 10, respectively. Spray photographs are shown in figure 11. The data for the models of fineness ratios 6, 9, and 12, without chine strips, are given in tables V, VI, and VII, and are plotted in figures 12, 13, and 14, respectively. Spray photographs are shown in figure 15. The data for the models of fineness ratios 6, 9, and 12, with chine strips, but with the tail cones removed, are given in tables VIII, IX, and X, and are plotted in figures 16, 17, and 18. Spray photographs are shown in figure 19.

Method of Data Presentation

The data in each table are presented in three groups. In the first four columns, the data are presented as hydrodynamic Froude scale coefficients. These coefficients are similar to conventional hydrodynamic Froude coefficients, except that the cube root of the total volume $Q^{1/3}$ is used as the characteristic linear dimension, rather than the beam. Since the volume is constant in this case, the use of $Q^{1/3}$ provides a direct comparison of the three fineness-ratio hulls.

In the next five columns the data are presented as hydrodynamic coefficients which, under low-speed displacement conditions, generally group along a single curve for all the speed-load combinations investigated. These coefficients and ratios are based on the cube root of the displaced volume $(\Delta/w)^{1/3}$ as the characteristic linear dimension because, under displacement conditions, buoyancy forces predominate.

In the last five columns the data are presented as hydrodynamic coefficients which, under high-speed planing conditions, generally group along a single curve for all the speed-load combinations investigated. These coefficients also are based on the characteristic linear dimension $Q^{1/3}$ and are analogous to fundamental aerodynamic coefficients because, under planing conditions, dynamic forces predominate. The lengths, x , l , and h , are expressed as ratios of overall length L to facilitate comparisons. The value of L for the models without tail cones is, of course, less than the value of L for the corresponding models with tail cones.

These "collapsing" coefficients, which are generally independent of speed and load, were obtained by the methods of references 9, 10, and 11.

In order to facilitate analysis, the collapsing coefficients were used exclusively in plotting the data. The displacement coefficients were plotted against the Froude speed coefficient $C_{V\Delta}$ and the planing coefficients against the dynamic lift coefficient C_{LQ} . At a given trim, the planing range for each load tested was assumed to extend up to C_{LQ} (or down to a speed) beyond which the C_{DQ} data began to deviate from the single curve. At all lower speeds, displacement conditions should be applied. Since there is no well-defined boundary between displacement and planing, the ranges of $C_{V\Delta}$ and C_{LQ} are overlapped, particularly for the lower values of $C_{\Delta Q}$ and τ .

General Characteristics

At very low trims the streamline bodies with chine strips had an increasing tendency to suck under the water surface with increase in C_V . However, this tendency decreased with increase in fineness ratio Δ . At 0° trim (figs. 5(a), 7(a), and 9(a)) the models for all three fineness ratios sucked under and no data were obtained for planing conditions. At 4° trim the fineness-ratio-6 model (fig. 5(b)) sucked under but only for a short range of C_V .

Under displacement conditions (figs. 5, 7, and 9), the drag coefficients $C_{D\Delta}$, for a given trim and fineness ratio, generally grouped along a single curve for all loads with a small and fairly uniform scatter.

Center-of-pressure ratio $\frac{x}{(\Delta/w)^{1/3}}$ and wetted-length ratio $\frac{l}{(\Delta/w)^{1/3}}$

also grouped along a single curve for the heavier loads, with very little scatter, but, with decrease in trim or fineness ratio, individual curves were required for an increasing number of the lighter loads. The height ratios $\frac{h}{(\Delta/w)^{1/3}}$ did not collapse at all.

With increase in speed coefficient $C_{V\Delta}$, the drag coefficient $C_{D\Delta}$ increased rapidly to a peak value at $C_{V\Delta} \approx 1.2$. In a more conventional plot of the Froude scale coefficients, C_{RQ} against C_{VQ} , the resistance corresponding to the peak at $C_{V\Delta}$ of about 1.2 would appear only as a slight protuberance on the upward slope of the curve. On the other hand, the resistance peak normally obtained in such a conventional plot appears on the plots of $C_{D\Delta}$ against $C_{V\Delta}$ only as a slight protuberance on the downward slope of that curve approximately at values of C_V where planing forces become predominant.

Under planing conditions (figs. 6, 8, and 10), the drag coefficients C_{DQ} , as well as the ratios for center of pressure x/L , wetted length l/L , and height h/L , for a given trim and fineness ratio, all grouped along single curves for all loads.

The simultaneous side and bottom photographs of the models with chine strips (fig. 11) show that the spray became heavier with increase in speed until planing began; after which the amount of spray decreased.

Effect of Trim

The effect of trim on the hydrodynamic characteristics of the models with chine strips is shown in figures 20, 21, and 22 for fineness ratios 6, 9, and 12, respectively. Data for resistance, center of pressure, ratio of center of pressure to wetted length, wetted length, and height of the center-line midpoint are plotted against $C_{V\Delta}$ and C_{LQ} for constant trims in parts (a), (b), (c), (d), and (e), respectively, of these figures. For trims at which more than one curve had to be drawn in figures 5 to 10, the curve for $C_{\Delta Q} = 0.3$ was used in figures 20, 21, or 22 as being representative.

Resistance.- For a given speed coefficient $C_{V\Delta}$, the drag coefficient $C_{D\Delta}$ generally increased with trim up to values of $C_{V\Delta}$ varying from about 3.5 for fineness ratio 6 to about 4.0 for fineness ratio 12. The plots of the drag coefficient C_{DQ} against the lift coefficient C_{LQ} are approximately parallel curves for all trims. For a given C_{LQ} , C_{DQ} generally decreased with increase in trim up to a best trim (trim for minimum resistance). For fineness ratio 6, best trim appeared to be just above 20° . For fineness ratio 9, best trim was between 16° and 20° ; and for fineness ratio 12, between 12° and 16° .

Center of pressure.- For a given $C_{V\Delta}$, the curves of the center-of-pressure ratio $\frac{x}{(\Delta/w)^{1/3}}$ show a slight rearward movement of the center of pressure with increase in trim. For a given C_{LQ} , the curves of the center-of-pressure ratio x/L show that the center of pressure moved rearward rapidly with increase in trim. At low values of C_{LQ} the variation in center of pressure with trim became considerable and at small trims, the center of pressure on the lower fineness-ratio models was calculated to be forward of the wetted portion of the model (figs. 20(c), 21(c), and 22(c)). Such calculated values indicate that negative pressures were acting near the rear portion of the wetted area.

Wetted length.- For a given $C_{V\Delta}$, the wetted-length ratio $\frac{l}{(\Delta/w)^{1/3}}$ decreased with increase in trim. For a given C_{LQ} , the wetted-length ratio l/L also decreased with increase in trim. At the low trims, l/L still had a substantial value as C_{LQ} approached zero.

Height.- For a given $C_{V\Delta}$, the height ratio $\frac{h}{(\Delta/w)^{1/3}}$ increased with trim. For a given C_{LQ} , the height ratio h/L also increased with trim. The curve for fineness ratio 6 at 4° trim shows how the model sucked under at a $C_{V\Delta}$ of about 4.5, while at higher trims the model rose with increase in $C_{V\Delta}$. The curve for fineness ratio 9 at 4° trim shows a tendency to suck down at a $C_{V\Delta}$ of about 6.5.

Spray.- The side photographs of the fineness-ratio-9 model in figure 23 show that an increase in trim resulted in considerable reduction in spray. This effect increased with decrease in fineness ratio.

Effect of Fineness Ratio

The effect of fineness ratio on the hydrodynamic characteristics of the streamline bodies with chine strips is shown in figure 24 for best trim and in figure 25 for the condition where the hydrodynamic trimming moment M about the midpoint of the center line was zero. For each of these conditions, separate comparisons are made in the displacement speed range and in the planing speed range. The curves of best trim in figure 24 indicate the trims at which approximately minimum resistance was obtained within the scope of the investigation.

Displacement speed range. - At best trim (fig. 24(a)) for a given speed coefficient $C_{V\Delta}$, an increase in fineness ratio decreased the trim τ , decreased the drag coefficient $C_{D\Delta}$, moved the center of pressure forward (the center-of-pressure ratio $\frac{x}{(\Delta/w)^{1/3}}$ increased), increased the wetted-length ratio $\frac{l}{(\Delta/w)^{1/3}}$, and decreased the height ratio $\frac{h}{(\Delta/w)^{1/3}}$. Similar effects were obtained at zero trimming moment (fig. 25(a)).

Planing speed range. - At best trim (fig. 24(b)), for a given lift coefficient C_{LQ} , an increase in fineness ratio decreased the trim τ ; had little effect on the drag coefficient C_{DQ} , the center-of-pressure ratio x/L , or the wetted-length ratio l/L ; but decreased the ratio of the height of the center-line midpoint to the overall length h/L . Similar effects were obtained at zero trimming moment (fig. 25(b)).

Reference lines of constant Δ/R were superimposed on the C_{DQ} curves in figures 24(b) and 25(b). For all three fineness ratios, Δ/R was approximately 3.5 at high values of C_{LQ} for both the best trim and the zero-trimming-moment conditions. However, with decrease in C_{LQ} , Δ/R increased to approximately 5.0 at best trim but decreased to approximately 2.0 for zero trimming moment.

Spray. - The side photographs in figure 26 show that at a trim of 8° , an increase in fineness ratio from 6 to 9 resulted in an appreciable reduction in spray. The reduction in spray was less marked with further increase in fineness ratio from 9 to 12. The effects of fineness ratio on the spray characteristics were similar at other trims but decreased somewhat with increase in trim.

Effect of Chine Strips

The effect of the chine strips on the hydrodynamic characteristics of the models is shown in figures 12, 13, and 14 for fineness ratios 6, 9, and 12, respectively. Faired curves through the data for the models without chine strips are shown as solid lines, together with corresponding curves for the models with chine strips, shown as dashed lines. Because the data for the models without strips were obtained only for low speeds, plots are given for displacement conditions only.

At 0° trim, the hydrodynamic characteristics of all three fineness-ratio models were just as poor with strips as without strips. At trims of 4° and higher, the chine strips still had practically no effect up to moderate speeds corresponding to a $C_{V\Delta}$ of about 2.7. However, there was a slight tendency for the strips to take effect at lower values of $C_{V\Delta}$ with increase in trim or fineness ratio. With further increase in $C_{V\Delta}$, the hydrodynamic characteristics of the models without chine strips deteriorated rapidly. The rapid increase in draft, coupled with the movement forward of the center of pressure of the models without chine strips, indicates the development of increasingly powerful suction forces. Thus, the chine strips effectively improved the hydrodynamic characteristics of the streamline bodies except at very low speeds.

The simultaneous side and bottom photographs in figure 15 show that without chine strips, the spray characteristics of the streamline bodies deteriorated rapidly with increase in speed and also, to a lesser degree, with decrease in fineness ratio.

Effect of Removing Tail Cones

The effect of removing the tail cones from the bodies with chine strips is shown in figures 16, 17, and 18 for fineness ratios 6, 9, and 12, respectively. Faired curves through the data for the models without tail cones are plotted as solid lines, together with corresponding curves for the models with tail cones, shown as dashed lines. The curves for the models without tail cones are practically the same as those for the models with tail cones; some of them being identical.

The simultaneous side and bottom photographs in figure 19 show that the spray characteristics of the models with the tail cones removed are approximately the same as those of the models with tail cones (fig. 11).

CONCLUSIONS

The data obtained in this investigation of the hydrodynamic forces and moments acting on a family of streamline bodies of three fineness ratios with chine strips indicate the following:

1. Under displacement conditions, for a given speed coefficient $C_{V\Delta}$, the drag coefficient $C_{D\Delta}$ increased with trim.
2. Under planing conditions, for a given lift coefficient C_{LQ} , the drag coefficient C_{DQ} decreased with increase in trim up to a best trim (trim for minimum resistance).
3. Best trim, as well as trim for zero trimming moment about center-line midpoint ($M = 0$), decreased with increase in fineness ratio from 6 to 12.
4. At best trim, or for zero trimming moment about the center-line midpoint, an increase in fineness ratio from 6 to 12 resulted in a decrease in the drag coefficient $C_{D\Delta}$ under displacement conditions but had little effect on the drag coefficient C_{DQ} under planing conditions.
5. With decrease in lift coefficient C_{LQ} , the load-resistance ratio increased from about 3.5 to about 5.0 at best trim and decreased from about 3.5 to about 2.0 at trim for zero trimming moment about the center-line midpoint.
6. An increase in fineness ratio resulted in an appreciable reduction in spray.
7. The chine strips effectively improved the hydrodynamic characteristics of the streamline bodies except at very low speeds.

8. Removal of the tail cones had a negligible effect on the hydrodynamic characteristics of the streamline bodies.

Langley Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va., October 29, 1954.

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TABLE I.-- NONDIMENSIONAL OFFSETS

d/L (a)	$2y/D$ (b)
0	0
.010	.213
.021	.289
.042	.402
.062	.483
.083	.552
.125	.663
.167	.746
.208	.813
.250	.865
.333	.943
.417	.985
.500	1.000
.583	.970
.667	.884
.750	.734
.833	.514
.875	.393
.917	.266
.958	.135
.979	.068
1.000	0

^aRatio of distance from nose
to total length of model.

^bRatio of diameter to maximum
diameter of model.

TABLE II
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 6 WITH CHINE STRIPS

C_{A_Q}	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(\Delta)^{1/3}}$	$\frac{l}{(\Delta)^{1/3}}$	$\frac{h}{(\Delta)^{1/3}}$	C_{L_Q}	C_{E_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 0^\circ$													
0	0	0	c	---	---	---	---	---	---	---	0.432	0.084	
0	.63	0	c	---	---	---	---	---	0	0	---	0.081	
0	1.06	.002	0	---	---	---	---	---	0	.0036	---	.514	.081
0	1.48	.005	0	---	---	---	---	---	0	.0046	---	---	.080
0	2.11	.011	.010	---	---	---	---	---	0	.0049	---	---	.072
0	2.53	.019	.025	---	---	---	---	---	0	.0059	---	.755	.069
0	3.17	.028	.048	---	---	---	---	---	0	.0056	---	.842	.067
0	3.59	.160	.194	---	---	---	---	---	0	.0249	---	---	.030
.10	0	0	.003	0	---	4.64	6.88	0.45	---	0.506	.749	.049	
.10	.63	.002	.012	.93	0.045	4.82	---	.45	.4988	.0100	.526	---	.047
.10	1.06	.009	.048	1.55	.075	5.62	7.73	.40	.1797	.0162	.613	.842	.044
.10	1.48	.016	.060	2.17	.068	5.87	---	.43	.0917	.0147	.640	---	.047
.10	2.11	.032	.075	3.10	.067	6.18	8.68	.40	.0449	.0144	.674	.946	.044
.10	2.53	.053	.099	3.72	.076	6.71	---	.33	.0312	.0165	.751	---	.036
.10	3.17	.122	.149	4.65	.113	7.79	9.19	.18	.0200	.0244	.849	1.000	.020
.10	3.59	.263	.229	5.26	.190	9.55	---	0	.0155	.0409	1.041	---	0
.20	0	0	.025	0	---	3.85	6.26	.25	---	---	.529	.859	.035
.20	.63	.004	.030	.83	.058	3.91	---	.24	.9975	.0200	.536	---	.033
.20	1.06	.018	.093	1.38	.094	4.44	7.30	.20	.3554	.0323	.610	1.000	.027
.20	1.48	.031	.123	1.93	.083	4.69	---	.20	.1833	.0284	.644	---	.028
.20	2.11	.048	.124	2.76	.063	4.69	7.30	.20	.0899	.0216	.644	1.000	.028
.20	2.53	.079	.129	3.31	.072	4.74	---	.16	.0624	.0246	.650	---	.022
.20	3.17	.219	.194	4.14	.128	5.30	7.30	-.18	.0399	.0437	.728	1.000	-.025
.30	0	0	.040	0	---	3.37	6.34	.14	---	---	.529	.996	.022
.30	.63	.004	.043	.77	.045	3.39	---	.11	1.4963	.0200	.532	---	.017
.30	1.06	.026	.123	1.29	.104	3.79	6.38	.06	.5391	.0467	.596	1.000	.010
.30	1.48	.039	.161	1.80	.080	3.99	---	.06	.2790	.0357	.627	---	.010
.30	2.11	.063	.146	2.58	.063	3.90	6.38	.06	.1348	.0283	.613	1.000	.010
.30	2.53	.118	.134	3.09	.082	3.84	---	.02	.0936	.0368	.603	---	.003
.30	3.17	.242	.095	3.87	.108	3.65	6.38	-.16	.0599	.0483	.573	1.000	-.025
.40	0	0	.055	0	---	3.08	5.79	.07	---	---	.532	1.000	.012
.40	.63	.006	.055	.74	.055	3.08	---	.04	1.9950	.0299	.532	---	.007
.40	1.06	.036	.143	1.23	.119	3.37	5.79	-.01	.7188	.0647	.583	1.000	-.001
.40	1.48	.056	.190	1.72	.094	3.53	---	-.01	.3666	.0513	.610	---	-.001
.40	2.11	.089	.152	2.46	.074	3.41	5.79	-.01	.1797	.0400	.590	1.000	-.002
.40	2.53	.129	.109	2.96	.074	3.26	---	-.06	.1248	.0402	.563	---	-.011
.50	0	0	.069	0	---	2.86	5.38	0	---	---	.532	1.000	0
.50	.63	.007	.056	.71	.056	2.82	---	-.03	2.4938	.0349	.526	---	-.006
.50	1.06	.048	.155	1.18	.156	3.08	5.38	-.09	.8985	.0863	.573	1.000	-.017
.50	1.48	.074	.194	1.66	.108	3.17	---	-.09	.4585	.0678	.590	---	-.017
.50	2.11	.099	.125	2.37	.070	2.99	5.38	-.10	.2246	.0445	.556	1.000	-.019
.50	2.53	.162	.085	2.84	.061	2.89	---	-.18	.1560	.0505	.539	---	-.034
$\tau = 40$													
0	0	0	0	---	---	---	---	---	0	0.0050	---	0.309	0.087
0	.63	.001	0	---	---	---	---	---	0	.0036	---	4.72	.088
0	1.06	.002	0	---	---	---	---	---	0	0.037	---	---	.085
0	1.48	.001	0	---	---	---	---	---	0	.0049	4.717	.657	.078
0	2.11	.011	.013	---	---	---	---	---	0	.0044	7.879	---	.071
0	2.53	.014	.031	---	---	---	---	---	0	.0046	8.131	.693	.070
0	3.17	.023	.052	---	---	---	---	---	0	.0045	8.159	---	.071
0	3.59	.029	.067	---	---	---	---	---	0	.0045	8.610	.696	.071
0	4.22	.040	.055	---	---	---	---	---	0	.0045	8.081	---	.073
0	4.64	.048	.109	---	---	---	---	---	0	.0044	8.452	.685	.071
0	5.28	.061	.144	---	---	---	---	---	0	0	0	0	0

TABLE II.- Continued

**EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 6 WITH CHINE STRIPS**

TABLE II - Continued

 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 6 WITH CHINE STRIPS

$C_{\Delta Q}$	C_{V_Q}	C_{P_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(\Delta)^{1/3}}$	$\frac{z}{(\Delta)^{1/3}}$	$\frac{y}{(\Delta)^{1/3}}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{y}{L}$
$\tau = 4^\circ$ - Concluded													
.30	5.28	0.162	0.598	6.45	0.026	6.05	5.52	0.18	0.0216	0.0116	0.950	0.867	0.029
.30	6.33	.161	.568	7.74	.018	5.92	5.11	.29	.0150	.0080	.930	.802	.046
.30	7.39	.182	.608	9.02	.015	6.09	4.98	.32	.0110	.0067	.957	.783	.050
.30	8.44	.206	.657	10.31	.013	6.31	4.80	.35	.0084	.0058	.991	.755	.054
.30	9.50	.244	.724	11.60	.012	6.61	4.54	.35	.0067	.0054	1.038	.750	.056
.30	10.55	.277	.785	12.89	.011	6.86	4.57	.37	.0054	.0050	1.078	.718	.058
.30	11.61	.310	.848	14.18	.010	7.12	4.47	.38	.0044	.0046	1.119	.702	.060
.40	0	0	-.054	0	-----	2.71	5.56	.06	-----	-----	.468	.963	.010
.40	.63	.005	-.034	.74	.046	2.77	-----	.03	1.9950	.0249	.479	-----	.005
.40	1.06	.031	.066	1.23	.103	3.10	5.74	0	.7188	.0557	.536	.993	0
.40	1.48	.047	.099	1.72	.079	3.22	-----	.02	.3666	.0431	.556	-----	.004
.40	2.11	.071	.133	2.46	.059	3.33	5.68	.02	.1797	.0319	.576	.982	.003
.40	2.55	.096	.147	2.96	.055	3.37	-----	-.01	.1248	.0299	.583	-----	-.002
.40	3.17	.190	.275	3.70	.070	3.78	5.79	-.09	.0799	.0379	.654	1.000	-.015
.40	3.59	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
.40	4.22	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
.40	4.64	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
.40	5.28	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
.40	6.33	.197	.264	7.39	.018	5.40	4.92	.20	.0200	.0098	.933	.850	.035
.40	7.39	.209	.764	8.62	.014	5.40	4.61	.27	.0147	.0077	.933	.797	.046
.40	8.44	.231	.785	9.85	.012	5.46	4.46	.30	.0112	.0065	.944	.772	.052
.50	0	0	-.042	0	-----	2.57	5.27	-.01	-----	-----	.479	.982	-.002
.50	.63	.005	-.019	.71	.040	2.63	-----	-.03	2.4958	.0249	.489	-----	-.006
.50	1.06	.045	.084	1.18	.128	2.89	5.38	-.06	.8985	.0509	.539	1.000	-.012
.50	1.48	.059	.115	1.66	.086	2.97	-----	-.04	.4583	.0541	.553	-----	-.007
.50	2.11	.089	.146	2.37	.063	3.04	5.38	-.05	.2246	.0400	.566	1.000	-.009
.50	2.55	.122	.161	2.84	.060	3.08	-----	-.08	.1560	.0381	.573	-----	-.015
.50	3.17	.192	.293	3.55	.061	3.40	5.38	-.19	.0999	.0383	.634	1.000	-.036
$\tau = 8^\circ$													
0	0	0	0	0	-----	-----	-----	-----	-----	-----	0.345	0.095	
0	.63	0	0	0	-----	-----	-----	0	0	-----	-----	.093	
0	1.06	.002	0	0	-----	-----	-----	0	.0036	.500	.488	.094	
0	1.48	.004	0	0	-----	-----	-----	0	.0037	.500	-----	.092	
0	2.11	.009	.005	0	-----	-----	-----	0	.0040	1.407	.519	.089	
0	2.55	.012	.015	0	-----	-----	-----	0	.0037	2.714	-----	.084	
0	3.17	.019	.031	0	-----	-----	-----	0	.0038	3.327	.530	.084	
0	3.59	.026	.040	0	-----	-----	-----	0	.0040	3.125	-----	.084	
0	4.22	.036	.055	0	-----	-----	-----	0	.0040	3.104	.533	.084	
0	4.64	.042	.065	0	-----	-----	-----	0	.0039	3.131	-----	.084	
0	5.28	.052	.080	0	-----	-----	-----	0	.0037	3.118	.536	.084	
0	6.33	.072	.123	0	-----	-----	-----	0	.0036	3.455	.522	.085	
0	7.39	.095	.169	0	-----	-----	-----	0	.0035	3.522	.528	.085	
0	8.44	.121	.203	0	-----	-----	-----	0	.0034	3.347	.533	.085	
0	9.50	.155	.273	0	-----	-----	-----	0	.0034	3.508	.528	.085	
0	10.55	.193	.324	0	-----	-----	-----	0	.0035	3.347	.553	.085	
0	11.61	.231	.402	0	-----	-----	-----	0	.0034	3.448	.525	.087	
0	12.66	.275	.469	0	-----	-----	-----	0	.0034	3.394	.528	.085	
0	13.72	.322	.544	0	-----	-----	-----	0	.0034	3.567	.547	.085	
0	14.77	.374	.610	0	-----	-----	-----	0	.0034	3.266	.519	.085	
0	15.83	.439	.679	0	-----	-----	-----	0	.0035	3.121	.516	.085	
0	16.88	.493	.796	0	-----	-----	-----	0	.0035	3.242	.519	.085	

TABLE II - Continued

 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 6 WITH CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{F_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(L)}$	$\frac{z}{(L)}$	$\frac{h}{(L)}$	c_{L_C}	c_{D_Q}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$\tau = 8^\circ$ - Continued													
.10	0	0	-0.065	0	----	3.09	6.31	0.51	0.4985	0.0190	0.337	0.687	0.056
.10	.63	.002	-.060	.93	0.046	3.28	6.49	.19	.1757	.0262	.357	-----	.054
.10	1.06	.003	-.032	1.55	.075	3.89	6.44	.19	.0917	.0147	.425	.702	.054
.10	1.48	.026	-.019	2.17	.066	4.17	6.44	.51	.0449	.0117	.570	.657	.056
.10	2.11	.026	.031	3.10	.054	5.22	6.03	.51	.0312	.0100	.537	-----	.056
.10	2.53	.032	.062	3.72	.046	5.84	6.03	.51	.0200	.0078	.681	.660	.058
.10	3.17	.039	.080	4.65	.036	6.24	6.05	.53	.0155	.0072	.687	-----	.062
.10	3.59	.046	.085	5.26	.033	6.30	6.00	.57	.0112	.0061	.711	.614	.056
.10	4.22	.054	.096	6.19	.028	6.52	5.64	.61	.0073	.0057	.725	-----	.069
.10	4.64	.061	.103	6.81	.026	6.64	5.58	.63	.0072	.0051	.744	.587	.070
.10	5.28	.071	.115	7.74	.024	6.83	5.38	.64	-----	-----	-----	-----	-----
.10	6.33	.092	.156	9.29	.021	7.57	5.15	.57	.0050	.0046	.826	.561	.073
.10	7.39	.114	.184	10.84	.019	8.00	5.12	.70	.0037	.0042	.873	.558	.076
.10	8.44	.142	.224	12.39	.019	8.65	5.12	.70	.0028	.0040	.944	.558	.076
.10	9.50	.156	.269	13.98	.017	9.70	5.07	.70	.0022	.0037	1.053	.553	.076
.10	10.55	.209	.335	15.49	.018	10.20	5.07	.71	.0018	.0036	1.112	.553	.077
.10	11.61	.244	.415	17.04	.017	11.31	4.92	.71	.0015	.0036	1.233	.536	.077
.10	12.66	.291	.475	18.59	.017	11.86	4.82	.71	.0013	.0036	1.294	.525	.077
.10	13.72	.338	.555	20.13	.017	12.73	5.02	.71	.0011	.0036	1.388	.547	.077
.10	14.77	.392	.620	21.68	.017	13.07	4.89	.71	.0009	.0036	1.426	.523	.077
.10	15.83	.458	.687	23.23	.017	13.69	4.82	.71	.0008	.0037	1.492	.525	.077
.20	0	0	-.110	0	----	2.67	5.66	.28	-----	-----	.367	.777	.038
.20	.63	.003	-.094	.83	.014	2.83	5.24	.24	.9975	.0150	.388	-----	.033
.20	1.06	.019	-.044	1.38	.100	3.26	5.87	.24	.5594	.0341	.448	.805	.033
.20	1.48	.025	-.025	1.93	.067	3.41	5.26	.25	.1833	.0229	.468	-----	.036
.20	2.11	.042	-.040	2.76	.035	3.98	5.23	.23	.0858	.0189	.546	.800	.032
.20	2.53	.052	.129	3.31	.056	4.69	5.23	.20	.0624	.0193	.644	-----	.028
.20	3.17	.072	.202	4.14	.042	5.30	5.83	.26	.0359	.0144	.727	.800	.035
.20	3.59	.075	.194	4.69	.034	5.23	5.23	.34	.0311	.0117	.726	-----	.046
.20	4.22	.083	.194	5.52	.026	5.23	4.97	.39	.0225	.0090	.718	.682	.053
.20	4.64	.086	.184	6.07	.023	5.13	5.13	.42	.0186	.0090	.704	-----	.058
.20	5.28	.094	.184	6.90	.020	5.13	4.54	.46	.0144	.0068	.704	.623	.063
.20	6.33	.114	.203	8.28	.017	5.25	5.00	.50	.0100	.0057	.721	-----	.069
.20	7.39	.134	.235	9.66	.014	5.48	4.40	.52	.0073	.0049	.752	.603	.072
.20	8.44	.162	.250	11.04	.013	5.65	4.23	.54	.0056	.0045	.775	.581	.074
.20	9.50	.187	.324	12.42	.012	6.11	4.19	.54	.0014	.0041	.839	.575	.074
.20	10.55	.228	.363	13.80	.012	6.33	4.13	.54	.0036	.0041	.869	.567	.074
.20	11.61	.268	.453	15.18	.012	6.78	4.05	.55	.0030	.0040	.930	.561	.076
.20	12.66	.307	.494	16.56	.011	7.15	4.05	.55	.0025	.0038	.951	.556	.076
.20	13.72	.355	.551	17.94	.011	7.44	3.93	.56	.0021	.0038	1.021	.539	.077
.30	0	0	-.154	0	----	2.51	5.29	.14	-----	-----	.394	.831	.023
.30	.63	.005	-.105	.77	.056	2.59	5.11	.11	1.4963	.0249	.414	-----	.017
.30	1.06	.028	-.044	1.29	.112	2.96	5.50	.11	.5391	.0563	.465	.867	.017
.30	1.48	.036	-.015	1.80	.074	3.11	5.26	.11	.2750	.0350	.489	-----	.023
.30	2.11	.056	.050	2.58	.056	5.41	5.45	.13	.1348	.0252	.536	.856	.020
.30	2.53	.085	.169	3.09	.061	3.99	5.26	.08	.0336	.0275	.627	-----	.013
.30	3.17	.123	.249	3.87	.055	4.35	5.45	.10	.0529	.0246	.694	.856	.016
.30	3.59	.116	.354	4.38	.040	4.87	5.26	.17	.0466	.0180	.765	-----	.027
.30	4.22	.115	.333	5.16	.029	4.72	4.73	.28	.0357	.0129	.741	.744	.044
.30	4.64	.116	.303	5.67	.024	4.62	4.62	.31	.0278	.0108	.725	-----	.048
.30	5.28	.122	.283	6.45	.020	4.53	4.29	.36	.0216	.0088	.711	.673	.051
.30	6.33	.140	.289	7.74	.016	4.54	4.00	.42	.0150	.0070	.714	.629	.066
.30	7.39	.160	.293	9.02	.013	4.54	3.88	.45	.0210	.0059	.714	.609	.071
.30	8.14	.184	.315	10.31	.012	4.63	3.70	.46	.0284	.0052	.728	.581	.072
.30	9.50	.206	.363	11.56	.010	4.85	3.61	.47	.0057	.0046	.762	.567	.074
.30	10.55	.245	.394	12.59	.010	4.95	3.57	.48	.0054	.0044	.778	.561	.075
.30	11.61	.284	.464	14.18	.009	5.23	3.57	.49	.0044	.0042	.822	.561	.077

TABLE II - Continued

 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 6 WITH CHINE STRIPS

$C_{\Delta Q}$	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(\frac{\Delta}{W})^{1/3}}$	$\frac{l}{(\frac{\Delta}{W})^{1/3}}$	$\frac{h}{(\frac{\Delta}{W})^{1/3}}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 8^\circ$ - Concluded													
.40	0	0	-0.141	0	.74	0.055	2.51	5.11	0.05	-----	0.415	0.884	0.009
.40	.63	.006	-.110	.74	0.055	2.51	-----	1.9950	.0299	.435	-----	.008	
.40	1.06	.038	-.032	1.23	.126	2.77	5.31	.04	.7188	.0683	.479	.918	.007
.40	1.48	.048	-.019	1.72	.081	2.83	-----	.05	.3666	.0440	.489	-----	.009
.40	2.11	.071	.070	2.46	.059	3.12	5.21	.04	.1797	.0319	.539	.901	.008
.40	2.53	.102	.194	2.96	.059	3.55	-----	.01	.1248	.0318	.610	-----	-.002
.40	3.17	.167	.465	3.70	.061	4.38	5.37	.04	.0799	.0333	.758	.929	-.007
.40	3.59	.181	.533	4.19	.052	4.60	-----	.04	.0622	.0281	.795	-----	.006
.40	4.22	.159	.500	4.93	.033	4.50	4.74	.33	.0449	.0179	.778	.819	.057
.40	4.64	.153	.461	5.42	.026	4.38	-----	.23	.0371	.0142	.758	-----	.040
.40	5.28	.154	.409	6.16	.020	4.21	4.15	.29	.0288	.0111	.728	.718	.050
.40	6.33	.167	.394	7.39	.015	4.17	3.86	.35	.0200	.0083	.721	.668	.061
.40	7.39	.183	.375	8.62	.012	4.09	3.65	.39	.0147	.0067	.708	.631	.068
.40	8.44	.207	.375	9.85	.011	4.07	3.52	.41	.0112	.0058	.704	.609	.071
.50	0	0	.127	0	-----	2.35	4.93	-.03	-----	-----	.438	.918	-.005
.50	.63	.007	-.086	.71	.055	2.46	-----	.05	2.4938	.0349	.458	-----	-.010
.50	1.06	.049	-.013	1.18	.140	2.64	5.12	.05	.8985	.0881	.492	.954	-.010
.50	1.48	.063	.011	1.66	.092	2.72	-----	.02	.4583	.0577	.506	-----	-.004
.50	2.11	.088	.090	2.37	.063	2.89	5.08	.04	.2246	.0395	.539	.946	-.008
.50	2.53	.125	.224	2.84	.062	3.22	-----	.09	.1560	.0390	.600	-----	-.018
.50	3.17	.209	.504	3.55	.066	3.89	5.26	.15	.0999	.0417	.725	.979	-.029
.50	3.59	.291	.703	4.03	.072	4.34	-----	.18	.0777	.0452	.809	-----	-.034
.50	4.22	.216	.703	4.74	.039	4.36	4.73	.05	.0562	.0243	.812	.881	.009
$\tau = 12^\circ$													
0	0	0	0	-----	-----	-----	-----	-----	0	0	0.393	.116	
0	.63	0	0	-----	-----	-----	-----	-----	0	0	-----	.109	
0	1.06	.001	0	-----	-----	-----	-----	-----	0	.0018	0.500	.356	.109
0	1.48	.003	0	-----	-----	-----	-----	-----	0	.0027	.500	-----	.109
0	2.11	.006	0	-----	-----	-----	-----	-----	0	.0027	.300	.373	.106
0	2.53	.007	0	-----	-----	-----	-----	-----	0	.0022	.500	-----	.104
0	3.17	.012	0	-----	-----	-----	-----	-----	0	.0024	.500	.393	.102
0	3.59	.016	.003	-----	-----	-----	-----	-----	0	.0025	.337	-----	.102
0	4.22	.021	.007	-----	-----	-----	-----	-----	0	.0024	.555	.399	.102
0	4.64	.022	.007	-----	-----	-----	-----	-----	0	.0020	.842	-----	.106
0	5.28	.029	.010	-----	-----	-----	-----	-----	0	.0021	.889	.401	.105
0	6.33	.045	.020	-----	-----	-----	-----	-----	0	.0022	1.010	.404	.105
0	7.39	.003	.027	-----	-----	-----	-----	-----	0	.0022	1.030	.396	.105
0	8.44	.076	.034	-----	-----	-----	-----	-----	0	.0021	1.010	.407	.105
0	9.50	.093	.046	-----	-----	-----	-----	-----	0	.0021	1.057	.407	.105
0	10.55	.115	.055	-----	-----	-----	-----	-----	0	.0021	1.044	.407	.105
0	11.61	.141	.066	-----	-----	-----	-----	-----	0	.0021	1.030	.399	.105
0	12.66	.169	.099	-----	-----	-----	-----	-----	0	.0021	1.165	.381	.105
0	13.72	.201	.089	-----	-----	-----	-----	-----	0	.0021	1.003	.404	.105
0	14.77	.235	.114	-----	-----	-----	-----	-----	0	.0022	1.050	.381	.104
0	15.83	.270	.124	-----	-----	-----	-----	-----	0	.0022	1.024	.384	.104
0	16.88	.301	.194	-----	-----	-----	-----	-----	0	.0021	1.236	.404	.104
.10	0	0	-.080	0	-----	2.81	5.51	0.62	-----	-----	.307	.601	.067
.10	.63	.003	-.075	.93	.070	2.94	-----	.59	.4988	.0150	.320	-----	.065
.10	1.06	.010	-.055	1.55	.084	3.40	5.59	.62	.1797	.0180	.371	.609	.066
.10	1.48	.018	-.039	2.17	.077	3.74	-----	.52	.0197	.0165	.408	-----	.067
.10	2.11	.026	0	3.10	.054	4.57	5.46	.62	.0449	.0117	.500	.595	.067
.10	2.53	.030	.004	3.72	.044	4.67	-----	.64	.0312	.0094	.509	-----	.070
.10	3.17	.036	.011	4.65	.033	4.82	4.95	.69	.0200	.0072	.526	.539	.076
.10	3.59	.041	.011	5.26	.030	4.79	-----	.76	.0155	.0064	.522	-----	.083
.10	4.22	.047	.011	6.19	.025	4.79	4.56	.79	.0112	.0053	.522	.497	.086
.10	4.64	.049	.004	6.81	.021	4.67	-----	.82	.0093	.0045	.509	-----	.089

TABLE II - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 6 WITH CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(\Delta)} \frac{1}{1/3}$	$\frac{l}{(\Delta)} \frac{1}{1/3}$	$\frac{h}{(\Delta)} \frac{1}{1/3}$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 12^\circ$ - Continued													
.10	5.28	0.056	0.007	7.74	0.016	4.70	L.33	0.84	0.0072	0.0040	0.312	0.472	0.092
.10	6.33	.069	.012	9.29	.016	4.82	4.09	.86	.0056	.0034	.226	.446	.094
.10	7.39	.086	.016	10.81	.015	4.88	3.97	.86	.0037	.0032	.532	.432	.094
.10	8.44	.102	.032	12.39	.013	5.16	3.97	.88	.0028	.0029	.563	.432	.096
.10	9.50	.121	.035	13.91	.013	5.19	3.97	.90	.0022	.0027	.566	.432	.098
.10	10.55	.142	.046	15.49	.012	5.35	3.27	.90	.0018	.0026	.583	.355	.098
.10	11.61	.169	.055	17.01	.012	5.47	3.89	.90	.0015	.0025	.596	.424	.098
.10	12.66	.195	.085	18.59	.011	5.87	3.63	.90	.0013	.0024	.540	.396	.098
.10	13.72	.228	.085	20.13	.011	5.87	3.76	.90	.0011	.0024	.640	.410	.098
.10	14.77	.263	.099	21.68	.011	6.02	3.68	.90	.0009	.0024	.657	.401	.098
.10	15.83	.296	.104	23.23	.011	6.02	3.71	.90	.0008	.0023	.657	.404	.098
.20	0	0	-1.35	0	-----	2.46	5.03	32	-----	-----	.337	.690	.043
.20	.63	.005	-.120	.85	.073	2.58	-----	.27	.9975	.0249	.354	-----	.037
.20	1.06	.021	-.084	1.38	.110	2.92	5.19	.28	.3599	.0377	.401	.713	.039
.20	1.48	.027	-.065	1.93	.072	3.07	-----	.31	.1833	.0247	.421	-----	.043
.20	2.11	.045	.030	2.76	.064	3.88	5.17	.28	.0896	.0220	.532	.710	.038
.20	2.55	.056	.065	3.31	.051	4.17	-----	.32	.0624	.0175	.573	-----	.044
.20	3.17	.063	.069	4.14	.037	4.20	4.60	.41	.0393	.0126	.576	.631	.056
.20	3.59	.059	.062	4.69	.046	4.15	-----	.46	.0311	.0107	.570	-----	.063
.20	4.22	.073	.050	5.52	.024	4.03	4.13	.51	.0225	.0082	.553	.567	.070
.20	4.61	.078	.035	6.07	.021	3.91	-----	.57	.0186	.0072	.536	-----	.078
.20	5.28	.083	.025	6.90	.018	3.83	3.76	.60	.0144	.0060	.526	.516	.082
.20	6.33	.096	.022	8.28	.014	3.80	3.56	.62	.0100	.0048	.522	.488	.085
.20	7.39	.112	.020	9.66	.022	3.78	3.37	.64	.0073	.0041	.519	.463	.088
.20	8.44	.130	.025	11.04	.011	3.83	3.23	.65	.0056	.0037	.526	.443	.089
.20	9.50	.148	.035	12.42	.010	3.91	3.25	.66	.0044	.0035	.535	.446	.091
.20	10.55	.159	.036	13.80	.009	3.91	3.21	.67	.0035	.0030	.536	.441	.092
.20	11.61	.194	.045	15.18	.008	3.96	3.05	.68	.0030	.0029	.543	.418	.094
.20	12.66	.223	.072	16.56	.008	4.15	3.07	.68	.0025	.0028	.570	.421	.094
.20	13.72	.259	.066	17.94	.008	4.10	3.17	.68	.0021	.0028	.563	.435	.094
.30	0	0	-1.68	0	-----	2.32	4.82	.17	-----	-----	.364	.758	.027
.30	.63	.006	-.145	.77	.057	2.14	-----	.14	1.4963	.0299	.384	-----	.022
.30	1.06	.032	-.101	1.29	.128	2.68	4.97	.16	.5591	.0575	.421	.780	.025
.30	1.48	.040	-.075	1.80	.082	2.81	-----	.18	.2750	.0367	.441	-----	.028
.30	2.11	.067	.045	2.58	.067	3.39	5.00	.13	.1348	.0301	.532	.786	.021
.30	2.55	.085	.139	3.09	.059	3.84	-----	.15	.0936	.0265	.603	-----	.024
.30	3.17	.099	.174	3.87	.044	4.01	4.54	.26	.0599	.0198	.630	.743	.042
.30	3.59	.101	.154	4.38	.033	3.90	-----	.34	.0466	.0157	.613	-----	.034
.30	4.22	.105	.119	5.16	.026	3.73	3.89	.41	.0337	.0118	.586	.612	.064
.30	4.64	.108	.092	5.67	.022	3.50	3.54	.45	.0278	.0100	.566	.556	.071
.30	5.28	.114	.059	5.45	.018	3.49	3.27	.50	.0216	.0082	.549	.514	.078
.30	6.33	.125	.049	7.74	.014	3.41	3.12	.53	.0150	.0062	.536	.491	.083
.30	7.39	.140	.040	9.02	.011	3.37	3.02	.56	.0110	.0051	.529	.474	.088
.30	8.44	.159	.035	10.31	.010	3.32	2.97	.57	.0084	.0045	.522	.466	.090
.30	9.50	.176	.035	11.60	.009	3.32	2.91	.57	.0067	.0039	.522	.437	.090
.30	10.55	.197	.035	12.89	.008	3.32	2.80	.60	.0054	.0035	.522	.411	.095
.30	11.61	.222	.040	14.18	.007	3.35	-----	.50	.0045	.0033	.526	-----	.095
.40	0	0	-1.80	0	-----	2.26	4.69	.05	-----	-----	.391	.611	.009
.40	.53	.008	-.149	.74	.073	2.36	-----	.04	1.9950	.0399	.408	-----	.006
.40	1.06	.046	-.089	1.23	.152	2.57	4.82	.04	.7388	.0827	.445	.833	.007
.40	1.48	.054	-.067	1.72	.091	2.65	-----	.08	.3666	.0495	.458	-----	.013
.40	2.11	.053	.068	2.46	.069	3.12	4.85	.02	.1797	.0373	.539	.839	.004
.40	2.53	.120	.224	2.96	.069	3.63	-----	.12	.1243	.0374	.527	-----	.003
.40	3.17	.136	.300	3.70	.050	3.86	L.52	.12	.0799	.0272	.667	.783	.021

TABLE II - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 6 WITH CHINE STRIPS

$C_{\Delta Q}$	C_{VQ}	C_{RQ}	C_{M_Q}	$C_{V\Delta}$	$C_{D\Delta}$	$\frac{x}{(\Delta)}^{1/3}$	$\frac{l}{(\Delta)}^{1/3}$	$\frac{h}{(\Delta)}^{1/3}$	C_{LQ}	C_{DQ}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 12^\circ$ - Concluded													
.40	3.59	0.141	0.277	1.19	0.040	3.78	---	0.21	0.0622	0.0219	0.654	----	0.036
.40	4.22	.110	.224	1.93	.029	3.60	3.79	.30	.0449	.0157	.623	0.657	.053
.40	4.64	.142	.174	5.42	.024	3.45	---	.36	.0371	.0132	.596	----	.063
.40	5.28	.146	.135	6.16	.019	3.31	3.40	.40	.0288	.0105	.573	.589	.070
.40	6.33	.155	.089	7.39	.014	3.17	3.10	.46	.0200	.0077	.549	.536	.079
.40	7.39	.169	.060	8.62	.011	3.08	2.95	.48	.0147	.0062	.552	.511	.064
.40	8.44	.183	.055	9.85	.009	3.06	2.84	.51	.0112	.0051	.529	.491	.088
.50	0	0	-.169	0	-----	2.24	4.62	-.04	-----	-----	.417	.861	-.007
.50	.63	.010	-.134	.71	.079	2.34	---	-.06	2.4938	.0499	.435	----	.012
.50	1.06	.059	-.087	1.18	.158	2.46	4.73	-.05	.8985	.1060	.458	.881	-.009
.50	1.48	.067	-.047	1.66	.097	2.55	---	.01	.4583	.0614	.475	----	.003
.50	2.11	.103	.095	2.37	.073	2.92	4.76	-.05	.2246	.0463	.545	.887	-.009
.50	2.53	.148	.322	2.84	.073	3.46	---	.10	.1560	.0462	.614	----	.019
.50	3.17	.179	.441	3.55	.057	3.73	4.53	-.01	.0999	.0357	.694	.844	-.001
.50	3.59	.179	.427	4.05	.044	3.71	---	.09	.0777	.0278	.691	----	.017
.50	4.22	.179	.354	4.74	.032	5.53	3.83	.20	.0562	.0201	.657	.713	.038
$\tau = 16^\circ$													
0	0	0	0	-----	-----	-----	-----	-----	-----	-----	0.289	0.139	
0	.63	0	0	-----	-----	-----	-----	0	0	0	-----	.216	.141
0	1.06	0	0	-----	-----	-----	-----	0	0	0	-----	.145	
0	1.48	0	0	-----	-----	-----	-----	0	0	0	-----	.101	.146
0	2.11	0	0	-----	-----	-----	-----	0	0	0	-----	.150	
0	4.64	0	0	-----	-----	-----	-----	0	0	0	-----	.151	
0	11.61	0	0	-----	-----	-----	-----	0	0	0	0	-----	
.10	0	0	-.094	0	-----	2.47	4.82	0.72	-----	0.270	.525	.078	
.10	.63	.006	-.089	.93	.019	2.60	---	.68	0.4988	.0299	.233	----	.074
.10	1.06	.013	-.079	1.55	.109	2.87	4.92	.72	.1797	.0254	.315	.556	.078
.10	1.48	.020	-.060	2.17	.065	3.31	---	.73	.0917	.0183	.361	----	.080
.10	2.11	.026	-.046	3.10	.054	3.62	4.51	.81	.0449	.0117	.394	.491	.088
.10	2.53	.028	-.049	3.72	.040	3.55	---	.85	.0312	.0087	.388	----	.092
.10	3.17	.029	-.058	4.62	.027	3.57	3.86	.94	.0200	.0058	.367	.421	.102
.10	3.59	.028	-.069	5.26	.020	3.15	---	.98	.0155	.0044	.344	----	.107
.10	4.22	.029	-.079	6.19	.015	2.94	3.35	1.04	.0112	.0033	.320	.365	.114
.10	4.64	.031	-.085	6.81	.013	2.81	---	1.07	.0093	.0029	.307	----	.116
.10	5.28	.031	-.094	7.74	.010	2.65	3.04	1.08	.0072	.0022	.286	.331	.118
.10	6.33	.029	-.115	9.29	.006	2.19	2.63	1.11	.0050	.0014	.239	.286	.121
.10	7.39	.031	-.143	10.84	.005	1.61	2.50	1.13	.0037	.0011	.175	.272	.123
.10	8.44	.031	-.159	12.39	.004	1.30	2.40	1.15	.0028	.0009	.142	.261	.125
.10	9.50	.033	-.180	13.94	.003	.87	2.24	1.16	.0022	.0007	.094	.244	.127
.10	10.55	.033	-.165	15.49	.003	1.21	2.14	1.17	.0018	.0006	.131	.233	.128
.10	11.61	.032	-.194	17.04	.002	.59	1.80	1.19	.0015	.0005	.064	.196	.129
.10	12.66	.031	-.201	18.59	.002	.43	1.73	1.19	.0013	.0004	.047	.188	.129
.10	13.72	.032	-.209	20.13	.001	.28	1.47	1.20	.0011	.0003	.030	.160	.130
.10	14.77	.031	-.230	21.68	.001	-.15	.51	1.20	.0009	.0003	-.170	.034	.130
.10	15.83	.031	-.209	23.23	.001	.26	1.13	1.19	.0008	.0002	.030	.123	.129
.20	0	0	-.155	0	-----	2.26	4.50	.37	-----	-----	.310	.617	.051
.20	.63	.006	-.147	.83	.087	2.33	---	.34	.9975	.0299	.320	----	.046
.20	1.06	.026	-.127	1.38	.137	2.52	4.68	.38	.3594	.0467	.347	.643	.052
.20	1.48	.037	-.087	1.93	.099	2.90	---	.38	.1833	.0359	.398	----	.052
.20	2.11	.054	-.032	2.76	.071	3.37	4.46	.41	.0868	.0243	.462	.612	.056
.20	2.53	.057	-.030	3.31	.052	3.39	---	.50	.0624	.0178	.465	----	.069
.20	3.17	.060	-.049	4.14	.055	3.24	3.68	.61	.0399	.0120	.445	.505	.083
.20	3.59	.060	-.067	4.69	.027	3.10	---	.66	.0311	.0093	.485	----	.090
.20	4.22	.059	-.090	5.52	.019	2.90	3.19	.72	.0225	.0066	.398	.438	.099

TABLE II - Continued
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 6 WITH CHINE STRIPS

C_{A_Q}	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(\frac{L}{w})^{1/3}}$	$\frac{l}{(\frac{L}{w})^{1/3}}$	$\frac{h}{(\frac{L}{w})^{1/3}}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 16^\circ$ - Concluded													
.20	4.61	0.059	-0.105	6.07	0.016	2.78	----	0.75	0.0186	0.0055	0.381	----	0.105
.20	5.28	.059	-.130	6.90	.012	2.58	2.80	.78	.0144	.0042	.354	0.384	.107
.20	6.33	.059	-.161	8.29	.008	2.31	2.60	.82	.0100	.0029	.317	.356	.113
.20	7.39	.061	-.200	9.56	.006	1.99	2.45	.83	.0073	.0022	.273	.337	.114
.20	5.44	.060	-.230	11.04	.005	1.74	2.25	.87	.0055	.0017	.239	.309	.119
.20	9.50	.062	-.250	12.42	.004	1.50	2.13	.88	.0044	.0014	.205	.292	.120
.20	10.55	.066	-.270	13.50	.004	1.42	2.15	.88	.0036	.0012	.195	.295	.120
.20	11.61	.071	-.308	15.18	.003	1.13	1.98	.89	.0030	.0011	.155	.272	.123
.20	12.66	.073	-.337	16.56	.003	.91	1.74	.90	.0025	.0009	.125	.238	.124
.20	13.72	.075	-.351	17.94	.002	.81	1.78	.90	.0021	.0008	.111	.214	.124
.30	0	0	-.190	0	----	2.19	4.39	.79	----	----	.344	.690	.029
.30	.63	.010	-.174	.77	.111	2.27	----	.77	1.4963	.0499	.357	----	.027
.30	1.06	.042	-.151	1.29	.168	2.43	4.50	.70	.5391	.3755	.581	.707	.051
.30	1.48	.054	-.101	1.80	.130	2.68	----	.71	.2750	.0495	.421	----	.033
.30	2.11	.089	0	2.58	.089	3.18	4.41	.73	.1348	.0400	.500	.693	.036
.30	2.55	.055	.015	3.09	.065	3.24	----	.75	.0936	.0296	.509	----	.039
.30	3.17	.098	0	3.87	.041	3.18	3.70	.74	.0599	.0196	.499	.581	.069
.30	3.59	.096	-.030	4.38	.033	3.02	----	.75	.0466	.0149	.475	----	.080
.30	4.22	.094	-.069	5.16	.024	2.85	3.12	.58	.0337	.0106	.448	.491	.090
.30	4.64	.092	-.100	5.67	.019	2.71	----	.61	.0278	.0085	.425	----	.096
.30	5.28	.083	-.132	6.45	.014	2.55	2.79	.65	.0216	.0064	.401	.458	.103
.30	6.33	.085	-.190	7.74	.010	2.27	2.50	.69	.0150	.0044	.357	.393	.108
.30	7.39	.090	-.230	9.02	.007	2.05	2.31	.72	.010	.0033	.327	.368	.113
.30	8.41	.092	-.255	10.31	.006	1.95	2.16	.74	.0024	.0026	.307	.340	.117
.30	9.50	.093	-.310	11.60	.005	1.69	2.02	.75	.0067	.0201	.266	.317	.119
.30	10.55	.095	-.350	12.89	.004	1.61	2.04	.76	.0054	.0017	.255	.326	.120
.30	11.61	.100	-.377	14.18	.003	1.39	1.91	.77	.0044	.0015	.219	.300	.121
.40	0	0	-.204	0	----	2.16	4.33	.05	----	----	.374	.749	.008
.40	.63	.012	-.188	.74	.110	2.22	----	.02	1.9950	----	.584	----	.005
.40	1.06	.057	-.167	1.23	.189	2.32	4.41	.05	.7188	.1024	.401	.763	.008
.40	1.48	.071	-.095	1.72	.120	2.55	----	.06	.3566	.0651	.441	----	.011
.40	2.11	.120	.045	2.46	.099	3.02	4.35	.05	.1797	.0539	.522	.752	.011
.40	2.53	.134	.089	2.96	.077	3.17	----	.14	.1245	.0418	.549	----	.024
.40	3.17	.139	.070	3.70	.051	3.12	3.75	.28	.0799	.0278	.539	.648	.048
.40	3.59	.137	.025	4.19	.039	2.96	----	.36	.0622	.0213	.512	----	.062
.40	4.22	.132	-.029	4.93	.027	2.79	3.13	.44	.0449	.0148	.482	.542	.077
.40	4.64	.132	-.069	5.42	.023	2.67	----	.50	.0373	.0123	.462	----	.086
.40	5.28	.128	-.120	6.16	.017	2.49	2.71	.54	.0288	.0092	.431	.469	.093
.40	6.33	.121	-.193	7.39	.011	2.26	2.43	.59	.0200	.0060	.391	.421	.102
.40	7.39	.121	-.250	8.62	.008	2.06	2.26	.61	.0147	.0041	.357	.390	.106
.40	8.44	.121	-.281	9.85	.006	1.97	2.16	.64	.0112	.0034	.340	.373	.110
.50	0	0	-.205	0	----	2.14	4.29	-.05	----	----	.398	.800	-.010
.50	.63	.015	-.179	.71	.119	2.21	----	-.08	2.4938	.0748	.411	----	-.016
.50	1.06	.073	-.155	1.18	.203	2.28	4.40	-.05	.8965	.1312	.425	.819	-.039
.50	1.48	.085	-.094	1.56	.124	2.46	----	-.08	.4583	.0779	.458	----	-.004
.50	2.11	.149	.070	2.37	.106	2.84	4.34	-.04	.2246	.0669	.529	.808	-.008
.50	2.53	.167	.163	2.34	.083	3.08	----	.02	.1560	.0521	.573	----	.004
.50	3.17	.179	.170	3.55	.057	3.08	3.69	.19	.0999	.0357	.573	.687	.035
.50	3.59	.176	.104	4.03	.043	2.93	----	.27	.0777	.0274	.546	----	.051
.50	4.22	.173	.025	4.74	.031	2.73	3.09	.37	.0562	.0194	.509	.575	.069

TABLE II - Continued
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 6 WITH CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(\frac{L}{W})^{1/3}}$	$\frac{l}{(\frac{L}{W})^{1/3}}$	$\frac{h}{(\frac{L}{W})^{1/3}}$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 20^\circ$													
0	0	0	0	-----	-----	-----	-----	-----	0	0	-----	0.233	0.172
0	.63	0	0	-----	-----	-----	-----	-----	0	0	-----	.123	.176
0	1.06	0	0	-----	-----	-----	-----	-----	0	0	-----	.178	.185
0	1.48	0	0	-----	-----	-----	-----	-----	0	0	-----	.084	.188
0	2.11	0	0	-----	-----	-----	-----	-----	0	0	-----	.188	.188
0	2.53	0	0	-----	-----	-----	-----	-----	0	0	-----	.188	.188
0	3.17	0	0	-----	-----	-----	-----	-----	0	0	-----	0	.188
0	3.59	0	0	-----	-----	-----	-----	-----	0	0	-----	.323	
0	4.22	0	0	-----	-----	-----	-----	-----	0	0	-----	0	.188
0	4.64	0	0	-----	-----	-----	-----	-----	0	0	-----	0	.188
0	5.28	0	0	-----	-----	-----	-----	-----	0	0	-----	0	.188
0	6.33	0	0	-----	-----	-----	-----	-----	0	0	-----	0	.188
0	12.66	0	0	-----	-----	-----	-----	-----	0	0	-----	0	.188
.10	0	0	-.095	0	-----	2.38	4.45	0.85	-----	0.259	.485	.092	
.10	.63	.008	-.090	.93	0.185	2.53	-----	.80	0.4988	0.0399	.279	-----	.087
.10	1.06	.026	-.086	1.55	0.134	2.72	4.48	.87	.1797	.0288	.297	.488	.095
.10	1.48	.025	-.069	2.17	.106	3.12	-----	.90	.0917	.0229	.340	-----	.098
.10	2.11	.027	-.069	3.10	.056	3.12	3.79	1.04	.0449	.0121	.340	.413	.114
.10	2.53	.024	-.080	3.72	.055	2.87	-----	1.13	.0312	.0075	.313	-----	.123
.10	3.17	.024	-.101	4.65	.022	2.44	2.96	1.21	.0200	.0048	.266	.323	.132
.10	3.59	.023	-.110	5.26	.017	2.26	-----	1.26	.0155	.0036	.246	-----	.138
.10	4.22	.021	-.125	6.19	.011	1.92	2.29	1.33	.0112	.0024	.209	.250	.145
.10	4.64	.019	-.139	6.81	.008	1.58	-----	1.36	.0093	.0018	.172	-----	.148
.10	5.28	.018	-.151	7.74	.006	1.33	1.80	1.39	.0072	.0013	.145	.196	.152
.10	6.33	.016	-.170	9.29	.004	.90	1.39	1.42	.0050	.0008	.098	.152	.155
.10	7.39	.016	-.180	10.64	.003	.68	1.11	1.46	.0037	.0006	.074	.121	.159
.10	8.44	.016	-.190	12.39	.002	.46	.85	1.46	.0028	.0004	.051	.093	.159
.10	9.50	.016	-.194	13.94	.002	.37	.88	1.48	.0022	.0004	.040	.096	.161
.10	10.55	.018	-.210	15.49	.001	.06	.75	1.49	.0018	.0003	.007	.081	.162
.10	11.61	.018	-.204	17.04	.001	.19	.62	1.49	.0015	.0003	.020	.067	.162
.10	12.66	.018	-.214	18.59	.001	-.06	.67	1.50	.0013	.0002	-.007	.073	.163
.10	13.72	.018	-.209	20.13	.001	-.06	.18	1.50	.0011	.0002	-.007	.020	.163
.10	14.77	.018	-.225	21.68	.001	-.28	.44	1.50	.0009	.0002	-.030	.048	.163
.10	15.83	.019	-----	23.23	.001	-----	.51	1.50	.0008	.0002	-----	.034	.163
.20	0	0	-.165	0	-----	2.11	4.17	.45	-----	-----	.290	.572	.060
.20	.63	.012	-.153	.83	0	2.26	-----	.42	.9975	.0599	.510	-----	.057
.20	1.06	.034	-.141	1.38	.179	2.43	4.27	.47	.3594	.0611	.334	.587	.064
.20	1.48	.052	-.102	1.93	.139	2.78	-----	.49	.1653	.0477	.361	-----	.067
.20	2.11	.059	-.080	2.76	.077	2.97	3.80	.61	.0896	.0255	.407	.522	.084
.20	2.53	.060	-.094	3.31	.055	2.87	-----	.70	.0624	.0187	.394	-----	.096
.20	3.17	.056	-.130	4.14	.053	2.55	3.01	.81	.0599	.0112	.350	.413	.112
.20	3.59	.053	-.159	4.69	.024	2.31	-----	.89	.0311	.0082	.317	-----	.122
.20	4.22	.047	-.194	5.52	.015	2.01	2.45	.95	.0225	.0053	.276	.337	.130
.20	4.64	.046	-.214	6.07	.013	1.84	-----	.98	.0186	.0043	.253	-----	.135
.20	5.28	.043	-.241	6.90	.009	1.60	2.05	1.01	.0144	.0031	.219	.281	.139
.20	6.33	.036	-.276	8.28	.005	1.28	1.64	1.05	.0100	.0018	.175	.225	.145
.20	7.39	.033	-.307	9.66	.004	1.01	1.44	1.08	.0073	.0012	.158	.197	.149
.20	8.44	.033	-.320	11.04	.003	.88	1.15	1.10	.0056	.0010	.121	.157	.152
.20	9.50	.034	-.352	12.42	.002	.61	1.11	1.14	.0044	.0008	.084	.153	.156
.20	10.55	.035	-.350	13.80	.002	.63	1.06	1.14	.0036	.0006	.087	.146	.156
.20	11.61	.034	-.381	15.18	.001	.37	.75	1.15	.0030	.0005	.051	.103	.157
.20	12.66	.033	-.391	16.56	.001	.27	.65	1.15	.0025	.0004	.037	.089	.157
.20	13.72	.033	-.401	17.94	.001	.20	.70	1.15	.0021	.0004	.027	.096	.157

TABLE II - Concluded

EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 6 WITH CHINE STRIPS

$c_{\Delta Q}$	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(\frac{\Delta}{w})^{1/3}}$	$\frac{z}{(\frac{\Delta}{w})^{1/3}}$	$\frac{h}{(\frac{\Delta}{w})^{1/3}}$	c_{L_Q}	c_{D_Q}	$\frac{x}{E}$	$\frac{z}{E}$	$\frac{h}{E}$
$\tau = 20^\circ$ - Concluded													
.30	0	0	-0.200	0	----	2.10	4.11	0.21	----	0.330	0.645	0.033	
.30	.63	.016	-.185	.77	0.178	2.21	----	.20	1.4963	0.0798	.347	----	.032
.30	1.06	.052	-.175	1.29	.203	2.30	4.20	.25	.5351	.0934	.361	.660	.039
.30	1.45	.072	-.111	1.80	.147	2.44	----	.25	.2750	.0660	.415	----	.039
.30	2.11	.098	-.060	2.58	.098	2.90	3.82	.36	.1348	.0440	.455	.601	.057
.30	2.53	.096	-.069	3.09	.067	2.85	----	.46	.0936	.0299	.448	----	.073
.30	3.17	.092	-.126	3.87	.041	2.57	3.04	.61	.0599	.0184	.404	.477	.096
.30	3.59	.088	-.169	4.38	.031	2.36	----	.69	.0466	.0137	.371	----	.108
.30	4.22	.080	-.216	5.16	.020	2.13	2.48	.76	.0337	.0090	.334	.390	.119
.30	4.64	.079	-.255	5.67	.016	1.95	----	.79	.0278	.0073	.307	----	.124
.30	5.28	.072	-.294	5.45	.012	1.74	2.13	.82	.0216	.0052	.273	.334	.130
.30	6.33	.062	-.355	7.74	.007	1.41	1.82	.88	.0150	.0031	.222	.286	.138
.30	7.39	.057	-.401	9.02	.005	1.18	1.61	.91	.0110	.0021	.185	.255	.142
.30	8.14	.052	-.421	10.31	.003	1.08	1.38	.93	.0084	.0015	.169	.216	.146
.30	9.50	.052	-.472	11.60	.003	.81	1.16	.95	.0067	.0012	.128	.182	.149
.30	10.55	.054	-.493	12.89	.002	.71	1.12	.96	.0054	.0010	.111	.177	.151
.30	11.61	.052	-.524	14.18	.002	.56	.95	.97	.0044	.0008	.088	.149	.152
.40	0	0	-.216	0	----	2.11	4.09	.05	----	----	.364	.707	.009
.40	.63	.018	-.200	.74	.165	2.18	----	.04	1.9950	.0693	.377	----	.006
.40	1.06	.072	-.186	1.23	.238	2.26	4.17	.08	.7188	.1294	.391	.721	.014
.40	1.48	.090	-.111	1.72	.152	2.52	----	.09	.3666	.0825	.435	----	.016
.40	2.17	.139	-.070	2.46	.115	2.79	3.91	.17	.1797	.0624	.482	.676	.030
.40	2.53	.185	-.019	2.96	.082	2.85	----	.27	.1248	.0446	.489	----	.047
.40	3.17	.181	-.086	3.70	.052	2.61	3.00	.41	.0799	.0282	.452	.519	.077
.40	3.59	.132	-.149	4.19	.038	2.40	----	.53	.0622	.0205	.415	----	.092
.40	4.22	.120	-.221	4.93	.025	2.16	2.53	.51	.0449	.0135	.374	.438	.106
.40	4.64	.113	-.267	5.42	.019	2.01	----	.65	.0371	.0105	.347	----	.112
.40	5.28	.105	-.328	6.16	.014	1.79	2.17	.70	.0288	.0076	.310	.376	.120
.40	6.33	.093	-.407	7.39	.008	1.52	1.88	.74	.0200	.0046	.263	.325	.129
.40	7.39	.085	-.471	8.62	.006	1.31	1.74	.78	.0147	.0031	.226	.300	.135
.40	8.44	.078	-.508	9.85	.004	1.17	1.49	.81	.0112	.0022	.202	.258	.140
.50	0	0	-.210	0	----	2.12	4.08	-.07	----	----	.394	.760	-.014
.50	.63	.024	-.190	.7-	.190	2.17	----	-.06	2.4938	.1197	.404	----	-.015
.50	1.06	.089	-.185	1.18	.254	2.21	4.14	-.03	.8935	.1599	.411	.772	-.005
.50	1.45	.105	-.101	1.66	.153	2.43	----	-.03	.4583	.0962	.452	----	-.005
.50	2.11	.180	-.010	2.37	.128	2.70	3.92	.05	.2246	.0809	.502	.730	.009
.50	2.53	.188	-.036	2.84	.093	2.77	----	.15	.1560	.0586	.516	----	.029
.50	3.17	.186	-.036	3.55	.059	2.59	3.13	.33	.0999	.0372	.482	.584	.061
.50	3.59	.177	-.101	4.03	.044	2.44	----	.42	.0777	.0275	.455	----	.078
.50	4.22	.162	-.204	4.74	.029	2.19	2.56	.52	.0562	.0162	.408	.477	.097

TABLE III
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 9 WITH CHINE STRIPS

$c_{\Delta Q}$	c_{V_Q}	c_{S_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(\frac{A}{V})^{1/3}}$	$\frac{l}{(\frac{A}{V})^{1/3}}$	$\frac{h}{(\frac{A}{V})^{1/3}}$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 0^\circ$													
0	0	0	0	---	---	---	---	---	0	0.0050	---	0.487	0.056
0	.63	.001	0	---	---	---	---	---	0	0.0056	---	.058	
0	1.06	.002	0	---	---	---	---	---	0	0.0036	---	.786	.058
0	1.48	.004	0	---	---	---	---	---	0	0.0037	---	.056	
0	2.11	.010	.011	---	---	---	---	---	0	0.0045	---	.816	.054
0	2.53	.018	.015	---	---	---	---	---	0	0.0056	---	.052	
0	3.17	.031	.035	---	---	---	---	---	0	0.0062	---	.865	.048
0	3.59	.036	.040	---	---	---	---	---	0	0.0056	---	.050	
0	4.22	.048	.067	---	---	---	---	---	0	0.0054	---	.861	.048
0	4.64	.056	.074	---	---	---	---	---	0	0.0052	---	.051	
0	5.23	.071	.100	---	---	---	---	---	0	0.0051	---	.861	.048
0	6.33	.056	.165	---	---	---	---	---	0	0.0048	---	.857	.048
0	7.39	.125	.222	---	---	---	---	---	0	0.0046	---	.865	.048
0	8.44	.165	.283	---	---	---	---	---	0	0.0046	---	.854	.048
0	9.50	.212	.384	---	---	---	---	---	0	0.0047	---	.867	.046
.10	0	0	.030	0	6.68	9.02	0.40	---	0	0.554	---	.748	.035
.10	.63	.002	.035	.93	0.046	6.77	.38	4988	.0100	.562	---	.031	
.10	1.06	.007	.067	1.35	.057	7.47	11.49	.37	.1797	.0124	.820	.953	.051
.10	1.48	.013	.081	2.17	.056	7.79	---	.36	.0917	.0119	.546	---	.030
.10	2.11	.025	.099	3.10	.051	8.16	11.35	.37	.0449	.0112	.677	.942	.031
.10	2.53	.036	.109	3.72	.051	8.38	---	.33	.0312	.0112	.695	---	.028
.10	3.17	.071	.145	4.55	.065	9.14	11.56	.28	.0200	.0142	.759	.959	.023
.10	3.59	.109	.163	5.26	.079	9.55	---	.26	.0155	.0169	.792	---	.021
.10	4.22	.245	.204	6.19	.130	10.39	12.69	.16	.0112	.0276	.862	1.053	.014
.20	0	0	.060	0	5.30	8.04	.23	---	0	0.554	---	.840	.024
.20	.63	.002	.066	.83	.029	5.35	---	.21	.9975	.0100	.559	---	.022
.20	1.06	.010	.116	1.38	.053	5.79	9.57	.18	.3594	.0180	.605	1.000	.019
.20	1.48	.021	.156	1.93	.056	6.10	---	.18	.1853	.0192	.638	---	.019
.20	2.11	.038	.190	2.76	.050	6.40	9.57	.18	.0898	.0171	.669	1.000	.019
.20	2.53	.055	.185	3.31	.050	6.35	---	.17	.0624	.0172	.664	---	.018
.20	3.17	.112	.189	4.12	.064	6.40	9.57	.14	.0399	.0224	.669	1.000	.015
.20	3.59	.183	.184	4.69	.082	6.35	---	.09	.0311	.0284	.664	---	.009
.30	0	0	.085	0	4.66	7.62	.12	---	0	0.557	---	.912	.014
.30	.63	.004	.090	.77	.045	4.65	---	.10	1.4963	.0200	.524	---	.015
.30	1.06	.016	.154	1.29	.065	5.08	8.36	.08	.5391	.0258	.508	1.000	.009
.30	1.48	.029	.201	1.80	.060	5.18	---	.07	.2750	.0266	.620	---	.008
.30	2.11	.056	.244	2.58	.056	5.40	8.36	.07	.1348	.0252	.646	1.000	.008
.30	2.53	.089	.228	3.09	.062	5.32	---	.06	.0936	.0278	.636	---	.007
.30	3.17	.169	.200	3.87	.076	5.17	8.36	.01	.0599	.0337	.618	1.000	.002
.40	0	0	.107	0	4.17	7.25	.05	---	0	0.549	---	.955	.007
.40	.63	.005	.105	.74	.046	4.15	---	.04	1.9950	.0249	.546	---	.005
.40	1.06	.020	.174	1.23	.066	4.38	7.59	.01	.7188	.0359	.577	1.000	.002
.40	1.48	.029	.214	1.72	.050	4.52	---	.004	.3666	.0266	.595	---	.001
.40	2.11	.073	.264	2.46	.061	4.69	7.59	.01	.1797	.0528	.618	1.000	.002
.40	2.53	.108	.250	2.96	.063	4.58	---	.03	.1248	.0337	.603	---	.004
.40	3.17	.181	.180	3.70	.066	4.40	7.59	.09	.0799	.0361	.579	1.000	.011
.50	0	0	.126	0	3.85	7.05	0	---	0	0.546	1.000	0	
.50	.63	.005	.113	.71	.040	3.81	---	.01	2.4938	.0249	.541	---	.002
.50	1.06	.024	.190	1.18	.068	4.00	7.05	.05	.8985	.0431	.567	1.000	.008
.50	1.48	.047	.248	1.66	.068	4.16	---	.06	.4583	.0431	.590	---	.009
.50	2.11	.084	.257	2.37	.060	4.17	7.05	.08	.2246	.0377	.592	1.000	.011
.50	2.53	.118	.205	2.84	.059	4.05	---	.10	.1560	.0368	.574	---	.014
.50	3.17	.219	.134	3.55	.070	3.87	7.05	.19	.0999	.0437	.549	1.000	.027

TABLE III - Continued
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 9 WITH CHINE STRIPS

C_{DQ}	C_{VQ}	C_{RQ}	C_{VQ}	C_V	C_D	$\frac{x}{(h)}$	$\frac{l}{(h)}$	$\frac{h}{(h)}$	C_L	C_D	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 4^\circ$													
0	0	0	0	0	0	0	0	0	0	0.0050	0.500	0.412	0.060
0	.63	.001	0	0	0	0	0	0	0	0.0036	0.500	.568	.065
0	1.06	.002	0	0	0	0	0	0	0	0.0018	0.500	0.568	.064
0	1.48	.002	0	0	0	0	0	0	0	0.0018	2.636	.579	.063
0	2.11	.008	.007	0	0	0	0	0	0	0.0044	2.697	-----	.062
0	2.53	.014	.012	0	0	0	0	0	0	0.0038	3.949	.597	.061
0	3.17	.019	.026	0	0	0	0	0	0	0.0040	4.077	-----	.060
0	3.59	.026	.036	0	0	0	0	0	0	0.0037	4.790	.611	.060
0	4.22	.033	.055	0	0	0	0	0	0	0.0038	5.543	-----	.059
0	4.64	.041	.080	0	0	0	0	0	0	0.0038	4.979	.630	.060
0	5.28	.053	.092	0	0	0	0	0	0	0.0038	4.805	-----	.060
0	6.33	.073	.149	0	0	0	0	0	0	0.0036	5.795	.617	.059
0	7.39	.096	.186	0	0	0	0	0	0	0.0035	5.466	.611	.060
0	8.44	.120	.244	0	0	0	0	0	0	0.0034	5.743	.611	.059
0	9.50	.150	.283	0	0	0	0	0	0	0.0033	5.364	.611	.060
0	10.55	.193	.335	0	0	0	0	0	0	0.0035	4.982	.600	.061
0	11.61	.230	.409	0	0	0	0	0	0	0.0034	5.079	.600	.060
0	12.66	.280	.480	0	0	0	0	0	0	0.0035	4.923	.609	.061
0	13.72	.320	.533	0	0	0	0	0	0	0.0034	4.792	.590	.060
0	14.77	.369	.630	0	0	0	0	0	0	0.0040	4.897	.600	.060
0	15.83	.418	.682	0	0	0	0	0	0	0.0030	4.702	.583	.060
0	16.88	.470	.785	0	0	0	0	0	0	0.0030	4.805	-----	.060
.10	0	0	-.054	0	0	4.85	9.30	0.40	-----	0.0000	4.03	.771	.033
.10	.63	.002	-.052	.93	0.016	4.91	9.30	.38	4.988	.0100	4.08	-----	.031
.10	1.06	.007	-.014	1.55	.058	5.71	9.45	.56	1.797	.0226	4.74	.782	.030
.10	1.48	.012	0	2.17	.051	6.03	-----	.56	.0917	.0110	5.00	-----	.030
.10	2.11	.020	.011	3.10	.042	6.40	9.22	.38	.0449	.0090	5.31	.765	.030
.10	2.53	.028	.032	3.72	.040	6.71	-----	.32	.0312	.0097	5.56	-----	.027
.10	3.17	.041	.114	4.65	.038	6.40	9.18	.29	.0200	.0082	.697	.786	.024
.10	3.59	.049	.155	5.26	.035	9.27	-----	.32	.0155	.0076	.769	-----	.027
.10	4.22	.059	.181	6.19	.031	9.76	8.99	.36	.0112	.0066	.810	.746	.030
.10	4.64	.068	.186	6.21	.029	9.88	-----	.40	.0093	.0063	.820	-----	.033
.10	5.28	.081	.201	7.74	.027	10.14	8.65	.41	.0072	.0058	.841	.718	.034
.10	6.33	.090	.255	9.29	.021	11.19	8.32	.44	.0050	.0045	.928	.690	.035
.10	7.39	.116	.280	10.84	.020	11.61	8.00	.45	.0037	.0043	.954	.664	.038
.10	8.44	.141	.304	12.39	.019	12.03	7.80	.49	.0028	.0040	.997	.647	.041
.10	9.50	.169	.395	13.94	.017	13.69	7.73	.49	.0022	.0037	1.136	.641	.041
.10	10.55	.204	.403	15.49	.017	15.54	7.60	.50	.0018	.0037	1.123	.630	.042
.10	11.61	.247	.464	17.04	.017	14.55	7.44	.52	.0015	.0037	1.208	.617	.043
.10	12.66	.294	.535	18.59	.017	15.66	7.52	.53	.0013	.0037	1.300	.624	.044
.10	13.72	.338	.595	20.13	.017	16.06	7.49	.52	.0011	.0036	1.359	.622	.043
.10	14.77	.385	.683	21.68	.016	17.70	7.29	.52	.0009	.0035	1.469	.605	.043
.10	15.83	.439	-----	23.23	.016	7.29	.52	.0008	.0035	-----	.605	-----	.043
.20	0	0	-.094	0	0	3.97	8.11	.21	-----	0.0000	.415	.848	.023
.20	.63	.003	-.080	.83	.044	4.10	-----	.20	.9975	.0150	4.28	-----	.021
.20	1.06	.012	-.050	1.38	.053	4.54	8.24	.18	.3594	.0216	4.74	.861	.019
.20	1.48	.020	0	1.93	.054	4.78	-----	.20	.1833	.0183	5.00	-----	.021
.20	2.11	.031	.025	2.76	.047	5.00	8.06	.20	.0898	.0139	.523	.842	.021
.20	2.53	.041	.043	3.31	.037	5.20	-----	.17	.0624	.0128	.544	-----	.018
.20	3.17	.063	.146	4.14	.037	6.01	8.30	.15	.0399	.0126	.628	.867	.016
.20	3.59	.082	.255	4.69	.037	6.92	-----	.12	.0311	.0127	.723	-----	.013
.20	4.22	.110	.403	5.52	.036	8.12	8.36	.10	.0225	.0124	.849	.874	.011
.20	4.64	.101	.394	6.07	.027	8.05	-----	.13	.0186	.0094	.841	-----	.014
.20	5.28	.105	.399	6.50	.022	8.08	7.64	.22	.0144	.0075	.844	.799	.023
.20	6.33	.127	.403	8.28	.018	8.09	7.28	.28	.0100	.0063	.846	.761	.029
.20	7.39	.150	.404	9.66	.016	8.27	6.77	.32	.0073	.0055	.864	.707	.033
.20	8.44	.166	.439	11.04	.014	8.34	6.56	.33	.0056	.0047	.872	.686	.037
.20	9.50	.195	.484	12.42	.013	8.69	6.38	.31	.0044	.0043	.908	.667	.039
.20	10.55	.221	.504	13.80	.012	8.80	6.24	.37	.0036	.0040	.920	.652	.039
.20	11.61	.263	.548	15.18	.011	9.10	6.09	.39	.0030	.0039	.951	.637	.041
.20	12.66	.308	.610	16.56	.011	9.52	6.08	.40	.0025	.0038	.995	.635	.042
.20	13.72	.357	.667	17.94	.011	9.88	5.97	.40	.0021	.0036	1.033	.624	.042

TABLE III - Continued
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 9 WITH CHINE STRIPS

C_{DQ}	C_{VQ}	C_{FQ}	C_{KQ}	$C_{V\Delta}$	$C_{D\Delta}$	$\frac{x}{(\frac{A}{w})^{1/3}}$	$\frac{l}{(\frac{A}{w})^{1/3}}$	$\frac{h}{(\frac{A}{w})^{1/3}}$	C_{LQ}	C_{DQ}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 4^\circ$ - Concluded													
.30	0	0	-0.109	0	-----	3.64	7.50	0.11	-----	0.436	0.897	0.013	
.30	.63	.003	-.094	.77	0.033	3.71	-----	.10	1.4963	0.0150	.444	-----	.012
.30	1.06	.016	-.019	1.29	.064	4.10	7.64	.08	.5391	.0288	.490	.914	.009
.30	1.43	.027	.015	1.80	.055	4.25	-----	.08	.2790	.0247	.508	-----	.009
.30	2.11	.042	.049	2.58	.042	4.41	7.50	.08	.1348	.0189	.528	.897	.010
.30	2.53	.056	.074	3.09	.039	4.55	-----	.08	.0936	.0175	.544	-----	.010
.30	3.17	.085	.174	5.87	.058	5.04	7.63	.05	.0599	.0170	.603	.912	.006
.30	3.59	.116	.293	4.38	.040	5.62	-----	.03	.0466	.0180	.672	-----	.004
.30	4.22	.162	.479	5.16	.041	6.49	7.86	-.01	.0337	.0182	.777	.940	-.001
.30	4.64	.209	.657	5.67	.043	7.31	-----	-.02	.0278	.0294	.874	-----	-.003
.30	5.28	.273	-----	6.45	.044	-----	7.95	-.05	.0216	.0198	-----	.951	-.006
.30	6.33	.150	.630	7.74	.017	7.22	6.65	.19	.0150	.0075	.864	.795	.022
.30	7.39	.179	-----	9.02	.015	-----	6.27	.24	.0110	.0066	-----	.750	.029
.30	8.44	.207	.565	10.31	.013	6.88	5.95	.28	.0084	.0058	.823	.711	.034
.30	9.50	.221	.616	11.60	.011	7.10	5.75	.30	.0067	.0049	.849	.688	.036
.30	10.55	.251	.620	12.89	.010	7.10	5.59	.32	.0054	.0045	.849	.669	.038
.30	11.61	.280	.636	14.18	.009	7.16	5.45	.34	.0044	.0042	.856	.652	.040
.40	0	0	-.132	0	-----	3.41	7.09	.04	-----	-----	.449	.934	.005
.40	.63	.005	-.092	.74	.046	3.49	-----	.03	1.9950	.0249	.559	-----	.004
.40	1.06	.021	-.004	1.23	.069	3.77	7.22	.01	.7188	.0377	.597	.951	.001
.40	1.43	.034	.036	1.72	.057	3.91	-----	.01	.3666	.0312	.515	-----	.002
.40	2.11	.053	.074	2.46	.044	4.05	7.11	.03	.1797	.0238	.533	.936	.003
.40	2.53	.071	.104	2.96	.041	4.15	-----	.01	.1248	.0221	.546	-----	.002
.40	3.17	.107	.201	3.70	.039	4.46	7.19	0	.0799	.0214	.587	.947	0
.40	3.59	.148	.301	4.19	.042	4.81	-----	-.03	.0622	.0230	.633	-----	-.004
.40	4.22	.238	.484	4.93	.049	5.38	7.43	-.07	.0449	.0267	.708	.979	-.010
.40	4.64	.320	.619	5.42	.055	5.79	-----	-.12	.0371	.0297	.762	-----	-.015
.40	5.28	.280	.828	6.16	.037	6.49	7.59	-.17	.0288	.0201	.854	1.000	-.023
.40	6.33	.193	.922	7.39	.018	6.83	6.45	.10	.0200	.0056	.900	.850	.013
.40	7.39	.201	.828	8.62	.014	6.52	5.81	.18	.0147	.0074	.859	.765	.024
.40	8.44	.231	.786	9.85	.012	6.36	5.70	.22	.0112	.0065	.858	.750	.029
.50	0	0	-.101	0	-----	3.27	6.79	-.02	-----	-----	.454	.964	-.003
.50	.63	.005	-.074	.71	.040	3.34	-----	-.03	2.4938	.0249	.474	-----	-.004
.50	1.06	.026	.011	1.18	.074	3.56	6.88	-.05	.8985	.0467	.505	.976	-.007
.50	1.43	.044	.066	1.66	.064	3.69	-----	-.03	.4563	.0403	.523	-----	-.005
.50	2.11	.066	.104	2.37	.047	3.78	6.81	-.03	.2246	.0296	.536	.966	-.004
.50	2.53	.088	.144	2.84	.044	3.88	-----	-.04	.1560	.0275	.551	-----	-.006
.50	3.17	.137	.218	3.55	.043	4.07	6.87	-.06	.0999	.0274	.577	.974	-.008
.50	3.59	.183	.280	4.03	.045	4.21	-----	-.08	.0777	.0284	.597	-----	-.011
.50	4.22	.360	.525	4.74	.064	4.79	7.05	-.15	.0562	.0404	.579	1.000	-.021
$\tau = 8^\circ$													
0	0	0	0	0	-----	-----	-----	-----	0	0	-----	0.374	0.075
0	.63	0	.007	-----	-----	-----	-----	-----	0	0	-----	-----	.075
0	1.06	0	.007	-----	-----	-----	-----	-----	0	0	-----	.306	.075
0	1.43	.001	.007	-----	-----	-----	-----	-----	0	.0008	.9.046	-----	.075
0	2.11	.002	.007	-----	-----	-----	-----	-----	0	.0010	4.164	.306	.075
0	2.53	.001	.007	-----	-----	-----	-----	-----	0	.0002	28.704	-----	.075
0	3.17	.005	.003	-----	-----	-----	-----	-----	0	.0010	1.354	.284	.074
0	3.59	.009	0	-----	-----	-----	-----	-----	0	.0014	.500	-----	.074
0	4.22	.013	0	-----	-----	-----	-----	-----	0	.0014	.500	.320	.074
0	4.64	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	5.28	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----

TABLE III - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 9 WITH CHINE STRIPS

$c_{\Delta Q}$	c_{VQ}	c_{RQ}	c_{MQ}	$c_{V\Delta}$	$c_{D\Delta}$	$\frac{x}{(\Delta)}^{1/3}$	$\frac{z}{(\Delta)}^{1/3}$	$\frac{h}{(\Delta)}^{1/3}$	c_{LQ}	c_{DQ}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$\tau = 8^\circ$ - Continued													
0	6.33	---	---	---	---	---	---	---	0	---	---	0	0.083
0	7.39	0	0	---	---	---	---	---	0	0	---	0	0.083
0	8.44	---	0	---	---	---	---	---	0	0	---	0	0.084
0	9.50	.002	0	---	---	---	---	---	0	0	0.500	0	0.084
0	10.55	---	.013	---	---	---	---	---	0	0	0.500	0	0.084
0	11.61	.002	0	---	---	---	---	---	0	0	.500	0	0.084
0	12.67	---	---	---	---	---	---	---	0	0	---	0	0.085
0	13.72	.005	0	---	---	---	---	---	0	0	.500	0	0.085
0	14.77	.005	0	---	---	---	---	---	0	0	.500	0	0.087
0	15.83	.002	.023	---	---	---	---	---	0	0	12.950	0	0.085
C	16.88	.006	.013	---	---	---	---	---	0	0.0001	3.210	0	.090
.10	0	0	-.120	0	---	3.43	7.16	0.51	---	---	.265	.594	.043
.10	.63	.002	-.105	.93	0.046	3.77	4.49	.4983	.0100	.313	---	0.041	
.10	1.06	.008	-.093	1.55	.067	4.02	7.14	.49	.1797	.0144	.333	.592	.041
.10	1.48	.011	-.082	2.17	.047	4.26	---	.53	.0917	.0101	.351	---	.044
.10	2.11	.021	-.129	3.10	.042	3.30	6.95	.53	.0449	.0090	.274	.577	.044
.10	2.55	.026	-.023	3.72	.038	5.57	---	.50	.0312	.0081	.462	---	.042
.10	3.17	.032	0	4.65	.030	6.03	6.59	.53	.0200	.0064	.500	.547	.044
.10	3.59	.037	0	5.26	.027	6.03	---	.57	.0155	.0058	.500	---	.047
.10	4.22	.042	0	6.19	.022	6.03	6.16	.62	.0112	.0047	.500	.511	.051
.10	4.64	.043	-.003	6.21	.019	5.87	---	.68	.0093	.0040	.487	---	.056
.10	5.26	.050	-.011	7.7	.017	5.81	5.61	.69	.0072	.0036	.482	.466	.058
.10	6.33	.061	-.012	9.29	.015	5.78	5.38	.72	.0050	.0032	.482	.447	.060
.10	7.39	.080	-.017	10.84	.013	5.68	5.15	.73	.0037	.0029	.472	.427	.061
.10	8.44	.098	-.020	12.39	.013	5.65	5.05	.75	.0026	.0028	.469	.439	.062
.10	9.50	.117	-.022	13.34	.012	5.62	5.12	.76	.0022	.0026	.456	.425	.063
.10	10.55	.135	-.028	15.49	.011	5.50	5.05	.76	.0018	.0024	.456	.419	.063
.10	11.61	.155	-.029	17.04	.011	5.50	4.97	.76	.0015	.0023	.456	.412	.063
.10	12.56	.178	-.052	18.59	.010	4.94	4.89	.76	.0013	.0022	.410	.406	.063
.10	13.72	.195	-.034	20.13	.010	5.44	4.79	.76	.0011	.0021	.451	.397	.063
.10	14.77	.213	-.079	21.68	.009	4.73	4.66	.75	.0009	.0020	.392	.387	.063
.10	15.83	.244	-.062	23.23	.009	5.01	4.48	.76	.0008	.0019	.415	.372	.063
.20	0	0	-.201	0	---	3.04	6.56	.28	---	---	.318	.686	.029
.20	.63	.005	-.186	.83	.073	3.19	---	.25	.9975	.0249	.333	---	.026
.20	1.06	.016	-.145	1.38	.084	3.53	6.66	.26	.3594	.0288	.359	.694	.027
.20	1.48	.020	-.129	1.93	.054	3.68	---	.28	.1833	.0183	.385	---	.029
.20	2.11	.034	-.075	2.76	.045	4.17	6.46	.28	.0898	.0153	.456	.675	.029
.20	2.53	.043	-.154	3.31	.039	3.65	---	.25	.0624	.0134	.382	---	.026
.20	3.17	.054	-.062	4.44	.032	5.30	6.30	.28	.0399	.0108	.554	.658	.029
.20	3.59	.060	.070	4.89	.027	5.35	---	.33	.0311	.0093	.559	---	.035
.20	4.22	.067	.070	5.52	.022	5.55	5.62	.38	.0225	.0075	.559	.588	.040
.20	5.64	.070	.042	6.07	.019	5.13	---	.44	.0186	.0065	.536	---	.046
.20	5.28	.074	.034	6.90	.015	5.05	5.11	.48	.0144	.0053	.528	.534	.052
.20	6.33	.086	.011	8.28	.013	4.88	4.72	.52	.0100	.0043	.510	.494	.055
.20	7.39	.098	0	9.66	.011	4.78	4.56	.55	.0073	.0036	.500	.476	.057
.20	8.44	.117	-.024	11.04	.010	4.56	4.48	.58	.0056	.0033	.480	.468	.060
.20	9.50	.139	-.024	12.42	.009	4.59	4.36	.58	.0044	.0031	.480	.455	.060
.20	10.55	.160	-.058	13.80	.008	4.49	4.19	.59	.0036	.0029	.469	.438	.061
.20	11.61	.186	-.027	15.18	.008	4.59	4.07	.60	.0030	.0028	.480	.425	.062
.20	12.66	.208	-.052	16.56	.008	4.39	4.09	.60	.0025	.0026	.459	.427	.062
.20	13.72	.237	-.032	17.94	.007	4.54	3.91	.60	.0021	.0025	.474	.408	.062
.30	0	0	-.241	0	---	2.96	6.27	.14	---	---	.354	.750	.017
.30	.63	.005	-.220	.77	.056	3.03	---	.13	1.4963	.0249	.369	---	.015
.30	1.06	.022	-.170	1.29	.086	3.32	6.38	.13	.5391	.0395	.597	.763	.016
.30	1.48	.032	-.149	1.80	.065	3.45	---	.16	.2750	.0293	.413	---	.019
.30	2.11	.047	-.083	2.58	.047	3.77	6.19	.16	.1348	.0211	.451	.741	.019
.30	2.53	.061	-.008	3.09	.042	4.14	---	.14	.0936	.0190	.495	---	.017
.30	3.17	.083	.102	3.87	.037	4.67	6.22	.13	.0599	.0166	.559	.744	.016
.30	3.59	.088	.184	4.38	.031	5.08	---	.19	.0466	.0137	.608	---	.023
.30	4.22	.093	.184	5.16	.023	5.06	5.52	.26	.0337	.0104	.605	.660	.031

TABLE III - Continued

 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 9 WITH CHINE STRIPS

C_{DQ}	C_{VQ}	C_{RQ}	C_{MQ}	$C_{V\Delta}$	$C_{D\Delta}$	$\frac{x}{(\Delta)}$	$\frac{z}{(\Delta)}$	$\frac{h}{(\Delta)}$	C_{LQ}	C_{DQ}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$\tau = 6^\circ$ - Concluded													
.30	4.64	0.093	0.146	5.67	0.019	4.89	----	0.33	0.0278	0.0086	0.585	----	0.040
.30	5.28	.104	.113	6.45	.017	4.71	4.87	.37	.0216	.0075	.564	0.583	.045
.30	6.33	.110	.065	7.74	.012	4.50	4.47	.42	.0150	.0055	.558	.534	.050
.30	7.39	.123	.032	9.02	.010	4.33	4.22	.46	.0110	.0045	.518	.504	.056
.30	8.44	.139	0	10.31	.009	4.18	3.93	.49	.0084	.0039	.500	.470	.059
.30	9.50	.158	-.014	11.60	.008	4.11	3.93	.50	.0067	.0035	.492	.470	.060
.30	10.55	.182	-.044	12.89	.007	3.99	3.88	.51	.0054	.0033	.477	.464	.061
.30	11.61	.206	-.034	14.18	.007	4.03	3.72	.52	.0044	.0031	.482	.454	.062
.40	0	0	-.258	0	----	2.92	6.18	.04	----	----	.385	.814	.006
.40	.63	.006	-.256	.74	.073	2.98	----	.04	1.9950	.0399	.592	----	.005
.40	1.06	.030	-.174	1.23	.099	3.21	6.23	.04	.7188	.0539	.423	.820	.006
.40	1.48	.041	-.150	1.72	.069	3.29	----	.06	.5666	.0376	.433	----	.008
.40	2.11	.056	-.081	2.46	.046	3.52	6.05	.06	.1797	.0252	.464	.797	.008
.40	2.53	.074	.013	2.96	.043	3.83	----	.04	.1248	.0231	.505	----	.006
.40	3.17	.110	.214	3.70	.041	4.50	6.08	.04	.0799	.0220	.592	.801	.005
.40	3.59	.122	.310	4.19	.035	4.81	----	.07	.0622	.0190	.633	----	.009
.40	4.22	.125	.321	4.93	.026	4.84	5.48	.15	.0449	.0140	.638	.722	.020
.40	4.64	.121	.281	5.42	.021	4.73	----	.22	.0371	.0112	.623	----	.029
.40	5.28	.126	.232	6.16	.017	4.56	4.78	.29	.0288	.0091	.600	.630	.038
.40	6.33	.136	.154	7.39	.013	4.31	4.40	.34	.0200	.0068	.567	.579	.045
.40	7.39	.145	.090	6.62	.010	4.09	4.07	.39	.0147	.0053	.538	.536	.052
.40	8.44	.166	.050	9.85	.009	3.95	3.88	.42	.0112	.0047	.520	.511	.055
.50	0	0	-.247	0	----	2.89	6.06	-.04	----	----	.410	.859	-.005
.50	.63	.008	-.220	.71	.063	2.96	----	-.05	2.4938	.0399	.420	----	-.007
.50	1.06	.038	-.164	1.18	.108	3.11	6.08	-.04	.6985	.0683	.441	.863	-.006
.50	1.48	.051	-.134	1.66	.074	3.18	----	-.03	.4583	.0467	.451	----	-.004
.50	2.11	.070	-.062	2.37	.050	3.36	5.87	-.03	.2246	.0314	.477	.833	-.004
.50	2.53	.093	.054	2.84	.046	3.65	----	-.04	.1560	.0290	.518	----	-.006
.50	3.17	.134	.275	3.55	.043	4.21	6.01	-.05	.0999	.0268	.597	.852	-.007
.50	3.59	.164	.441	4.03	.040	4.61	----	-.05	.0777	.0255	.654	----	-.007
.50	4.22	.153	.189	4.74	.027	4.74	5.50	.02	.0562	.0172	.672	.780	.003
$\tau = 12^\circ$													
0	0	0	0	----	----	----	----	----	0	0	0	0	0.299
0	.63	0	-.007	----	----	----	----	----	0	0	0	0	.105
0	1.06	0	-.007	----	----	----	----	----	0	0	0	0	.231
0	1.48	0	-.007	----	----	----	----	----	0	0	0	0	.107
0	2.11	0	-.007	----	----	----	----	----	0	0	0	0	.143
0	2.53	0	-.008	----	----	----	----	----	0	0	0	0	.108
0	3.17	0	-.012	----	----	----	----	----	0	0	0	0	.064
0	3.59	----	----	----	----	----	----	----	0	0	0	0	----
0	4.22	----	----	----	----	----	----	----	0	0	0	0	----
0	4.64	----	----	----	----	----	----	----	0	0	0	0	----
0	5.28	----	----	----	----	----	----	----	0	0	0	0	----
0	6.33	0	-.013	----	----	----	----	----	0	0	0	0	.112
0	7.39	----	----	----	----	----	----	----	0	0	0	0	----
0	8.44	----	----	----	----	----	----	----	0	0	0	0	----
0	9.50	----	----	----	----	----	----	----	0	0	0	0	----
0	10.55	0	-.007	----	----	----	----	----	0	0	0	0	----
0	11.61	----	----	----	----	----	----	----	0	0	0	0	----
0	12.66	----	----	----	----	----	----	----	0	0	0	0	----
0	13.72	.005	-.027	----	----	----	----	----	0	0	-3.960	0	.112
0	14.77	.005	-.054	----	----	----	----	----	0	0	-5.070	----	.094
0	15.83	----	----	----	----	----	----	----	0	0	-9.020	0	.110
0	16.88	.005	-.052	----	----	----	----	----	0	0	0	0	----

TABLE III - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 9 WITH CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{B_Q}	c_{X_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(\frac{A}{w})^{1/3}}$	$\frac{l}{(\frac{A}{w})^{1/3}}$	$\frac{h}{(\frac{A}{w})^{1/3}}$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 12^\circ$ - Continued													
.10	0	0	-0.146	0	----	2.81	6.08	0.68	----	0.0100	0.233	0.504	0.056
.10	.63	.002	-1.14	.93	0.046	2.97	6.77	.68	0.4988	0.246	-----	-----	.056
.10	1.05	.003	-1.131	1.55	.075	3.21	6.10	.71	.1797	.0162	.267	.506	.059
.10	1.43	.014	-1.13	2.17	.059	3.62	-----	.72	.0917	.0128	.300	-----	.060
.10	2.11	.019	-0.86	3.10	.039	4.20	5.82	.74	.0449	.0085	.349	.483	.061
.10	2.53	.023	-0.82	3.72	.033	4.50	-----	.77	.0512	.0072	.356	-----	.064
.10	3.17	.027	-0.92	4.65	.025	5.11	5.10	.83	.0200	.0054	.341	.423	.069
.10	3.59	.027	-1.07	5.26	.019	3.80	-----	.90	.0155	.0042	.325	-----	.071
.10	4.22	.027	-1.23	6.19	.014	3.46	4.33	.95	.0112	.0030	.287	.359	.079
.10	4.64	.025	-1.34	6.81	.011	3.21	-----	.97	.0093	.0023	.267	-----	.081
.10	5.26	.027	-1.54	7.74	.009	2.81	3.76	1.00	.0072	.0019	.233	.312	.083
.10	6.33	.026	-1.86	9.29	.006	2.16	3.30	1.05	0.0050	.0013	.179	.273	.087
.10	7.39	.026	-2.06	10.84	.005	1.73	2.78	1.07	.0037	.0010	.144	.232	.089
.10	8.44	.027	-2.14	12.39	.004	1.58	2.52	1.07	.0028	.0008	.131	.209	.099
.10	9.50	.027	-2.35	13.94	.003	1.14	-----	1.09	.0022	.0006	.093	-----	.090
.10	10.55	.028	-2.47	15.49	.002	.90	-----	1.10	.0018	.0005	.074	-----	.091
.10	11.61	.028	-2.55	17.04	.002	.71	-----	1.14	.0015	.0004	.056	-----	.095
.10	12.66	.028	-2.87	18.59	.001	.06	.02	1.14	.0013	.0003	.005	.002	.095
.10	13.72	.028	-2.75	20.15	.001	.28	.02	1.15	.0011	.0003	.023	.002	.094
.10	14.77	.027	-2.75	21.58	.001	.51	.02	1.13	.0009	.0002	.026	.002	.094
.10	15.83	.026	-2.61	23.23	.001	.16	.02	1.12	.0008	.0002	.013	.002	.093
.20	0	C	-2.35	0	----	2.73	5.64	.35	-----	-----	.285	.590	.037
.20	.63	.007	-2.17	.83	.102	2.90	-----	.34	.9975	.0349	.303	-----	.036
.20	1.06	.019	-2.06	1.38	.100	3.01	5.74	.35	.3504	.0341	.315	.600	.037
.20	1.48	.027	-1.82	1.93	.072	3.23	-----	.37	.1833	.0247	.358	-----	.039
.20	2.11	.042	-1.11	2.76	.055	3.83	5.64	.38	.0858	.0189	.400	.590	.040
.20	2.53	.047	-0.86	3.31	.043	4.08	-----	.40	.0624	.0147	.426	-----	.042
.20	3.17	.052	-0.86	4.14	.030	4.08	5.07	.49	.0399	.0104	.426	.530	.052
.20	3.59	.052	-1.04	4.69	.024	3.92	-----	.56	.0311	.0081	.410	-----	.058
.20	4.22	.055	-1.44	5.52	.018	3.58	4.32	.61	.0225	.0062	.374	.451	.063
.20	4.64	.055	-1.67	6.07	.025	3.41	-----	.66	.0186	.0051	.356	-----	.069
.20	5.28	.055	-1.94	6.90	.012	3.19	3.78	.69	.0144	.0040	.333	.395	.072
.20	6.33	.054	-2.46	8.28	.008	2.75	3.39	.74	.0100	.0027	.287	.355	.077
.20	7.39	.051	-3.02	9.66	.006	2.28	3.02	.78	.0073	.0019	.258	.316	.082
.20	8.44	.051	-3.21	11.04	.004	2.13	2.76	.79	.0056	.0014	.223	.288	.083
.20	9.50	.052	-3.73	12.42	.004	1.69	2.62	.81	.0044	.0012	.177	.273	.085
.20	10.55	.057	-3.87	13.80	.003	1.60	2.21	.82	.0036	.0010	.167	.231	.086
.20	11.51	.058	-4.29	15.18	.003	1.25	2.02	.84	.0030	.0009	.151	.212	.088
.20	12.66	.061	-4.39	16.55	.002	1.18	-----	.84	.0025	.0008	.123	-----	.088
.20	13.72	.054	-4.69	17.94	.002	.93	.02	.83	.0021	.0007	.097	.002	.087
.30	0	0	-2.87	0	----	2.72	5.53	.17	-----	-----	.326	.662	.020
.30	.63	.007	-2.71	.77	.078	2.81	-----	.15	1.4963	.0349	.336	-----	.018
.30	1.05	.032	-2.50	1.29	.128	2.93	5.66	.18	.5391	.0375	.351	.577	.021
.30	1.48	.036	-2.23	1.80	.074	3.08	-----	.21	.2750	.0330	.359	-----	.025
.30	2.11	.057	-1.29	2.58	.057	3.56	5.52	.20	.1348	.0256	.426	.660	.024
.30	2.53	.071	-0.60	3.09	.049	3.88	-----	.22	.0936	.0221	.464	-----	.027
.30	3.17	.079	-0.36	3.87	.035	4.00	4.97	.30	.0599	.0158	.479	.594	.036
.30	3.59	.053	-0.62	4.38	.029	3.88	-----	.39	.0466	.0129	.464	-----	.046
.30	4.22	.084	-1.07	5.16	.021	3.66	4.27	.46	.0337	.0094	.438	.511	.055
.30	4.64	.084	-1.40	5.67	.017	3.51	-----	.50	.0278	.0078	.420	-----	.060
.30	5.28	.093	-1.90	6.45	.013	3.25	3.73	.55	.0216	.0060	.390	.447	.065
.30	5.33	.084	-2.71	7.74	.009	2.88	3.58	.59	.0150	.0042	.344	.404	.071
.30	7.39	.080	-3.48	9.02	.006	2.51	3.04	.63	.0120	.0029	.300	.363	.076
.30	8.44	.079	-3.93	10.31	.005	2.27	2.80	.66	.0084	.0022	.272	.335	.079
.30	9.50	.079	-4.45	11.60	.004	1.99	2.77	.67	.0067	.0018	.238	.331	.080
.30	10.55	.085	-5.01	12.89	.003	1.78	2.48	.68	.0054	.0015	.213	.297	.081
.30	11.61	.089	-5.31	14.16	.003	1.63	2.41	.71	.0044	.0013	.195	.268	.085

TABLE III - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 9 WITH CHINE STRIPS

$C_{\Delta Q}$	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(A/W)^{1/3}}$	$\frac{l}{(A/W)^{1/3}}$	$\frac{h}{(A/W)^{1/3}}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 12^\circ$ - Concluded													
.40	0	0	-0.308	0	-----	2.73	5.60	0.04	-----	0.359	0.737	0.006	
.40	.63	.010	-0.268	.74	0.092	2.80	-----	.05	1.9950	0.0499	.369	-----	.004
.40	1.06	.041	-0.269	1.23	.136	2.88	5.60	.05	.7188	0.0737	.379	.737	.007
.40	1.48	.049	-0.235	1.72	.083	3.00	-----	.09	.3666	0.0449	.395	-----	.011
.40	2.11	.074	-0.114	2.46	.061	3.41	5.48	.06	.1797	0.0322	.449	.722	.008
.40	2.55	.093	-0.040	2.96	.053	3.66	-----	.08	.1248	0.0290	.482	-----	.010
.40	3.17	.106	.042	3.70	.039	3.93	5.03	.17	.0799	0.0212	.518	.662	.022
.40	3.59	.111	.021	4.19	.032	3.87	-----	.24	.0622	0.0173	.510	-----	.032
.40	4.22	.114	-.042	4.93	.028	3.66	4.24	.33	.0449	0.0128	.482	.558	.043
.40	4.64	.114	-.087	5.42	.020	3.51	-----	.38	.0371	0.0106	.462	-----	.050
.40	5.26	.112	-.159	6.16	.015	3.27	3.72	.43	.0288	0.0081	.451	.489	.057
.40	6.33	.112	-.271	7.39	.010	2.90	5.31	.51	.0200	0.0056	.382	.436	.067
.40	7.39	.114	-.358	8.62	.008	2.63	3.05	.53	.0147	0.0042	.346	.402	.070
.40	8.44	.107	-.426	9.85	.006	2.39	2.79	.56	.0112	0.0030	.315	.367	.073
.50	0	0	-3.07	0	-----	2.73	5.54	-.05	-----	-----	.387	.786	-.008
.50	.63	.009	-.287	.71	.071	2.78	-----	-.05	2.4938	0.0449	.395	-----	.006
.50	1.06	.050	-.262	1.18	.143	2.86	5.51	-.03	.8985	0.0898	.405	.782	-.004
.50	1.48	.062	-.226	1.66	.090	2.96	-----	-.01	.4583	0.0568	.420	-----	.001
.50	2.11	.088	-.087	2.37	.063	3.31	5.42	-.02	.2246	0.0395	.469	.769	-.003
.50	2.55	.115	.012	2.84	.056	3.56	-----	-.01	.1560	0.0273	.505	-----	.001
.50	3.17	.139	.135	3.55	.044	3.85	5.05	.09	.0999	0.0278	.546	.716	.013
.50	3.59	.140	.119	4.03	.035	3.81	-----	.13	.0777	0.0218	.541	-----	.018
.50	4.22	.144	.056	4.74	.026	3.67	4.23	.23	.0562	0.0162	.520	.600	.033
$\tau = 16^\circ$													
0	0	0	0	-----	-----	-----	-----	-----	0	-----	-----	0.077	0.139
0	.63	0	0	-----	-----	-----	-----	-----	0	-----	-----	-----	.140
0	1.06	0	0	-----	-----	-----	-----	-----	0	-----	-----	0.043	.140
0	1.48	0	0	-----	-----	-----	-----	-----	0	-----	-----	-----	.140
0	2.11	.001	0	-----	-----	-----	-----	-----	0	0.0004	0.500	-----	.140
0	2.55	.001	0	-----	-----	-----	-----	-----	0	0.0003	0.500	-----	.140
0	3.17	.001	0	-----	-----	-----	-----	-----	0	0.0002	.500	0	.140
0	3.59	0	0	-----	-----	-----	-----	-----	0	0	-----	-----	.139
0	4.22	0	0	-----	-----	-----	-----	-----	0	0	-----	0	.139
0	4.64	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	5.28	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	6.33	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	7.39	.001	0	-----	-----	-----	-----	-----	0	-----	.500	0	.143
0	8.44	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	9.50	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	0	.142
0	10.55	-----	-.011	-----	-----	-----	-----	-----	0	-----	-----	0	.142
0	11.61	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	12.66	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	13.72	.002	-.012	-----	-----	-----	-----	-----	0	-----	2.797	.002	.142
0	14.77	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	15.83	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	16.88	.004	-.022	-----	-----	-----	-----	-----	0	-----	3.346	0	.140
.10	0	0	-.138	0	-----	2.90	5.41	0.83	-----	-----	.241	.449	.069
.10	.63	.005	-.135	.93	0.116	3.06	-----	.82	.4988	0.0249	.254	-----	.068
.10	1.06	.014	-.135	1.55	.117	3.12	5.36	.86	.1797	0.0252	.259	.444	.071
.10	1.48	.015	-.119	2.17	.064	3.46	-----	.87	.0917	0.0137	.287	-----	.072
.10	2.11	.019	-.101	3.10	.039	3.89	4.84	.97	.0449	0.0065	.323	.402	.061
.10	2.55	.022	-.191	5.72	.032	2.01	-----	1.05	.0312	0.0069	.167	-----	.087
.10	3.17	.021	-.147	4.65	.019	2.90	3.56	1.17	.0200	0.0042	.241	.295	.097
.10	3.59	.020	-.167	5.26	.014	2.47	-----	1.23	.0155	0.0031	.205	-----	.102
.10	4.22	.019	-.183	6.19	.010	2.13	2.58	1.28	.0112	0.0021	.177	.214	.107
.10	4.64	.019	-.195	6.81	.008	1.88	-----	1.31	.0093	0.0018	.156	-----	.108
.10	5.28	.018	-.206	7.74	.006	1.64	2.22	1.35	.0072	0.0023	.136	.184	.112

TABLE III - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 9 WITH CHINE STRIPS

C_{Δ_x}	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_A}	C_{D_A}	$\frac{x}{(A)} \frac{1/3}{(A)}$	$\frac{l}{(A)} \frac{1/3}{(A)}$	$\frac{h}{(A)} \frac{1/3}{(A)}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 15^\circ$ - Continued													
.10	6.33	0.019	-0.222	9.29	0.004	1.30	1.75	1.40	0.0050	0.0009	0.108	0.145	0.116
.10	7.39	.019	-0.241	10.84	.003	.93	1.49	1.46	.0057	.0007	.077	.124	.121
.10	8.44	.018	-0.251	12.39	.002	.68	1.08	1.19	.0028	.0005	.056	.090	.124
.10	9.50	.019	-0.260	13.94	.002	.50	1.06	1.19	.0022	.0004	.041	.088	.124
.10	10.55	.019	-0.271	15.49	.001	.28	.98	1.50	.0018	.0003	.023	.061	.125
.10	11.61	.019	-0.267	17.04	.001	.37	.02	1.51	.0015	.0003	.031	.002	.126
.10	12.66	.023	-0.271	18.59	.001	.34	.59	1.51	.0013	.0003	.028	.049	.126
.10	13.72	.021	-0.266	20.13	.001	.05	.62	1.51	.0011	.0002	-.005	.002	.126
.10	14.77	.023	-0.287	21.68	.002	.06	.02	1.51	.0009	.0002	-.005	.002	.126
.10	15.83	.022	-0.287	23.23	.001	0	.02	1.51	.0008	.0002	0	.002	.126
.20	0	0	-0.237	0	---	2.67	5.17	.44	---	---	.279	.541	.046
.20	.63	.009	-0.214	.83	.131	2.90	---	.42	.9975	.0449	.303	---	.04
.20	1.06	.024	-0.211	1.38	.126	2.97	5.21	.48	.3594	.0451	.310	.545	.050
.20	1.48	.032	-0.195	1.93	.086	3.12	---	.51	.1833	.0293	.326	---	.053
.20	2.11	.046	-0.261	2.76	.061	3.43	4.76	.59	.0598	.0207	.359	.498	.062
.20	2.53	.050	-0.169	3.32	.046	3.39	---	.67	.0524	.0156	.354	---	.070
.20	3.17	.051	-0.208	1.14	.030	3.06	3.80	.78	.0399	.0102	.320	.397	.081
.20	3.59	.048	-0.239	1.69	.022	2.79	---	.85	.0311	.0075	.292	---	.089
.20	4.22	.044	-0.283	5.52	.014	2.40	3.13	.92	.0225	.0049	.231	.327	.096
.20	4.64	.041	-0.307	6.07	.011	2.21	---	.97	.0186	.0033	.231	---	.102
.20	5.28	.036	-0.356	6.90	.008	1.94	2.41	1.02	.0144	.0026	.203	.252	.107
.20	6.33	.037	-0.383	8.28	.005	1.55	2.02	1.06	.0100	.0018	.262	.212	.111
.20	7.39	.036	-0.427	9.66	.001	1.18	1.84	1.14	.0073	.0013	.223	.192	.119
.20	8.44	.037	-0.450	11.04	.003	.99	1.35	1.16	.0056	.0010	.103	.141	.121
.20	9.50	.036	-0.471	12.42	.002	.81	1.33	1.13	.0044	.0008	.085	.139	.123
.20	10.55	.037	-0.491	13.80	.002	.63	1.19	1.19	.0035	.0007	.066	.124	.124
.20	11.61	.037	-0.497	15.18	.001	.59	.92	1.19	.0030	.0005	.062	.095	.124
.20	12.66	.039	---	16.56	.001	---	.99	1.20	.0025	.0005	---	.103	.125
.20	13.72	.037	-0.501	17.94	.001	.54	.81	1.21	.0021	.0004	.056	.085	.126
.30	0	0	-0.287	0	---	2.67	5.14	.23	---	---	.320	.615	.027
.30	.63	.010	-0.276	.77	.111	2.77	---	.22	1.4953	.0459	.331	---	.026
.30	1.06	.039	-0.274	1.29	.156	2.81	5.06	.27	.5391	.0701	.336	.605	.033
.30	1.48	.046	-0.232	1.80	.098	3.03	---	.29	.2750	.0440	.362	---	.035
.30	2.11	.074	-0.176	2.58	.074	3.32	4.79	.34	.1348	.0322	.397	.573	.041
.30	2.53	.078	-0.170	3.09	.054	3.37	---	.42	.0936	.0243	.403	---	.050
.30	3.17	.076	-0.216	3.87	.035	3.13	3.93	.55	.0599	.0156	.374	.470	.066
.30	3.59	.080	-0.259	4.58	.028	2.93	---	.63	.0466	.0124	.351	---	.075
.30	4.22	.072	-0.321	5.16	.018	2.62	3.27	.70	.0337	.0081	.313	.391	.084
.30	4.64	.069	-0.367	5.67	.014	2.40	---	.75	.0278	.0064	.287	---	.091
.30	5.28	.065	-0.427	6.45	.010	2.10	2.70	.80	.0216	.0047	.251	.323	.096
.30	6.33	.059	-0.496	7.74	.006	1.76	2.07	.86	.0150	.0029	.213	.248	.103
.30	7.39	.054	-0.561	9.02	.004	1.41	1.89	.93	.0110	.0020	.169	.226	.112
.30	8.44	.054	-0.612	10.31	.003	1.15	1.66	.96	.0084	.0015	.138	.199	.115
.30	9.50	.055	-0.629	11.60	.003	1.10	1.52	.98	.0367	.0012	.131	.182	.117
.30	10.55	.059	-0.662	12.89	.002	.92	1.25	.99	.0054	.0011	.110	.150	.118
.30	11.61	.054	-0.670	14.18	.002	.88	1.18	1.00	.0044	.0008	.105	.141	.119
.40	0	0	-0.308	0	---	2.20	5.16	.07	---	---	.356	.679	.009
.40	.63	.014	-0.297	.74	.129	2.76	---	.06	1.9950	.0698	.364	---	.008
.40	1.06	.051	-0.297	1.23	.169	2.79	5.11	.12	.7188	.0916	.367	.673	.016
.40	1.48	.060	-0.255	1.72	.101	2.75	---	.15	.3666	.0550	.362	---	.020
.40	2.11	.098	-0.192	2.46	.081	3.15	4.79	.19	.1797	.0440	.415	.630	.025
.40	2.53	.108	-0.147	2.96	.062	3.31	---	.26	.1246	.0357	.436	---	.034
.40	3.17	.110	-0.188	3.70	.041	3.18	3.99	.40	.0799	.0220	.418	.526	.053
.40	3.59	.111	-0.237	4.19	.032	3.01	---	.48	.0622	.0173	.397	---	.064
.40	4.22	.106	-0.327	4.93	.022	2.73	3.34	.57	.0449	.0119	.359	.440	.076
.40	4.64	.099	-0.401	5.42	.017	2.48	---	.61	.0371	.0092	.326	---	.084
.40	5.28	.093	-0.463	6.16	.012	2.26	2.71	.63	.0288	.0067	.297	.357	.089
.40	6.33	.086	-0.572	7.39	.006	1.89	2.39	.74	.0200	.0043	.249	.314	.098
.40	7.39	.075	-0.659	8.62	.005	1.59	2.08	.82	.0147	.0028	.210	.273	.108
.40	8.44	.071	-0.736	9.85	.004	1.32	1.75	.84	.0112	.0020	.174	.231	.111

TABLE III - Continued
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 9 WITH CHINE STRIPS

c_{A_Q}	c_{T_Q}	c_{F_Q}	c_{M_Q}	c_{V_A}	c_{D_A}	$\frac{x}{(A)} \frac{1/3}{(A)}$	$\frac{l}{(A)} \frac{1/3}{(A)}$	$\frac{h}{(A)} \frac{1/3}{(A)}$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 16^{\circ}$ - Concluded													
.50	0	.63	0	-0.307	0	-----	2.71	5.18	-0.06	-----	0.385	0.735	-0.009
.50	.06	.064	.064	-0.295	.71	0.111	2.75	5.05	-0.06	2.4938	0.0698	.390	-----
.50	1.06	.064	.064	-0.301	1.18	.185	2.76	5.05	0	.6985	.1150	.392	.716
.50	1.48	.074	.074	-0.247	1.66	.108	2.91	-----	.01	.4583	.0678	.413	-----
.50	2.11	.120	.120	-0.155	2.37	.086	3.14	4.86	.04	.2246	.0539	.446	.690
.50	2.53	.139	.139	-0.113	2.84	.069	3.26	-----	.12	.1560	.0434	.462	-----
.50	3.17	.146	.146	-0.129	3.55	.046	3.21	4.14	.24	.0999	.0292	.456	.588
.50	3.59	.146	.146	-0.196	4.03	.026	3.05	3.39	.34	.0777	.0227	.433	-----
.50	4.22	.142	.142	-0.314	4.74	.025	2.76	3.39	.45	.0562	.0159	.392	.481
$\tau = 20^{\circ}$													
0	0	0	0	0	-----	-----	-----	-----	-----	0	-----	0	0.172
0	.63	0	0	0	-----	-----	-----	-----	0	0	-----	0	.173
0	1.06	0	0	0	-----	-----	-----	-----	0	0	-----	0	.178
0	1.48	0	0	-.012	-----	-----	-----	-----	0	0	-----	0	.179
0	2.11	0	0	0	-----	-----	-----	-----	0	0	-----	0	.186
0	2.53	0	0	0	-----	-----	-----	-----	0	0	-----	0	.185
0	3.17	0	0	0	-----	-----	-----	-----	0	0	-----	0	.186
0	3.59	0	0	0	-----	-----	-----	-----	0	0	-----	0	.188
0	4.22	0	0	0	-----	-----	-----	-----	0	0	-----	0	.188
0	4.64	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
0	5.28	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	6.33	-----	-----	-----	-----	-----	-----	-----	0	-----	-----	0	0.172
0	7.39	0	0	-.006	-----	-----	-----	-----	0	-----	0	0	.190
0	8.44	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
0	9.50	-----	-----	-----	-----	-----	-----	-----	0	-----	0	0	-----
0	10.55	.002	-.013	-----	-----	-----	-----	-----	0	-----	0	0	.189
0	11.61	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
0	12.66	-----	-----	-----	-----	-----	-----	-----	0	-----	0	0	-----
0	13.72	.002	-.022	-----	-----	-----	-----	-----	0	-----	0	0	.188
0	14.77	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
0	15.83	-----	-----	-----	-----	-----	-----	-----	0	-----	0	0	-----
0	16.88	.002	-.012	-----	-----	-----	-----	-----	0	-----	0	0	.168
.10	0	0	-.147	0	-----	2.63	4.95	.97	-----	.218	.410	.081	
.10	.63	.007	-.152	.93	.162	2.63	-----	.97	.4988	.0349	.218	-----	.081
.10	1.06	.016	-.145	1.55	.134	2.87	4.85	1.04	.1797	.0288	.238	.402	.086
.10	1.48	.022	-.141	2.17	.094	3.03	-----	1.10	.0917	.0202	.251	-----	.091
.10	2.11	.023	-.153	3.10	.048	2.78	3.79	1.29	.0849	.0103	.251	.314	.107
.10	2.53	.020	-.163	3.72	.029	2.55	-----	1.40	.0312	.0062	.210	-----	.116
.10	3.17	.019	-.174	4.65	.018	2.29	2.60	1.51	.0200	.0038	.190	.216	.125
.10	3.59	.020	-.195	5.26	.014	1.85	-----	1.59	.0155	.0031	.154	-----	.132
.10	4.22	.019	-.213	6.19	.010	1.45	1.98	1.64	.0112	.0021	.121	.165	.136
.10	4.64	.019	-.215	6.81	.008	1.42	-----	1.68	.0095	.0018	.118	-----	.159
.10	5.28	.019	-.224	7.74	.006	1.21	1.49	1.72	.0072	.0014	.100	.124	.143
.10	6.33	.019	-.247	9.29	.004	.74	1.24	1.76	.0050	.0009	.062	.103	.146
.10	7.39	.021	-.255	10.84	.004	.56	.85	1.80	.0057	.0008	.046	.071	.149
.10	8.44	.021	-.255	12.39	.003	.56	.85	1.81	.0026	.0006	.046	.071	.150
.10	9.50	.022	-.275	13.94	.002	.18	.72	1.82	.0022	.0005	.015	.060	.151
.10	10.55	.022	-.275	15.49	.002	.18	.77	1.82	.0018	.0004	.015	.064	.151
.10	11.61	.023	-.303	17.04	.001	-.46	.02	1.83	.0015	.0003	-.038	.002	.152
.10	12.66	.026	-.311	18.59	.001	-.50	.02	1.83	.0013	.0003	-.041	.002	.152
.10	13.72	.026	-.308	20.13	.001	-.43	.02	1.85	.0011	.0003	-.036	.002	.154
.10	14.77	.027	-.311	21.68	.001	-.46	.02	1.83	.0009	.0002	-.038	.002	.152
.10	15.83	.027	-.297	23.23	.001	-.15	.02	1.85	.0008	.0002	-.013	.002	.154

TABLE III - Concluded
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 9 WITH CHINE STRIPS

C_{DQ}	C_{VQ}	C_{RQ}	C_{KQ}	C_{VJ}	C_D	$\frac{x}{(A)} \cdot \frac{1}{V}$	$\frac{l}{(A)} \cdot \frac{1}{V}$	$\frac{h}{(A)} \cdot \frac{1}{V}$	C_{rQ}	C_{DQ}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 20^\circ$ - Concluded													
.20	0	0	-0.247	0	----	2.53	4.82	0.50	----	0.264	0.504	0.052	
.20	.63	.013	-0.247	.83	0.189	2.60	4.80	.56	0.5975	0.068	.272	.052	
.20	1.06	.032	-0.244	1.58	.168	2.67	4.80	.56	.3594	.0575	.279	.502	
.20	1.48	.041	-0.220	1.93	.118	2.92	4.80	.61	.1853	.0403	.305	.064	
.20	2.11	.055	-0.228	2.76	.072	2.90	4.01	.78	.0898	.0247	.303	.419	
.20	2.53	.052	-0.247	3.31	.047	2.73	4.80	.88	.0624	.0162	.285	.092	
.20	3.17	.049	-0.257	4.14	.029	2.38	3.02	1.01	.0399	.0095	.249	.316	
.20	3.59	.046	-0.318	4.59	.021	2.10	4.80	1.11	.0310	.0072	.220	.117	
.20	4.22	.042	-0.360	5.52	.014	1.74	2.27	1.20	.0225	.0047	.182	.237	
.20	4.64	.041	-0.379	6.07	.011	1.57	4.80	1.24	.0186	.0038	.164	----	
.20	5.28	.041	-0.401	6.90	.008	1.40	1.78	1.27	.0144	.0029	.146	.186	
.20	6.35	.042	-0.429	8.25	.006	1.15	1.45	1.32	.0100	.0021	.120	.152	
.20	7.39	.043	-0.460	9.56	.005	.91	1.27	1.36	.0073	.0016	.095	.132	
.20	8.44	.043	-0.480	11.04	.004	.74	1.08	1.49	.0056	.0012	.077	.113	
.20	9.50	.042	-0.489	12.42	.003	.64	.98	1.51	.0044	.0009	.067	.103	
.20	10.55	.041	-0.511	13.80	.002	.47	.88	1.42	.0036	.0007	.049	.092	
.20	11.61	.043	-0.542	15.18	.002	.22	.71	1.42	.0030	.0006	.023	.075	
.20	12.66	.044	-0.531	16.56	.001	.30	.57	1.42	.0025	.0005	.031	.060	
.20	13.72	.046	-0.567	17.94	.001	.03	.68	1.44	.0021	.0005	.003	.071	
.30	0	0	-0.297	0	----	2.59	4.82	.25	----	----	.310	.577	.030
.30	.63	.014	-0.296	.77	.156	2.63	4.80	.25	1.4963	.0698	.315	----	.030
.30	1.06	.049	-0.297	1.29	.197	2.70	4.75	.32	.5391	.0881	.323	.562	.038
.30	1.48	.064	-0.251	1.80	.131	2.93	4.80	.36	.2750	.0587	.351	----	.044
.30	2.11	.089	-0.261	2.58	.089	2.28	4.22	.50	.1348	.0400	.344	.504	.060
.30	2.53	.090	-0.276	3.09	.085	2.22	4.22	.61	.0536	.0281	.356	----	.073
.30	3.17	.084	-0.348	3.87	.037	2.51	3.20	.77	.0599	.0158	.300	.382	.092
.30	3.59	.079	-0.400	4.38	.027	2.25	4.80	.86	.0466	.0123	.269	----	.103
.30	4.22	.073	-0.460	5.16	.016	1.93	2.48	.95	.0337	.0082	.231	.297	.113
.30	4.64	.068	-0.489	5.67	.014	1.78	4.80	.99	.0278	.0063	.213	----	.119
.30	5.28	.064	-0.529	6.45	.010	1.59	1.96	1.05	.0216	.0046	.190	.235	.126
.30	6.35	.062	-0.596	7.74	.007	1.25	1.53	1.11	.0150	.0031	.149	.194	.132
.30	7.39	.064	-0.639	9.02	.005	1.05	1.36	1.15	.0110	.0023	.126	.163	.138
.30	8.44	.064	-0.680	10.31	.004	.84	1.18	1.18	.0084	.0023	.100	.141	.141
.30	9.50	.064	-0.710	11.60	.003	.69	1.04	1.21	.0067	.0014	.082	.124	.144
.30	10.55	.064	-0.732	12.89	.003	.58	.95	1.21	.0054	.0012	.069	.109	.145
.30	11.61	.063	-0.751	14.18	.002	.47	.82	1.23	.0044	.0009	.056	.098	.147
.40	0	0	-0.316	0	----	2.65	4.87	.07	----	----	.349	.641	.010
.40	.63	.017	-0.316	.74	.156	2.67	4.80	.07	1.9950	.0848	.351	----	.010
.40	1.06	.064	-0.336	1.23	.22	2.65	4.75	.15	.7128	.1150	.349	.626	.020
.40	1.48	.079	-0.287	1.72	.133	2.82	4.80	.19	.3666	.0724	.372	----	.024
.40	2.11	.122	-0.276	2.46	.101	2.90	4.22	.32	.1797	.0548	.382	.556	.043
.40	2.53	.125	-0.285	2.96	.072	2.86	4.80	.42	.1248	.0390	.377	----	.056
.40	3.17	.121	-0.368	3.70	.045	2.59	3.31	.60	.0799	.0242	.341	.436	.079
.40	3.59	.113	-0.437	4.19	.032	2.36	4.80	.69	.0622	.0176	.313	----	.091
.40	4.22	.103	-0.521	4.93	.022	2.08	2.60	.80	.0449	.0118	.274	.342	.105
.40	4.64	.100	-0.571	5.42	.017	1.91	4.80	.84	.0371	.0093	.251	----	.110
.40	5.26	.092	-0.636	6.16	.012	1.67	2.08	.90	.0268	.0065	.220	.273	.119
.40	6.33	.086	-0.731	7.39	.007	1.34	1.72	.97	.0200	.0040	.177	.226	.128
.40	7.39	.086	-0.809	8.62	.006	1.09	1.47	1.01	.0147	.0032	.144	.194	.133
.40	8.44	.088	-0.850	9.85	.005	.96	1.28	1.04	.0112	.0025	.126	.169	.137
.50	0	0	-0.324	0	----	2.66	4.92	-.09	----	----	.377	.697	-.013
.50	.63	.024	-0.315	.71	.190	2.69	4.80	-.10	2.4938	.1197	.382	----	-.014
.50	1.06	.076	-0.343	1.18	.217	2.66	4.76	-.01	.8935	.1366	.377	.677	-.001
.50	1.48	.092	-0.275	1.66	.134	2.84	4.80	-.01	.4583	.0843	.403	----	.001
.50	2.11	.150	-0.284	2.37	.107	2.84	4.32	.14	.2246	.0574	.403	.613	.020
.50	2.53	.163	-0.265	2.84	.081	2.69	4.80	.26	.1560	.0508	.410	----	.036
.50	3.17	.159	-0.356	3.55	.050	2.65	3.45	.42	.0999	.0317	.377	.489	.060
.50	3.59	.155	-0.444	4.03	.038	2.46	4.80	.50	.0777	.0241	.349	----	.071
.50	4.22	.143	-0.549	5.71	.026	2.19	2.73	.63	.0562	.0161	.310	.387	.090

TABLE IV
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 12 WITH CHINE STRIPS

c_{DQ}	c_{VQ}	c_{PQ}	c_{M_Q}	$c_{V\Delta}$	$c_{D\Delta}$	$\frac{x}{(A/w)^{1/3}}$	$\frac{l}{(A/w)^{1/3}}$	$\frac{h}{(A/w)^{1/3}}$	c_{LQ}	c_{DQ}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$	
$\tau = 0^\circ$														
0	0	0	0	.003	----	----	----	----	0	0	0.473	0.042		
0	.63	0	0	.002	0.07	----	----	----	0	.0036	----	.480	.041	
0	1.06	0	0	.002	.007	----	----	----	0	.0027	----	----	.040	
0	1.48	0	0	.003	.007	----	----	----	0	.0031	----	.519	.040	
0	2.11	0	0	.007	.009	----	----	----	0	.0044	----	----	.040	
0	2.53	0	0	.014	.009	----	----	----	0	.0052	----	.705	.037	
0	3.17	0	0	.026	.020	----	----	----	0	0.0054	----	----	.038	
0	3.59	0	0	.035	.040	----	----	----	0	.0055	----	.807	.037	
0	4.22	0	0	.049	.060	----	----	----	0	.0055	----	----	.038	
0	4.64	0	0	.059	.074	----	----	----	0	.0051	----	.823	.038	
0	5.28	0	0	.071	.099	----	----	----	0	.0048	----	----	.038	
0	6.33	0	0	.096	.149	----	----	----	0	.0047	----	.823	.038	
0	7.59	0	0	.129	.200	----	----	----	0	0.0047	----	----	.038	
.10	0	0	0	.010	0	7.51	13.34	0.38	----	0.515	.915	0.26		
.10	.63	0	0	.002	.015	.93	0.046	7.63	.40	.4988	.0100	.524	0.27	
.10	1.06	0	0	.007	.044	1.55	.058	8.22	13.21	.37	.1797	.0126	.564	.025
.10	1.48	0	0	.011	.065	2.17	.047	8.68	----	.0917	.0101	.596	0.26	
.10	2.11	0	0	.022	.084	3.10	.046	9.12	13.21	.38	.0449	.0099	.605	.026
.10	2.53	0	0	.035	.092	3.72	.048	9.27	----	.0312	.0103	.636	0.26	
.10	3.17	0	0	.052	.114	4.65	.048	9.73	13.21	.37	.0200	.0104	.668	.025
.10	3.59	0	0	.067	.150	5.26	.048	10.54	----	.0155	.0104	.723	0.25	
.10	4.22	0	0	.103	.194	6.19	.054	11.51	13.65	.56	.0112	.0116	.769	.025
.10	4.64	0	0	.152	.229	6.81	.070	12.24	----	.0093	.0150	.860	0.25	
.10	5.28	0	0	.262	.293	7.74	.087	13.63	13.75	.31	.0072	.0087	.935	.021
.20	0	0	0	.031	0	6.07	11.13	.23	----	----	----	.524	.961	.020
.20	.63	0	0	.003	.035	.83	.044	6.09	----	.9975	.0150	.526	0.20	
.20	1.06	0	0	.009	.074	1.38	.047	6.43	11.16	.22	.3594	.0262	.555	.019
.20	1.48	0	0	.016	.115	1.93	.043	6.77	----	.1633	.0147	.505	0.18	
.20	2.11	0	0	.033	.159	2.76	.063	7.14	11.16	.20	.0896	.0148	.617	.017
.20	2.53	0	0	.046	.182	3.31	.042	7.36	----	.0624	.0144	.636	0.19	
.20	3.17	0	0	.069	.203	4.14	.040	7.54	11.20	.20	.0399	.0158	.651	.017
.20	3.59	0	0	.099	.214	4.69	.055	7.58	----	.0511	.0254	.655	0.21	
.20	4.22	0	0	.157	.235	5.52	.051	7.80	11.29	.20	.0225	.0176	.674	.017
.20	4.64	0	0	.216	.260	6.07	.058	8.02	----	.0186	.0200	.693	0.14	
.30	0	0	0	.048	0	5.30	9.93	.12	----	----	----	.524	.982	.012
.30	.63	0	0	.004	.054	.77	.045	5.32	----	.14963	.0200	.526	0.11	
.30	1.06	0	0	.012	.094	1.29	.048	5.53	10.12	.09	.5591	.0216	.547	1.000
.30	1.48	0	0	.022	.166	1.80	.045	5.90	----	.2750	.0202	.585	0.10	
.30	2.11	0	0	.041	.214	2.58	.041	6.13	10.12	.09	.1548	.0184	.606	1.000
.30	2.53	0	0	.056	.241	3.09	.039	6.26	----	.0936	.0175	.619	0.11	
.30	3.17	0	0	.094	.274	3.87	.042	6.45	10.12	.10	.0599	.0168	.636	1.000
.30	3.59	0	0	.136	.273	4.38	.047	6.43	----	.0866	.0211	.636	0.10	
.30	4.22	0	0	.226	.269	5.16	.057	6.41	10.12	.09	.0337	.0254	.634	1.000
.40	0	0	0	.066	0	4.82	9.15	.05	----	----	----	.524	.996	.006
.40	.63	0	0	.004	.067	.74	.037	4.83	----	.19950	.0200	.526	0.05	
.40	1.06	0	0	.014	.115	1.23	.046	4.99	9.19	.02	.738	.0252	.543	1.000
.40	1.48	0	0	.028	.200	1.72	.047	5.28	----	.3666	.0257	.575	0	
.40	2.11	0	0	.054	.249	2.46	.045	5.43	9.19	.01	.1797	.0243	.591	1.000
.40	2.53	0	0	.079	.283	2.96	.045	5.53	----	.1248	.0246	.604	0.02	
.40	3.17	0	0	.139	.309	3.70	.051	5.65	9.19	0	.0799	.0278	.615	1.000
.40	3.59	0	0	.207	.289	4.19	.059	5.77	----	.0622	.0322	.606	0.01	
.40	4.22	0	0	.331	.259	4.93	.069	5.48	9.19	-.04	.0449	.0372	.596	1.000

TABLE IV - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 12 WITH CHINE STRIPS

C_{A_Q}	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{L}$ ($\frac{A}{W}$) $^{1/3}$	$\frac{l}{L}$ ($\frac{A}{W}$) $^{1/3}$	$\frac{h}{L}$ ($\frac{A}{W}$) $^{1/3}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 0^\circ$ - Concluded													
.50	0	0	0.085	0	-----	4.39	8.53	0	-----	0.526	1.000	0	
.50	.63	.004	.082	.71	0.052	4.47	-----	-.01	2.4952	0.0200	.524	-----	-.002
.50	1.06	.116	.137	.118	.046	4.62	8.53	-.04	.0288	.547	1.000	-.004	
.50	1.48	.033	.223	1.66	.048	4.53	-----	-.05	.4583	.0302	.566	-----	-.005
.50	2.11	.065	.270	2.37	.047	4.96	8.53	-.05	.2246	.0296	.581	1.000	-.006
.50	2.53	.111	.304	2.84	.050	5.03	-----	-.04	.1560	.0315	.589	-----	-.004
.50	3.17	.169	.289	3.55	.053	4.99	8.53	-.05	.0999	.0337	.585	1.000	-.006
.50	3.59	.245	.254	4.03	.060	4.91	-----	-.07	.0777	.0381	.575	-----	-.008
$\tau = 1^\circ$													
0	0	0	0	-----	-----	-----	-----	0	-----	0.433	0.051		
0	.63	.001	0	-----	-----	-----	-----	0	0.0050	0.500	-----	.050	
0	1.06	.002	0	-----	-----	-----	-----	0	0.0036	.500	.470	.049	
0	1.48	.002	0	-----	-----	-----	-----	0	0.0018	.500	-----	.049	
0	2.11	.007	0	-----	-----	-----	-----	0	0.0031	.500	.462	.047	
0	2.53	.012	0	-----	-----	-----	-----	0	0.0037	.500	-----	.047	
0	3.17	.020	.005	-----	-----	-----	-----	0	0.0040	.994	.505	.045	
0	3.59	.026	.010	-----	-----	-----	-----	0	0.0037	1.798	.523	.045	
0	4.22	.033	.020	-----	-----	-----	-----	0	0.0038	1.787	-----	.045	
0	5.64	.044	.025	-----	-----	-----	-----	0	0.0035	2.243	.526	.045	
0	5.26	.049	.040	-----	-----	-----	-----	0	-----	-----	-----	-----	
0	6.33	.063	.066	-----	-----	-----	-----	0	0.0031	2.733	.523	.044	
0	7.39	.087	.080	-----	-----	-----	-----	0	0.0032	2.472	.510	.044	
0	8.44	.113	.114	-----	-----	-----	-----	0	0.0032	2.646	.523	.043	
0	9.50	.145	.139	-----	-----	-----	-----	0	0.0032	2.542	.526	.045	
0	10.55	.179	.174	-----	-----	-----	-----	0	0.0032	2.580	.523	.046	
0	11.61	.219	.214	-----	-----	-----	-----	0	0.0033	2.589	.523	.045	
0	12.66	.247	.219	-----	-----	-----	-----	0	0.0032	2.650	.519	.046	
0	13.72	.290	.289	-----	-----	-----	-----	0	0.0031	2.632	.523	.045	
0	14.77	.326	.324	-----	-----	-----	-----	0	0.0030	2.616	.523	.044	
0	15.83	.374	.364	-----	-----	-----	-----	0	0.0030	2.572	.523	.045	
0	16.88	.423	.409	-----	-----	-----	-----	0	0.0030	2.559	.522	.044	
.10	0	C	-.110	C	-----	4.91	10.20	0.43	-----	.337	.699	.030	
.10	.63	.002	-.105	.93	0.046	5.04	-----	.43	0.4988	.0100	.346	-----	.030
.10	1.06	.006	-.080	-.55	.050	5.57	10.10	.42	.1797	.0108	.382	.692	.029
.10	1.48	.022	-.059	2.17	.051	5.81	-----	.42	.0917	.0120	.399	-----	.029
.10	2.11	.021	-.049	3.10	.044	7.17	9.82	.42	.0449	.0094	.492	.673	.029
.10	2.57	.029	-.045	3.72	.042	7.21	-----	.41	.0312	.0090	.494	-----	.028
.10	3.17	.046	0	4.65	.037	7.29	9.99	.38	.0200	.0086	.500	.685	.026
.10	3.59	.055	.049	5.26	.032	7.38	-----	.39	.0155	.0070	.506	-----	.027
.10	4.22	.054	.095	6.19	.028	9.27	9.97	.39	.0112	.0061	.636	.685	.027
.10	4.64	.058	.103	6.81	.025	9.42	-----	.43	.0093	.0054	.647	-----	.030
.10	5.23	.066	.119	7.74	.022	9.73	9.38	.45	.0072	.0047	.668	.643	.031
.10	6.33	.085	.129	9.29	.019	9.92	8.81	.50	.0050	.0042	.682	.604	.034
.10	7.39	.102	.144	10.84	.017	10.20	8.45	.51	.0037	.0037	.700	.579	.035
.10	8.44	.132	.163	12.39	.017	10.55	8.45	.52	.0028	.0037	.723	.579	.036
.10	9.50	.165	.169	13.94	.017	10.97	8.14	.56	.0022	.0037	.753	.558	.038
.10	10.55	.193	.219	15.19	.016	11.50	8.14	.57	.0018	.0035	.789	.558	.039
.10	11.61	.230	.255	17.04	.016	12.02	8.06	.56	.0015	.0034	.825	.553	.038
.10	12.66	.267	.279	18.59	.015	12.36	8.06	.57	.0013	.0033	.848	.553	.039
.10	13.72	.306	.323	20.13	.015	13.01	7.83	.57	.0011	.0033	.893	.557	.039
.10	14.77	.362	.360	21.68	.015	13.48	7.63	.57	.0009	.0031	.924	.583	.039
.10	15.83	.390	.394	23.23	.014	13.94	-----	.57	.0008	.0031	.956	-----	.039

TABLE IV - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 12 WITH CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(A)}^{1/3}$	$\frac{z}{(A)}^{1/3}$	$\frac{h}{(A)}^{1/3}$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$\tau = 4^\circ$ - Concluded													
.20	0	0	-c.180	0	----	4.25	9.00	0.24	----	0.367	0.777	0.021	
.20	.63	.003	-.170	.83	0.344	4.54	9.25	.22	0.9975	0.0150	.375	0.020	
.20	1.06	.009	-.127	1.38	0.47	4.71	9.12	.22	.5594	0.162	.407	.786	.019
.20	1.48	.018	-.105	1.93	0.48	4.89	----	.23	.1833	0.165	.422	----	.020
.20	2.11	.031	-.079	2.76	0.41	5.13	8.83	.24	.0898	0.139	.443	.763	.021
.20	2.53	.040	-.060	3.31	0.37	5.28	----	.23	.0624	0.125	.456	----	.020
.20	3.17	.058	0	4.14	0.34	5.79	8.91	.20	.0399	0.116	.500	.770	.017
.20	3.59	.071	.075	4.69	0.32	6.43	----	.20	.0311	0.110	.555	----	.017
.20	4.22	.082	.214	5.52	0.27	7.58	9.12	.19	.0225	0.092	.655	.788	.016
.20	4.64	.088	.264	6.07	0.25	8.00	----	.19	.0186	0.080	.691	----	.016
.20	5.28	.095	.283	6.90	0.20	8.15	8.5-	.25	.0144	.0068	.704	.735	.021
.20	6.33	.10-	.279	8.28	.015	8.11	7.91	.31	.0100	.0050	.700	.683	.027
.20	7.39	.125	.264	9.66	.013	7.98	7.48	.35	.0073	.0046	.689	.646	.030
.20	8.44	.155	.264	11.04	.013	7.96	7.12	.37	.0056	.0044	.687	.615	.032
.20	9.50	.181	.269	12.42	.012	7.98	7.03	.40	.0044	.0040	.689	.607	.035
.20	10.55	.216	.294	13.80	.011	8.15	6.73	.41	.0036	.0039	.704	.581	.036
.20	11.61	.250	.315	15.18	.011	8.30	6.67	.43	.0030	.0037	.717	.576	.038
.20	12.66	.287	.339	16.56	.011	8.44	6.52	.44	.0025	.0036	.729	.563	.038
.20	13.72	.327	.375	17.94	.010	8.67	6.48	.44	.0021	.0035	.749	.560	.038
.30	0	0	-.220	0	----	3.97	8.50	.13	----	----	.392	.841	.013
.30	.63	.003	-.204	.77	.033	4.06	----	.12	1.4963	.0150	.401	----	.010
.30	1.06	.012	-.149	1.29	0.48	4.31	8.56	.10	.559	.0216	.426	.846	.010
.30	1.48	.024	-.114	1.80	0.49	4.50	----	.12	.2750	.0220	.445	----	.012
.30	2.11	.040	-.080	2.58	0.40	4.67	8.38	.13	.1348	.0180	.462	.828	.013
.30	2.53	.051	-.028	3.09	0.35	4.94	----	.12	.0956	.0159	.488	----	.012
.30	3.17	.073	.005	3.87	0.353	5.08	8.32	.11	.0599	.0156	.502	.823	.011
.30	3.59	.093	.102	4.38	0.32	5.55	----	.09	.0466	.0145	.549	----	.009
.30	4.22	.121	.289	5.16	0.30	6.47	8.56	.07	.0337	.0136	.640	.846	.007
.30	4.64	.130	.419	5.67	0.27	7.10	----	.07	.0278	.0121	.702	----	.006
.30	5.28	.129	.516	6.45	0.21	7.57	8.21	.11	.0216	.0093	.748	.812	.011
.30	6.33	.156	.475	7.74	.015	7.32	7.61	.20	.0150	.0066	.727	.752	.020
.30	7.39	.141	.424	9.02	.012	7.16	6.95	.24	.0110	.0052	.708	.687	.023
.30	8.44	.172	.403	10.31	.011	6.99	6.72	.28	.0084	.0048	.691	.664	.028
.30	9.50	.204	.395	11.60	.010	6.95	6.36	.31	.0067	.0045	.687	.629	.031
.30	10.55	.233	.384	12.89	.009	6.89	6.18	.34	.0054	.0042	.681	.611	.033
.30	11.61	.268	.395	14.18	.009	6.93	6.04	.35	.0044	.0040	.685	.597	.035
.40	0	0	-.229	0	----	3.82	6.14	.05	----	----	.416	.886	.005
.40	.63	.003	-.209	.74	.046	3.90	----	.04	1.9950	.0249	.424	----	.004
.40	1.06	.016	-.145	1.23	.053	4.11	8.22	.02	.7388	.0288	.447	.894	.003
.40	1.48	.031	-.101	1.72	.052	4.26	----	.04	.3666	.0282	.464	----	.004
.40	2.11	.049	-.006	2.46	0.45	4.58	8.05	.04	.1797	.0220	.498	.876	.005
.40	2.53	.062	-.039	2.96	0.36	4.46	----	.04	.1248	.0193	.485	----	.005
.40	3.17	.088	.029	3.70	0.52	4.70	8.05	.02	.0799	.0176	.511	.876	.005
.40	3.59	.113	.123	4.19	0.32	5.01	----	.01	.0622	.0176	.545	----	.001
.40	4.22	.146	.318	4.93	0.30	5.65	8.22	.02	.0449	.0164	.615	.894	-.002
.40	4.64	.182	.528	5.42	0.31	6.33	----	.03	.0373	.0168	.689	----	-.003
.40	5.28	.197	.744	6.16	0.26	7.05	8.18	.02	.0286	.0142	.767	.890	-.003
.40	6.33	.162	.703	7.39	0.15	6.92	7.35	.10	.0200	.0081	.753	.800	.011
.40	7.39	.186	.636	8.62	0.13	6.70	6.78	.17	.0147	.0068	.729	.738	.019
.40	8.44	.188	.574	9.85	0.10	6.49	6.34	.22	.0112	.0053	.706	.690	.024
.50	0	0	-.209	0	----	3.75	7.88	-.02	----	----	.439	.924	-.002
.50	.63	.005	-.189	.71	.040	3.80	----	-.02	2.4938	.0249	.445	----	-.002
.50	1.06	.015	-.120	1.18	.054	3.96	7.94	-.03	.8985	.0341	.464	.931	-.003
.50	1.48	.036	-.079	1.66	.052	4.07	----	-.02	.4583	.0330	.477	----	-.002
.50	2.11	.060	-.045	2.37	0.43	4.16	7.75	0	.2246	.0270	.488	.908	0
.50	2.53	.074	0	2.84	0.37	4.27	7.77	-.01	.1560	.0231	.500	----	-.001
.50	3.17	-.05	.066	3.55	0.33	4.43	7.77	-.02	.0999	.0210	.519	.911	-.003
.50	3.59	1.34	.159	4.03	0.33	4.57	----	-.04	.0777	.0208	.547	----	-.005
.50	4.22	.187	.380	4.74	0.33	5.21	7.93	-.07	.0562	.0210	.611	.929	-.008

TABLE IV - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 12 WITH CHINE STRIPS

C_{A_Q}	C_{V_Q}	C_{P_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(A)} \frac{1}{L}$	$\frac{l}{(A)} \frac{1}{L}$	$\frac{h}{(A)} \frac{1}{L}$	C_{T_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$		
$\tau = 8^\circ$															
0	0	0	0	0	0	-----	-----	-----	0	0	0.314	0.070			
0	.63	0	0	0	0	-----	-----	-----	0	0	0.076	0.080			
0	1.06	0	0	0	0	-----	-----	-----	0	0	0	0.082			
0	1.48	0	0	0	0	-----	-----	-----	0	0	0	0.082			
0	2.11	0	c	0	0	-----	-----	-----	0	0	0	0.082			
0	2.53	0	0	0	0	-----	-----	-----	0	0	0	0.082			
0	3.17	0	0	0	0	-----	-----	-----	0	0	0	0.077			
0	3.59	0	0	0	0	-----	-----	-----	0	0	0	0.076			
0	4.22	0	0	0	0	-----	-----	-----	0	0	0	0.076			
0	4.64	0	0	0	0	-----	-----	-----	0	0	0	0.076			
0	5.28	0	0	0	0	-----	-----	-----	0	0	0	0.076			
0	6.33	0	0	0	0	-----	-----	-----	0	0	0	0.076			
0	7.39	0	0	0	0	-----	-----	-----	0	0	0	0.077			
0	8.44	0	0	0	0	-----	-----	-----	0	0	0	0.077			
0	9.50	0	0	0	0	-----	-----	-----	0	0	0	0.077			
0	10.55	0	0	0	0	-----	-----	-----	0	0	0	0.077			
0	11.61	0	0	0	0	-----	-----	-----	0	0	0	0.077			
0	12.66	0	0	0	0	-----	-----	-----	0	0	0	0.079			
0	13.72	0	0	0	0	-----	-----	-----	0	0	0	0.079			
0	14.77	0	0	0	0	-----	-----	-----	0	0	0	0.079			
0	15.83	0	0	0	0	-----	-----	-----	0	0	0	0.079			
0	16.88	0	0	0	0	-----	-----	-----	0	0	0	0.079			
.10	0	0	0	0	0	0.170	0	0.58	7.80	0.61	0.246	0.535	0.042		
.10	.63	.002	0	0	0	0.159	0.93	0.046	4.54	0.59	0.4988	0.0100	0.312		
.10	1.06	.007	0	0	0	0.147	1.55	0.058	4.30	0.61	0.126	0.295	0.042		
.10	1.48	.012	0	0	0	0.141	2.17	0.051	4.26	0.62	0.110	0.293	0.042		
.10	2.11	.018	0	0	0	0.126	3.10	0.038	4.61	0.60	0.081	0.315	0.042		
.10	2.53	.023	0	0	0	0.101	3.72	0.033	5.19	0.61	0.0312	0.072	0.356		
.10	3.17	.028	0	0	0	0.079	1.65	0.026	5.66	0.62	0.0203	0.056	0.398		
.10	3.59	.031	0	0	0	0.074	5.26	0.022	5.75	0.68	0.0155	0.048	0.394		
.10	4.22	.034	0	0	0	0.079	6.19	0.018	5.66	0.72	0.0112	0.038	0.388		
.10	4.64	.038	0	0	0	0.086	6.81	0.016	5.53	0.73	0.0093	0.035	0.379		
.10	5.28	.041	0	0	0	0.090	7.74	0.013	5.44	0.76	0.0072	0.029	0.373		
.10	6.33	.046	0	0	0	0.115	9.29	0.011	4.94	5.51	.80	0.023	0.339	0.378	
.10	7.39	.056	0	0	0	0.145	10.84	0.010	4.56	4.97	.54	0.002	0.299	0.341	
.10	8.44	.059	0	0	0	0.174	12.39	0.008	3.77	4.78	.88	0.028	0.259	0.328	
.10	9.50	.070	0	0	0	0.209	13.94	0.007	3.15	4.58	.88	0.022	0.216	0.314	
.10	10.55	.075	0	0	0	0.209	15.49	0.006	3.59	4.26	.90	0.016	0.246	0.293	
.10	11.61	.082	0	0	0	0.249	17.04	0.005	2.41	4.09	.91	0.013	0.212	0.281	
.10	12.66	.082	0	0	0	0.260	18.59	0.005	2.22	4.07	.93	0.013	0.210	0.279	
.10	13.72	.083	0	0	0	0.279	20.13	0.004	1.83	3.63	.93	0.011	0.009	0.249	
.10	14.77	.089	0	0	0	0.291	21.68	0.004	1.66	5.50	.93	0.008	.114	0.225	
.10	15.83	.088	0	0	0	0.289	23.23	0.003	1.67	3.14	.93	0.007	.114	0.215	
.20	0	0	0	0	0	0.269	0	0	3.46	7.30	.31	0	0.299	0.630	
.20	.63	.004	0	0	0	0.259	.63	0.058	3.56	0.30	0.9975	0.0200	0.307	0.026	
.20	1.06	.013	0	0	0	0.231	1.38	0.068	3.81	7.14	.31	0.3594	0.0234	0.329	0.027
.20	1.48	.019	0	0	0	0.225	1.93	0.051	3.88	0	1.853	0.0174	0.335	0.027	
.20	2.11	.029	0	0	0	0.194	2.76	0.058	4.15	7.12	.32	0.0898	0.030	0.358	0.028
.20	2.53	.039	0	0	0	0.150	3.31	0.056	4.54	0	0.624	0.022	0.392	0.027	
.20	3.17	.050	0	0	0	0.075	4.14	0.029	5.15	6.73	.31	0.0399	0.0100	0.445	0.583
.20	3.59	.053	0	0	0	0.054	1.69	0.021	5.35	0	0.031	0.0082	0.462	0.332	
.20	4.22	.060	0	0	0	0.050	5.52	0.020	5.37	6.26	.41	0.0225	0.0067	0.464	0.540
.20	4.64	.063	0	0	0	0.060	6.07	0.017	5.50	0	0.0186	0.0058	0.458	0.539	

TABLE IV - Continued
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 12 WITH CHINE STRIPS

$c_{\Delta Q}$	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(L)}$ $1/3$	$\frac{z}{(L)}$ $1/3$	$\frac{h}{(L)}$ $1/3$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$\tau = 8^\circ$ - Concluded													
.20	5.28	0.068	-0.080	6.90	0.014	5.23	5.69	0.49	0.0144	0.0049	0.443	0.491	0.042
.20	6.33	.073	-.125	8.28	.011	4.76	5.17	.54	.0100	.0036	4.21	4.47	.046
.20	7.39	.062	-.164	9.66	.009	4.42	4.83	.58	.0073	.0050	3.62	4.17	.050
.20	8.44	.087	-.204	11.04	.007	4.17	4.56	.62	.0056	.0024	3.56	3.94	.054
.20	9.50	.103	-.261	12.42	.007	3.68	4.27	.64	.0044	.0023	3.18	3.69	.055
.20	10.55	.118	-.275	13.80	.006	3.59	4.19	.65	.0036	.0021	3.10	3.62	.056
.20	11.61	.130	-.331	15.18	.006	3.16	3.95	.65	.0030	.0019	2.73	3.41	.056
.20	12.66	.142	-.371	16.56	.005	2.87	3.87	.66	.0025	.0018	2.48	3.24	.057
.20	13.72	.157	-.397	17.94	.005	2.70	3.66	.67	.0021	.0017	2.33	3.16	.058
.30	0	0	-.330	0	-----	3.39	6.95	.16	-----	-----	.335	.687	.016
.30	.63	.005	-.320	.77	.056	3.45	-----	.33	1.4963	.0249	.311	-----	.013
.30	1.06	.019	-.285	1.29	.076	5.64	6.98	.15	.5591	.0341	.360	.690	.014
.30	1.48	.028	-.269	1.80	.057	5.73	-----	.16	.2750	.0257	.369	-----	.016
.30	2.11	.041	-.229	2.58	.041	3.92	6.72	.17	.1348	.0181	.388	.664	.017
.30	2.53	.053	-.170	3.09	.037	4.23	-----	.16	.0536	.0165	.418	-----	.016
.30	3.17	.069	-.049	3.87	.031	4.83	6.74	.15	.0599	.0158	.477	.666	.015
.30	3.59	.078	0	4.38	.027	5.06	-----	.19	.0466	.0121	.500	-----	.019
.30	4.22	.085	.011	5.16	.021	5.11	6.20	.24	.0337	.0095	.505	.613	.023
.30	4.64	.088	0	5.67	.018	5.06	-----	.29	.0278	.0082	.500	-----	.029
.30	5.28	.095	-.019	6.45	.015	4.98	5.50	.35	.0216	.0068	.492	.514	.035
.30	6.33	.101	-.081	7.74	.011	4.67	5.06	.40	.0150	.0050	.462	.500	.040
.30	7.39	.107	-.145	9.02	.009	4.35	4.72	.45	.0110	.0039	.430	.466	.044
.30	8.44	.120	-.210	10.31	.008	4.06	4.39	.49	.0084	.0034	.401	.434	.049
.30	9.50	.133	-.280	11.60	.006	3.73	4.16	.52	.0067	.0025	.369	.411	.052
.30	10.55	.147	-.300	12.89	.006	3.64	3.89	.53	.0054	.0026	.360	.385	.053
.30	11.61	.163	-.356	14.18	.005	3.39	3.80	.55	.0044	.0024	.333	.376	.055
.40	0	0	-.355	0	-----	3.37	6.94	.05	-----	-----	.367	.756	.005
.40	.63	.007	-.340	.74	.064	3.43	-----	.03	1.9950	.0349	.373	-----	.005
.40	1.06	.026	-.306	1.23	.086	3.57	6.89	.05	.7188	.0467	.388	.730	.005
.40	1.48	.040	-.285	1.72	.068	3.62	-----	.07	.3666	.0567	.394	-----	.008
.40	2.11	.054	-.239	2.15	.045	3.80	6.70	.05	.1797	.0243	.413	.729	.009
.40	2.53	.066	-.170	2.96	.038	4.03	-----	.05	.248	.0206	.439	-----	.006
.40	3.17	.089	-.019	3.70	.033	4.54	6.73	.05	.0799	.0178	.494	.733	.005
.40	3.59	.100	.070	4.19	.029	4.83	-----	.06	.0622	.0155	.525	-----	.007
.40	4.22	.107	.115	4.93	.022	4.97	6.21	.13	.0449	.0120	.541	.676	.014
.40	4.64	.114	.105	5.42	.020	4.94	-----	.18	.0371	.0106	.528	-----	.019
.40	5.28	.122	.067	6.16	.016	4.82	5.48	.24	.0288	.0088	.524	.597	.026
.40	6.33	.130	-.079	7.39	.012	4.35	4.97	.32	.0200	.0065	.473	.540	.034
.40	7.39	.139	-.094	8.62	.009	4.25	4.64	.37	.0147	.0051	.462	.505	.041
.40	8.44	.141	-.180	9.85	.007	4.02	4.32	.41	.0112	.0040	.437	.470	.045
.50	0	0	-.346	0	-----	3.38	6.87	-.01	-----	-----	.396	.805	-.004
.50	.63	.007	-.336	.7-	.055	3.41	-----	-.05	2.4938	.0349	.401	-----	-.005
.50	1.06	.030	-.306	1.18	.086	3.49	6.83	-.03	.895	.0539	.409	.800	-.004
.50	1.48	.045	-.280	1.66	.065	3.57	-----	0	.585	.0412	.418	-----	0
.50	2.11	.062	-.221	2.37	.044	3.71	6.59	0	.2246	.0279	.435	.772	0
.50	2.53	.078	-.139	2.84	.039	3.92	-----	-.01	.1560	.0243	.460	-----	-.001
.50	3.17	.110	.015	3.55	.035	4.31	6.63	-.02	.0999	.0220	.505	.777	-.003
.50	3.59	.125	.124	4.03	.031	4.57	-----	-.02	.0777	.0194	.536	-----	-.003
.50	4.22	.134	.241	4.74	.024	4.86	6.24	-.04	.0562	.0150	.570	.731	.004

TABLE IV - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 12 WITH CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_A}	c_{D_A}	$\frac{x}{(A)} \frac{1}{\sqrt{w}}$	$\frac{l}{(A)} \frac{1}{\sqrt{w}}$	$\frac{h}{(A)} \frac{1}{\sqrt{w}}$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 12^\circ$													
0	0	0	0	0	0	-----	-----	-----	0	0.0100	-5.064	0.154	0.05
0	.63	.002	-.014	0	0	-----	-----	-----	0	.0036	-3.952	.178	.106
0	1.06	.002	-.014	0	0	-----	-----	-----	0	.0027	-3.210	-----	.108
0	1.48	.002	-.014	0	0	-----	-----	-----	0	.0009	-2.256	.095	.113
0	2.11	.002	-.009	0	0	-----	-----	-----	0	.0003	-10.630	-----	.116
0	2.53	.001	-.014	0	0	-----	-----	-----	0	-----	-----	.004	.119
0	3.17	0	-.025	0	0	-----	-----	-----	0	-----	-----	0	.120
0	3.59	0	0	0	0	-----	-----	-----	0	-----	-----	0	.121
0	4.22	0	0	0	0	-----	-----	-----	0	-----	-----	0	.122
0	4.64	0	-.001	0	0	-----	-----	-----	0	-----	-----	0	.122
0	5.28	0	-.004	0	0	-----	-----	-----	0	-----	-----	.004	.122
0	6.33	0	0	0	0	-----	-----	-----	0	0	-----	0	.122
0	7.39	0	-.019	0	0	-----	-----	-----	0	0	-----	0	.122
0	8.44	.001	0	0	0	-----	-----	-----	0	0	-.500	0	.122
0	9.50	-----	-----	0	0	-----	-----	-----	0	-----	-----	0	-----
0	10.55	.002	-.029	0	0	-----	-----	-----	0	0	-8.828	.004	.120
0	11.61	-----	-----	0	0	-----	-----	-----	0	-----	-----	0	-----
0	12.66	.002	-.020	0	0	-----	-----	-----	0	0	-5.860	.002	.118
0	13.72	-----	-----	0	0	-----	-----	-----	0	-----	-----	0	-----
0	14.77	.002	-.009	0	0	-----	-----	-----	0	0	-2.256	0	.118
0	15.83	-----	-----	0	0	-----	-----	-----	0	0	-----	0	-----
0	16.88	.004	-.009	0	0	-----	-----	-----	0	0	-17.121	0	.118
.10	0	0	-.185	0	0.116	3.21	6.57	0.79	0.4988	.0249	.220	.450	.054
.10	.63	.005	-.180	.93	0.116	3.37	-----	.79	0.4988	.0249	.231	-----	.054
.10	1.06	.012	-.180	1.55	.100	3.35	6.41	.81	.1797	.0216	.235	.440	.058
.10	1.48	.015	-.163	2.17	.064	3.58	-----	.86	.0917	.0137	.252	-----	.059
.10	2.11	.022	-.159	3.10	.046	3.92	6.03	.88	.0449	.0099	.259	.43	.061
.10	2.53	.021	-.153	3.72	.031	4.08	-----	.95	.0312	.0056	.280	-----	.065
.10	3.17	.021	-.165	4.65	.019	3.83	5.02	1.03	.0200	.0042	.263	.344	.070
.10	3.59	.024	-.180	5.26	.017	3.52	-----	.93	.0155	.0037	.242	-----	.075
.10	4.22	.022	-.200	6.19	.012	3.09	4.20	1.16	.0112	.0025	.212	.288	.079
.10	4.64	.022	-.220	6.81	.009	2.66	-----	1.20	.0093	.0020	.182	-----	.082
.10	5.28	.021	-.229	7.74	.007	2.47	3.24	1.25	.0072	.0015	.170	.222	.086
.10	6.33	.022	-.254	9.29	.005	1.95	2.43	1.31	.0050	.0011	.134	.170	.090
.10	7.39	.022	-.280	10.84	.004	1.39	2.21	1.32	.0037	.0008	.095	.132	.091
.10	8.44	.022	-.289	12.39	.003	1.20	1.96	1.35	.0028	.0006	.083	.134	.093
.10	9.50	.021	-.320	13.94	.002	.56	1.70	1.38	.0022	.0005	.038	.117	.093
.10	10.55	.024	-.325	15.49	.002	.46	1.44	1.32	.0018	.0006	.052	.099	.094
.10	11.61	.022	-.310	17.04	.001	.77	1.18	1.39	.0015	.0003	.053	.081	.095
.10	12.66	.022	-.350	18.59	.001	-.09	1.13	1.39	.0013	.0003	-.006	.078	.095
.10	13.72	.024	-.360	20.13	.001	-.26	.98	1.40	.0011	.0003	-.019	.067	.096
.10	14.77	.025	-.350	21.68	.001	-.06	.71	1.40	.0009	.0002	-.004	.049	.096
.10	15.83	.022	-.350	23.23	.001	-.09	.80	1.39	.0008	.0002	-.006	.055	.095
.20	0	0	-.295	0	-----	3.20	6.30	.41	-----	-----	.276	.544	.036
.20	.63	.007	-.289	.83	.102	3.27	-----	.41	.9975	.0349	.282	-----	.036
.20	1.06	.021	-.281	1.38	.110	3.39	6.25	.45	.3594	.0377	.295	.540	.039
.20	1.48	.020	-.269	1.93	.070	3.51	-----	.49	.1833	.0258	.305	-----	.042
.20	2.11	.041	-.236	2.76	.054	3.81	6.01	.49	.C566	.0181	.329	.519	.042
.20	2.53	.045	-.220	3.31	.041	3.95	-----	.54	.0624	.0140	.341	-----	.046
.20	3.17	.047	-.224	4.14	.027	3.93	5.20	.62	.0399	.0094	.339	.449	.054
.20	3.59	.046	-.245	4.69	.022	3.75	-----	.69	.0311	.0075	.324	-----	.060
.20	4.22	.049	-.255	5.52	.016	3.44	4.38	.76	.0225	.0055	.297	.378	.066
.20	4.64	.048	-.300	6.07	.013	3.29	-----	.82	.0156	.0045	.281	-----	.070

TABLE IV - Continued

**EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 12 WITH CHINE STRIPS**

TABLE IV - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 12 WITH CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_A}	c_{D_A}	$\frac{x}{(\Delta)^{1/3}}$	$\frac{l}{(\Delta)^{1/3}}$	$\frac{h}{(\Delta)^{1/3}}$	c_{L_Q}	c_{D_Q}	$\frac{L}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 15^\circ$ - Continued													
0	6.33	0	0	----	----	----	----	----	0	0	----	0	C.142
0	7.39	----	----	----	----	----	----	0	0	----	----	----	----
0	8.44	----	----	----	----	----	----	0	0	----	----	----	----
0	9.50	----	----	----	----	----	0	0	0	0	0	0	0
0	10.55	0	0	----	----	----	----	0	0	0	0	0	0
0	11.61	----	----	----	----	----	0	0	0	0	0	0	0
0	12.66	----	----	----	----	----	0	0	0	0	0	0	0
0	13.72	0	0	----	----	----	0	0	0	0	.002	.138	0
0	14.77	----	----	----	----	----	0	0	0	0	0	0	0
0	15.83	----	----	----	----	----	0	0	0	0	0	0	0
0	16.88	0	-.101	----	----	----	0	0	0	0	0	0	.138
.10	0	0	-.185	0	-.162	3.12	5.67	1.01	----	0.214	.403	.069	C.142
.10	.63	.007	-.192	.93	1.55	3.05	5.82	1.01	.4958	.0349	.210	.069	0
.10	1.06	.012	-.186	1.55	1.00	3.24	5.82	1.07	.1797	.0216	.223	.399	.074
.10	1.48	.019	-.185	2.17	.081	3.37	5.82	1.10	.0917	.0174	.231	----	.075
.10	2.11	.024	-.194	3.10	.050	3.21	4.97	1.20	.0449	.0108	.220	.341	.083
.10	2.53	.021	-.194	3.72	.031	3.18	5.82	1.34	.0312	.0066	.218	----	.092
.10	3.17	.022	-.214	4.65	.020	2.76	3.71	1.45	.0200	.0044	.19	.254	.100
.10	3.59	.022	-.229	5.26	.016	2.48	5.82	1.54	.0155	.0034	.170	----	.106
.10	4.22	.021	-.247	6.19	.011	2.07	2.73	1.65	.0112	.0024	.142	.187	.113
.10	4.64	.021	-.250	6.81	.009	2.01	5.82	1.70	.0093	.0019	.138	----	.117
.10	5.23	.020	-.260	7.74	.006	1.76	1.93	1.75	.0072	.0014	.121	.132	.120
.10	6.33	.020	-.296	9.29	.005	.99	1.60	1.69	.0050	.0010	.068	.109	.116
.10	7.39	.021	-.301	10.54	.004	.63	1.18	1.78	.0037	.0008	.058	.081	.122
.10	8.44	.021	-.306	12.39	.003	.60	1.08	1.79	.0022	.0006	.055	.074	.123
.10	9.50	.021	-.320	13.94	.002	.31	.93	1.83	.0022	.0005	.023	.064	.125
.10	10.55	.022	-.310	15.49	.002	.77	.83	1.83	.0018	.0004	.053	.060	.125
.10	11.61	.024	-.336	17.01	.002	.25	.67	1.34	.0015	.0004	.017	.046	.126
.10	12.66	.021	-.352	18.59	.001	-.09	.77	1.85	.0013	.0003	-.006	.055	.127
.10	13.72	.025	-.352	20.13	.001	-.09	0	1.87	.0011	.0003	-.006	0	.128
.10	14.77	.025	-.361	21.68	.001	-.28	.26	1.86	.0009	.0002	-.019	.018	.128
.10	15.83	.024	-.381	23.23	.001	-.71	.49	1.85	.0008	.0002	-.049	.034	.127
.20	0	0	-.304	0	----	3.07	5.79	.53	----	0.265	.500	.046	0
.20	.63	.010	-.303	.83	.146	3.14	5.79	.52	.9975	.0499	.271	----	.045
.20	1.06	.025	-.316	1.38	.131	3.07	5.68	.58	.5594	.0449	.265	.491	.051
.20	1.48	.033	-.290	1.93	.088	3.34	5.82	.61	.1833	.0302	.288	----	.052
.20	2.11	.047	-.303	2.76	.062	3.27	5.10	.70	.0898	.0211	.288	.440	.061
.20	2.53	.049	-.295	3.3	.045	3.34	5.82	.81	.0624	.0153	.286	----	.070
.20	3.17	.049	-.326	4.14	.029	3.09	4.15	.94	.0399	.0098	.267	.358	.081
.20	3.59	.049	-.350	4.59	.022	2.80	5.82	1.02	.0311	.0076	.242	----	.088
.20	4.22	.047	-.405	5.52	.015	2.41	3.18	1.12	.0253	.0053	.208	.275	.097
.20	4.64	.045	-.431	6.07	.012	2.19	5.82	1.14	.0186	.0042	.189	----	.099
.20	5.28	.043	-.468	6.90	.009	1.86	2.58	1.20	.0144	.0031	.161	.222	.104
.20	6.33	.043	-.509	8.26	.006	1.52	2.00	1.23	.0100	.0021	.131	.173	.106
.20	7.39	.043	-.547	9.66	.005	1.20	1.72	1.31	.0073	.0016	.104	.142	.123
.20	8.44	.041	-.551	11.04	.004	1.16	1.35	1.35	.0056	.0012	.100	.117	.116
.20	9.50	.040	-.591	12.42	.003	.81	1.15	1.38	.0044	.0009	.070	.099	.119
.20	10.55	.040	-.601	13.60	.002	.71	1.03	1.39	.0056	.0007	.061	.094	.120
.20	11.61	.042	-.516	15.18	.002	.61	.94	1.40	.0030	.0006	.053	.081	.121
.20	12.66	.045	-.655	16.56	.002	.29	0	1.41	.0025	.0006	.025	0	.122
.20	13.72	.045	-.649	17.94	.001	.37	.72	1.40	.0022	.0005	.032	.062	.121
.30	0	0	-.361	0	----	3.07	5.79	.26	----	.303	.572	.026	0
.30	.63	.010	-.377	.77	.11	3.14	5.79	.26	1.4963	.0499	.310	----	.025
.30	1.06	.035	-.357	1.29	.140	3.11	5.60	.34	.5331	.0629	.307	.554	.033
.30	1.48	.043	-.362	1.80	.086	3.26	5.82	.55	.2750	.0394	.322	----	.034
.30	2.11	.069	-.373	2.58	.069	3.24	5.16	.44	.1346	.0320	.320	.510	.043
.30	2.53	.078	-.357	3.09	.054	3.35	5.82	.53	.0936	.0243	.331	----	.053
.30	3.17	.078	-.387	3.67	.056	3.20	4.29	.56	.0599	.0260	.316	.424	.065
.30	3.59	.078	-.428	4.38	.027	3.00	5.82	.76	.0466	.0121	.297	----	.073
.30	4.22	.075	-.495	5.16	.019	2.66	3.41	.86	.0337	.0084	.263	.337	.085

TABLE IV - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 12 WITH CHINE STRIPS

C_{A_Q}	C_{V_Q}	C_{P_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(A)} \frac{1}{\sqrt{2}}$	$\frac{l}{(A)} \frac{1}{\sqrt{2}}$	$\frac{h}{(A)} \frac{1}{\sqrt{2}}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 16^\circ$ - Concluded													
.30	4.64	0.077	-0.537	5.67	0.015	2.45	---	0.93	0.0278	0.0066	0.242	----	0.092
.30	5.28	.068	-.597	6.45	.011	2.16	2.80	.98	.0216	.0049	.218	0.277	.097
.30	6.33	.066	-.679	7.74	.007	1.74	2.29	.99	.0150	.0033	.172	.226	.098
.30	7.39	.065	-.747	9.02	.005	1.42	1.89	1.07	.0110	.0024	.140	.187	.106
.30	8.44	.063	-.766	10.31	.004	1.30	1.63	1.12	.0084	.0018	.129	.161	.111
.30	9.50	.062	-.832	11.60	.003	.99	1.38	1.14	.0067	.0014	.098	.136	.112
.30	10.55	.061	-.852	12.89	.002	.90	1.29	1.17	.0054	.0011	.089	.127	.115
.30	11.61	.061	-.902	14.18	.002	.65	1.04	1.18	.0044	.0009	.064	.102	.117
.40	0	0	-.409	0	----	3.15	5.78	.07	----	----	.343	.629	.008
.40	.63	.014	-.409	.74	.129	3.18	----	.08	1.9950	.0698	.346	----	.009
.40	1.06	.047	-.427	1.23	.156	3.13	5.58	.16	.7188	.0843	.341	.607	.017
.40	1.48	.059	-.587	1.72	.100	3.29	----	.16	.3666	.0541	.358	----	.018
.40	2.11	.093	-.346	2.45	.077	3.45	5.35	.20	.1757	.0418	.375	.563	.021
.40	2.55	.103	-.391	2.96	.059	3.31	----	.24	.1248	.0321	.360	----	.038
.40	3.17	.108	-.401	3.70	.040	3.27	4.48	.16	.0799	.0216	.356	.487	.050
.40	3.59	.110	-.457	4.19	.031	3.10	----	.55	.0622	.0171	.337	----	.060
.40	4.22	.103	-.539	4.93	.021	2.82	3.59	.57	.0449	.0116	.307	.390	.073
.40	4.64	.101	-.603	5.42	.017	2.61	----	.70	.0371	.0094	.284	----	.076
.40	5.28	.099	-.687	6.16	.013	2.32	3.01	.77	.0288	.0071	.252	.328	.084
.40	6.33	.089	-.812	7.39	.008	1.91	2.39	.84	.0200	.0044	.208	.250	.091
.40	7.39	.086	-.902	8.62	.006	1.60	2.21	.92	.0147	.0032	.174	.240	.100
.40	8.44	.083	-.961	9.85	.004	1.41	1.75	.96	.0112	.0023	.153	.191	.104
.50	0	0	-.405	0	----	3.20	5.85	-.07	----	----	.375	.685	-.009
.50	.63	.024	-.407	.71	.111	3.20	----	-.05	2.4938	.0698	.375	----	-.006
.50	1.06	.054	-.437	1.18	.154	3.15	5.67	.02	.8965	.0970	.369	.664	.002
.50	1.48	.071	-.387	1.66	.103	3.29	----	.05	.4563	.0651	.386	----	.006
.50	2.11	.108	-.320	2.37	.077	3.47	5.38	.09	.2246	.0485	.407	.650	.011
.50	2.55	.132	-.407	2.84	.065	3.28	----	.20	.1560	.0412	.384	----	.023
.50	3.17	.143	-.397	3.55	.045	3.31	4.54	.35	.0999	.0286	.386	.532	.039
.50	3.59	.142	-.454	4.03	.055	3.17	----	.44	.0777	.022	.371	----	.052
.50	4.22	.136	-.568	4.74	.024	2.89	3.66	.57	.0562	.0153	.339	.429	.066
$\tau = 20^\circ$													
0	0	0	0	0	----	----	----	----	0	0.0050	-3.740	0.104	0.171
0	.63	.001	-.007	----	----	----	----	----	0	0	----	.005	.167
0	1.06	0	-.004	----	----	----	----	----	0	0	----	.179	----
0	1.48	0	-.004	----	----	----	----	----	0	0	----	.161	----
0	2.11	0	0	----	----	----	----	----	0	0	----	0	.186
0	2.55	0	-.068	----	----	----	----	----	0	0	----	.185	----
0	3.17	0	-.004	----	----	----	----	----	0	0	----	0	.185
0	3.59	.001	-.068	----	----	----	----	----	0	0.0002	-23.526	----	.184
0	4.22	0	-.004	----	----	----	----	----	0	0	----	.002	.184
0	4.64	0	-.009	----	----	----	----	----	0	0	----	.184	----
0	5.28	0	-.009	----	----	----	----	----	0	0	----	.002	.184
0	6.33	0	-.005	----	----	----	----	----	0	0	----	0	.184
0	7.39	----	----	----	----	----	----	----	0	0	----	----	----
0	8.44	.001	-.004	----	----	----	----	----	0	0	-1.317	.002	.185
0	9.50	----	----	----	----	----	----	----	0	0	----	.011	.184
0	10.55	.002	----	----	----	----	----	----	0	0	----	0	----
0	11.61	----	----	----	----	----	----	----	0	0	-1.121	.005	.184
0	12.66	.002	-.009	----	----	----	----	----	0	0	-6.856	.002	.183
0	13.72	----	----	----	----	----	----	----	0	0	-14.215	.002	.185
0	14.77	.002	-.040	----	----	----	----	----	0	0	----	----	----
0	15.83	----	----	----	----	----	----	----	0	0	----	----	----
0	16.88	.002	-.079	----	----	----	----	----	0	0	----	----	----

TABLE IV - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 12 WITH CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{l}$	$\frac{z}{l}$	$\frac{h}{l}$	c_{L_Q}	c_{D_Q}	$\frac{x}{l}$	$\frac{l}{L}$	$\frac{a}{L}$
$\tau = 20^\circ$ - Continued													
.10	0	c	-0.194	0	----	2.54	5.43	1.25	----	0.195	0.373	0.065	
.10	.63	.009	-.210	.93	0.208	2.66	----	1.23	0.4982	0.0449	.182	----	.087
.10	1.06	.016	-.210	1.55	.134	2.75	5.18	1.30	.1797	0.0288	.189	.355	.089
.10	1.48	.025	-.226	2.17	.106	2.53	----	1.42	.0917	0.0229	.174	----	.095
.10	2.11	.027	-.229	3.10	.056	2.50	4.12	1.60	.0449	0.021	.172	.283	.110
.10	2.53	.024	-.233	3.72	.035	2.44	----	1.72	.0312	0.0075	.167	----	.113
.10	3.17	.024	-.255	4.65	.022	1.92	2.81	1.87	.0200	0.0048	.131	.192	.128
.10	3.59	.026	-.276	5.25	.019	1.51	----	1.95	.0255	0.0040	.104	----	.134
.10	4.22	.026	-.280	6.19	.013	1.42	1.98	2.05	.0112	0.0029	.098	.136	.140
.10	4.64	.024	-.291	6.87	.010	1.14	----	2.10	.0033	0.0022	.078	----	.144
.10	5.28	.024	-.310	7.74	.008	.74	1.44	2.14	.0072	0.0017	.051	.099	.147
.10	6.33	.027	-.330	9.29	.006	.46	1.13	2.23	.0050	0.0013	.028	.076	.153
.10	7.39	.026	-.330	10.94	.005	.36	.93	2.29	.0037	0.0010	.025	.064	.157
.10	8.44	.027	-.330	12.39	.004	.40	.75	2.33	.0028	0.0008	.028	.051	.160
.10	9.50	.027	-.355	13.34	.003	1.12	4.1	2.36	.0022	0.0006	.008	.028	.162
.10	10.55	.028	-.310	15.19	.002	1.8	.41	2.37	.0018	0.0005	.013	.030	.163
.10	11.51	.028	-.360	17.04	.002	.22	.93	2.37	.0015	0.0004	.015	.064	.163
.10	12.66	.05	-.372	18.59	.002	.34	.67	2.37	.0013	0.0004	.023	.046	.165
.10	13.72	.032	-.371	20.13	.001	.34	.16	2.37	.0011	0.0003	.023	.011	.165
.10	14.77	.031	-.411	21.68	.001	1.16	.16	2.38	.0009	0.0003	.061	.011	.164
.10	15.83	.033	----	23.23	.001	1.6	2.38	2.38	.0008	0.0003	----	.011	.164
.20	0	0	-.320	0	----	2.87	5.44	.64	----	2.48	.470	.055	
.20	.63	.015	-.342	.83	.219	2.78	----	.68	.9975	.0748	.240	----	.058
.20	1.06	.032	-.348	1.38	.168	2.80	5.21	.74	.5594	.0575	.242	.450	.064
.20	1.48	.042	-.355	1.93	.113	2.98	----	.78	.1833	.0585	.257	----	.067
.20	2.11	.056	-.377	2.76	.074	2.72	4.12	.56	.0898	.0522	.235	.381	.083
.20	2.53	.056	-.363	3.31	.051	2.88	----	.09	.0624	.0175	.242	----	.094
.20	3.17	.051	-.109	4.11	.032	2.41	3.35	1.24	.0339	.0108	.205	.292	.107
.20	3.59	.051	-.442	4.69	.025	2.11	1.34	.0311	.0084	.158	----	.115	
.20	4.22	.052	-.478	5.52	.017	1.82	2.45	1.45	.0225	.0058	.157	.212	.125
.20	4.64	.051	-.498	6.07	.014	1.64	----	1.50	.0186	.0047	.142	----	.130
.20	5.28	.051	-.523	6.90	.011	1.42	1.92	1.57	.0144	.0037	.123	.156	.136
.20	6.33	.051	-.561	8.28	.007	1.10	1.44	1.57	.0100	.0025	.095	.124	.145
.20	7.39	.049	-.595	9.66	.005	.81	1.19	1.73	.0073	.0018	.070	.102	.149
.20	8.44	.051	-.605	11.04	.004	.74	1.06	1.77	.0056	.0014	.064	.092	.153
.20	9.50	.052	-.645	12.12	.004	.42	.90	1.80	.0044	.0012	.036	.078	.155
.20	10.55	.053	-.663	13.80	.003	.27	.74	1.82	.0036	.0010	.023	.064	.157
.20	11.61	.053	-.674	15.18	.002	.17	.53	1.83	.0030	.0008	.015	.046	.158
.20	12.56	.051	-.671	15.56	.002	.20	.53	1.84	.0025	.0007	.017	.046	.159
.20	13.72	.053	-.704	17.94	.002	1.12	1.85	.0021	.0006	----	.011	.160	
.30	0	0	-.407	0	----	2.89	5.50	.32	----	2.86	.544	.051	
.30	.63	.018	-.411	.77	.200	2.91	----	.74	1.4963	.0698	.288	----	.054
.30	1.06	.046	-.436	1.29	.185	2.87	5.25	.43	.5391	.0827	.284	.519	.062
.30	1.48	.059	-.402	1.80	.121	3.07	----	.46	.2750	.0541	.303	----	.066
.30	2.11	.059	-.472	2.52	.089	2.81	4.59	.53	.1348	.0400	.278	.454	.063
.30	2.53	.059	-.453	3.39	.062	2.89	----	.74	.0936	.0278	.256	----	.074
.30	3.17	.089	-.502	3.57	.040	2.64	3.55	.82	.0599	.0178	.261	.351	.061
.30	3.59	.089	-.587	4.38	.029	2.23	----	1.02	.0466	.0132	.220	----	.101
.30	4.22	.080	-.620	5.16	.020	2.06	2.68	1.14	.0337	.0090	.204	.265	.113
.30	4.54	.078	-.658	5.67	.016	1.86	----	1.20	.0278	.0072	.184	----	.119
.30	5.28	.076	-.709	6.45	.012	1.61	2.03	1.25	.0216	.0055	.159	.201	.124
.30	6.33	.078	-.787	7.74	.009	1.24	1.56	1.37	.0150	.0039	.123	.164	.136
.30	7.39	.078	-.862	9.02	.006	.92	1.50	1.42	.0110	.0029	.091	.148	.140
.30	8.44	.074	-.851	10.31	.005	.92	1.54	1.47	.0084	.0021	.091	.152	.146
.30	9.50	.074	-.888	11.60	.004	.73	.89	1.51	.0067	.0016	.072	.088	.149
.30	10.55	.075	-.918	12.89	.003	.50	.88	1.53	.0054	.0013	.059	.087	.151
.30	11.61	.078	-.938	14.18	.003	.52	.82	1.54	.0044	.0012	.051	.081	.153

TABLE IV - Concluded
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 12 WITH CHINE STRIPS

C_{A_Q}	C_{V_Q}	C_{R_Q}	C_{K_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{1/3}$ ($\frac{A}{w}$)	$\frac{l}{1/3}$ ($\frac{A}{w}$)	$\frac{h}{1/3}$ ($\frac{A}{w}$)	C_{T_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 20^\circ$ - Concluded													
.40	0	0	-0.456	0	-----	3.02	5.5-	0.09	-----	-----	0.329	0.599	0.010
.40	.63	.022	-0.454	.74	0.202	2.98	-----	.13	1.9950	0.1097	.324	-----	.014
.40	1.06	.060	-0.474	1.23	.199	2.98	5.27	.23	.7188	.1078	.324	.574	.025
.40	1.48	.073	-0.456	1.72	.123	3.12	-----	.26	.5666	.0669	.339	-----	.028
.40	2.11	.118	-0.528	2.46	.098	2.87	4.69	.42	.1797	.0530	.312	.510	.045
.40	2.55	.125	-0.503	2.96	.072	2.98	-----	.52	.1248	.0390	.324	-----	.056
.40	3.17	.125	-0.573	3.70	.046	2.73	5.78	.69	.0799	.0290	.297	.411	.075
.40	3.59	.122	-0.637	4.19	.035	2.54	-----	.80	.0622	.0190	.276	-----	.087
.40	4.22	.115	-0.737	4.93	.024	2.18	2.89	.92	.0449	.0129	.257	.314	.101
.40	4.64	.109	-0.791	5.42	.019	2.00	-----	.91	.0371	.0101	.218	-----	.108
.40	5.28	.106	-0.864	6.16	.014	1.76	2.30	1.07	.0286	.0076	.191	.251	.117
.40	6.33	.102	-0.972	7.39	.009	1.59	1.83	1.18	.0200	.0051	.151	.200	.126
.40	7.39	.101	-1.031	8.62	.007	1.19	1.56	1.24	.0147	.0037	.129	.170	.135
.40	8.44	.103	-1.100	9.85	.005	.97	1.30	1.29	.0112	.0029	.106	.141	.141
.50	0	0	-0.431	0	-----	3.11	5.59	-1.10	-----	-----	.365	.555	-.012
.50	.63	.024	-0.448	.71	.190	3.10	-----	-.04	2.4938	.1197	.365	-----	-.005
.50	1.06	.072	-0.494	1.18	.205	3.00	5.35	.05	.8985	.1294	.352	.627	.005
.50	1.48	.089	-0.543	1.66	.129	2.89	-----	.07	.4583	.0816	.339	-----	.009
.50	2.11	.150	-0.574	2.37	.107	2.88	4.79	.23	.2246	.0674	.337	.562	.027
.50	2.55	.159	-0.543	2.84	.079	2.97	-----	.35	.1560	.0496	.348	-----	.042
.50	3.17	.161	-0.595	3.55	.051	2.84	3.86	.51	.0999	.0321	.333	.452	.060
.50	3.59	.155	-0.676	4.05	.036	2.64	-----	.63	.0777	.0241	.310	-----	.074
.50	4.22	.150	-0.806	4.74	.027	2.31	2.99	.76	.0562	.0168	.271	.351	.090

TABLE V
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 6 WITHOUT CHINE STRIPS

C_{DQ}	C_{VQ}	C_{RQ}	C_{HQ}	$C_{V\Delta}$	$C_{D\Delta}$	$\frac{x}{(\Delta)}^{1/3}$	$\frac{z}{(\Delta)}^{1/3}$	$\frac{h}{(\Delta)}^{1/3}$	C_{LQ}	C_{CQ}	$\frac{E}{L}$	$\frac{L}{L}$	$\frac{E}{L}$
$\tau = 0^\circ$													
0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	.63	0	0	0	0	0	0	0	0	0	0	0	0
0	1.06	.001	0	0	0	0	0	0	0	0	0	0	0
0	1.46	.004	0	0	0	0	0	0	0	0	0	0	0
0	2.11	.012	.011	0	0	0	0	0	0	0	0	0	0
0	2.53	.026	.031	0	0	0	0	0	0	0	0	0	0
0	3.17	.065	.087	0	0	0	0	0	0	0	0	0	0
0	3.59	.122	.179	0	0	0	0	0	0	0	0	0	0
0	4.22	.216	.476	0	0	0	0	0	0	0	0	0	0
0	4.64	.349	.738	0	0	0	0	0	0	0	0	0	0
.10	0	0	0	.011	0	4.79	6.82	0.45	0	0	0.522	.744	.049
.10	.63	.002	.016	.35	0.046	4.98	-----	.41	4.988	.0100	.542	-----	.048
.10	1.06	.009	.052	1.55	.075	5.69	7.73	.42	1.797	.0161	.520	.842	.045
.10	1.48	.016	.062	2.17	.068	5.90	-----	.43	.0917	.0147	.643	-----	.047
.10	2.11	.033	.072	3.10	.069	6.12	8.81	.40	.0449	.0248	.667	.960	.044
.10	2.53	.051	.105	3.72	.074	5.77	-----	.51	.0312	.0259	.737	-----	.034
.10	3.17	.113	.158	4.65	.104	7.53	9.19	.20	.0200	.0225	.832	1.000	.021
.10	3.59	.212	.174	5.26	.153	8.31	-----	.03	.055	.0329	.906	-----	.003
.20	0	0	0	.034	0	3.93	5.34	.25	0	0	.539	.870	.035
.20	.63	.002	.042	.53	.029	3.97	-----	.23	0	0	.545	-----	.032
.20	1.06	.015	.097	1.38	.084	4.47	7.30	.19	.3594	.0287	.613	1.000	.026
.20	1.48	.026	.128	1.93	.070	4.74	-----	.19	.1833	.0238	.650	-----	.026
.20	2.11	.042	.177	2.76	.055	4.63	7.30	.19	.0998	.0188	.536	1.000	.026
.20	2.53	.075	.127	3.31	.068	4.71	-----	.14	.0624	.0234	.515	-----	.019
.20	3.17	.189	.159	4.14	.107	4.51	-----	.03	.0399	.0365	.660	-----	-.001
.20	3.59	.318	.177	4.69	.144	4.63	-----	.31	.0511	.0494	.656	-----	-.043
.30	0	0	0	.050	0	3.43	5.89	.14	0	0	.539	.926	.022
.30	.63	.005	.054	.77	.056	3.43	-----	.12	1.4963	.0249	.539	-----	.019
.30	1.06	.028	.127	1.29	.112	3.81	6.38	.08	.539	.0502	.599	1.000	.012
.30	1.48	.045	.174	1.80	.092	4.03	-----	.09	.2750	.0412	.633	-----	.013
.30	2.11	.068	.154	2.58	.068	3.95	6.38	.08	.1348	.0305	.620	1.000	.012
.30	2.53	.113	.139	3.09	.079	3.86	-----	.02	.0936	.0352	.606	-----	.003
.30	3.17	.223	.117	3.57	.099	3.75	-----	.17	.0599	.0415	.589	-----	-.026
.40	0	0	0	.064	0	3.09	5.60	.07	0	0	.535	.968	.012
.40	.63	.005	.062	.74	.046	3.09	-----	.04	1.9950	.0249	.535	-----	.007
.40	1.06	.040	.154	1.23	.132	3.41	5.79	.02	.7158	.0177	.589	1.000	-.002
.40	1.48	.061	.195	1.72	.103	3.54	-----	.01	.3666	.0259	.613	-----	-.002
.40	2.11	.082	.149	2.46	.065	3.59	5.79	.02	.1797	.0368	.586	1.000	-.001
.40	2.53	.122	.123	2.96	.070	3.29	-----	.07	.1248	.0380	.569	-----	-.012
.40	3.17	.285	.057	3.70	.105	3.08	-----	.35	.0799	.0568	.532	-----	-.060
.50	0	0	0	.077	0	2.87	5.38	0	0	0	.535	1.000	0
.50	.63	.007	.067	.71	.055	2.81	5.38	-.04	2.1958	.0349	.529	1.000	-.007
.50	1.06	.052	.169	1.18	.148	3.11	5.38	-.11	.8985	.0533	.579	1.000	-.020
.50	1.48	.075	.201	1.66	.106	3.18	5.38	-.10	.4523	.0669	.593	1.000	-.019
.50	2.11	.099	.134	2.37	.071	3.02	5.38	-.11	.2246	.0444	.562	1.000	-.020
.50	2.53	.157	.097	2.84	.078	2.93	5.38	-.20	.1560	.0489	.545	1.000	-.038
.50	3.17	.356	.007	3.55	.113	2.70	5.38	-.14	.0999	.0710	.502	1.000	-.082
$\tau = 4^\circ$													
0	0	0	0	0	0	0	0	0	0	0	0.323	0.087	
0	.63	0	0	0	0	0	0	0	0	0	0.500	.421	.082
0	1.06	.001	0	0	0	0	0	0	0	0	0.500	-----	.079
0	1.46	.004	0	0	0	0	0	0	0	0	0.500	-----	.070
0	2.11	.012	.011	0	0	0	0	0	0	0	3.360	.645	.070
0	2.53	.026	.031	0	0	0	0	0	0	0	0.081	4.458	-----
0	3.17	.065	.087	0	0	0	0	0	0	0	.0336	4.875	.314
0	3.59	.122	.179	0	0	0	0	0	0	0	.0190	5.495	-----
0	4.22	.216	.476	0	0	0	0	0	0	0	.0243	7.973	-----
0	4.64	.349	.738	0	0	0	0	0	0	0	.0324	7.636	-----

TABLE V - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 6 WITHOUT CHINE STRIPS

$c_{\Delta Q}$	c_{VQ}	c_{BQ}	c_{M_Q}	$c_{r\Delta}$	$c_{D\Delta}$	$\frac{x}{(\Delta)}^{1/3}$	$\frac{l}{(\Delta)}^{1/3}$	$\frac{h}{(\Delta)}^{1/3}$	c_{I_Q}	c_{DQ}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 4^\circ$ - Concluded													
.10	0	.63	0	-0.029	0	-----	3.96	6.85	0.45	-----	0.431	0.746	0.049
.10	1.06	.009	.007	1.55	.075	4.75	7.70	.41	.1797	.0161	.515	.839	.044
.10	1.48	.014	.017	2.17	.059	4.94	-----	.43	.0917	.0128	.559	-----	.047
.10	2.11	.028	.034	3.10	.059	5.28	8.06	.40	.0449	.0126	.576	.878	.044
.10	2.53	.047	.057	3.72	.068	5.78	-----	.35	.0312	.0146	.630	-----	.038
.10	3.17	.101	.141	4.65	.095	7.42	8.42	.25	.0200	.0201	.808	.918	.027
.10	3.59	.146	.283	5.26	.105	10.14	-----	.13	.0135	.0227	1.104	-----	.014
.10	4.22	.262	.556	6.19	.137	14.77	-----	.11	.0112	.0294	1.609	-----	-.012
.20	0	0	-.046	0	-----	3.23	6.44	.25	-----	-----	.444	.884	.035
.20	.63	.002	-.040	.83	.029	3.29	-----	.22	.9975	.0100	.451	-----	.030
.20	1.06	.015	.021	1.38	.084	3.80	6.69	.19	.3594	.0287	.522	.918	.026
.20	1.48	.028	.047	1.93	.075	4.02	-----	.21	.1653	.0256	.592	-----	.029
.20	2.11	.045	.064	2.76	.059	4.17	6.69	.21	.0696	.0202	.572	.918	.029
.20	2.53	.066	.009	3.31	.060	4.36	-----	.17	.0624	.0206	.599	-----	.023
.20	3.17	.110	.209	4.14	.064	5.55	6.97	.08	.0399	.0219	.754	.957	.011
.20	3.59	.163	.335	4.69	.074	6.35	-----	.02	.0311	.0253	.872	-----	-.002
.20	4.22	.350	.637	5.52	.115	8.49	-----	.25	.0225	.0390	1.165	-----	-.035
.30	0	0	-.058	0	-----	2.90	5.88	.14	-----	-----	.455	.923	.022
.30	.63	.004	-.045	.77	.045	2.96	-----	.12	1.4963	.0200	.455	-----	.019
.30	1.06	.024	.037	1.29	.096	3.37	6.16	.08	.359	.0430	.529	.968	.013
.30	1.48	.038	.071	1.80	.078	3.51	-----	.10	.2750	.0348	.552	-----	.015
.30	2.11	.059	.098	2.58	.059	3.64	6.25	.09	.1348	.0265	.572	.982	.014
.30	2.53	.078	1.9	3.09	.054	3.75	-----	.07	.0936	.0243	.589	-----	.011
.30	3.17	.146	.241	3.87	.065	4.33	-----	.01	.0599	.0291	.680	-----	-.001
.30	3.59	.247	.382	4.38	.086	4.97	-----	.12	.0466	.0384	.781	-----	-.019
.40	0	0	-.556	0	-----	2.69	5.55	.06	-----	-----	.465	.960	.010
.40	.63	.005	-.040	.74	.046	2.75	-----	.04	1.9950	.0249	.475	-----	.007
.40	1.06	.051	.062	1.23	.102	3.09	5.79	0	.7188	.0556	.555	1.000	0
.40	1.48	.045	.098	1.72	.076	3.22	-----	.01	.3666	.0412	.556	-----	.001
.40	2.11	.071	.135	2.46	.059	3.33	5.79	0	.1797	.0319	.576	1.000	0
.40	2.53	.094	.151	2.36	.054	3.39	-----	.02	.1248	.0293	.586	-----	-.004
.40	3.17	.163	.283	3.70	.060	3.82	5.79	.12	.0799	.0325	.660	1.000	-.021
.40	3.59	.317	.449	4.19	.091	4.32	-----	.33	.1622	.0492	.747	-----	-.057
.50	0	0	-.046	0	-----	2.57	5.36	.01	-----	-----	.478	1.000	-.001
.50	.63	.005	-.020	.71	.040	2.62	-----	.03	2.4938	.0249	.488	-----	-.006
.50	1.06	.045	.077	1.18	.128	2.87	5.38	.07	.8935	.0807	.535	1.000	-.013
.50	1.48	.061	.117	1.66	.089	2.95	-----	.05	.4563	.0559	.552	-----	-.010
.50	2.11	.089	.146	2.37	.063	3.04	5.38	.07	.2246	.0399	.566	1.000	-.013
.50	2.53	.120	.169	2.84	.059	3.09	-----	.10	.1560	.0374	.576	-----	-.018
.50	3.17	.242	.332	3.55	.077	3.49	-----	.25	.0999	.0463	.650	-----	-.046
$\tau = 8^\circ$													
0	0	0	0	0	0	-----	-----	-----	0	0	-----	0.480	0.095
0	.63	0	0	0	0	-----	-----	-----	0	0	-----	-----	0.094
0	1.06	.001	0	0	0	-----	-----	-----	0	0.0018	0.500	.438	0.094
0	1.48	.004	0	0	0	-----	-----	-----	0	0.037	0.500	-----	0.091
0	2.11	.009	0	0	0	-----	-----	-----	0	0.060	0.500	.522	0.084
0	2.53	.021	.011	0	0	-----	-----	-----	0	.0066	1.401	-----	.076
0	3.17	.066	.087	0	0	-----	-----	-----	0	.0132	2.801	.727	.570
0	3.59	.116	.235	0	0	-----	-----	-----	0	.0285	3.865	-----	.046
0	4.22	.226	.667	0	0	-----	-----	-----	0	.0254	5.502	-----	.010
0	4.54	.324	.958	0	0	-----	-----	-----	0	.0301	5.515	-----	-.010

TABLE V - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 6 WITHOUT CEINE STRIPS

$C_{\Delta Q}$	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(h)}^{1/3}$	$\frac{l}{(h)}^{1/3}$	$\frac{h}{(h)}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 0^\circ$ - Concluded													
.10	0	0	-0.067	0	-----	3.12	6.31	0.52	-----	0.340	0.587	0.056	
.10	.63	.002	-0.064	.95	0.046	3.18	6.57	.45	0.4986	0.0100	.347	-----	.050
.10	1.36	.009	-0.034	1.55	.075	3.66	6.57	.44	.1797	.0161	.121	.716	.053
.10	1.48	.014	-0.029	2.17	.059	3.96	-----	.47	.0917	.0128	.431	-----	.052
.10	2.11	.031	-0.007	3.10	.024	4.42	6.57	.44	.0149	.0139	.481	.716	.048
.10	2.53	.049	.027	3.72	.071	5.15	-----	.37	.0312	.0153	.559	-----	.041
.10	3.17	.103	.179	4.65	.055	7.97	7.34	.24	.0200	.0205	.569	.800	.027
.10	3.59	.157	.354	5.26	.113	10.91	-----	.10	.0155	.0244	1.189	-----	.011
.10	4.22	.266	.774	6.19	.136	15.81	-----	.13	.0112	.0298	1.632	-----	.015
.20	0	0	-1.07	0	-----	2.72	5.64	.28	-----	-----	.374	.775	.038
.20	.63	.004	-0.092	.83	.059	2.85	-----	.27	.9975	.0200	.391	-----	.036
.20	1.06	.019	-0.046	1.38	.100	3.27	5.91	.26	.3594	.0341	.444	.811	.055
.20	1.18	.026	-0.034	1.93	.070	3.39	-----	.26	.1833	.0238	.465	-----	.058
.20	2.11	.042	-0.03	2.76	.055	3.61	5.83	.27	.0898	.0188	.495	.800	.036
.20	2.53	.063	.047	3.31	.057	4.00	-----	.20	.0624	.0196	.549	-----	.028
.20	3.17	.129	.250	4.14	.075	5.28	6.42	.09	.0399	.0257	.724	.881	.012
.20	3.59	.176	.454	4.69	.050	6.08	-----	.01	.0311	.0273	.855	-----	.001
.20	4.22	.324	.860	5.52	.106	6.21	-----	.19	.0225	.0364	.852	-----	.026
.50	0	0	-1.34	0	-----	2.51	5.31	.15	-----	-----	.394	.833	.023
.50	.63	.005	-1.07	.77	.056	2.64	-----	.12	1.4963	.0249	.444	-----	.018
.50	1.06	.028	-0.47	1.29	.112	2.93	5.50	.11	.5391	.0502	.461	.864	.017
.50	1.48	.036	-0.025	1.80	.078	3.04	-----	.13	.2750	.0348	.478	-----	.020
.50	2.11	.059	.011	2.58	.059	3.23	5.48	.12	.1348	.0265	.508	.862	.018
.50	2.53	.080	.072	3.09	.056	3.51	-----	.07	.0936	.0249	.552	-----	.011
.50	3.17	.139	.354	3.87	.062	4.72	5.95	.05	.0599	.0277	.741	.934	.008
.50	3.59	.233	.566	4.35	.081	5.16	-----	.14	.0466	.0362	.811	-----	.021
.40	0	0	-1.44	0	-----	2.39	5.11	.05	-----	-----	.414	.884	.009
.40	.63	.005	-1.07	.74	.045	2.51	-----	.02	.9950	.0249	.434	-----	.004
.40	1.06	.038	-0.029	1.23	.126	2.78	5.34	.01	.7188	.0682	.481	.923	.001
.40	1.48	.052	-0.03	1.72	.058	2.88	-----	.03	.3666	.0476	.498	-----	.006
.40	2.11	.075	.042	2.16	.062	3.02	5.26	.02	.1797	.0337	.522	.909	.003
.40	2.53	.103	.154	2.56	.059	3.59	-----	.04	.1248	.0521	.586	-----	.007
.40	3.17	.188	.429	3.70	.059	4.26	5.63	.16	.0759	.0375	.737	.974	.027
.40	3.59	.282	.738	4.19	.081	5.20	-----	.25	.0622	.0438	.899	-----	.044
.50	0	c	-1.31	0	-----	2.35	4.93	.03	-----	-----	.438	.918	-.005
.50	.63	.005	-1.03	.71	.040	2.40	-----	.05	2.4938	.0249	.448	-----	.010
.50	1.06	.049	-0.03	1.18	.140	2.64	5.14	.07	.8985	.0879	.492	.957	-.013
.50	1.48	.063	.007	1.66	.092	2.70	-----	.04	.4583	.0577	.502	-----	.008
.50	2.11	.087	.072	2.37	.062	2.86	5.05	.06	.2246	.0590	.532	.940	-.011
.50	2.53	.108	.201	2.94	.054	3.18	-----	.12	.1560	.0337	.593	-----	.023
.50	3.17	.221	.556	3.55	.070	4.01	5.38	.25	.0999	.0441	.747	1.000	-.047
.50	3.59	.335	.559	4.05	.084	4.59	-----	.36	.0777	.0526	.855	-----	-.067
$\tau = 12^\circ$													
0	0	0	0	0	-----	-----	-----	-----	0	0	-----	0.379	0.111
0	.63	0	0	0	-----	-----	-----	-----	0	0	-----	-----	0.113
0	1.06	0	0	0	-----	-----	-----	-----	0	0	-----	0.337	0.113
0	1.48	.001	0	0	-----	-----	-----	-----	0	.0009	0.500	-----	.111
0	2.11	.006	0	0	-----	-----	-----	-----	0	.0027	.500	.404	.109
0	2.53	.016	.008	0	-----	-----	-----	-----	0	.0050	1.077	-----	.094
0	3.17	.076	.127	0	-----	-----	-----	-----	0	.0156	2.384	.643	.066
0	3.59	.443	.328	0	-----	-----	-----	-----	0	.0222	3.118	-----	.045
0	4.22	.259	.744	0	-----	-----	-----	-----	c	.0291	3.751	-----	.012

TABLE V - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 6 WITHOUT CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_A}	c_{D_A}	$\frac{x}{(A)} \frac{1}{1/3}$	$\frac{l}{(A)} \frac{1}{1/3}$	$\frac{h}{(A)} \frac{1}{1/3}$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 12^\circ$ - Concluded													
.10	0	0	-0.091	0	-----	2.57	5.49	0.62	-----	0.279	0.598	0.067	
.10	.63	.003	-.078	.53	0.070	2.87	-----	.59	0.4988	.0150	.313	-----	.065
.10	1.06	.012	-.062	1.55	.100	3.25	5.77	.59	.1797	.0215	.354	.629	.065
.10	1.48	.016	-.056	2.17	.068	3.37	-----	.60	.0917	.0147	.367	-----	.073
.10	2.11	.033	-.029	3.10	.069	3.99	6.90	.55	.0449	.0188	.434	.752	.060
.10	2.53	.056	.031	3.72	.081	5.19	6.82	.46	.0312	.0175	.566	.744	.050
.10	3.17	.125	.248	4.65	.116	9.67	-----	.27	.0200	.0249	1.054	-----	.029
.10	3.59	.200	.476	5.26	.104	11.56	-----	.11	.0155	.0311	1.303	-----	.012
.10	4.22	.301	.930	6.19	.157	17.18	-----	-.09	.0112	.0358	1.872	-----	-.010
.20	0	0	-.147	0	-----	2.33	4.99	.31	-----	.320	.685	.043	
.20	.63	.005	-.127	.83	.073	2.53	-----	.28	.9975	.0269	.347	-----	.038
.20	1.06	.021	-.097	1.38	.110	2.82	5.19	.29	.3594	.0377	.587	.743	.040
.20	1.48	.028	-.085	1.93	.075	2.92	-----	.31	.1833	.0256	.401	-----	.043
.20	2.11	.049	-.029	2.76	.064	3.59	5.25	.27	.0898	.0220	.465	.721	.037
.20	2.53	.075	.067	3.31	.068	4.17	5.87	.20	.0624	.0234	.572	.805	.027
.20	3.17	.153	.335	4.14	.089	5.16	-----	.05	.0399	.0305	.845	-----	.006
.20	3.59	.214	.556	4.69	.097	7.61	-----	-.04	.0311	.0332	1.044	-----	-.005
.20	4.22	.306	.930	5.52	.100	10.45	-----	-.19	.0225	.0343	1.454	-----	-.027
.30	0	0	-.184	0	-----	2.23	4.79	.17	-----	.350	.752	.027	
.30	.63	.005	-.159	.77	.056	2.36	-----	.13	1.4963	.0249	.370	-----	.021
.30	1.06	.035	-.107	1.29	.140	2.64	5.02	.15	.5391	.0268	.414	.759	.024
.30	1.48	.042	-.100	1.80	.086	2.68	-----	.17	.2750	.0385	.421	-----	.027
.30	2.11	.066	-.025	2.58	.066	3.04	5.07	.15	.1348	.0296	.478	.797	.024
.30	2.53	.101	.123	3.09	.070	3.75	-----	.06	.0956	.0315	.589	-----	.010
.30	3.17	.183	.413	3.87	.081	5.04	5.48	-.04	.0599	.0365	.791	.662	-.006
.30	3.59	.247	.651	4.38	.086	6.00	-----	-.13	.0466	.0584	.943	-----	-.020
.40	0	0	-.196	0	-----	2.20	4.69	.05	-----	.380	.611	.009	
.40	.63	.008	-.164	.74	.074	2.32	-----	.02	1.9950	.0399	.401	-----	.004
.40	1.06	.047	-.107	1.23	.155	2.51	4.90	.03	.7188	.0843	.434	.848	.006
.40	1.48	.056	-.087	1.72	.095	2.59	-----	.05	.3666	.0553	.448	-----	.006
.40	2.11	.080	-.003	2.16	.066	2.88	4.90	-.03	.1797	.0359	.498	.848	.006
.40	2.53	.122	.159	2.96	.070	3.41	-----	-.04	.1248	.0380	.589	-----	-.007
.40	3.17	.212	.480	3.70	.078	4.38	5.24	-.14	.0799	.0423	.758	.906	-.024
.40	3.59	.292	.878	4.19	.083	5.53	-----	-.23	.0622	.0453	.956	-----	-.040
.50	0	0	-.186	0	-----	2.21	4.60	-.04	-----	.411	.856	-.007	
.50	.63	.009	-.151	.72	.071	2.30	-----	-.07	2.4938	.0449	.428	-----	-.013
.50	1.06	.063	-.052	1.18	.179	2.44	4.75	-.05	.8985	.1130	.452	.884	-.010
.50	1.48	.075	-.057	1.66	.109	2.51	-----	-.04	.4583	.0687	.468	-----	-.007
.50	2.11	.103	.047	2.37	.073	2.79	4.78	-.07	.2246	.0462	.519	.890	-.013
.50	2.53	.143	.229	2.84	.071	3.24	-----	-.13	.1560	.0446	.603	-----	-.024
.50	3.17	.247	.581	3.55	.078	4.03	-----	-.23	.0999	.0493	.751	-----	-.042
.50	3.59	.343	.889	4.03	.085	4.03	-----	-.29	.0777	.0533	.872	-----	-.054
$\tau = 16^\circ$													
0	0	0	0	0	-----	-----	-----	-----	0	0	0	0.275	0.139
0	.63	0	0	0	-----	-----	-----	-----	0	0	0	-----	-----
0	1.06	0	0	0	-----	-----	-----	-----	0	0	0	0.275	0.141
0	1.48	.002	0	0	-----	-----	-----	-----	0	0.0018	0.500	-----	0.140
0	2.11	.006	0	0	-----	-----	-----	-----	0	0.0027	.500	.537	.133
0	2.53	.026	.018	0	-----	-----	-----	-----	0	0.0081	1.104	.581	.113
0	3.17	.103	.188	0	-----	-----	-----	-----	0	0.0206	2.047	-----	.075
0	3.59	.176	.409	0	-----	-----	-----	-----	0	0.0274	2.492	-----	.053
0	4.22	.296	.823	0	-----	-----	-----	-----	0	0.0332	2.889	-----	.026
.10	0	0	-.097	0	-----	2.44	4.84	.72	-----	.266	.528	.078	
.10	.63	.006	-.088	.93	.139	2.35	-----	.66	.4988	.0299	.256	-----	.072
.10	1.06	.014	-.080	1.55	.117	2.84	5.02	.71	.1797	.0251	.310	.547	.077
.10	1.48	.019	-.070	2.17	.081	3.09	-----	.72	.0917	.0174	.357	-----	.079
.10	2.11	.045	-.013	3.10	.094	4.30	5.56	.62	.0449	.0202	.468	.584	.067
.10	2.53	.075	.058	3.72	.109	5.62	6.31	.50	.0312	.0234	.613	.687	.055
.10	3.17	.150	.286	4.65	.139	8.31	-----	.28	.0200	.0299	.906	-----	.037
.10	3.59	.228	.530	5.26	.154	11.77	-----	.15	.0155	.0354	1.263	-----	.016
.10	4.22	.322	.989	6.19	.168	16.16	-----	-.05	.0112	.0361	1.761	-----	-.006

TABLE V - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 6 WITHOUT CHINE STRIPS

$c_{\Delta Q}$	c_{VQ}	c_{RQ}	c_{M_Q}	$c_{T\Delta}$	$c_{D\Delta}$	$\frac{x}{(L)} \frac{1}{1/3}$	$\frac{2}{(L)} \frac{1}{1/3}$	$\frac{h}{(L)} \frac{1}{1/3}$	c_{LQ}	c_{DQ}	$\frac{x}{L}$	$\frac{2}{L}$	$\frac{h}{L}$
$\tau = 15^\circ$ - Concluded													
.20	0	0	-0.159	0	-----	2.21	4.52	0.37	-----	0.303	0.620	0.051	
.20	.63	.036	-1.145	.53	0.087	2.35	-----	.34	0.9975	0.299	.323	-----	.046
.20	1.06	.028	-1.21	1.36	.147	2.60	4.70	.37	0.592	.357	.615	0.051	
.20	1.48	.032	-1.07	1.93	.102	2.72	-----	.37	0.183	0.343	.374	-----	.051
.20	2.11	.065	-0.17	2.76	.087	3.45	4.93	.29	0.088	0.298	.478	.676	.039
.20	2.53	.103	.097	3.51	.094	4.39	-----	.22	0.024	0.321	.665	-----	.030
.20	3.17	.188	-3.73	1.14	.110	5.72	5.58	.07	0.099	0.375	.785	.766	.010
.20	3.59	.268	.655	1.69	.122	6.30	-----	.03	0.0311	0.416	.865	-----	-.004
.30	0	0	-1.96	0	-----	2.23	4.39	.19	-----	0.350	.690	0.029	
.30	.63	.011	-1.74	.77	.123	2.32	-----	.15	1.4963	.0549	.364	-----	.024
.30	1.06	.044	-1.44	1.29	.176	2.44	4.61	.18	0.539	.0759	.388	.724	0.028
.30	1.48	.053	-1.23	1.80	.108	2.57	-----	.19	0.2790	0.485	.404	-----	.030
.30	2.11	.062	-0.04	2.58	.082	3.15	4.66	.12	0.1368	0.368	.495	.732	.018
.30	2.53	.125	.142	3.09	.087	3.34	-----	.05	0.0936	0.390	.603	-----	.010
.30	3.17	.226	.164	3.27	.102	5.11	5.11	-.05	0.0599	0.452	.808	.802	-.008
.30	3.59	.301	.758	4.36	.104	6.24	-----	-.13	0.0466	0.467	.980	-----	-.020
.40	0	0	-2.11	0	-----	2.14	4.35	.05	-----	0.370	.752	0.008	
.40	.63	.011	-1.92	.74	.101	2.20	-----	.04	1.9950	.0549	.380	-----	.007
.40	1.06	.039	-1.54	1.23	.195	2.35	1.19	.06	.7138	.1058	.407	.777	.011
.40	1.48	.068	-1.17	1.72	.115	2.49	-----	.09	0.3666	.0623	.431	-----	.015
.40	2.11	.096	.007	2.46	.079	2.86	4.60	.03	0.1797	0.431	.495	.795	.006
.40	2.53	.153	.214	2.96	.086	3.56	-----	-.04	0.1248	.0477	.626	-----	-.007
.40	3.17	.259	.561	3.70	.095	4.38	4.98	-.15	0.0799	.0516	.758	.862	-.026
.40	3.59	.338	.879	4.19	.097	5.37	-----	-.23	0.0622	.0525	.929	-----	-.040
.50	0	0	-2.07	0	-----	2.13	4.41	-.05	-----	0.397	.820	0.010	
.50	.63	.020	-1.74	.71	.158	2.22	-----	-.07	2.4538	.0998	.414	-----	-.013
.50	1.06	.075	-1.43	1.18	.214	2.31	4.43	-.03	.8685	.1318	.431	.825	0.005
.50	1.48	.085	-1.07	1.66	.124	2.41	-----	-.01	0.4585	.0778	.448	-----	-.002
.50	2.11	.125	.082	2.37	.089	2.87	4.55	-.08	0.2246	.0561	.535	.848	0.015
.50	2.53	.174	.276	2.94	.086	3.33	-----	-.13	0.1560	.0542	.620	-----	-.023
.50	3.17	.275	.572	3.55	.087	4.19	-----	-.20	0.0999	.0548	.761	-----	-.038
.50	3.59	.371	1.000	4.03	.092	4.84	-----	-.27	0.0777	.0575	.902	-----	-.050
$\tau = 20^\circ$													
C	C	C	C	C	-----	-----	-----	-----	0	0	-----	0.255	0.172
0	.63	C	-.019	-----	-----	-----	-----	-----	0	0	-----	-----	.178
0	1.06	.001	-.019	-----	-----	-----	-----	-----	0	.0018	8.929	.224	.179
0	1.48	.002	-.019	-----	-----	-----	-----	-----	0	.0018	4.215	-----	.175
0	2.11	.009	-.004	-----	-----	-----	-----	-----	0	.0040	.209	.300	.161
0	2.53	.038	.017	-----	-----	-----	-----	-----	0	.0119	.815	-----	.134
0	3.17	.115	.159	-----	-----	-----	-----	-----	0	.0230	1.448	.533	.097
0	3.59	.195	.373	-----	-----	-----	-----	-----	0	.0303	1.818	-----	.078
0	4.22	.310	.779	-----	-----	-----	-----	-----	0	.0348	2.229	-----	.047
.10	0	0	-1.12	0	-----	2.01	4.43	0.85	-----	0.219	.463	0.092	
.10	.63	.006	-1.07	.93	0.159	2.16	-----	.84	4.988	.0299	.236	-----	.091
.10	1.06	.016	-1.03	1.55	.133	2.35	4.51	.26	1.797	.0267	.256	.491	.094
.10	1.48	.021	-.087	2.17	.089	2.72	-----	.86	.0927	.0192	.296	-----	.094
.10	2.11	.056	-.013	3.10	.117	4.33	4.95	.69	.0449	.0251	.471	.539	.076
.10	2.53	.094	.057	3.72	.136	5.56	-----	.58	.0312	.0293	.606	-----	.063
.10	3.17	.176	.275	4.65	.163	8.44	5.90	.39	.0200	.0351	.919	.643	.043
.10	3.59	.251	.505	5.26	.181	10.63	-----	.24	.0155	.0390	1.158	-----	.026
.10	4.22	.378	.950	6.19	.197	13.72	-----	.03	.0112	.0424	1.495	-----	.003

TABLE V - Concluded
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 6 WITHOUT CHINE STRIPS

C_{A_Q}	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_A}	C_{D_A}	$\frac{x}{(\Delta)}^{1/3}$	$\frac{l}{(\Delta)}^{1/3}$	$\frac{b}{(\Delta)}^{1/3}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{b}{L}$
$\tau = 20^\circ$ - Concluded													
.20	0	0	-0.174	0	-----	2.03	1.19	0.43	-----	0.279	0.575	0.060	
.20	.63	.009	-.164	.83	0.131	2.16	----	.43	0.9975	0.4449	.296	----	.059
.20	1.06	.035	-.154	1.38	1.73	2.30	4.33	.47	.5594	.0592	.316	.595	.065
.20	1.48	.040	-.127	1.93	.107	2.55	----	.47	.1833	.0366	.330	----	.065
.20	2.11	.085	-.004	2.76	.111	3.61	4.56	.35	.0898	.0381	.495	.626	.047
.20	2.53	.127	.097	5.31	.116	4.54	----	.25	.0624	.0596	.296	----	.059
.20	3.17	.223	.372	4.14	.130	5.03	5.23	.12	.0399	.0415	.828	.718	.016
.20	3.59	.296	.637	4.69	.135	7.41	----	.01	.0311	.0460	1.027	----	.001
.30	0	0	-.212	0	-----	2.06	4.09	.21	-----	.323	.643	.033	
.30	.63	.014	-.201	.77	.156	2.12	----	.18	1.4933	.0698	.333	----	.029
.30	1.06	.052	-.18	1.29	.208	2.25	4.59	.23	.5591	.0933	.354	.721	.036
.30	1.48	.061	-.147	1.80	.125	2.44	----	.25	.2750	.0559	.384	----	.036
.30	2.11	.103	0	2.58	.103	3.17	4.48	.13	.1348	.0462	.500	.704	.020
.30	2.53	.157	.145	3.09	.109	3.81	----	.05	.0936	.0489	.599	----	.008
.30	3.17	.270	.494	3.87	.120	5.14	4.84	.05	.0599	.0538	.808	.760	-.006
.30	3.59	.395	.779	4.58	.125	6.07	----	.12	.0466	.0521	.953	----	-.019
.40	0	0	-.232	0	-----	2.05	4.06	.05	-----	.354	.702	.009	
.40	.63	.016	-.217	.74	.147	2.11	----	.02	1.9950	.0798	.365	----	.004
.40	1.06	.071	-.201	1.23	.235	2.20	4.17	.06	.7188	.1274	.580	.721	.010
.40	1.48	.082	-.139	1.72	.138	2.42	----	.06	.3666	.0751	.418	----	.010
.40	2.11	.132	.040	2.46	.109	3.02	4.35	.03	.1797	.0592	.522	.752	-.004
.40	2.53	.190	.219	2.96	.109	3.56	----	.07	.1248	.0592	.616	----	-.015
.40	3.17	.306	.556	3.70	.112	4.46	4.61	.16	.0799	.0610	.771	.797	-.027
.40	3.59	.393	.879	4.19	.112	5.22	----	.22	.0622	.0610	.902	----	-.038
.50	0	0	-.226	0	-----	2.06	4.08	.07	-----	.384	.760	-.015	
.50	.63	.024	-.211	.71	.190	2.12	----	.09	2.4938	.1197	.394	----	.016
.50	1.06	.094	-.191	1.18	.268	2.19	4.16	.03	.8985	.1686	.407	.775	-.005
.50	1.48	.103	-.118	1.66	.150	2.58	----	.03	.4583	.0943	.444	----	-.005
.50	2.11	.157	.092	2.37	.112	2.89	4.32	.10	.2246	.0705	.539	.805	-.019
.50	2.53	.219	.275	2.84	.108	3.31	----	.14	.1560	.0683	.616	----	-.026
.50	3.17	.334	.667	3.55	.106	4.12	----	.22	.0999	.0666	.768	----	-.042

TABLE VI
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 9 WITHOUT CHINE STRIPS

C_{Δ_2}	C_{V_Q}	C_{T_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(\Delta)}^{1/3}$	$\frac{z}{(\Delta)}^{1/3}$	$\frac{h}{(\Delta)}^{1/3}$	C_{T_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$\tau = 0^\circ$													
0	0	0	0.001	-----	-----	-----	-----	-----	0	-----	0.458	0.058	
0	.63	0	0.001	-----	-----	-----	-----	-----	0	0.0036	-----	.057	
0	1.06	.002	.007	-----	-----	-----	-----	-----	0	0.0037	-----	.491	.056
0	1.48	.004	.007	-----	-----	-----	-----	-----	0	0.0040	-----	.057	
0	2.11	.009	.013	-----	-----	-----	-----	-----	0	0.0044	-----	.598	.056
0	2.53	.014	.012	-----	-----	-----	-----	-----	0	0.0070	-----	.748	.054
0	3.17	.035	.024	-----	-----	-----	-----	-----	0	0.0084	-----	.053	
0	3.59	.054	.024	-----	-----	-----	-----	-----	0	0.0112	-----	.046	
0	4.22	.105	.03	-----	-----	-----	-----	-----	0	0.0195	-----	.044	
0	4.64	.210	.276	-----	-----	-----	-----	-----	0	0.027	-----		
.10	0	0	.024	0	-----	6.55	8.96	0.40	-----	0.544	.744	.033	
.10	.63	.001	.029	.93	0.023	6.51	-----	.38	.4983	.0050	.551	.051	
.10	1.06	.007	.066	1.55	.059	7.45	9.86	.56	.1797	.0126	.618	.030	
.10	1.48	.011	.070	2.17	.047	7.54	-----	.56	.0917	.0101	.626	.030	
.10	2.11	.023	.090	3.10	.048	7.97	9.48	.37	.0449	.0103	.662	.786	.031
.10	2.53	.032	.062	3.72	.046	8.03	-----	.55	.0312	.0100	.667	-----	.029
.10	3.17	.077	.129	4.65	.072	8.81	11.80	.31	.0200	.0154	.731	.979	.026
.10	3.59	.111	.155	5.26	.080	9.36	-----	.27	.0155	.0172	.777	-----	.022
.10	4.22	.210	.276	5.19	.110	11.93	-----	.16	.0112	.0236	.990	-----	.013
.10	4.64	.259	.249	6.81	.111	11.43	-----	.02	.0093	.0240	.949	-----	.001
.20	0	0	.050	0	-----	5.23	8.12	.23	0	-----	.544	.848	.024
.20	.63	.002	.050	.83	.029	5.20	-----	.21	.9975	.0100	.544	-----	.022
.20	1.06	.009	.102	1.38	.047	5.66	9.06	.19	.3594	.0161	.592	.947	.020
.20	1.48	.016	.134	1.93	.048	5.94	-----	.19	.1833	.0165	.621	-----	.020
.20	2.11	.037	.170	2.76	.049	6.23	9.47	.19	.0898	.0166	.651	.989	.020
.20	2.53	.053	.176	3.31	.048	6.28	-----	.18	.0624	.0165	.656	-----	.019
.20	3.17	.098	.202	4.41	.057	6.50	9.57	.14	.0399	.0195	.679	1.000	.015
.20	3.59	.180	.259	4.69	.062	6.97	-----	.08	.0511	.0279	.728	-----	.008
.20	4.22	-----	-----	5.52	-----	-----	-----	.16	.3225	-----	-----	-----	.019
.30	0	0	.071	0	-----	4.55	7.73	.12	-----	-----	.544	.925	.014
.30	.63	.002	.071	.77	.022	4.55	-----	.12	1.4963	.0100	.544	-----	.014
.30	1.06	.015	.153	1.29	.060	4.95	8.36	.08	.5391	.0269	.592	1.000	.010
.30	1.48	.023	.188	1.80	.047	5.12	-----	.09	.2750	.0211	.613	-----	.010
.30	2.11	.051	.249	2.58	.051	5.42	8.36	.08	.1348	.0229	.649	1.000	.009
.30	2.53	.075	.221	3.09	.052	5.27	-----	.07	.0936	.0234	.631	-----	.008
.30	3.17	.138	.229	3.87	.061	5.32	-----	.05	.0599	.0275	.636	-----	.004
.30	3.59	.237	.428	4.38	.082	5.62	-----	.09	.0466	.0368	.672	-----	.011
.40	0	0	.086	0	-----	4.09	7.30	.05	-----	-----	.538	.961	.007
.40	.63	.004	.080	.74	.037	4.07	-----	.05	1.9950	.0200	.536	-----	.006
.40	1.06	.002	.197	1.23	.007	4.46	7.59	.01	.7188	.0036	.587	1.000	.002
.40	1.48	.033	.226	1.72	.056	4.53	-----	.01	.3666	.0302	.597	-----	.001
.40	2.11	.064	.249	2.46	.053	4.66	7.59	0	.1797	.0288	.613	1.000	0
.40	2.53	.100	.234	2.96	.057	4.59	-----	.02	.1246	.0312	.605	-----	.003
.40	3.17	.169	.208	3.70	.069	4.50	7.59	.10	.0799	.0377	.592	1.000	.014
.50	0	0	.102	0	-----	3.78	7.05	0	-----	-----	.536	1.000	0
.50	.63	.005	.097	.71	.395	3.78	-----	.01	2.4958	.0249	.536	-----	.002
.50	1.06	.025	.132	1.18	.071	4.01	7.05	.05	.3985	.0449	.569	1.000	.008
.50	1.48	.042	.238	1.66	.061	4.12	-----	.05	.4583	.0385	.585	-----	.006
.50	2.11	.077	.255	2.37	.054	4.11	-----	.06	.2246	.0346	-----	-----	.006
.50	2.53	.121	.213	2.84	.060	4.00	-----	.07	.1560	.0377	-----	-----	.010
.50	3.17	.187	.222	3.55	.059	4.02	7.05	.05	.0999	.0373	-----	1.000	.011

TABLE VI - Continued
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 9 WITHOUT CHINE STRIPS

$c_{\Delta Q}$	c_{VQ}	c_{RQ}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(\frac{A}{w})^{1/3}}$	$\frac{z}{(\frac{A}{w})^{1/3}}$	$\frac{h}{(\frac{A}{w})^{1/3}}$	c_{LQ}	c_{DQ}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$\tau = 4^\circ$													
0	0	0	0	---	---	---	---	---	0	0	---	0.370	0.063
0	.63	0	0	---	---	---	---	---	0	.0018	0.500	.449	.063
0	1.06	.001	0	---	---	---	---	---	0	.0018	.500	---	.062
0	1.48	.002	0	---	---	---	---	---	0	.0018	0.500	---	.062
0	2.11	.003	.007	---	---	---	---	---	0	.0036	3.320	.554	.062
0	2.55	.013	.012	---	---	---	---	---	0	.0041	2.808	---	.057
0	3.17	.029	.024	---	---	---	---	---	0	.0058	2.808	.664	.055
0	3.59	.048	.040	---	---	---	---	---	0	.0075	2.697	---	.050
0	4.22	.098	.097	---	---	---	---	---	0	.0110	2.979	.754	.044
0	4.64	.159	.216	---	---	---	---	---	0	.0148	3.951	---	.037
0	5.28	.262	.476	---	---	---	---	---	0	.0188	5.169	---	.025
.10	0	0	-.064	0	---	4.67	9.07	0.40	---	---	.387	.752	.033
.10	.63	.002	.060	.93	0.046	4.73	---	.40	0.4988	.0100	.392	---	.033
.10	1.06	.006	-.031	1.55	.050	5.38	9.09	.37	.1797	.0108	.446	.754	.031
.10	1.48	.011	-.017	2.17	.047	5.65	---	.37	.0917	.0101	.469	---	.031
.10	2.11	.021	-.003	3.10	.043	5.96	8.91	.37	.0449	.0094	.495	.759	.031
.10	2.53	.033	.007	3.72	.048	6.18	---	.36	.0312	.0103	.513	---	.030
.10	3.17	.055	.028	4.65	.051	6.61	9.40	.31	.0200	.0110	.549	.780	.026
.10	3.59	.086	.067	5.26	.062	7.39	---	.30	.0255	.0134	.613	---	.025
.10	4.22	.154	.196	6.19	.080	9.86	10.20	.21	.0112	.0173	.818	.846	.018
.10	4.64	.212	.328	6.81	.091	12.21	---	.16	.0093	.0197	1.013	---	.013
.10	5.28	.321	.618	7.74	.107	16.93	---	.03	.0072	.0230	1.405	---	.002
.20	0	0	-.111	0	---	3.83	7.91	.22	---	---	.400	.827	.023
.20	.63	.002	-.100	.83	.029	3.92	---	.22	.9975	.0100	.410	---	.023
.20	1.06	.009	-.052	1.38	.047	4.34	8.08	.20	.3595	.0161	.454	.844	.021
.20	1.48	.016	-.020	1.93	.043	4.62	---	.20	.1833	.0147	.486	---	.021
.20	2.11	.030	.007	2.76	.040	4.86	7.89	.20	.0858	.0135	.508	.825	.021
.20	2.53	.047	.003	3.31	.043	4.81	---	.20	.0624	.0147	.503	---	.021
.20	3.17	.079	.066	4.14	.046	5.35	8.14	.16	.0399	.0158	.559	.850	.017
.20	3.59	.121	.122	4.69	.053	5.79	---	.14	.0311	.0185	.605	---	.015
.20	4.22	.198	.269	5.52	.065	6.95	8.75	.09	.0225	.0222	.726	.914	.010
.20	4.64	.257	.429	6.07	.070	8.14	---	.04	.0186	.0238	.851	---	.004
.20	5.26	.345	---	6.90	.072	---	---	.10	.0144	.0246	---	---	-.011
.30	0	0	-.133	0	---	3.62	7.36	.11	---	---	.433	.880	.013
.30	.63	.002	-.111	.77	.022	3.62	---	.10	1.4963	.0100	.433	---	.011
.30	1.06	.012	-.046	1.29	.048	3.95	7.50	.08	.5391	.0215	.472	.897	.009
.30	1.48	.023	-.008	1.80	.047	4.14	---	.09	.2750	.0211	.495	---	.011
.30	2.11	.043	-.034	2.52	.043	4.36	7.43	.09	.1348	.0193	.521	.889	.011
.30	2.53	.062	.054	3.09	.043	4.44	---	.08	.0926	.0193	.551	---	.009
.30	3.17	.102	.102	3.87	.045	4.67	7.50	.06	.0599	.0203	.559	.897	.007
.30	3.59	.147	.159	4.38	.051	4.95	---	.05	.0466	.0228	.592	---	.006
.30	4.22	.231	.344	5.16	.056	5.81	8.11	.01	.0337	.0259	.695	.970	-.001
.30	4.64	.326	.629	5.67	.067	7.10	---	.10	.0278	.0302	.849	---	-.012
.30	5.28	.473	-.000	6.45	.075	8.69	---	.18	.0216	.0340	1.040	---	-.021
.40	0	0	-.133	0	---	3.33	6.98	.04	---	---	.432	.919	.005
.40	.63	.004	-.115	.74	.037	3.41	---	.05	1.9950	.0200	.449	---	.004
.40	1.06	.019	-.031	1.23	.063	3.70	7.12	.01	.7188	.0341	.487	.958	.001
.40	1.48	.032	.012	1.72	.054	3.83	---	.03	.3666	.0293	.505	---	.003
.40	2.11	.056	.060	2.46	.046	3.99	7.04	.03	.1797	.0252	.526	.927	.003
.40	2.55	.079	.087	2.96	.045	4.09	---	.01	.1248	.0246	.558	---	.001
.40	3.17	.132	.149	3.70	.049	4.28	7.14	.01	.0799	.0264	.564	.940	-.001
.40	3.59	.183	.222	4.19	.052	4.53	---	.02	.0622	.0284	.597	---	-.002
.40	4.22	.300	.528	4.92	.062	5.49	---	.11	.0449	.0337	.723	---	-.015
.40	4.64	.410	.730	5.42	.070	6.11	---	.15	.0371	.0381	.805	---	-.020

TABLE VI - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 9 WITHOUT CHINE STRIPS

$C_{\Delta Q}$	C_{VQ}	C_{RQ}	C_{MQ}	$C_{V\Delta}$	$C_{D\Delta}$	$\frac{x}{(L)}$ $(\frac{A}{W})^{1/3}$	$\frac{l}{(L)}$ $(\frac{A}{W})^{1/3}$	$\frac{h}{(L)}$ $(\frac{A}{W})^{1/3}$	C_{LQ}	C_{DQ}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 4^C$ - Concluded													
.50	0	c	-0.115	0	-----	3.24	6.75	-0.02	-----	0.459	0.957	-0.003	
.50	.63	.004	-.100	.71	0.032	3.27	-----	-.03	2.4938	0.0200	.454	-----	-.004
.50	1.06	.022	-.013	1.18	.063	3.49	6.85	-.05	.895	.0355	.455	.972	-.007
.50	1.48	.040	-.034	1.56	.058	3.62	-----	-.04	.4565	.0357	.513	-----	-.005
.50	2.11	.065	.081	2.37	.046	3.72	6.75	-.04	.2246	.0292	.588	.957	-.005
.50	2.53	.052	.113	2.84	.046	3.81	-----	-.04	.1560	.0287	.541	-----	-.005
.50	3.17	.142	.197	3.55	.015	4.01	6.93	-.07	.0999	.0284	.569	.979	-.009
.50	3.59	.228	.344	4.03	.055	4.38	-----	-.12	.0777	.0518	.621	-----	-.016
.50	4.22	.340	.561	4.74	.061	4.88	-----	-.15	.0562	.0382	.692	-----	-.020
$\tau = 8^C$													
0	0	0	0	-----	-----	-----	-----	-----	0	0.0050	6.559	0.459	0.075
c	.63	.001	-.007	-----	-----	-----	-----	-----	0	.0018	.5184	.419	.075
c	1.06	.001	-.003	-----	-----	-----	-----	-----	0	.0018	1.987	-----	.075
c	1.48	.002	.003	-----	-----	-----	-----	-----	c	.0027	-.254	.408	.076
c	2.11	.006	-.003	-----	-----	-----	-----	-----	0	.0025	.928	-----	.072
c	2.53	.008	.003	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	3.17	.029	0	-----	-----	-----	-----	-----	0	.0056	.500	.466	.066
0	3.59	.049	.040	-----	-----	-----	-----	-----	0	.0076	1.487	-----	.061
0	4.22	.114	.186	-----	-----	-----	-----	-----	0	.0125	2.590	.600	.050
0	4.64	.175	.350	-----	-----	-----	-----	-----	c	.0162	3.064	-----	.033
0	5.28	.253	.750	-----	-----	-----	-----	-----	c	.0189	4.143	-----	.026
.10	0	c	-.132	0	-----	3.15	7.34	0.52	-----	-----	.262	.609	.043
.10	.63	.004	-.115	.93	0.093	3.52	-----	.51	.4988	.0200	.292	-----	.042
.10	1.06	.007	-.094	1.55	.059	3.99	7.16	.51	.1797	.0126	.331	.594	.042
.10	1.48	.014	-.094	2.17	.059	4.02	-----	.52	.0917	.0128	.333	-----	.043
.10	2.11	.023	-.083	3.10	.048	4.26	7.16	.52	.0449	.0123	.354	.594	.043
.10	2.53	.036	-.062	3.72	.052	4.73	-----	.51	.0312	.0112	.392	-----	.042
.10	3.17	.068	.019	4.65	.063	6.40	7.76	.42	.0200	.0136	.531	.645	.035
.10	3.59	.127	.119	5.26	.077	8.28	-----	.35	.0155	.0166	.667	-----	.029
.10	4.22	.168	.344	6.19	.087	12.08	8.58	.23	.0112	.0168	1.003	.711	.019
.10	4.64	.228	.560	6.81	.098	15.20	-----	.13	.0093	.0211	1.262	-----	.011
.10	5.28	.290	.397	7.74	.097	12.21	-----	.04	.0072	.0208	1.013	-----	.003
.20	0	0	-.195	0	-----	3.09	6.73	.28	-----	-----	.323	.703	.029
.20	.63	.001	-.175	.83	.025	3.09	-----	.26	.9575	.0050	.523	-----	.027
.20	1.06	.012	-.141	1.32	.063	3.58	6.69	.26	.3554	.0215	.374	.699	.027
.20	1.48	.020	-.127	1.93	.054	3.70	-----	.28	.1833	.0183	.387	-----	.029
.20	2.11	.035	-.115	2.76	.046	3.80	6.50	.28	.0898	.0157	.397	.679	.029
.20	2.53	.049	-.073	3.31	.045	4.17	-----	.27	.0624	.0153	.436	-----	.028
.20	3.17	.089	.034	4.14	.052	5.05	6.91	.22	.0399	.0177	.568	.722	.023
.20	3.59	.124	.159	4.69	.056	5.88	-----	.16	.0511	.0193	.615	-----	.017
.20	4.22	.194	.423	5.52	.064	8.00	7.61	.08	.0225	.0218	.586	.795	.009
.20	4.64	.237	.623	6.07	.064	9.42	-----	.02	.0186	.0220	.985	-----	.002
.20	5.28	.322	-----	6.90	.065	-----	-----	.05	.0144	.0231	-----	-----	-.005
.30	0	0	-.241	0	-----	2.98	6.36	.14	-----	-----	.356	.761	.017
.30	.63	.005	-.216	.77	.056	3.08	-----	.13	1.4963	.0249	.369	-----	.016
.30	1.06	.023	-.169	1.29	.092	3.24	6.36	.13	.5591	.0413	.400	.761	.015
.30	1.48	.033	-.147	1.80	.057	3.45	-----	.15	.2750	.0302	.413	-----	.018
.30	2.11	.051	-.111	2.58	.051	3.64	6.25	.14	.1348	.0229	.426	.748	.017
.30	2.53	.065	-.082	3.09	.045	3.77	-----	.14	.0926	.0203	.451	-----	.017
.30	3.17	.103	.060	3.87	.046	4.46	6.57	.08	.0599	.0205	.533	.786	.010
.30	3.59	.147	.228	4.38	.051	5.25	-----	.05	.0466	.0226	.628	-----	.005
.30	4.22	.222	.544	5.16	.056	6.56	6.93	-.01	.0337	.0249	.797	.829	-.001
.30	4.64	.265	.764	5.67	.054	7.61	-----	-.05	.0278	.0244	.910	-----	-.005
.30	5.28	.338	-----	6.45	.054	-----	-----	-.10	.0216	.0243	-----	-----	-.012

TABLE VI - Continued
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 9 WITHOUT CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(A)} \frac{1}{v}$	$\frac{z}{(A)} \frac{1}{v}$	$\frac{h}{(A)} \frac{1}{v}$	c_{T_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$\tau = 8^\circ$ - Concluded													
.40	0	0	-0.254	0	-----	2.92	6.17	0.04	-----	-----	0.385	0.812	0.006
.40	.63	.006	-0.234	.74	0.055	3.00	-----	.04	1.9950	0.0299	.395	-----	.005
.40	1.06	.028	-0.180	1.23	0.093	3.20	6.26	.04	.7188	.0503	.421	.825	.005
.40	1.48	.042	-0.149	1.72	0.071	3.29	-----	.05	.3666	.0585	.433	-----	.007
.40	2.11	.063	-0.106	2.46	0.052	3.45	6.10	.06	.1797	.0283	.454	.803	.008
.40	2.53	.082	-0.052	2.96	0.047	3.62	-----	.05	.1248	.0256	.477	-----	.006
.40	3.17	.126	.189	3.70	0.046	4.22	6.34	0	.0799	.0252	.556	.835	.001
.40	3.59	.181	.328	4.19	0.052	4.84	-----	.04	.0622	.0281	.638	-----	-.005
.40	4.22	.255	.628	4.93	0.053	5.79	-----	.09	.0449	.0286	.762	-----	-.012
.40	4.64	.327	-----	5.42	0.056	-----	-----	.14	.0371	.0304	-----	-----	-.018
.50	0	0	-0.244	0	-----	2.91	6.04	.04	-----	-----	.413	.857	-.005
.50	.63	.006	-0.228	.71	0.048	2.95	-----	.04	2.4958	0.0299	.418	-----	-.006
.50	1.06	.037	-0.159	1.18	0.106	3.13	6.15	.04	.8585	.0665	.444	.872	-.005
.50	1.48	.051	-0.133	1.66	0.074	3.18	-----	.03	.4583	.0467	.451	-----	-.004
.50	2.11	.079	-.067	2.37	0.056	3.36	6.04	.02	.2246	.0355	.477	.857	-.003
.50	2.53	.105	0	2.84	0.052	3.52	-----	.04	.1560	.0288	.500	-----	-.006
.50	3.17	.189	.201	3.55	0.047	4.01	6.27	.06	.0999	.0297	.569	.889	-.008
.50	3.59	.218	.436	4.03	0.054	4.55	-----	.13	.0777	.0339	.646	-----	-.018
.50	4.22	.313	.624	4.74	0.056	5.03	-----	.13	.0562	.0351	.713	-----	-.019
$\tau = 12^\circ$													
0	0	0	0	-----	-----	-----	-----	-----	0	0	-----	0.273	0.105
0	.63	0	0	-----	-----	-----	-----	-----	0	0	-----	0.105	0
0	1.06	.001	-.008	-----	-----	-----	-----	-----	0	0.0018	2.577	.220	.104
0	1.48	.001	-.003	-----	-----	-----	-----	-----	0	0.009	-.782	-----	.104
0	2.11	.004	-.008	-----	-----	-----	-----	-----	0	0.018	-.056	.246	.100
0	2.53	.008	-.002	-----	-----	-----	-----	-----	0	0.025	.308	-----	.098
0	3.17	.021	.012	-----	-----	-----	-----	-----	0	.0042	1.013	.380	.093
0	3.59	.089	.114	-----	-----	-----	-----	-----	0	.0158	1.590	-----	.071
0	4.22	.134	.259	-----	-----	-----	-----	-----	0	.0150	2.154	.547	.061
0	4.64	.176	.407	-----	-----	-----	-----	-----	0	.0163	2.497	-----	.054
0	5.28	.234	.698	-----	-----	-----	-----	-----	0	.0168	3.069	-----	.060
.10	0	0	-.147	0	-----	0.28	6.21	0.68	-----	-----	.231	.515	.056
.10	.63	.004	-.140	.93	0.093	2.97	-----	.64	4.988	.0200	.246	-----	.053
.10	1.06	.011	-.132	1.55	0.091	3.16	6.33	.66	.1797	.0197	.264	.526	.055
.10	1.48	.015	-.121	2.17	0.064	3.46	-----	.70	.0917	.0137	.287	-----	.058
.10	2.11	.027	-.100	3.10	0.056	3.96	6.23	.68	.0449	.0121	.328	.517	.056
.10	2.53	.043	-.054	3.72	0.062	4.94	-----	.62	.0312	.0134	.410	-----	.052
.10	3.17	.078	.039	4.65	0.072	6.77	7.00	.53	.0200	.0156	.562	.582	.044
.10	3.59	.117	.139	5.26	0.065	8.47	-----	.14	.0155	.0182	.703	-----	.037
.10	4.22	.166	.349	6.19	0.086	11.74	7.93	.36	.0112	.0186	.974	.658	.050
.10	4.65	.205	.589	6.81	0.088	14.43	-----	.29	.0093	.0190	1.197	-----	.024
.10	5.28	.261	.971	7.74	0.094	19.31	-----	.15	.0072	.0202	1.603	-----	.012
.20	0	0	-.233	0	-----	2.75	5.77	.35	-----	-----	.287	.603	.057
.20	.63	.006	-.217	.83	0.087	2.90	-----	.33	.9975	.0299	.303	-----	.055
.20	1.06	.020	-.196	1.38	0.105	3.12	5.91	.35	.3594	.0359	.326	.617	.037
.20	1.48	.027	-.191	1.93	0.072	3.17	-----	.37	.1833	.0247	.331	-----	.039
.20	2.11	.042	-.147	2.76	0.055	3.56	5.79	.29	.0898	.0189	.372	.605	.037
.20	2.53	.063	-.079	3.31	0.057	4.14	-----	.31	.0624	.0196	.433	-----	.033
.20	3.17	.107	.063	4.14	0.062	5.27	6.54	.24	.0399	.0213	.551	.684	.026
.20	3.59	.144	.213	4.69	0.066	6.40	-----	.20	.0311	.0224	.669	-----	.021
.20	4.22	.203	.508	5.52	0.057	8.44	6.77	.13	.0225	.0228	.882	.707	.013
.20	4.64	.246	.719	6.07	0.057	9.77	-----	.08	.0186	.0228	1.021	-----	.008
.20	5.28	.319	1.119	6.90	0.067	12.07	-----	0	.0144	.0229	1.262	-----	0

TABLE VI - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 9 WITHOUT CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(\frac{L}{w})^{1/3}}$	$\frac{l}{(\frac{L}{w})^{1/3}}$	$\frac{z}{(\frac{L}{w})^{1/3}}$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{z}{L}$
$\tau = 12^\circ$ - Concluded													
.30	0	0	-0.285	0	-----	2.74	5.64	0.17	-----	0.328	0.675	0.020	
.30	.63	.005	-.267	.77	0.056	2.83	-----	.15	1.4963	0.0249	.335	-----	.018
.30	1.06	.028	-.239	1.29	.112	2.98	5.73	.17	.5391	.0502	.356	.686	.020
.30	1.48	.037	-.222	1.30	.076	3.08	-----	.21	.2750	.0339	.369	-----	.025
.30	2.11	.056	-.164	2.58	.056	3.37	5.61	.20	.1348	.0251	.403	.671	.024
.30	2.53	.079	-.073	3.09	.055	3.54	-----	.14	.0936	.0246	.459	-----	.017
.30	3.17	.132	.115	3.87	.059	4.70	6.07	.10	.0599	.0253	.562	.726	.012
.30	3.59	.183	.318	4.38	.063	5.62	-----	.05	.0465	.0284	.672	-----	.006
.30	4.22	.248	.647	5.16	.062	6.99	6.52	-.02	.0337	.0278	.836	.780	-.002
.30	4.64	.288	.847	5.67	.060	7.76	-----	-.05	.0276	.0267	.928	-----	-.006
.40	0	0	-.302	0	-----	2.75	5.57	.04	-----	0.362	.733	.006	
.40	.63	.008	-.281	.74	.074	2.82	-----	.03	1.9950	.0399	.372	-----	.004
.40	1.06	.037	-.255	1.23	.123	2.94	5.68	.05	.7188	.0665	.387	.748	.007
.40	1.48	.051	-.235	1.72	.086	3.00	-----	.08	.3666	.0467	.395	-----	.010
.40	2.11	.075	-.154	2.45	.062	3.29	5.58	.06	.1797	.0337	.433	.735	.008
.40	2.53	.097	-.056	2.96	.056	3.62	-----	.04	.1248	.0503	.477	-----	.005
.40	3.17	.162	.179	3.70	.060	4.36	5.94	-.02	.0799	.0323	.574	.782	-.002
.40	3.59	.213	.370	4.19	.060	4.94	-----	-.05	.0622	.0326	.651	-----	-.007
.40	4.22	.290	.730	4.93	.060	6.00	-----	-.09	.0449	.0326	.790	-----	-.012
.40	4.64	.350	1.032	5.42	.062	6.85	-----	-.14	.0371	.0334	.895	-----	-.019
.50	0	0	-.297	0	-----	2.76	5.54	-.06	-----	0.392	.735	-.008	
.50	.63	.009	-.275	.71	.071	2.82	-----	-.07	2.4938	.0449	.400	-----	-.009
.50	1.06	.049	-.249	1.18	.140	2.89	5.60	-.04	.8955	.0581	.410	.795	-.006
.50	1.48	.063	-.226	1.66	.092	2.95	-----	-.01	.4583	.0577	.418	-----	-.002
.50	2.11	.092	-.135	2.37	.066	3.20	5.54	-.02	.2246	.0413	.454	.786	-.003
.50	2.53	.121	-.004	2.84	.060	3.50	-----	-.04	.1560	.0377	.497	-----	-.006
.50	3.17	.191	.249	3.55	.061	4.12	5.81	-.11	.0999	.0381	.585	.825	-.014
.50	3.59	.255	.486	4.03	.063	4.65	-----	-.05	.0777	.0396	.659	-----	-.007
.50	4.22	.333	.843	4.74	.059	5.42	-----	-.15	.0562	.0374	.769	-----	-.019
$\tau = 15^\circ$													
0	0	0	0	0	-----	-----	-----	-----	0	0.0100	-3.164	-----	.124
0	.63	.002	-.013	-----	-----	-----	-----	-----	0	.0090	-3.943	.179	.129
0	1.06	.005	-.035	-----	-----	-----	-----	-----	0	.0037	-9.94	-----	.125
0	1.48	.008	-.008	-----	-----	-----	-----	-----	0	.0063	-1.462	.239	.125
0	2.11	.011	-.020	-----	-----	-----	-----	-----	0	.0078	.262	.365	.116
0	2.53	.023	-.009	-----	-----	-----	-----	-----	0	-----	-----	-----	-----
0	3.17	.057	.059	-----	-----	-----	-----	-----	0	.0114	.938	-----	.108
0	3.59	.092	.117	-----	-----	-----	-----	-----	0	.0143	1.331	-----	.098
0	4.22	.160	.296	-----	-----	-----	-----	-----	0	.0180	1.705	.504	.085
0	4.64	.212	.444	-----	-----	-----	-----	-----	0	.0197	1.859	-----	.075
0	5.28	.286	.771	-----	-----	-----	-----	-----	0	.0206	2.244	-----	.066
.10	0	0	-.161	0	-----	2.41	5.46	0.83	-----	.200	.455	.069	
.10	.63	.005	-.153	.93	0.116	2.63	-----	.78	.4988	.0249	.218	-----	.065
.10	1.06	.016	-.158	1.55	.133	2.66	5.56	.81	.1797	.0287	.221	.461	.070
.10	1.48	.017	-.133	2.17	.072	3.18	-----	.88	.0917	.0156	.264	-----	.071
.10	2.11	.036	-.068	3.10	.075	4.23	5.69	.81	.0449	.0162	.357	.472	.067
.10	2.53	.060	-.040	3.72	.087	5.25	-----	.71	.0312	.0187	.436	-----	.059
.10	3.17	.106	.070	4.65	.098	7.23	6.44	.63	.0200	.0211	.600	.534	.052
.10	3.59	.146	.191	5.26	.107	9.02	-----	.54	.0155	.0230	.749	-----	.045
.10	4.22	.222	.455	6.19	.116	12.17	7.24	.42	.0112	.0249	1.010	.600	.035
.10	4.64	.269	.638	6.81	.116	14.12	-----	.36	.0093	.0249	1.172	-----	.030
.10	5.28	.323	.965	7.74	.108	17.24	-----	.27	.0072	.0232	1.431	-----	.022

TABLE VI - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
OF FINENESS RATIO 9 WITHOUT CHINE STRIPS

C_{D_Q}	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(A)}^{1/3}$	$\frac{z}{(A)}^{1/3}$	$\frac{h}{(A)}^{1/3}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$\tau = 16^\circ$ - Concluded													
.20	0	0	-0.251	0	-----	2.55	5.23	0.44	-----	0.267	0.547	0.046	
.20	.63	.006	-0.233	.63	0.087	2.73	-----	.41	0.9975	0.0299	.285	-----	.043
.20	1.06	.027	-0.238	1.38	.142	2.75	5.26	.47	.3594	.0484	.287	.551	.049
.20	1.48	.032	-0.207	1.93	.056	3.01	-----	.49	.1833	0.0293	.315	-----	.051
.20	2.11	.057	-0.137	2.76	.075	3.65	5.34	.46	.0898	0.0256	.382	.558	.048
.20	2.53	.083	-0.040	3.31	.076	4.47	-----	.39	.0624	0.0259	.467	-----	.041
.20	3.17	.114	.177	4.14	.084	5.65	5.77	.32	.0399	0.0287	.590	.603	.033
.20	3.59	.190	.271	4.69	.086	6.57	-----	.27	.0311	0.0295	.697	-----	.028
.20	4.22	.257	.536	5.52	.084	8.27	-----	.20	.0225	0.0268	.864	-----	.021
.20	4.64	.307	.765	6.07	.083	9.64	-----	.17	.0186	0.0285	1.008	-----	.018
.30	0	0	-0.302	0	-----	2.62	5.16	.23	-----	-----	.313	.617	.027
.30	.63	.009	-0.281	.77	.100	2.72	-----	.23	1.4965	.0449	.326	-----	.027
.30	1.06	.041	-0.226	1.29	.164	2.77	5.22	.27	.5391	.0735	.331	.624	.033
.30	1.48	.062	-0.255	1.80	.127	2.93	-----	.29	.2750	.0568	.351	-----	.035
.30	2.11	.075	-0.141	2.58	.075	3.49	5.32	.24	.1348	0.0337	.418	.637	.029
.30	2.53	.105	-0.040	3.09	.074	3.99	-----	.18	.0956	0.0350	.477	-----	.022
.30	3.17	.169	.144	3.87	.075	4.82	5.64	.15	.0599	0.0337	.577	.675	.017
.30	3.59	.222	.323	4.38	.077	5.55	-----	.11	.0466	0.0245	.664	-----	.013
.30	4.22	.300	.771	5.16	.075	7.29	-----	.05	.0337	0.0337	.872	-----	.006
.40	0	0	-0.329	0	-----	2.63	5.16	.07	-----	-----	.346	.679	.009
.40	.63	.011	-0.302	.74	.101	2.75	-----	.07	1.9950	.0549	.362	-----	.009
.40	1.06	.053	-0.310	1.23	.175	2.75	5.16	.11	.7188	.0552	.362	.679	.014
.40	1.48	.062	-0.269	1.72	.105	2.88	-----	.11	.3666	.0568	.379	-----	.015
.40	2.11	.089	-0.158	2.46	.074	3.27	5.19	.10	.1797	.0400	.431	.654	.013
.40	2.53	.131	.020	2.96	.075	3.86	-----	.06	.1248	.0409	.508	-----	.008
.40	3.17	.209	.201	3.70	.077	4.42	5.40	.01	.0799	.0417	.582	.711	.001
.40	3.59	.260	.397	4.19	.074	4.98	-----	.02	.0621	.0404	.656	-----	.003
.50	0	0	-0.314	0	-----	2.69	5.17	-.06	-----	-----	.382	.733	-.009
.50	.63	.014	-0.302	.71	.111	2.75	-----	-.05	2.4956	.0698	.390	-----	-.007
.50	1.06	.065	-0.299	1.18	.185	2.76	5.15	0	.8985	.1168	.392	.731	0
.50	1.48	.078	-0.261	1.66	.114	2.88	-----	0	.1585	.0725	.408	-----	.004
.50	2.11	.108	-0.101	2.37	.077	3.27	5.21	-.03	.2246	.0485	.464	.739	-.004
.50	2.53	.155	.054	2.81	.077	3.65	-----	-.05	.1560	.0481	.518	-----	-.007
.50	3.17	.243	.288	3.55	.077	4.19	5.24	-.09	.0999	.0485	.595	.744	-.013
.50	3.59	.304	.539	4.03	.075	4.74	-----	-.12	.0777	.0473	.672	-----	-.017
.50	4.22	.374	.905	4.74	.067	5.49	-----	-.15	.0562	.0420	.779	-----	-.019
$\tau = 20^\circ$													
0	0	0	0	0	-----	-----	-----	-----	0	0.050	-3.346	0.239	0.172
0	.63	.001	-.010	-----	-----	-----	-----	-----	0	0.036	-1.423	.229	.172
0	1.06	.002	-.010	-----	-----	-----	-----	-----	0	0.037	-.782	-----	.172
0	1.48	.004	-.010	-----	-----	-----	-----	-----	0	0.031	-.013	.226	.170
0	2.11	.007	-.007	-----	-----	-----	-----	-----	0	0.044	.423	-----	.167
0	2.53	.014	-.002	-----	-----	-----	-----	-----	0	0.0054	.641	.316	.160
0	3.16	.027	.007	-----	-----	-----	-----	-----	0	0.096	.928	-----	.155
0	3.59	.062	.050	-----	-----	-----	-----	-----	0	0.056	.577	-----	.157
0	4.22	.050	.007	-----	-----	-----	-----	-----	0	0.0149	1.179	-----	.123
0	4.64	.160	.208	-----	-----	-----	-----	-----	0	0.0162	1.334	-----	.112
0	5.28	.226	.370	-----	-----	-----	-----	-----	0	0.0051	.641	.316	.160
.10	0	0	-.157	0	-----	2.38	4.74	0.97	-----	-----	.191	.393	.081
.10	.63	.007	-.153	.53	0.162	2.60	-----	.99	.4985	.0349	.235	-----	.082
.10	1.06	.018	-.162	1.55	.150	2.55	5.07	.99	.1797	.0325	.210	.421	.082
.10	1.48	.023	-.147	2.17	.058	2.90	-----	.99	.0917	.0211	.241	-----	.082
.10	2.11	.044	-.086	3.10	.091	4.33	5.36	.93	.0449	.0197	.359	.444	.077
.10	2.53	.067	-.048	3.72	.097	5.16	-----	.90	.0312	.0209	.428	-----	.075

TABLE VI - Concluded
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 9 WITHOUT CHINE STRIPS

$C_{\Delta Q}$	C_{V_Q}	C_{Z_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{L}$ $(\frac{A}{W})^{1/3}$	$\frac{l}{L}$ $(\frac{A}{W})^{1/3}$	$\frac{h}{L}$ $(\frac{A}{W})^{1/3}$	C_{L_Q}	C_{Q_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 20^\circ$ - Concluded													
.10	3.17	0.117	0.049	4.65	0.108	6.83	5.77	0.78	0.0200	0.0233	0.367	0.479	0.065
.10	3.59	.153	.151	5.26	.111	7.94	----	.73	.0155	.0258	.659	----	.060
.10	4.22	.215	.312	6.19	.122	10.04	----	.65	.0112	.0241	.853	----	.054
.10	4.63	.296	.450	6.81	.110	11.37	----	.59	.0093	.0237	.944	----	.049
.10	5.28	.321	.633	7.74	.107	12.73	----	.57	.0072	.0230	1.056	----	.048
.20	0	0	--243	0	----	2.55	4.78	.50	----	----	.267	.500	.052
.20	.63	.014	-.255	.63	.204	2.53	----	.49	.9975	.0696	.264	----	.051
.20	1.06	.054	-.255	1.58	.178	2.60	4.91	.54	.3594	.0610	.272	.513	.056
.20	1.45	.042	-.232	1.93	.113	2.82	----	.54	.1853	.0385	.295	----	.056
.20	2.11	.070	-.136	2.76	.092	3.68	5.03	.49	.0898	.0314	.385	.526	.051
.20	2.53	.099	-.073	3.31	.090	4.22	----	.46	.0624	.0309	.441	----	.048
.20	3.17	.165	.070	4.11	.096	5.27	5.36	.38	.0399	.0329	.551	.560	.059
.20	3.59	.204	.196	4.69	.093	6.09	----	.36	.0311	.0317	.636	----	.038
.20	4.22	.273	.423	5.52	.090	7.36	----	.32	.0225	.0506	.769	----	.035
.20	4.64	.311	.540	5.07	.095	7.90	----	.33	.0186	.0291	.826	----	.034
.20	5.28	.379	.750	6.90	.080	8.83	----	.33	.0144	.0272	.923	----	.034
.30	0	0	--309	0	----	2.53	4.75	.25	----	----	.303	.568	.050
.30	.63	.018	-.309	.77	.260	2.57	----	.25	-.14663	.0898	.508	----	.030
.30	1.06	.050	-.314	1.29	.200	2.62	4.80	.30	.5791	.0897	.313	.575	.036
.30	1.48	.058	-.276	1.80	.119	2.81	----	.32	.2750	.0552	.336	----	.036
.30	2.11	.092	-.156	2.58	.096	3.43	4.93	.26	.1348	.0451	.410	.590	.051
.30	2.53	.134	-.057	3.09	.093	3.92	----	.22	.0936	.0413	.469	----	.026
.30	3.17	.209	.118	3.87	.095	4.67	5.13	.19	.0599	.0417	.559	.613	.022
.30	3.59	.259	.276	4.38	.090	5.29	----	.17	.0466	.0402	.533	----	.020
.30	4.22	.330	.529	5.16	.083	6.17	----	.15	.0337	.0370	.738	----	.018
.30	4.64	.375	.699	5.67	.078	6.73	----	.15	.0273	.0348	.805	----	.018
.30	5.28	.452	.961	6.45	.073	7.18	----	.15	.0215	.0325	.855	----	.018
.40	0	0	--335	0	----	2.57	4.92	.07	----	----	.338	.647	.010
.40	.63	.018	-.341	.74	.165	2.29	----	.09	1.5951	.0898	.341	----	.012
.40	1.06	.065	-.350	1.23	.215	2.61	4.70	.14	.7188	.1168	.344	.620	.018
.40	1.48	.074	-.294	1.72	.125	2.80	----	.15	.3666	.0678	.369	----	.020
.40	2.11	.113	-.148	2.46	.094	3.31	4.95	.11	.1797	.0508	.436	.652	.014
.40	2.53	.160	.041	2.96	.092	3.93	----	.09	.1218	.0499	.518	----	.012
.40	3.17	.245	.165	3.70	.090	4.28	5.05	.07	.0799	.0489	.564	.654	.009
.40	3.59	.295	.349	4.19	.087	4.79	----	.06	.0622	.0459	.631	----	.008
.40	4.22	.368	.654	4.93	.076	5.57	----	.05	.0449	.0453	.735	----	.007
.40	4.64	.414	.843	5.42	.077	6.01	----	.04	.0371	.0358	.792	----	.005
.50	0	0	--319	C	----	2.66	4.78	-.09	----	----	.377	.677	-.03
.50	.63	.025	-.330	.71	.198	2.66	----	-.09	2.4938	----	.1247	.377	-.012
.50	1.06	.061	-.346	1.18	.231	2.66	4.90	-.09	.8985	----	.1456	.377	-.012
.50	1.48	.092	-.276	1.66	.134	2.84	----	0	.4583	.0843	.403	----	-.001
.50	2.11	.137	-.112	2.37	.098	3.26	4.87	-.04	.2246	.0615	.452	.690	-.005
.50	2.53	.186	-.014	2.81	.092	3.49	----	-.04	.1560	.0580	.495	----	-.005
.50	3.17	.279	.213	3.55	.088	4.00	4.99	-.06	.0999	.0557	.567	.707	-.008
.50	3.59	.357	.417	4.03	.085	4.43	----	-.08	.0777	.0524	.628	----	-.011
.50	4.22	.419	.776	4.74	.075	5.12	----	----	.0562	.0477	.726	----	----

TABLE VII
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION OF
FINENESS RATIO 12 WITHOUT CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_A}	c_{D_A}	$\frac{x}{(\Delta)}^{1/3}$	$\frac{l}{(\Delta)}^{1/3}$	$\frac{h}{(\Delta)}^{1/3}$	c_{L_Q}	c_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 0^\circ$													
0	0	0	0	-----	-----	-----	-----	-----	0	-----	0.415	0.042	0.042
0	.63	0	0	-----	-----	-----	-----	-----	0	-----	.410	0.042	0.042
0	1.06	0	0	-----	-----	-----	-----	-----	0	-----	.410	0.042	0.042
0	1.48	.002	0	-----	-----	-----	-----	-----	0	.0018	-----	-----	0.042
0	2.11	.006	.003	-----	-----	-----	-----	-----	0	.0027	-----	.578	.040
0	2.53	.010	.007	-----	-----	-----	-----	-----	0	.0031	-----	.037	0.037
0	3.17	.024	.016	-----	-----	-----	-----	-----	0	.0048	-----	.689	.036
0	3.59	.040	.027	-----	-----	-----	-----	-----	0	.0062	-----	-----	.036
0	4.22	.066	.058	-----	-----	-----	-----	-----	0	.0074	-----	.825	.033
0	4.64	.092	.087	-----	-----	-----	-----	-----	0	.0085	-----	-----	.031
0	5.28	.193	.180	-----	-----	-----	-----	-----	0	.0139	-----	-----	.026
.10	0	0	.015	0	0.046	7.64	10.92	0.38	-----	0.523	.749	.026	.026
.10	.63	.002	.021	.93	0.046	7.76	-----	.36	.4988	.0100	.532	-----	.024
.10	1.06	.006	.052	1.55	.050	8.40	12.59	.34	.1797	.0108	.576	.865	.023
.10	1.48	.009	.067	2.17	.058	8.74	-----	.34	.0927	.0082	.600	-----	.023
.10	2.11	.021	.087	3.10	.044	9.18	12.59	.33	.0449	.0094	.629	.863	.022
.10	2.53	.031	.096	3.72	.045	9.42	-----	.33	.0312	.0097	.646	-----	.022
.10	3.17	.047	.103	4.65	.044	9.52	13.26	.33	.0200	.0094	.653	.909	.022
.10	3.59	.068	.129	5.26	.049	10.07	-----	.31	.0155	.0106	.691	-----	.022
.10	4.22	.127	.180	6.19	.066	11.21	13.75	.27	.0112	.0143	.769	.943	.019
.10	4.64	.165	.220	6.81	.071	12.14	-----	.24	.0093	.0153	.833	-----	.016
.10	5.28	.306	.342	7.74	.102	14.67	-----	.19	.0072	.0220	1.006	-----	.013
.20	0	0	.058	0	-----	6.11	9.98	.23	-----	-----	.528	.862	.020
.20	.63	.002	.042	.83	.029	6.14	-----	.23	.9975	.0100	.530	-----	.020
.20	1.06	.008	.087	1.38	.042	6.53	11.24	.22	.3504	.0144	.564	.971	.019
.20	1.48	.015	.129	1.93	.040	6.89	-----	.21	.1853	.0137	.595	-----	.018
.20	2.11	.031	.168	2.76	.041	7.21	11.12	.21	.0898	.0139	.623	.961	.018
.20	2.53	.043	.194	3.31	.039	7.46	-----	.20	.0625	.0134	.644	-----	.017
.20	3.17	.075	.210	4.14	.044	7.58	11.16	.20	.0399	.0150	.655	.964	.017
.20	3.59	.106	.228	4.69	.048	7.72	-----	.19	.0311	.0165	.667	-----	.017
.20	4.22	.157	.261	5.52	.0515	8.02	11.45	.16	.0225	.0176	.693	.989	.014
.30	0	0	.054	0	-----	5.31	9.47	.12	-----	-----	.525	.936	.012
.30	.63	.003	.058	.77	.034	5.36	-----	.11	1.4963	.0150	.530	-----	.011
.30	1.06	.012	.102	1.29	.048	5.57	10.11	.09	.5391	.0216	.551	1.000	.008
.30	1.48	.024	.170	1.80	.049	5.92	-----	.09	.2750	.0220	.585	-----	.008
.30	2.11	.041	.211	2.58	.041	6.11	10.11	.09	.1348	.0184	.604	1.000	.008
.30	2.53	.059	.250	3.05	.041	6.30	-----	.08	.0936	.0184	.623	-----	.008
.30	3.17	.101	.261	3.87	.047	6.36	10.11	.08	.0599	.0202	.629	1.000	.008
.30	3.59	.139	.250	4.38	.048	6.30	-----	.07	.0466	.0216	.623	-----	.007
.30	4.22	.207	.250	5.16	.052	6.30	-----	.03	.0337	.0232	.623	-----	.003
.30	4.64	.306	.261	5.67	.053	6.36	-----	0	.0278	.0284	.629	-----	0
.40	0	0	.072	0	-----	4.83	9.18	.05	-----	-----	.525	1.000	.006
.40	.63	.004	.072	.74	.037	4.83	-----	.04	1.9950	.0201	.525	-----	.005
.40	1.06	.014	.135	1.23	.046	5.05	9.18	.03	.7188	.0252	.549	1.000	.005
.40	1.48	.028	.210	1.72	.047	5.31	-----	.02	.3666	.0257	.578	-----	.002
.40	2.11	.047	.255	2.46	.059	5.45	9.18	.01	.1797	.0211	.593	1.000	.001
.40	2.53	.066	.291	2.96	.058	5.59	-----	0	.1248	.0206	.608	-----	0
.40	3.17	.125	.291	3.70	.046	5.59	9.18	.01	.0799	.0250	.608	1.000	-.001
.40	3.59	.179	.281	4.19	.051	5.59	-----	.03	.0622	.0278	.608	-----	-.003
.40	4.22	.327	.261	4.53	.068	5.40	-----	.08	.0449	.0367	.587	-----	-.008
.50	0	0	.087	0	-----	4.48	8.53	0	-----	-----	.525	1.000	0
.50	.63	.005	.087	.71	.040	4.48	-----	.01	2.4938	.0249	.525	-----	-.001
.50	1.06	.014	.139	1.18	.040	4.61	8.53	.03	.8655	.0252	.540	1.000	-.004
.50	1.48	.033	.236	1.66	.048	4.86	-----	.04	.4583	.0302	.570	-----	-.005
.50	2.11	.061	.281	2.37	.044	4.97	8.53	.04	.2246	.0274	.583	1.000	-.005
.50	2.53	.089	.307	2.84	.044	5.01	-----	.06	.1560	.0278	.587	-----	-.007
.50	3.17	.155	.271	3.55	.049	4.96	8.53	.07	.0999	.0309	.581	1.000	-.008
.50	3.59	.240	.250	4.03	.059	4.90	-----	.11	.0777	.0373	.574	-----	-.013

TABLE VII.- Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION OF
FINENESS RATIO 12 WITHOUT CHINE STRIPS

$C_{\Delta Q}$	C_{VQ}	C_{RQ}	C_{KQ}	$C_{V\Delta}$	C_{Δ}	$\frac{x}{(\Delta)^{1/3}}$	$\frac{l}{(\Delta)^{1/3}}$	$\frac{b}{(\Delta)^{1/3}}$	C_{-Q}	C_{CQ}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{b}{L}$
$T = 10^0$													
0	0	0	0	0	0	0	0	0	0	0.0050	0.500	0.364	0.049
0	.63	.001	0	0	0	0	0	0	0	0.0036	.500	.332	.049
0	1.06	.002	0	0	0	0	0	0	0	0.0018	.500	0.45	.049
0	1.48	.002	0	0	0	0	0	0	0	0.0031	.500	.445	.048
0	2.11	.007	0	0	0	0	0	0	0	0.0024	.500	0.45	.045
0	2.53	.011	0	0	0	0	0	0	0	0.0013	.500	0.45	.045
0	3.17	.020	0	0	0	0	0	0	0	0.0040	.500	.193	.044
0	3.59	.029	0	0	0	0	0	0	0	0.0045	.500	0.43	.043
0	4.22	.047	.012	0	0	0	0	0	0	0.0053	1.045	.549	.040
0	4.64	.078	.027	0	0	0	0	0	0	0.0072	1.206	0.38	.038
0	5.28	.157	.154	0	0	0	0	0	0	0.0113	2.564	0.051	.051
.10	0	0	-.117	0	0	4.76	9.81	0.43	0	0	.526	.673	.030
.10	.63	.001	-.113	.93	0.023	1.85	0.44	.4988	.0050	.333	0.30	.030	
.10	1.06	.005	-.091	1.55	.042	5.32	10.10	.45	.1797	.0090	.364	.692	.030
.10	1.48	.009	-.080	2.17	.058	5.59	0	.13	.0917	.0052	.383	0.30	.030
.10	2.11	.020	-.066	3.10	.042	5.90	9.76	.43	.0449	.0090	.405	.669	.030
.10	2.53	.029	-.060	3.72	.042	6.03	0	.42	.0312	.0090	.43	0.29	.029
.10	3.17	.047	-.048	4.65	.041	6.27	9.89	.39	.0200	.0094	.430	.678	.027
.10	3.59	.065	-.035	5.26	.048	6.58	0	.38	.0155	.0133	.451	0.26	.026
.10	4.22	.110	-.021	6.19	.058	7.73	10.43	.35	.0112	.0124	.530	.715	.024
.10	4.64	.139	-.019	6.81	.060	9.64	0	.31	.0033	.0129	.661	0.21	.021
.10	5.28	.256	-.025	7.74	.072	12.55	0	.24	.0072	.0155	.860	0.016	.016
.20	0	0	-.189	C	0	4.17	8.96	.24	0	0	.350	.774	.021
.20	.63	.002	-.175	.83	.029	4.27	0	.23	.9975	.0100	.359	0.019	.019
.20	1.06	.009	-.133	1.38	.047	4.67	9.02	.20	.3594	.0162	.403	.779	.018
.20	1.48	.015	-.113	1.93	.040	4.83	0	.22	.1853	.0137	.417	0.019	.019
.20	2.11	.032	-.086	2.76	.042	5.05	8.87	.23	.0898	.0144	.436	.766	.019
.20	2.53	.041	-.069	3.31	.037	5.20	0	.22	.0624	.0128	.449	0.019	.019
.20	3.17	.066	-.046	4.14	.039	5.42	9.04	.19	.0399	.0132	.468	.781	.017
.20	3.59	.087	-.035	4.69	.040	5.42	0	.18	.0311	.0135	.496	0.016	.016
.20	4.22	.132	-.026	5.52	.043	5.74	9.12	.16	.0225	.0145	.555	.788	.014
.20	4.64	.176	-.020	6.07	.048	7.41	0	.11	.0186	.0163	.640	0.010	.010
.20	5.28	.243	-.039	6.90	.051	8.71	0	.07	.0144	.0175	.752	0.006	.006
.30	0	0	-.233	0	0	3.90	8.38	.13	0	0	.386	.828	.012
.30	.63	.002	-.221	.77	.022	3.95	0	.12	.14963	.0100	.390	0.012	.012
.30	1.06	.012	-.159	1.29	.048	4.27	8.48	.11	.5391	.0216	.422	.839	.011
.30	1.48	.021	-.123	1.80	.043	4.46	0	.12	.2750	.0192	.441	0.012	.012
.30	2.11	.041	-.092	2.58	.041	4.61	8.45	.13	.1348	.0184	.456	.835	.013
.30	2.53	.053	-.060	3.09	.037	4.75	0	.12	.0596	.0165	.470	0.012	.012
.30	3.17	.082	-.023	3.87	.037	5.00	8.31	.12	.0599	.0164	.494	.821	.012
.30	3.59	.110	-.037	4.56	.038	5.25	0	.10	.0466	.0171	.517	0.010	.010
.30	4.22	.165	-.071	5.26	.041	5.90	8.66	.07	.0337	.0185	.585	.857	.007
.30	4.64	.207	-.087	5.67	.043	6.43	0	.05	.0278	.0192	.636	0.005	.005
.30	5.28	.285	-.043	6.45	.046	7.59	0	0	.0216	.0205	.750	0	0
.40	0	0	-.247	0	0	3.76	8.06	.05	0	0	.409	.878	.005
.40	.63	.003	-.226	.74	.029	3.81	0	.04	1.5950	.0150	.425	0.004	.004
.40	1.06	.016	-.153	1.23	.053	4.07	8.19	.02	.7188	.0288	.443	.892	.003
.40	1.48	.026	-.113	1.72	.047	4.21	0	.04	.3666	.0257	.458	0.004	.004
.40	2.11	.047	-.073	2.45	.039	4.37	8.05	.05	.1797	.0211	.475	.876	.005
.40	2.53	.065	-.040	2.96	.037	4.46	0	.04	.1248	.0203	.485	0.005	.005
.40	3.17	.106	.019	3.70	.039	4.65	8.05	.04	.0799	.0212	.506	.876	.004
.40	3.59	.141	.097	4.19	.040	4.93	0	.01	.0622	.0219	.556	0.001	.001
.40	4.22	.200	.246	4.93	.041	5.11	8.05	-.01	.0449	.0225	.589	.876	-.001
.40	4.64	.268	.423	5.42	.046	5.97	0	-.05	.0371	.0249	.650	0.005	-.005
.40	5.28	.364	.697	6.16	.048	6.84	0	-.07	.0288	.0262	.744	0.008	-.008

TABLE VII.- Continued
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION OF
 FINENESS RATIO 12 WITHOUT CHINE STRIPS

c_{A_Q}	c_{V_Q}	c_{R_Q}	c_{M_Q}	c_{V_Δ}	c_{D_Δ}	$\frac{x}{(\Delta)^{1/3}}$	$\frac{l}{(\Delta)^{1/3}}$	$\frac{h}{(\Delta)^{1/3}}$	c_{L_Q}	c_{D_Q}	$\frac{x}{\Sigma}$	$\frac{l}{\Sigma}$	$\frac{h}{\Sigma}$
$\tau = 4^\circ$ - Concluded													
.50	0	0	-0.231	0	-----	3.69	7.80	-0.02	2.4958	0.0200	0.432	0.915	-0.002
.50	.63	.004	-.206	.71	0.032	3.75	-----	-.03	-----	.439	-----	-----	-.003
.50	1.06	.019	-.131	1.18	.054	3.92	7.92	-.04	.8856	0.0341	.460	.929	-.005
.50	1.48	.033	-.066	1.66	.048	4.05	-----	-.05	.4553	0.0202	.475	-----	-.005
.50	2.11	.055	-.048	2.37	.039	4.14	7.74	-.02	.2216	0.0247	.455	.908	-.003
.50	2.53	.076	-.009	2.81	.039	4.25	-----	-.03	.1560	0.0243	.498	-----	-.003
.50	3.17	.127	.077	3.55	.040	4.46	7.80	-.05	.0999	0.0254	.523	.915	-.005
.50	3.59	.172	-.169	4.03	.042	4.68	-----	-.06	.0777	0.0267	.549	-----	-.007
.50	4.22	.254	.362	4.74	.045	5.15	-----	-.09	.0562	0.0285	.604	-----	-.011
$\tau = 8^\circ$													
0	0	0	0	0	-----	-----	-----	-----	0	0	-----	.233	.073
0	.63	0	0	0	-----	-----	-----	-----	0	0	-----	-----	.075
0	1.06	0	-.004	0	-----	-----	-----	-----	0	0	-----	.154	.075
0	1.48	0	-.004	0	-----	-----	-----	-----	0	0	-----	-----	.075
0	2.11	.002	-.004	0	-----	-----	-----	-----	0	.0009	-1.317	.148	.074
0	2.53	.003	-.004	0	-----	-----	-----	-----	0	.0009	-1.090	-----	.072
0	3.17	.009	-.003	0	-----	-----	-----	-----	0	.0018	.197	.222	.070
0	3.59	.014	0	0	-----	-----	-----	-----	0	.0022	.500	-----	.069
0	4.22	.047	.021	0	-----	-----	-----	-----	0	.0053	.988	.399	.069
0	4.64	.092	-.099	0	-----	-----	-----	-----	0	.0085	1.658	-----	.052
0	5.28	.183	.303	0	-----	-----	-----	-----	0	.0132	2.265	.558	.041
.10	0	0	-.176	0	-----	3.46	7.57	.61	-----	-----	.237	.519	.042
.10	.63	.002	-.164	.93	.046	3.74	-----	.59	.4988	.0100	.256	-----	.041
.10	1.06	.008	-.153	1.55	.067	3.99	7.57	.60	.1797	.0144	.273	.519	.041
.10	1.48	.012	-.146	2.17	.051	4.17	-----	.60	.0917	.0110	.286	-----	.041
.10	2.11	.021	-.145	3.10	.044	4.23	7.29	.61	.0449	.0094	.290	.500	.041
.10	2.53	.032	-.129	3.72	.046	4.60	-----	.61	.0312	.0100	.316	-----	.041
.10	3.17	.059	-.070	4.65	.055	5.87	7.86	.54	.0200	.0118	.403	.539	.037
.10	3.59	.085	-.013	5.26	.051	7.05	-----	.50	.0155	.0132	.483	-----	.034
.10	4.22	.134	.098	6.19	.070	9.12	8.50	.44	.0112	.0150	.625	.585	.030
.10	4.64	.174	.230	6.81	.075	11.34	-----	.36	.0093	.0162	.778	-----	.025
.10	5.28	.250	.464	7.74	.084	14.80	8.91	.26	.0072	.0180	1.02	.611	.018
.20	0	0	-.278	0	-----	3.38	7.07	.31	-----	-----	.292	.611	.027
.20	.63	.005	-.265	.83	.073	3.53	-----	.29	.9975	.0249	.305	-----	.025
.20	1.06	.014	-.237	1.38	.074	3.78	7.07	.30	.3554	.0252	.326	.611	.026
.20	1.48	.021	-.226	1.93	.056	3.86	-----	.32	.1833	.0192	.333	-----	.028
.20	2.11	.033	-.212	2.76	.043	4.00	6.87	.33	.0898	.0148	.345	.593	.029
.20	2.53	.049	-.194	3.31	.045	4.17	-----	.29	.0624	.0153	.360	-----	.025
.20	3.17	.080	-.092	4.14	.047	5.03	7.12	.26	.0399	.0160	.434	.615	.022
.20	3.59	.115	0	4.69	.052	5.79	-----	.24	.0311	.0179	.500	-----	.021
.20	4.22	.174	.200	5.52	.057	7.33	7.52	.17	.0223	.0195	.633	.650	.014
.20	4.64	.219	.251	6.07	.059	7.68	-----	.12	.0186	.0203	.663	-----	.011
.20	5.28	.290	.622	6.90	.061	10.26	-----	.05	.0144	.0208	.886	-----	.005
.30	0	0	-.336	0	-----	3.37	6.89	.16	-----	-----	.333	.682	.016
.30	.63	.005	-.321	.77	.056	3.45	-----	.12	1.4963	.0249	.341	-----	.012
.30	1.06	.021	-.288	1.29	.064	3.52	6.98	.15	.5332	.0377	.358	.690	.015
.30	1.48	.028	-.271	1.80	.057	3.71	-----	.18	.2750	.0257	.367	-----	.018
.30	2.11	.047	-.259	2.58	.047	3.79	6.79	.15	.1348	.0211	.375	.671	.015
.30	2.53	.061	-.216	3.09	.042	4.01	-----	.16	.0956	.0190	.396	-----	.015
.30	3.17	.105	-.080	3.87	.047	4.67	6.89	.13	.0599	.0212	.462	.682	.012
.30	3.59	.139	.052	4.38	.048	5.21	-----	.10	.0466	.0216	.515	-----	.010
.30	4.22	.204	.267	5.16	.051	6.28	7.25	.05	.0337	.0229	.621	.717	.005
.30	4.64	.254	.334	5.67	.053	7.01	-----	.03	.0278	.0236	.693	-----	.003
.30	5.28	.306	.698	6.45	.049	8.12	-----	-.01	.0216	.0220	.805	-----	-.001

TABLE VII.-- Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION OF
FINENESS RATIO 12 WITHOUT CENE STRIPS

C_{A_Q}	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(\Delta)}^{1/3}$	$\frac{z}{(\Delta)}^{1/3}$	$\frac{h}{(\Delta)}^{1/3}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$	
$\tau = 8^\circ$ - Concluded														
.10	0	0	-0.362	C	-----	3.35	6.81	0.05	-----	-----	0.364	0.742	0.005	
.10	.63	.007	-0.350	.74	0.064	3.41	-----	.05	1.9950	0.0349	.371	-----	.006	
.10	1.06	.026	-0.311	1.23	.086	3.55	6.81	.05	.7188	0.0467	.586	0.742	.006	
.10	1.48	.035	-0.289	1.72	.064	3.62	-----	.09	.3666	0.0348	.394	-----	.009	
.10	2.11	.061	-0.224	2.46	.051	3.83	6.57	.09	.1797	0.0274	.417	.715	.010	
.10	2.53	.076	-0.212	2.96	.045	3.90	-----	.07	.1218	0.0243	.424	-----	.008	
.40	3.17	.122	-0.055	3.70	.045	4.42	6.78	.04	.0793	0.0244	.481	.738	.005	
.40	3.59	.160	.053	4.19	.046	4.77	-----	.03	.0622	0.0249	.519	-----	.003	
.40	4.22	.222	.302	4.93	.046	5.55	7.07	0	.0449	0.0248	.604	.770	0	
.40	4.64	.266	.162	5.42	.046	6.04	-----	.04	.0371	0.0247	.557	-----	-.005	
.40	5.28	.341	.789	6.16	.045	7.01	-----	.04	.0288	0.0245	.763	-----	-.005	
.50	0	0	-0.352	0	-----	3.36	6.79	-.04	-----	-----	.394	.796	-.004	
.50	.63	.006	-0.342	.72	0.048	3.40	-----	-.03	2.4928	0.0299	.398	-----	-.004	
.50	1.06	.032	-0.301	1.18	.091	3.51	6.85	-.02	.8985	0.0575	.411	.803	-.003	
.50	1.48	.047	-0.287	1.66	.068	3.54	-----	0	.4583	0.0431	.415	-----	0	
.50	2.11	.074	-0.243	2.37	.057	3.65	6.61	0	.2246	0.0319	.428	.775	0	
.50	2.53	.094	-0.184	2.84	.047	3.81	-----	-.01	.1560	0.0293	.447	-----	-.001	
.50	3.17	.143	-.006	3.55	.045	4.25	6.72	-.03	.0999	0.0286	.498	.788	-.004	
.50	3.59	.188	.139	4.03	.046	4.61	-----	-.05	.0777	0.0292	.540	-----	-.006	
.50	4.22	.259	.414	4.74	.046	5.21	6.93	-.08	.0562	0.0291	.611	.812	-.009	
$\tau = 12^\circ$														
0	0	0	0	0	0	0	0	0	0	0.0050	.500	0	.164	.105
0	.63	.001	0	0	0	0	0	0	0	.0018	.500	0	.095	.108
0	1.06	.002	0	0	0	0	0	0	0	.0018	.500	0	.108	.108
0	1.48	.004	0	0	0	0	0	0	0	.0018	.500	0	.134	.104
0	2.11	.005	0	0	0	0	0	0	0	.0016	.500	0	0	.102
0	3.17	.014	0	0	0	0	0	0	0	.0028	.500	0	.152	.094
0	3.59	.024	.007	0	0	0	0	0	0	.0037	.704	0	0	.091
0	4.22	.059	.037	0	0	0	0	0	0	.0065	.949	.343	.081	0
0	4.64	.106	.118	0	0	0	0	0	0	.0098	1.298	0	.072	0
0	5.28	.183	.312	0	0	0	0	0	0	.0132	.716	.653	0	.059
.10	0	0	-0.185	0	-----	3.21	6.54	.79	-----	-----	.220	.449	.054	
.10	.63	.005	-0.184	.93	.116	3.28	-----	.79	.4988	0.0249	.223	-----	.054	
.10	1.06	.011	-0.180	1.55	.092	3.40	6.39	.83	.1797	0.0198	.233	.438	.057	
.10	1.48	.015	-0.174	2.17	.064	5.62	-----	.86	.0917	0.0137	.248	-----	.059	
.10	2.11	.027	-0.153	3.10	.056	4.11	6.41	.82	.0449	0.0121	.252	.440	.056	
.10	2.53	.042	-0.113	3.72	.061	5.01	-----	.77	.0312	0.0131	.243	-----	.053	
.10	3.17	.073	-.050	4.65	.068	6.33	6.44	.69	.0200	0.0146	.434	.441	.047	
.10	3.59	.103	0	5.26	.074	7.29	-----	.65	.0155	0.0160	.500	-----	.045	
.10	4.22	.150	.133	6.19	.078	9.52	7.73	.56	.0112	0.0168	.553	.530	.038	
.10	4.64	.190	.257	6.81	.082	10.66	-----	.51	.0093	0.0176	.731	-----	.035	
.10	5.26	.271	.474	7.74	.092	11.50	-----	.40	.0072	0.0195	.788	-----	.028	
.20	0	0	0	-0.300	0	-----	3.16	6.26	.41	-----	-----	.273	.540	.036
.20	.63	.006	-0.294	.83	.087	3.24	-----	.41	.9975	0.0299	.280	-----	.036	
.20	1.06	.021	-0.283	1.38	.110	3.36	6.42	.45	.3594	0.0377	.290	.554	.039	
.20	1.48	.028	-0.279	1.93	.075	3.40	-----	.48	.1833	0.0257	.294	-----	.041	
.20	2.11	.046	-0.243	2.76	.061	3.78	6.34	.45	.0898	0.0207	.326	.547	.039	
.20	2.53	.063	-0.180	3.31	.058	4.32	-----	.41	.0624	0.0197	.373	-----	.036	
.20	3.17	.105	-.055	4.14	.061	5.35	6.34	.35	.0399	0.0210	.462	.547	.030	
.20	3.59	.137	0.26	4.69	.062	5.99	-----	.31	.0311	0.0213	.517	-----	.027	
.20	4.22	.200	.216	5.52	.066	7.36	6.97	.28	.0225	0.0225	.636	.602	.024	
.20	4.64	.242	.357	6.07	.066	8.27	-----	.24	.0186	0.0225	.714	-----	.020	
.20	5.28	.306	.638	6.90	.064	10.01	-----	.19	.0144	0.0220	.864	-----	.016	

TABLE VII - Continued
 EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION
 OF FINENESS RATIO 12 WITH CHINE STRIPS

C_{DQ}	C_{VQ}	C_{RQ}	C_{MQ}	$C_{V\Delta}$	$C_{D\Delta}$	$\frac{x}{(A)}^{1/3}$	$\frac{l}{(A)}^{1/3}$	$\frac{h}{(A)}^{1/3}$	C_{LQ}	C_{DQ}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 12^\circ$ - Concluded													
.30	0	0	-0.373	0	-----	3.15	6.22	0.21	-----	0.311	0.615	0.021	
.30	.63	.008	-.362	.77	0.089	3.22	6.18	.25	1.4963	0.0399	.318	-----	.021
.30	1.06	.028	-.356	1.29	.112	3.28	6.18	.25	.5392	0.0503	.324	.611	.022
.30	1.48	.040	-.342	1.80	.082	3.35	6.18	.25	.2750	0.0367	.331	-----	.026
.30	2.11	.059	-.289	2.58	.059	3.64	6.18	.25	.1248	0.0265	.360	.611	.024
.30	2.53	.078	-.207	3.09	.054	4.05	6.18	.21	.0936	0.0243	.400	-----	.021
.30	3.17	.127	-.040	3.87	.057	4.87	6.11	.17	.0599	0.0254	.481	.604	.016
.30	3.59	.169	.067	4.38	.059	5.36	6.18	.14	.0456	0.0263	.530	-----	.014
.30	4.22	.233	.295	5.16	.059	6.34	6.57	.11	.0357	0.0262	.627	.650	.011
.30	4.64	.280	.464	5.67	.058	7.03	6.18	.09	.0278	0.0260	.595	-----	.009
.30	5.28	.350	.779	6.45	.056	8.25	6.18	.05	.0216	0.0252	.816	-----	.005
.40	0	0	-.403	0	-----	3.19	6.20	.06	-----	-----	.347	.675	.007
.40	.63	.007	-.355	.74	.064	3.24	6.18	.07	1.9950	0.0349	.352	-----	.008
.40	1.06	.038	-.384	1.23	.126	3.29	6.18	.11	.7188	0.0683	.358	.673	.012
.40	1.48	.052	-.371	1.72	.088	3.35	6.18	.13	.3666	0.0477	.364	-----	.014
.40	2.11	.075	-.294	2.46	.062	5.62	6.13	.10	.1797	0.0357	.394	.667	.011
.40	2.53	.099	-.180	2.96	.057	4.01	6.18	.07	.1248	0.0309	.436	-----	.008
.40	3.17	.148	.007	3.70	.054	4.61	6.16	.05	.0799	0.0295	.502	.671	.005
.40	3.59	.193	.119	4.19	.055	4.96	6.18	.02	.0622	0.0300	.540	-----	.002
.40	4.22	.251	.337	4.93	.052	5.62	6.31	.02	.0449	0.0282	.612	.687	.002
.40	4.64	.289	.516	5.42	.049	6.15	6.18	.01	.0371	0.0268	.669	-----	.001
.40	5.28	.348	.614	6.16	.046	6.97	6.18	.01	.0268	0.0250	.758	-----	-.001
.50	0	0	-.398	0	-----	3.23	6.24	-.06	-----	-----	.379	.731	-.007
.50	.63	.009	-.394	.71	.071	3.25	6.18	-.07	2.4958	0.0449	.381	-----	-.008
.50	1.06	.046	-.386	1.18	.131	3.29	6.18	-.03	.8585	0.0827	.386	.724	-.004
.50	1.48	.061	-.368	1.66	.089	3.34	6.18	0	.4583	0.0559	.392	-----	0
.50	2.11	.092	-.267	2.37	.066	3.60	6.18	0	.2246	0.0413	.422	.724	-.001
.50	2.53	.113	-.170	2.84	.056	3.85	6.18	-.03	.1560	0.0353	.451	-----	-.004
.50	3.17	.169	-.004	3.55	.054	4.25	6.06	-.03	.0999	0.0337	.498	.710	-.005
.50	3.59	.216	.130	4.03	.053	4.57	6.18	-.06	.0777	0.0336	.536	-----	-.006
.50	4.22	.280	.389	4.74	.050	5.17	6.18	-.08	.0562	0.0314	.606	.724	-.007
$\tau = 16^\circ$													
0	0	0	0	0	-----	-----	-----	-----	-----	-----	.124	.139	
0	.63	.001	-.004	-----	-----	-----	-----	-----	-----	-----	.142	-----	
0	1.06	.001	-.004	-----	-----	-----	-----	-----	0	0.0018	-----	.111	.143
0	1.48	.001	-.007	-----	-----	-----	-----	-----	0	0.0009	-----	.090	.143
0	2.11	.002	-.004	-----	-----	-----	-----	-----	0	0.0009	-----	.124	.145
0	2.53	.002	-.004	-----	-----	-----	-----	-----	0	0.0006	-----	.1422	.146
0	3.17	.007	-.023	-----	-----	-----	-----	-----	0	0.0016	-----	.155	.134
0	3.59	.021	.012	-----	-----	-----	-----	-----	0	0.0033	-----	.816	.123
0	4.22	.056	.027	-----	-----	-----	-----	-----	0	0.0063	-----	.765	.105
0	4.64	.094	.006	-----	-----	-----	-----	-----	0	0.0087	-----	.535	.094
0	5.28	.174	.241	-----	-----	-----	-----	-----	0	0.0125	1.249	-----	.079
.10	0	0	-.196	0	-----	2.91	5.87	1.01	-----	-----	.199	.403	.069
.10	.63	.007	-.206	.93	.162	2.75	5.66	1.01	.4988	.0349	.189	-----	.069
.10	1.06	.014	-.197	1.55	.117	3.03	5.66	1.03	.1797	.0252	.208	.388	.071
.10	1.48	.019	-.197	2.17	.081	3.12	5.98	1.07	.0917	.0174	.214	-----	.073
.10	2.11	.035	-.194	3.10	.073	3.34	5.98	1.07	.0449	.0157	.229	.410	.073
.10	2.53	.052	-.154	3.72	.075	4.30	5.98	1.00	.0312	.0162	.294	-----	.068
.10	3.17	.075	-.129	4.65	.070	4.91	6.23	.95	.0200	.0150	.337	.427	.065
.10	3.59	.107	0	5.26	.077	7.29	6.18	.84	.0155	.0166	.500	-----	.058
.10	4.22	.153	.129	6.19	.080	9.30	6.18	.75	.0112	.0172	.658	-----	.051
.10	4.64	.193	.216	6.81	.085	10.26	6.18	.71	.0093	.0179	.703	-----	.049
.10	5.28	.254	.414	7.74	.085	11.46	6.18	.63	.0072	.0183	.786	-----	.045

TABLE VII - Continued
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION OF
FINENESS RATIO 12 WITHOUT CHINE STRIPS

$C_{\Delta Q}$	C_{VQ}	C_{RQ}	C_{MQ}	$C_{V\Delta}$	$C_{D\Delta}$	$\frac{x}{(A)}^{1/3}$	$\frac{l}{(A)}^{1/3}$	$\frac{h}{(A)}^{1/3}$	C_{LQ}	C_{DQ}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 16^\circ$ - Concluded													
.20	0	0	-0.320	0	-----	2.94	5.73	0.53	-----	0.0449	0.254	0.494	0.046
.20	.63	.009	-.326	.83	0.131	2.92	-----	.53	0.9975	0.0449	.252	-----	.046
.20	1.06	.025	-.321	1.38	.131	3.02	5.60	.50	.3594	0.0449	.261	.484	.052
.20	1.48	.033	-.306	1.93	.088	3.18	-----	.62	.1833	0.0302	.275	-----	.053
.20	2.11	.054	-.237	2.76	.071	3.83	5.73	.56	.0895	0.0243	.331	.494	.049
.20	2.53	.076	-.186	3.31	.069	4.30	-----	.54	.0624	0.0237	.377	-----	.047
.20	3.17	.120	-.086	4.14	.070	5.13	5.97	.49	.0399	0.0240	.443	.516	.042
.20	3.59	.155	0	4.69	.071	5.79	-----	.47	.0311	0.0241	.500	-----	.041
.20	4.22	.207	.150	5.52	.068	7.02	-----	.42	.0225	0.0232	.606	-----	.036
.20	4.64	.247	.302	6.07	.067	7.76	-----	.39	.0186	0.0229	.672	-----	.033
.20	5.28	.306	.547	6.90	.064	9.17	-----	.38	.0144	0.0220	.792	-----	.035
.30	0	0	-.387	0	-----	3.04	5.82	.26	-----	-----	.301	.575	.026
.30	.63	.012	-.394	.77	.134	3.04	-----	.28	1.4963	.0599	.301	-----	.027
.30	1.06	.026	-.403	1.29	.144	3.04	5.64	.34	.5331	.0647	.301	.558	.033
.30	1.48	.045	-.373	1.80	.098	3.22	-----	.35	.2750	.0440	.318	-----	.035
.30	2.11	.071	-.265	2.56	.071	3.65	5.79	.31	.1348	.0329	.362	.572	.031
.30	2.53	.098	-.210	3.09	.068	4.05	-----	.27	.0936	.0306	.400	-----	.027
.30	3.17	.197	-.076	3.87	.088	4.71	5.97	.26	.0599	.0393	.466	.590	.026
.30	3.59	.193	.104	4.38	.067	5.50	-----	.26	.0466	.0300	.544	-----	.025
.30	4.22	.243	.222	5.16	.061	5.98	-----	.24	.0337	.0273	.592	-----	.023
.30	4.64	.284	.322	5.67	.059	6.36	-----	.22	.0278	.0264	.629	-----	.022
.30	5.28	.343	.587	6.45	.055	7.35	-----	.21	.0216	.0247	.727	-----	.021
.40	0	0	-.414	0	-----	3.13	5.76	.07	-----	-----	.341	.627	.008
.40	.63	.014	-.425	.74	.129	3.12	-----	.09	1.9950	.0698	.339	-----	.010
.40	1.06	.047	-.436	1.23	.156	3.12	5.58	.15	.7188	.0845	.339	.607	.017
.40	1.48	.060	-.403	1.72	.101	3.24	-----	.17	.3666	.0550	.352	-----	.019
.40	2.11	.087	-.281	2.46	.072	3.66	5.65	.13	.1797	.0391	.398	.615	.014
.40	2.53	.118	-.196	2.96	.068	3.95	-----	.11	.1246	.0368	.130	-----	.012
.40	3.17	.179	-.046	3.70	.066	4.46	5.74	.11	.0799	.0357	.485	.625	.012
.40	3.59	.223	.077	4.19	.064	4.83	-----	.10	.0622	.0347	.525	-----	.011
.40	4.22	.289	.322	4.93	.060	5.53	-----	.09	.0449	.0325	.602	-----	.010
.40	4.64	.329	.496	5.42	.056	6.02	-----	.07	.0371	.0305	.655	-----	.008
.40	5.28	.394	.749	6.16	.052	6.66	-----	.09	.0288	.0283	.729	-----	.010
.50	0	0	-.411	0	-----	3.18	5.72	-.07	-----	-----	.373	.671	-.009
.50	.63	.018	-.425	.71	.143	3.17	-----	-.04	2.4938	.0898	.371	-----	-.005
.50	1.06	.061	-.441	1.18	.174	3.15	5.69	.02	.8985	.1096	.369	.667	.002
.50	1.48	.075	-.399	1.66	.111	3.25	-----	.05	.4583	.0697	.381	-----	.004
.50	2.11	.109	-.357	2.37	.078	3.38	5.77	0	.2246	.0430	.396	.676	0
.50	2.53	.143	-.163	2.84	.071	3.86	-----	0	.1560	.0446	.453	-----	0
.50	3.17	.220	.007	3.55	.067	4.28	5.72	-.01	.0999	.0419	.502	.571	-.001
.50	3.59	.256	.149	4.05	.065	4.61	-----	-.01	.0777	.0440	.540	-----	-.001
.50	4.22	.315	.434	4.74	.061	5.22	-----	-.02	.0362	.0387	.612	-----	-.002
$\tau = 20^\circ$													
0	0	0	0	0	-----	-----	-----	-----	-----	-----	-----	-----	.122
0	.63	.001	-.009	-----	-----	-----	-----	-----	0	.0050	-2.562	-----	.168
0	1.06	.002	-.009	-----	-----	-----	-----	-----	0	.0035	-1.468	.099	.168
0	1.48	.003	-.010	-----	-----	-----	-----	-----	0	.0027	-1.014	-----	.169
0	2.11	.005	-.010	-----	-----	-----	-----	-----	0	.0022	-.336	.088	.170
0	2.53	.007	-.010	-----	-----	-----	-----	-----	0	.0022	-.123	-----	.170
0	3.17	.008	-.010	-----	-----	-----	-----	-----	0	.0016	-.030	.072	.170
0	3.59	.009	-.013	-----	-----	-----	-----	-----	0	.0014	-.123	-----	.172
0	4.22	.006	-.022	-----	-----	-----	-----	-----	0	.0007	-.387	-----	.178
0	4.64	.054	-.010	-----	-----	-----	-----	-----	0	.0050	.419	-----	.119
0	5.22	.099	.021	-----	-----	-----	-----	-----	0	.0071	.595	-----	.106

TABLE VII - Concluded

EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION OF
FINENESS RATIO 12 WITHOUT CHINE STRIPS

$c_{\Delta Q}$	c_{VQ}	c_{RQ}	c_{M_Q}	$c_{V\Delta}$	$c_{D\Delta}$	$\frac{x}{(\frac{\Delta}{w})^{1/3}}$	$\frac{z}{(\frac{\Delta}{w})^{1/3}}$	$\frac{h}{(\frac{\Delta}{w})^{1/3}}$	c_{LQ}	c_{DQ}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$T = 20^\circ$ - Concluded													
.10	0	0	-0.190	0	-----	2.91	5.49	1.23	-----	-----	0.199	0.376	0.085
.10	.63	.012	-.206	.93	0.278	2.75	-----	1.27	0.4988	0.0599	.189	-----	.087
.20	1.06	.024	-.201	1.55	.200	3.06	5.25	1.34	.1797	.0431	.210	.360	.092
.10	1.48	.026	-.185	2.17	.111	3.43	-----	1.31	.0917	.0258	.235	-----	.090
.10	2.11	.049	-.165	3.10	.102	4.05	5.56	1.25	.0449	.0220	.278	.381	.086
.10	2.53	.066	-.147	3.72	.096	4.57	-----	1.21	.0312	.0206	.314	-----	.083
.10	3.17	.101	-.090	4.65	.094	5.79	5.67	1.18	.0200	.0202	.396	.388	.081
.10	3.59	.129	-.050	5.26	.093	6.52	-----	1.14	.0155	.0201	.447	-----	.078
.10	4.22	.179	-.032	6.19	.093	7.76	-----	1.07	.0112	.0201	.532	-----	.074
.10	4.64	.200	-.088	6.81	.066	8.47	-----	1.05	.0093	.0186	.561	-----	.072
.10	5.28	.249	-.209	7.74	.083	9.55	-----	1.04	.0072	.0179	.655	-----	.071
.20	0	0	-.303	0	-----	3.05	5.42	.64	-----	-----	.263	.468	.055
.20	.63	.015	-.326	.83	.219	2.90	-----	.68	.9975	.0748	.250	-----	.059
.20	1.06	.033	-.350	1.38	.175	2.96	5.28	.74	.5594	.0593	.256	.456	.064
.20	1.48	.042	-.300	1.93	.113	3.24	-----	.73	.1833	.0385	.280	-----	.062
.20	2.11	.071	-.241	2.76	.093	3.80	5.36	.68	.0898	.0319	.328	.464	.059
.20	2.53	.099	-.210	3.31	.090	4.17	-----	.67	.0624	.0309	.360	-----	.058
.20	3.17	.150	-.113	4.14	.087	4.98	5.52	.63	.0399	.0299	.430	.477	.054
.20	3.59	.183	-.040	4.69	.083	5.52	-----	.63	.0311	.0284	.477	-----	.054
.20	4.22	.226	-.068	5.52	.074	6.23	-----	.61	.0225	.0254	.538	-----	.052
.20	4.64	.268	-.180	6.07	.073	6.89	-----	.61	.0186	.0249	.595	-----	.052
.20	5.28	.322	-.322	6.90	.068	7.65	-----	.62	.0244	.0231	.661	-----	.053
.30	0	0	-.383	0	-----	3.02	5.43	.31	-----	-----	.299	.537	.031
.30	.63	.021	-.403	.77	.234	2.97	-----	.36	1.4963	.1047	.294	-----	.035
.30	1.06	.049	-.414	1.29	.197	2.97	5.32	.41	.5391	.0881	.294	.526	.041
.30	1.48	.059	-.377	1.80	.121	3.20	-----	.40	.2750	.0541	.316	-----	.040
.30	2.11	.094	-.300	2.58	.094	3.62	5.36	.37	.1348	.0422	.358	.530	.037
.30	2.53	.132	-.243	3.09	.092	3.95	-----	.37	.0936	.0412	.390	-----	.036
.30	3.17	.188	-.143	3.87	.083	4.44	5.47	.37	.0599	.0375	.439	.540	.037
.30	3.59	.220	-.040	4.58	.076	4.89	-----	.37	.0466	.0342	.483	-----	.037
.30	4.22	.254	-.082	5.16	.064	5.38	-----	.41	.0337	.0285	.532	-----	.041
.30	4.64	.291	-.189	5.67	.060	5.81	-----	.41	.0278	.0270	.574	-----	.041
.30	5.28	.358	-.348	6.45	.054	6.36	-----	.45	.0216	.0243	.629	-----	.044
.40	0	0	-.436	0	-----	3.01	5.27	.09	-----	-----	.328	.574	.010
.40	.63	.028	-.445	.74	.257	3.01	-----	.15	1.9950	.1397	.328	-----	.016
.40	1.06	.065	-.455	1.23	.215	3.04	5.34	.21	.7188	.1168	.331	.581	.022
.40	1.48	.075	-.403	1.72	.127	3.22	-----	.21	.3666	.0687	.350	-----	.022
.40	2.11	.113	-.310	2.46	.094	3.58	5.39	.21	.1797	.0508	.390	.586	.022
.40	2.53	.157	-.253	2.96	.090	3.80	-----	.21	.1248	.0490	.413	-----	.022
.40	3.17	.226	-.138	3.70	.083	4.19	5.35	.21	.0799	.0451	.456	.583	.022
.40	3.59	.265	-.028	4.19	.076	4.52	-----	.21	.0622	.0409	.492	-----	.023
.40	4.22	.315	-.149	4.93	.065	4.03	-----	.23	.0449	.0354	.547	-----	.025
.40	4.64	.343	-.261	5.42	.059	5.31	-----	.25	.0371	.0318	.578	-----	.027
.40	5.28	.395	-.454	6.16	.052	5.80	-----	.31	.0288	.0284	.631	-----	.034
.50	0	0	-.403	0	-----	3.18	5.36	-.10	-----	-----	.373	.629	-.012
.50	.63	.028	-.430	.71	.222	3.13	-----	-.03	2.4935	.1397	.367	-----	-.003
.50	1.06	.078	-.450	1.18	.223	3.13	5.39	.04	.8985	.1402	.367	.632	-.005
.50	1.48	.089	-.394	1.66	.130	3.27	-----	.03	.1583	.0816	.383	-----	-.004
.50	2.11	.134	-.284	2.37	.096	3.57	5.39	.03	.2246	.0602	.419	.632	-.004
.50	2.53	.179	-.216	2.84	.089	3.76	-----	.04	.1560	.0558	.441	-----	-.005
.50	3.17	.266	-.070	3.55	.084	4.10	5.27	.05	.0999	.0531	.481	.618	-.006
.50	3.59	.310	-.027	4.03	.077	4.32	-----	.05	.0777	.0462	.506	-----	-.006
.50	4.22	.367	-.241	4.74	.065	4.77	-----	.10	.0562	.0412	.559	-----	-.012

TABLE VIII
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION OF FINENESS
RATIO 6 WITH CHINE STRIPS BUT WITHOUT TAIL CONE

C_{A_Q}	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_Δ}	C_{Δ}	$\frac{x}{(\Delta)^{1/3}}$	$\frac{z}{(\Delta)^{1/3}}$	$\frac{h}{(\Delta)^{1/3}}$	C_{L_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{z}{L}$	$\frac{h}{L}$
$\tau = 8^\circ$													
.20	0	0	-0.105	0	----	2.04	4.96	0.28	----	0.313	0.748	0.042	
.20	.63	.034	-.069	.83	0.058	2.22	----	.23	0.9975	0.0200	.335	----	.035
.20	1.06	.019	-.036	1.38	.099	2.69	5.18	.23	----	.0341	.406	.781	.035
.20	1.48	.025	-.015	1.93	.067	2.56	----	.26	.1833	.0229	.432	----	.039
.20	2.11	.045	.055	2.76	.058	3.44	5.13	.23	.0895	.0202	.520	.774	.035
.20	2.55	.063	.147	3.31	.058	4.21	----	.20	.0624	.0197	.635	----	.031
.20	3.17	.071	.209	4.14	.041	4.70	4.96	.27	.0399	.0142	.709	.748	.040
.20	3.59	.075	.200	4.69	.035	4.62	----	.34	.0311	.0116	.698	----	.051
.20	4.22	.081	.200	5.52	.026	4.62	4.32	.40	.0225	.0091	.698	.651	.060
.20	4.64	.086	.200	6.07	.023	4.60	----	.43	.0186	.0080	.695	----	.065
.20	5.28	.094	.200	6.90	.020	4.60	3.90	.46	.0144	.0068	.695	.589	.070
.20	6.33	.113	.214	8.28	.018	4.70	5.66	.49	.0100	.0057	.709	.552	.074
.20	7.39	.139	.243	9.66	.015	4.90	5.51	.52	.0073	.0051	.739	.529	.079
.20	8.44	.167	.279	11.04	.015	5.14	5.41	.53	.0056	.0047	.776	.528	.080
.20	9.50	.199	.339	12.42	.012	5.56	5.41	.53	.0044	.0044	.839	.515	.080
.20	10.55	.233	.474	13.80	.012	6.51	5.41	.54	.0036	.0042	.983	.515	.082
.20	11.61	.275	.154	15.13	.012	6.27	5.36	.55	.0030	.0041	.946	.507	.083
.20	12.66	.320	.504	16.56	.012	6.54	5.26	.54	.0025	.0038	.987	.495	.082
.20	13.72	.367	.590	17.94	.012	7.03	5.36	.56	.0021	.0040	1.061	.507	.085
.40	0	0	-.132	0	----	1.92	4.55	.05	----	----	.365	.866	.010
.40	.63	.005	-.105	.74	.046	2.01	----	.02	1.9950	.0249	.383	----	.004
.40	1.06	.059	-.015	1.25	.129	2.51	4.75	.01	.7188	.0702	.459	.903	.002
.40	1.48	.052	.011	1.72	.088	2.40	----	.04	.3666	.0477	.457	----	.007
.40	2.11	.077	.095	2.46	.064	2.68	4.71	.02	.1797	.0346	.509	.896	.004
.40	2.53	.110	.244	2.96	.063	3.16	----	.03	.1248	.0343	.602	----	.006
.40	3.17	.181	.521	3.70	.052	4.04	4.93	.09	.0799	.0262	.769	.937	.017
.40	3.59	.183	.564	4.19	.052	4.13	----	.02	.0622	.0284	.795	----	.004
.40	4.22	.162	.515	4.93	.053	4.04	4.17	.15	.0449	.0181	.769	.792	.028
.40	4.64	.158	.479	5.42	.026	3.92	----	.20	.0371	.0143	.746	----	.038
.40	5.28	.156	.424	6.16	.020	3.75	3.58	.28	.0285	.0112	.713	.681	.053
.40	6.33	.168	.394	7.39	.015	3.63	3.29	.34	.0200	.0084	.691	.626	.064
.40	7.59	.183	.379	8.52	.012	3.59	3.12	.37	.0147	.0068	.683	.592	.070
.40	8.44	.212	.389	9.85	.011	3.61	2.94	.40	.0112	.0059	.687	.559	.075

TABLE IX
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION OF FINENESS
RATIO 9 WITH CHINE STRIPS BUT WITHOUT TAIL CONE

C_{A_Q}	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{V_Δ}	C_{D_Δ}	$\frac{x}{(\frac{L}{w})^{1/3}}$	$\frac{l}{(\frac{L}{w})^{1/3}}$	$\frac{h}{(\frac{L}{w})^{1/3}}$	C_{I_Q}	C_{D_Q}	$\frac{x}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 8^\circ$													
.20	0	0	-0.196	0	-----	2.11	5.54	0.28	-----	0.0200	0.262	-----	0.032
.20	.63	.004	-.174	.83	0.058	2.23	-----	.24	0.9975	0.0200	-----	-----	.029
.20	1.06	.017	-.154	1.38	.089	2.58	5.67	.24	3594	.0305	.303	.666	.029
.20	1.48	.023	-.107	1.93	.062	2.82	-----	.27	.1833	.0211	.331	-----	.031
.20	2.11	.034	-.063	2.76	.045	3.19	5.47	.27	.0898	.0153	.375	.643	.031
.20	2.53	.042	0	3.31	.038	3.73	-----	.24	.0624	.0131	.438	-----	.029
.20	3.17	.050	.055	4.14	.029	4.20	5.18	.29	.0399	.0100	.493	.608	.034
.20	3.59	.056	.057	4.69	.025	4.29	-----	.34	.0311	.0087	.504	-----	.040
.20	4.22	.064	.056	5.52	.021	4.20	4.51	.40	.0225	.0072	.493	.531	.047
.20	4.61	.067	.047	6.07	.018	4.21	-----	.43	.0186	.0062	.494	-----	.050
.20	5.28	.072	.037	6.90	.015	4.03	4.07	.46	.0144	.0052	.473	.479	.054
.20	6.33	.084	.007	8.28	.012	3.73	3.73	.51	.0100	.0042	.438	.438	.060
.20	7.39	.095	0	9.66	.010	3.73	3.51	.53	.0073	.0035	.438	.412	.062
.20	8.44	.112	-.013	11.04	.009	3.64	3.56	.55	.0056	.0031	.427	.395	.065
.20	9.50	.134	-.022	12.42	.009	3.61	3.23	.56	.0044	.0029	.427	.380	.066
.20	10.55	.155	-.017	13.80	.008	3.61	3.19	.57	.0036	.0028	.424	.375	.067
.20	11.61	.179	-.007	15.18	.008	3.68	3.07	.58	.0030	.0026	.432	.360	.068
.20	12.66	.203	-.007	16.56	.007	3.68	3.02	.58	.0025	.0025	.432	.355	.068
.20	13.72	.224	-.007	17.94	.007	3.68	2.97	.58	.0021	.0024	.432	.349	.068
.40	0	0	-.253	0	-----	2.10	5.31	.04	-----	-----	.311	.786	.007
.40	.63	.009	-.251	.74	.083	2.11	-----	.03	1.9950	.0449	.523	-----	.004
.40	1.06	.034	-.170	1.23	.113	2.39	5.37	.03	.7188	.0611	.354	.796	.004
.40	1.48	.043	-.139	1.72	.073	2.49	-----	.06	.3666	.0394	.369	-----	.009
.40	2.11	.060	-.064	2.46	.050	2.74	5.24	.06	.1797	.0270	.466	.776	.009
.40	2.53	.079	.050	2.96	.045	3.14	-----	.04	.1248	.0246	.464	-----	.005
.40	3.17	.103	.251	3.70	.038	3.80	5.24	.03	.0799	.0206	.562	.776	.004
.40	3.59	.111	.311	4.19	.032	3.99	-----	.08	.0622	.0172	.591	-----	.011
.40	4.22	.122	.311	4.93	.025	3.97	4.56	.17	.0449	.0137	.588	.675	.025
.40	4.64	.128	.275	5.42	.020	3.86	-----	.22	.0371	.0110	.571	-----	.032
.40	5.28	.122	.228	6.16	.016	3.70	3.95	.27	.0268	.0088	.548	.585	.040
.40	6.33	.135	.153	7.39	.012	3.47	3.53	.34	.0200	.0067	.513	.523	.051
.40	7.39	.144	.097	8.62	.010	3.27	3.26	.39	.0147	.0053	.484	.482	.057
.40	8.44	.164	.060	9.85	.009	3.16	3.08	.42	.0112	.0046	.467	.456	.062

TABLE X
EXPERIMENTAL HYDRODYNAMIC DATA FOR A BODY OF REVOLUTION OF FINENESS
RATIO 12 WITH CHINE STRIPS BUT WITHOUT TAIL CONE

$C_{\Delta Q}$	C_{V_Q}	C_{R_Q}	C_{M_Q}	C_{v_Δ}	C_{D_Δ}	$\frac{x}{(\frac{h}{w})^{1/3}}$	$\frac{l}{(\frac{h}{w})^{1/3}}$	$\frac{h}{(\frac{h}{w})^{1/3}}$	C_{-Q}	C_{D_Q}	$\frac{y}{L}$	$\frac{l}{L}$	$\frac{h}{L}$
$\tau = 8^\circ$													
.20	0	0	-0.253	0	----	2.24	6.03	0.31	----	0.219	0.589	0.030	
.20	.63	.005	-.242	.83	0.073	2.31	----	.30	0.9975	0.0249	.226	----	.029
.20	1.06	.014	-.205	1.38	0.074	2.66	6.03	.30	.5594	0.0252	.250	.589	.029
.20	1.45	.022	-.183	1.93	0.059	2.80	----	.29	.1833	0.0202	.274	----	.029
.20	2.11	.032	-.155	2.76	0.042	3.12	5.84	.29	.0896	0.0144	.305	.571	.029
.20	2.53	.039	-.111	3.31	0.056	3.49	----	.30	.0624	0.0122	.341	----	.029
.20	3.17	.049	-.072	4.11	0.029	4.15	5.81	.31	.0399	0.0096	.406	.568	.030
.20	3.59	.054	-.014	4.69	0.025	4.31	----	.35	.0311	0.0094	.421	----	.035
.20	4.22	.060	-.019	5.52	0.020	4.28	5.08	.42	.0225	0.0067	.418	.496	.041
.20	4.64	.063	-.031	6.07	0.017	4.15	----	.46	.0186	0.0058	.406	----	.045
.20	5.28	.070	-.049	6.90	0.015	4.03	4.42	.51	.0144	0.0050	.394	.431	.050
.20	6.33	.074	-.088	8.25	0.011	3.69	3.97	.56	.0100	0.0027	.361	.385	.055
.20	7.39	.081	-.126	9.66	0.009	3.10	3.66	.59	.0073	0.0030	.332	.357	.057
.20	8.14	.089	-.154	11.04	0.007	3.17	3.41	.62	.0056	0.0025	.310	.333	.061
.20	9.50	.105	-.180	12.42	0.007	2.98	3.19	.63	.0044	0.0023	.291	.311	.062
.20	10.55	.129	-.201	13.50	0.006	2.80	3.04	.65	.0036	0.0021	.274	.297	.064
.20	11.61	.134	-.228	15.18	0.006	2.63	2.90	.66	.0030	0.0020	.257	.283	.065
.20	12.66	.147	-.268	16.56	0.005	2.31	2.72	.66	.0025	0.0018	.226	.266	.065
.20	15.72	.143	-.280	17.94	0.004	2.21	----	.67	.0021	0.0015	.216	----	.066
.40	0	0	-.322	C	----	2.40	5.93	.95	----	----	.296	.731	.006
.40	.63	.007	-.311	.74	0.064	2.44	----	.05	1.9950	0.0555	.300	----	.006
.40	1.06	.027	-.269	1.23	0.090	2.60	5.92	.05	.7188	0.0481	.320	.728	.006
.40	1.48	.041	-.252	1.72	0.070	2.66	----	.08	.3666	0.0374	.327	----	.010
.40	2.11	.056	-.201	2.45	0.046	2.63	5.68	.08	.1797	0.0252	.349	.700	.010
.40	2.53	.069	-.134	2.96	0.011	3.07	----	.06	.1248	0.0226	.378	----	.008
.40	3.17	.094	-.025	3.70	0.035	3.59	5.72	.05	.0799	0.0187	.442	.704	.006
.40	3.59	.102	.140	4.19	.029	3.98	----	.05	.0622	0.0158	.490	----	.006
.40	4.22	.109	.184	4.93	.022	4.12	5.32	.07	.0449	0.0122	.507	.654	.009
.40	4.64	.116	.170	5.42	.020	4.08	----	.16	.0371	0.0108	.502	----	.020
.40	5.23	.122	.123	6.16	.016	3.92	4.54	.25	.0288	0.0088	.483	.559	.031
.40	6.33	.129	.028	7.39	.012	5.61	4.00	.35	.0200	0.0064	.445	.495	.041
.40	7.39	.139	-.046	8.62	0.009	3.35	3.50	.38	.0147	0.0051	.413	.443	.047
.40	8.14	.150	-.095	9.85	0.007	3.20	3.36	.41	.0112	0.0042	.394	.413	.051

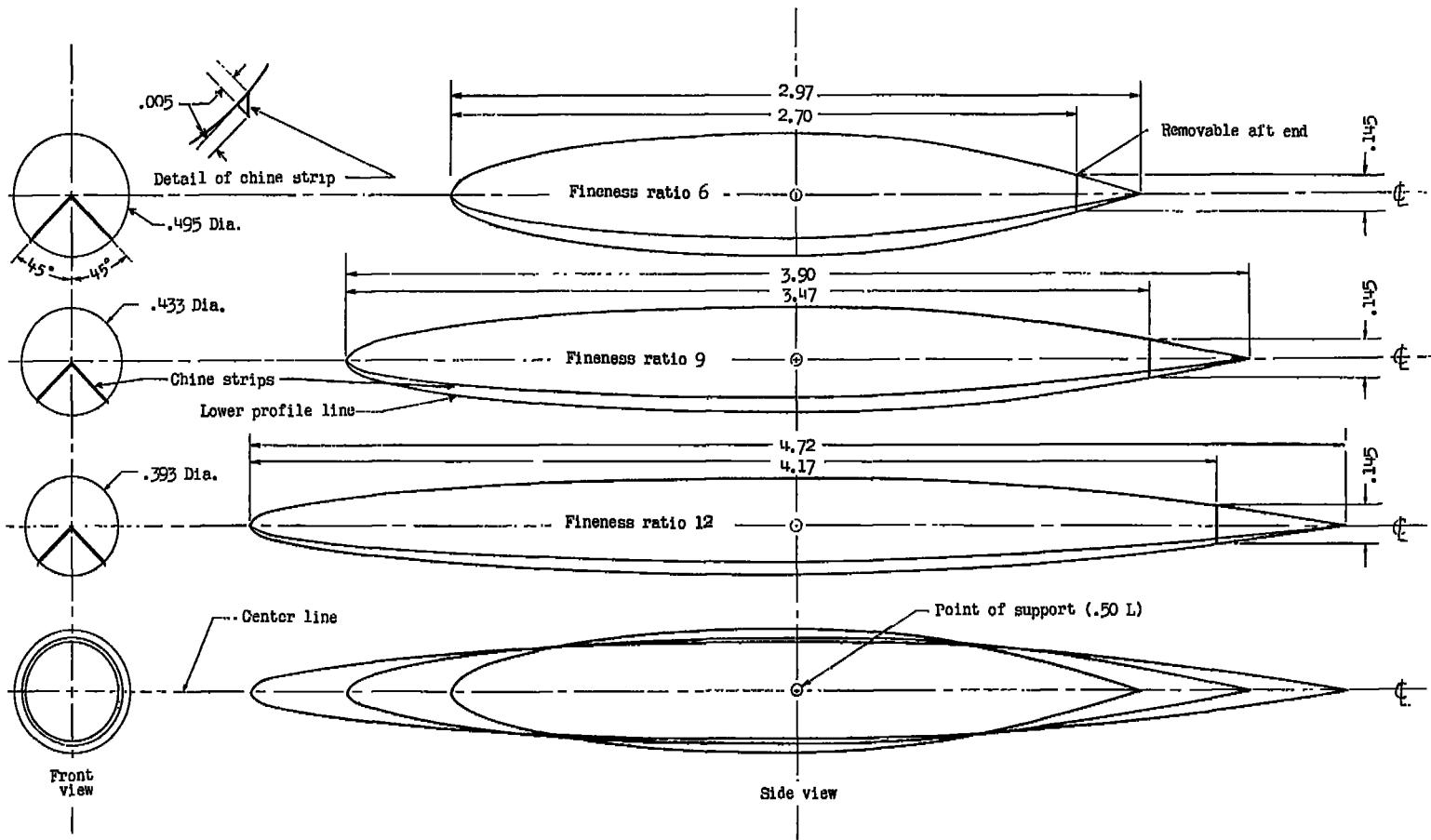
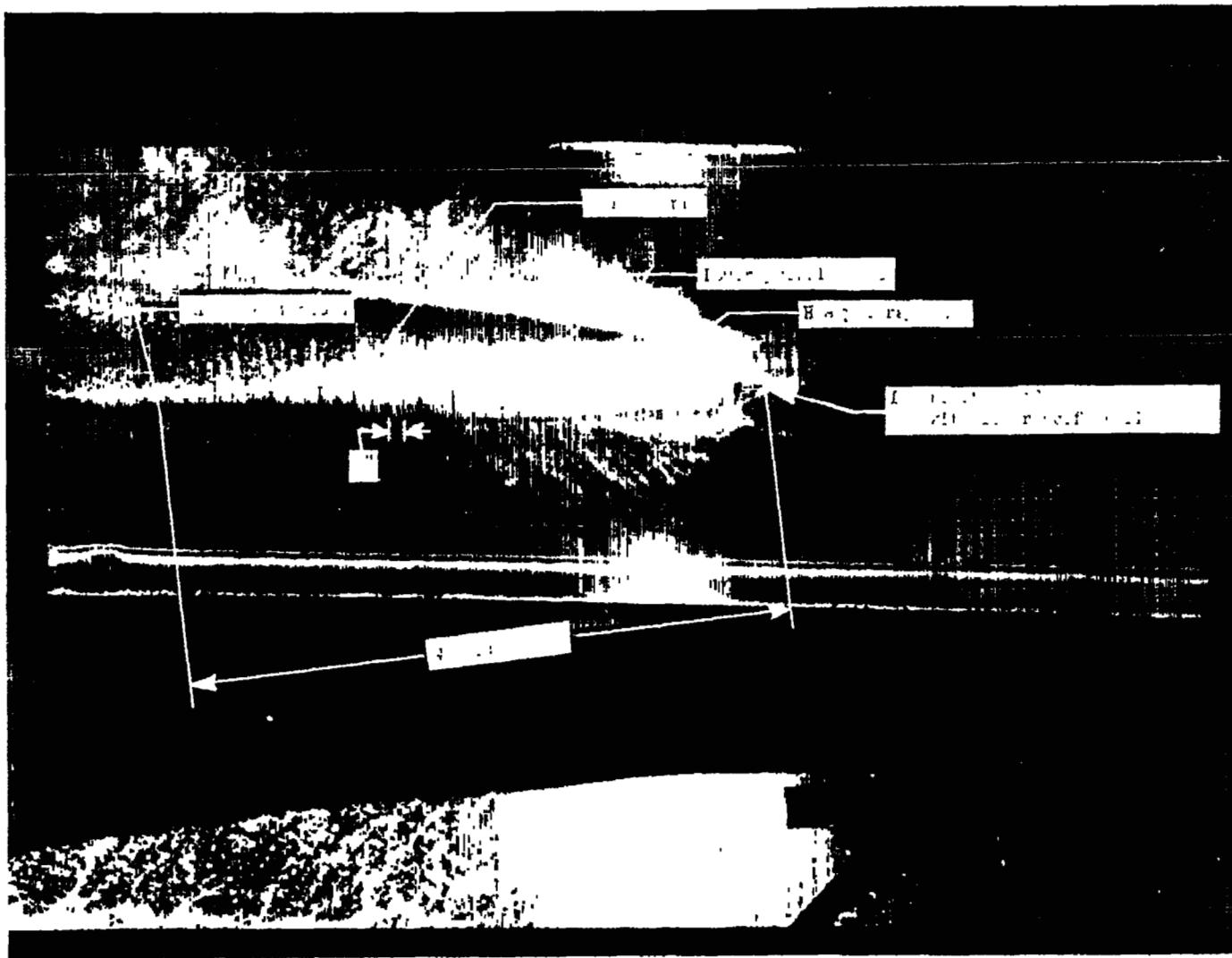


Figure 1.- Principal dimensions of models given in feet.



L-86474

Figure 2.- Underwater picture illustrating method of measuring wetted length.

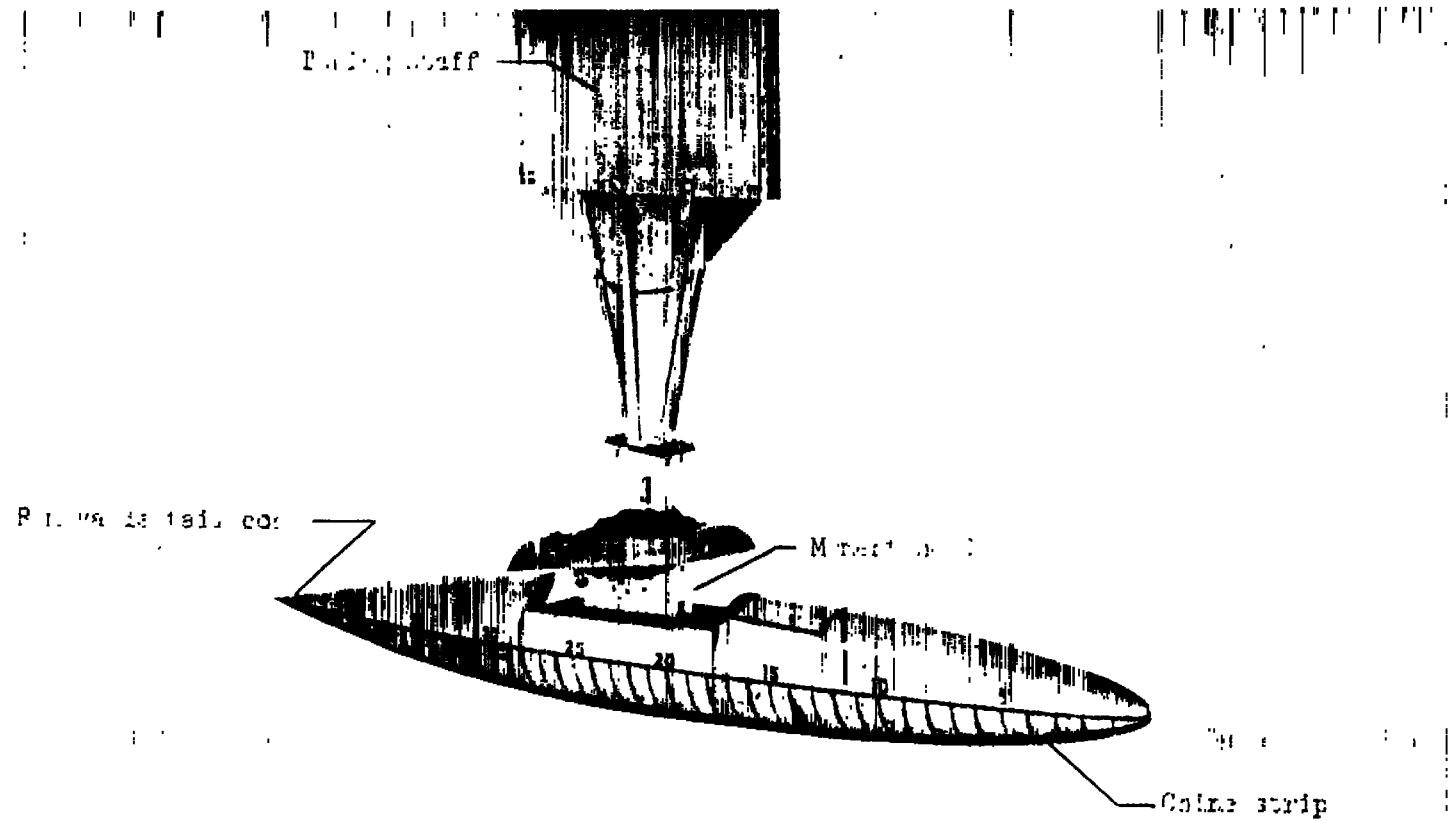


Figure 3.- Model mounted on towing staff.

L-73051.1

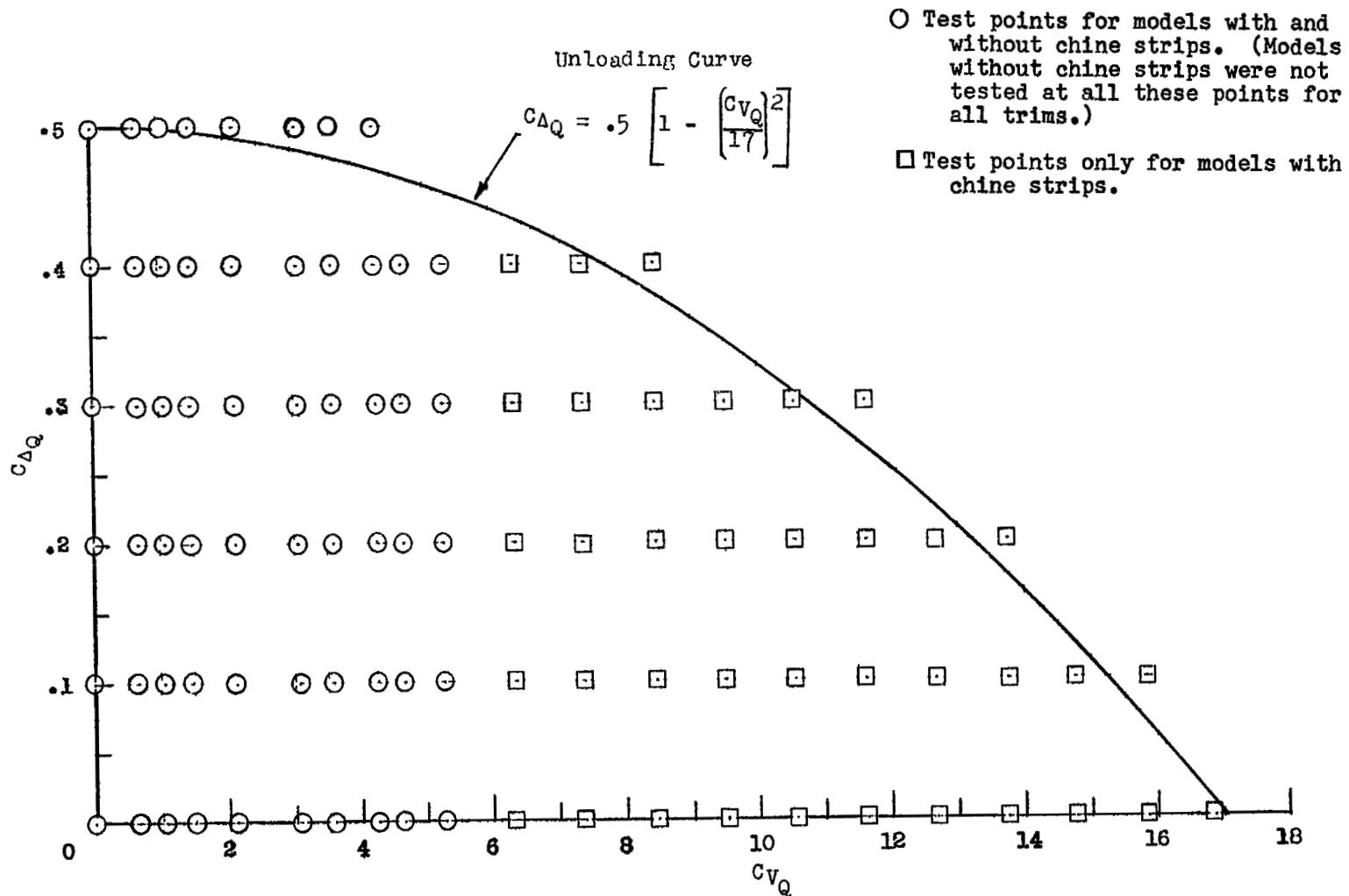


Figure 4.- Load-speed range investigated.

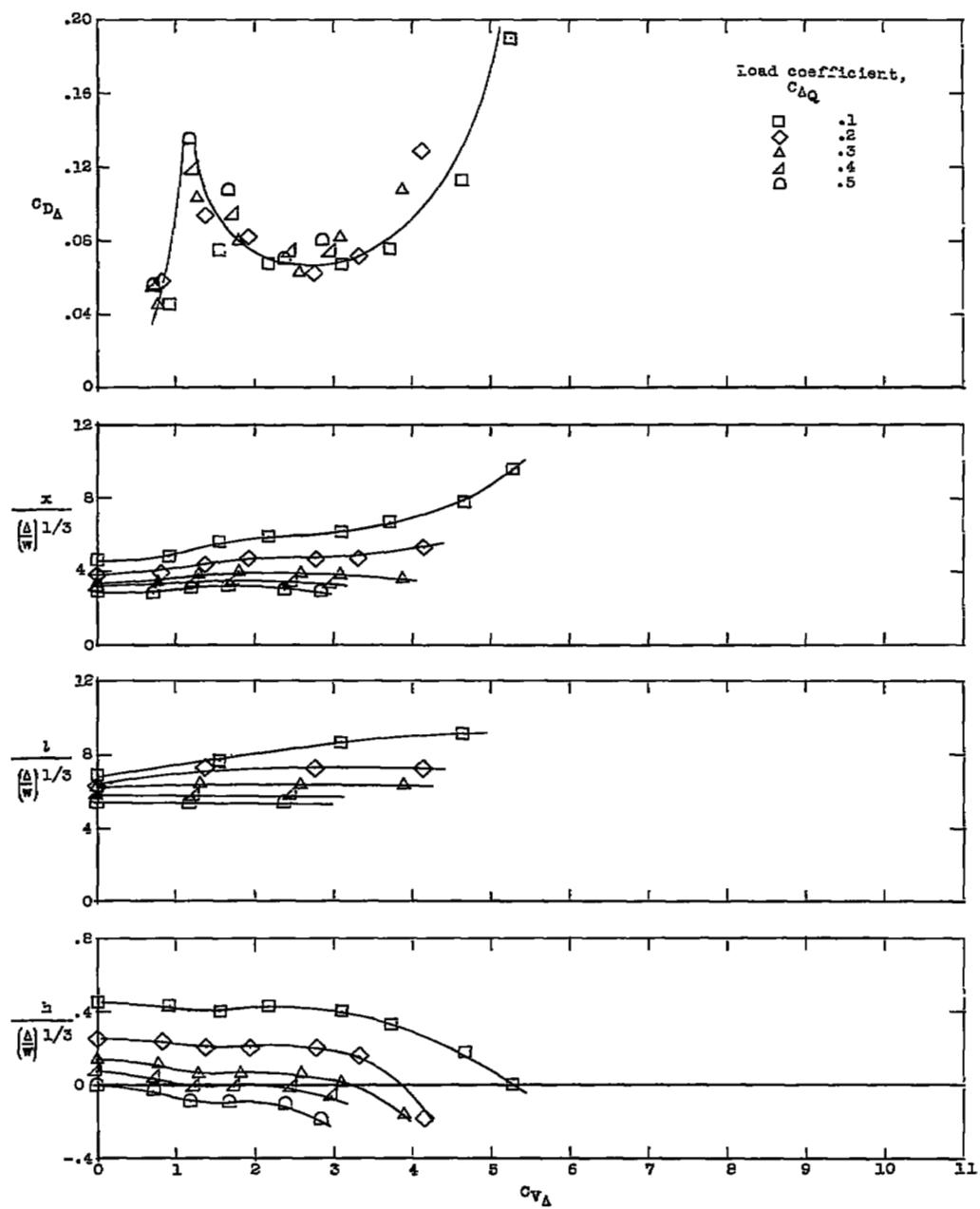
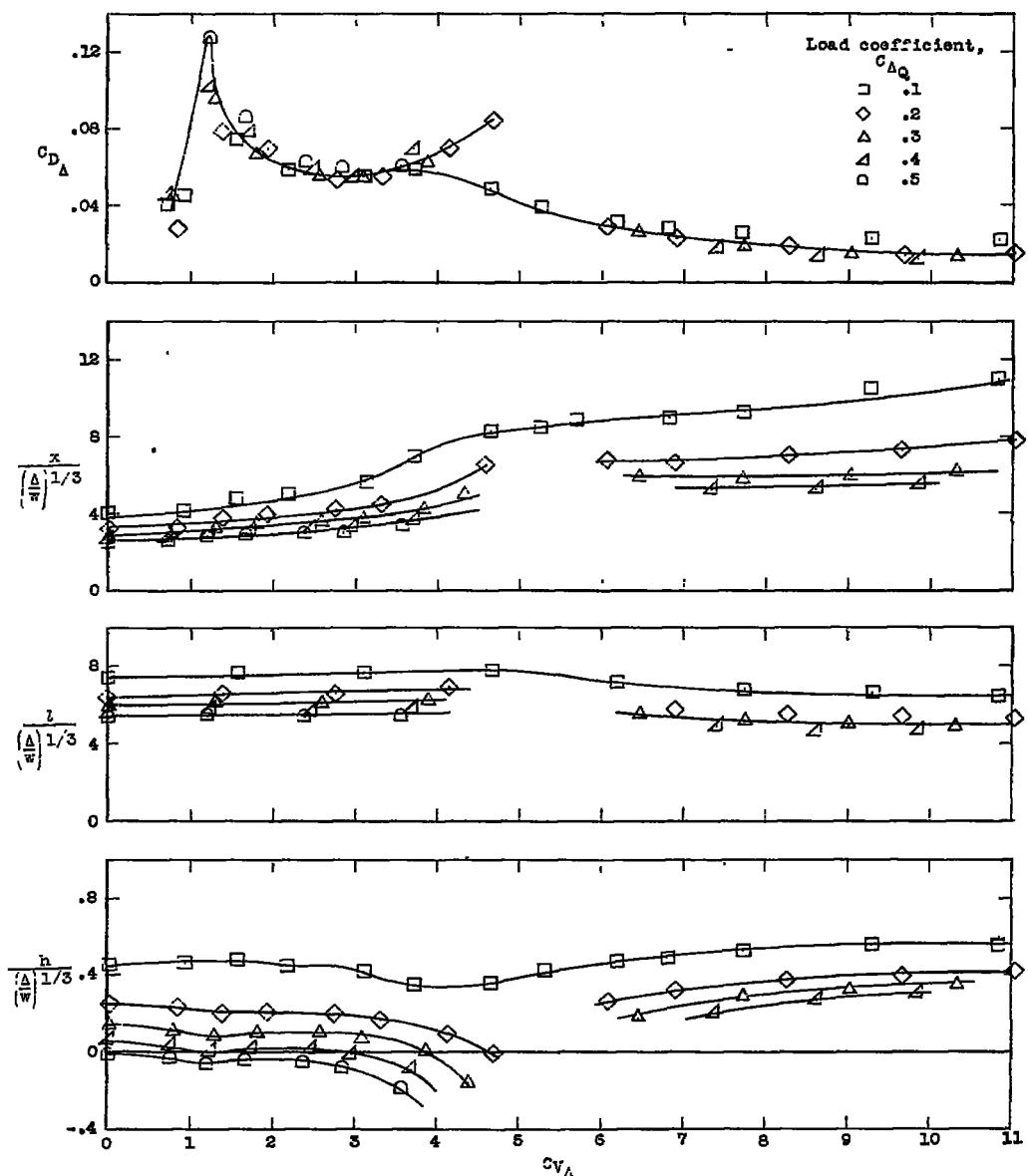
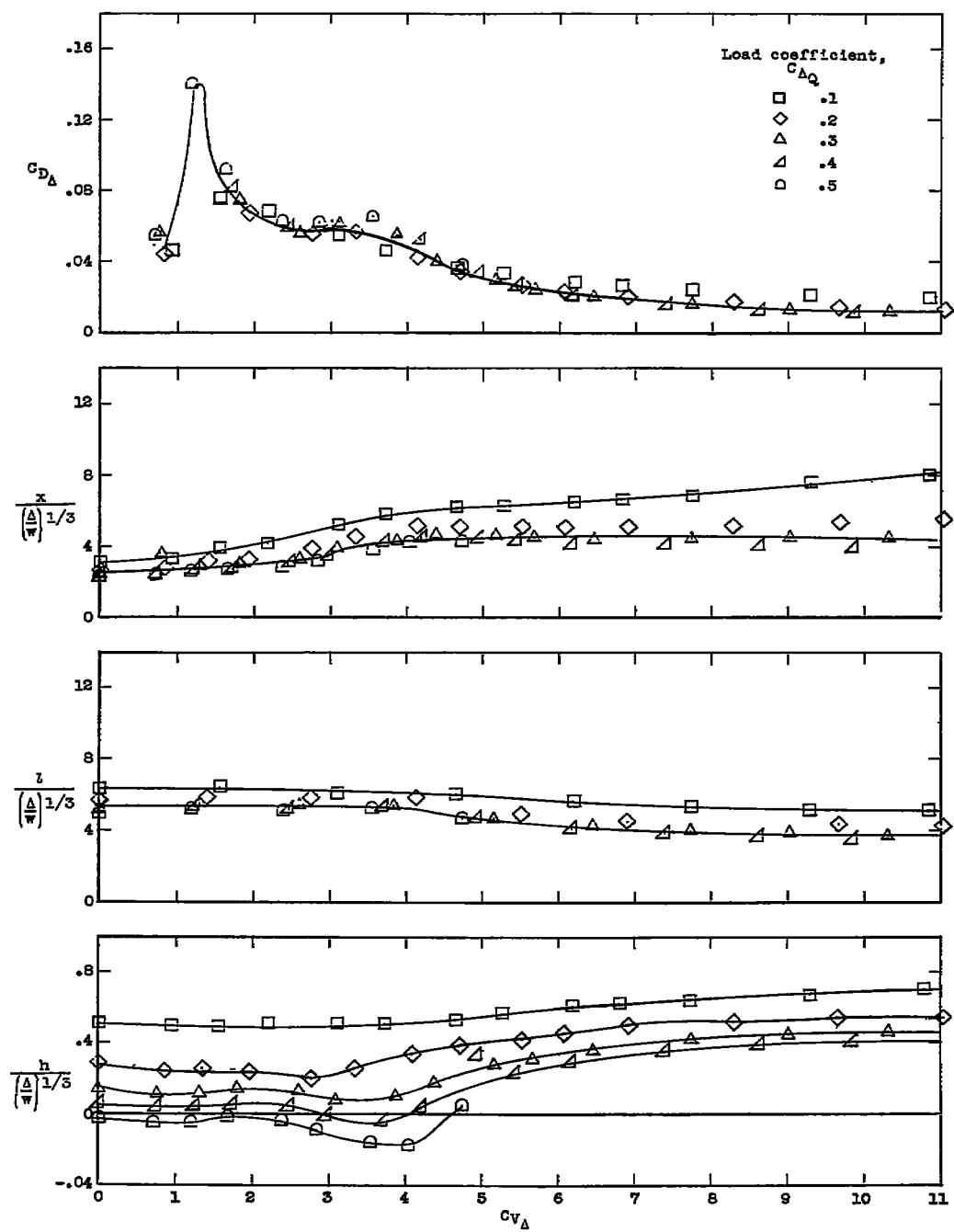
(a) Trim, 0° .

Figure 5.- Hydrodynamic characteristics of model with chine strips.
Fineness ratio 6; displacement condition.



(o) Trim, 4° .

Figure 5.- Continued.



(c) Trim, 8°.

Figure 5.- Continued.

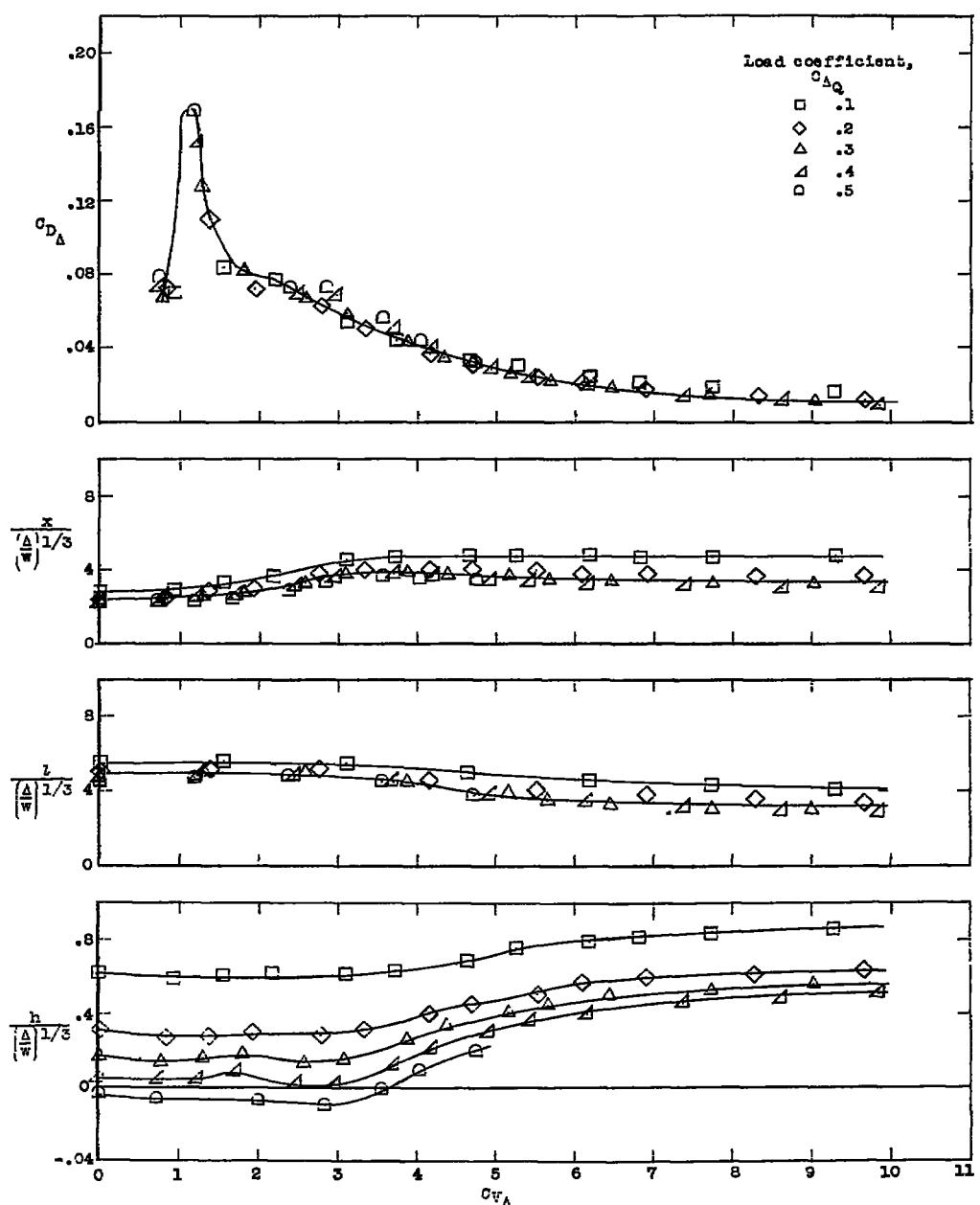
(d) Trim, 12° .

Figure 5.- Continued.

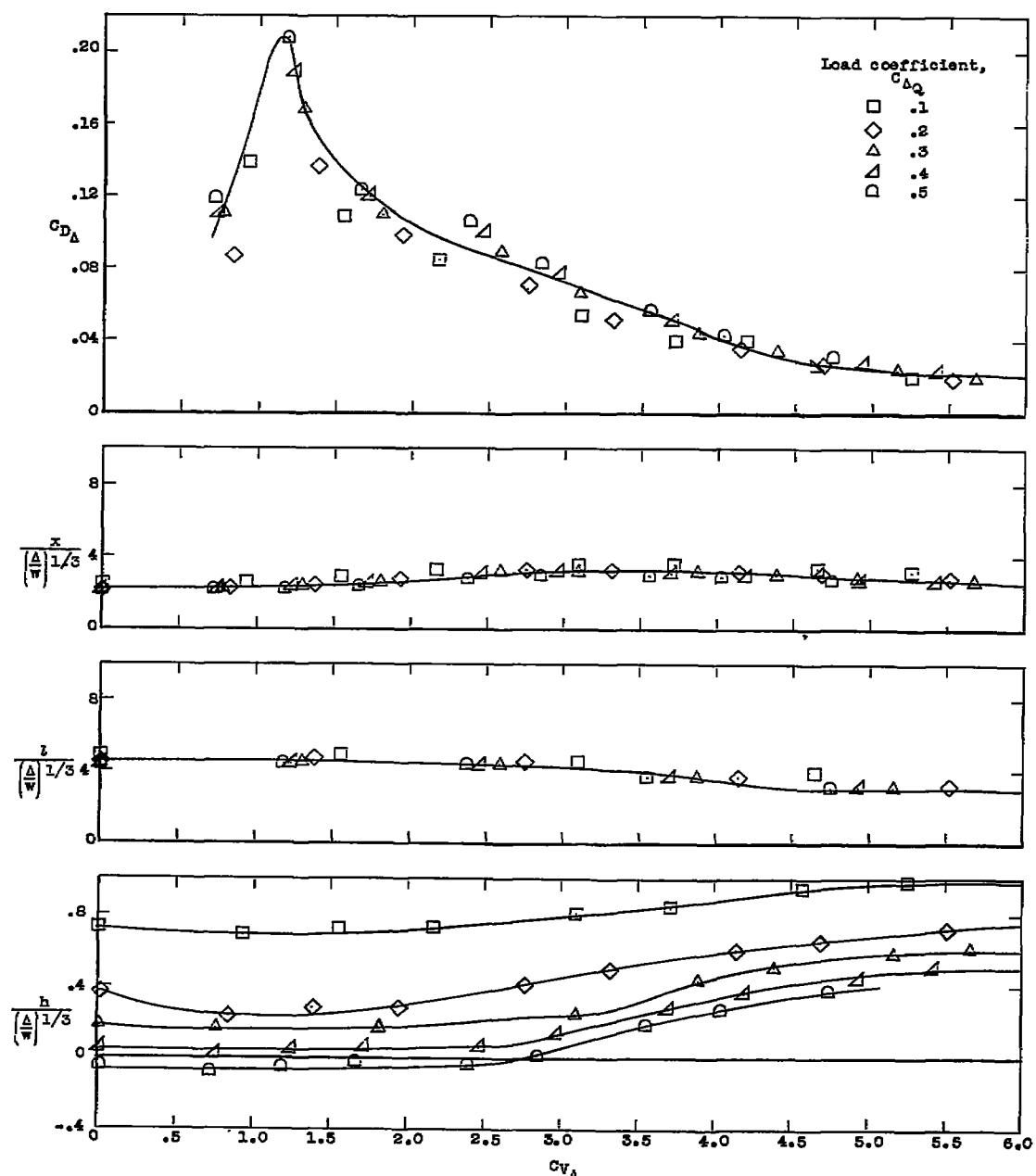
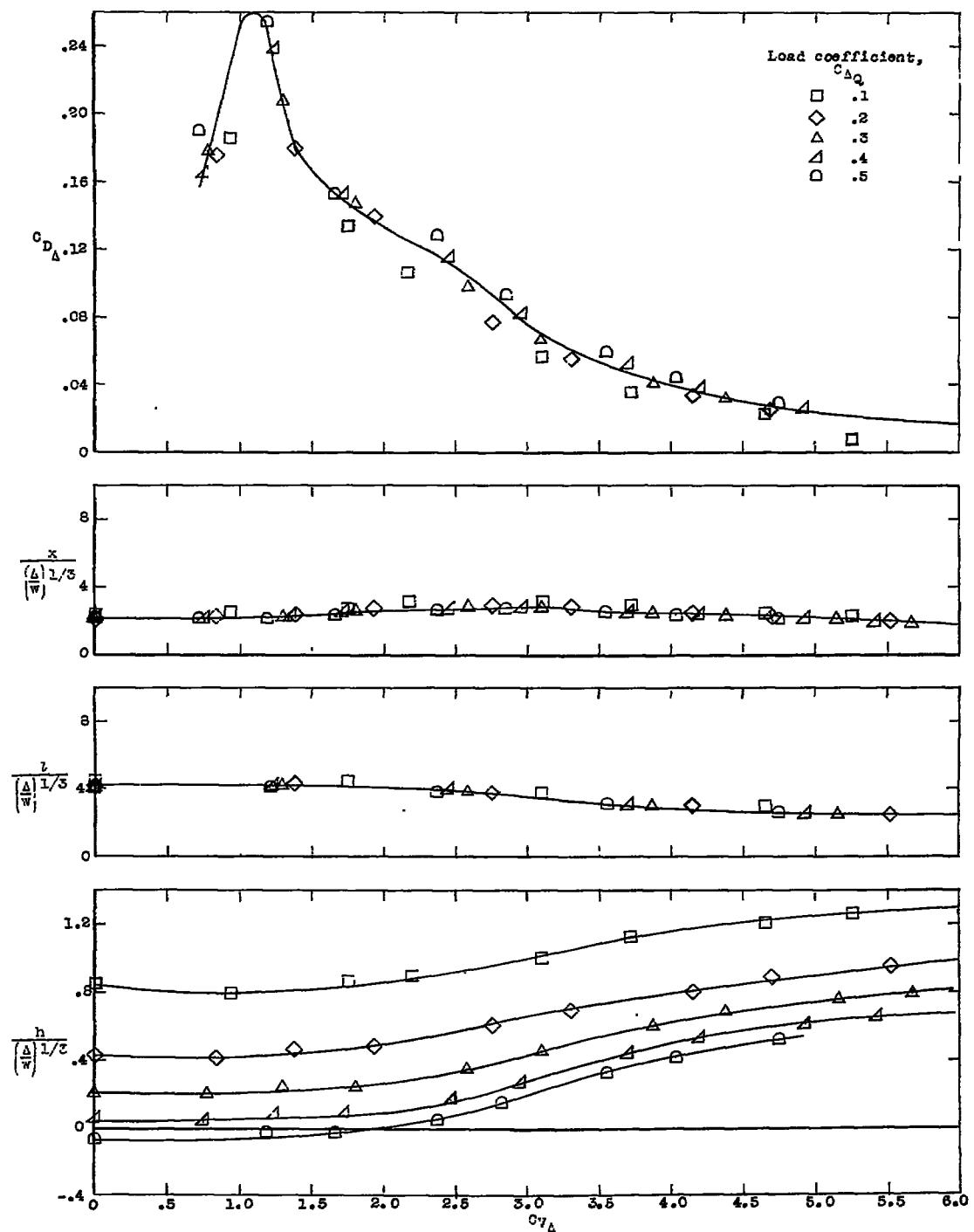
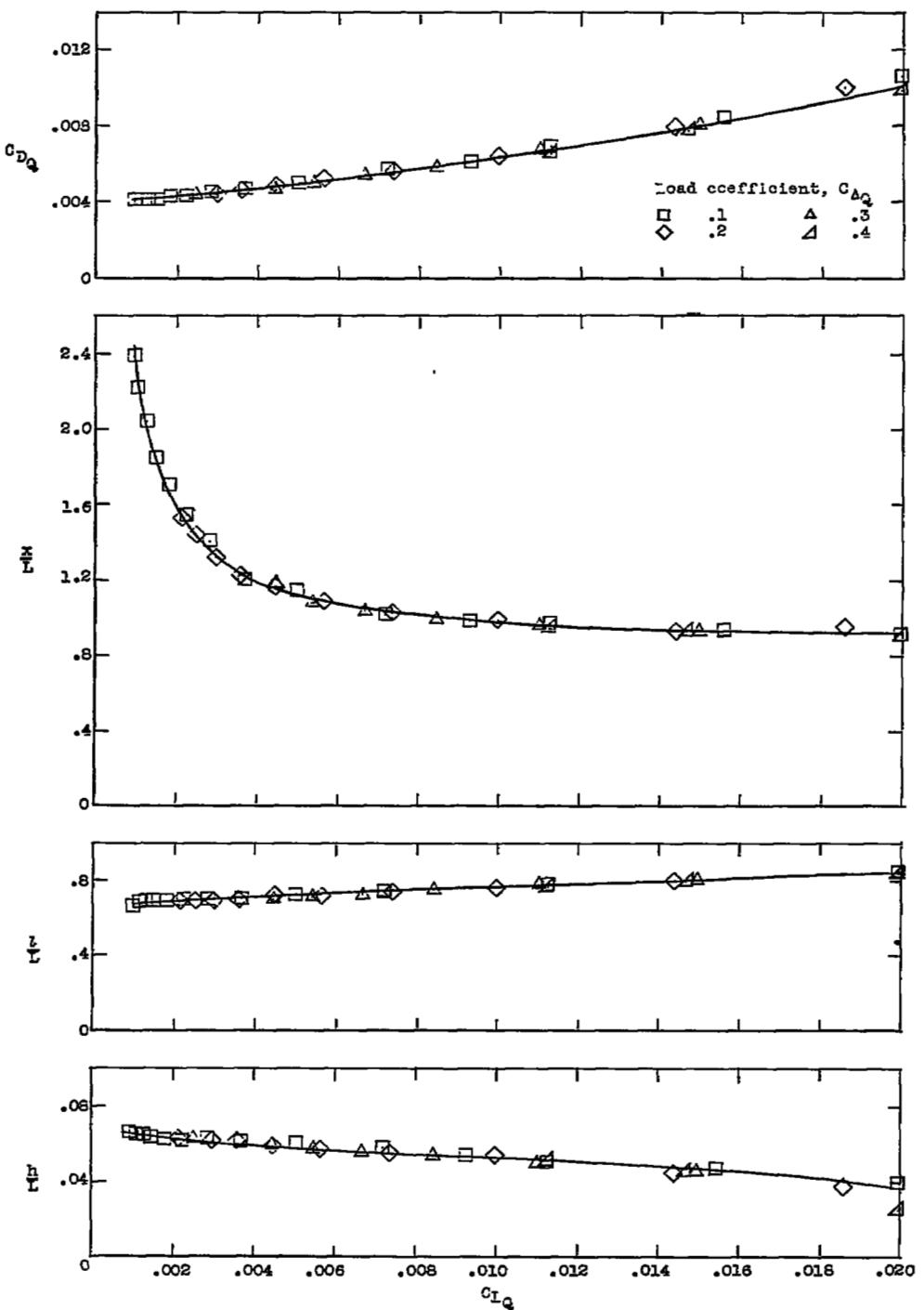
(e) Trim, 16° .

Figure 5.- Continued.



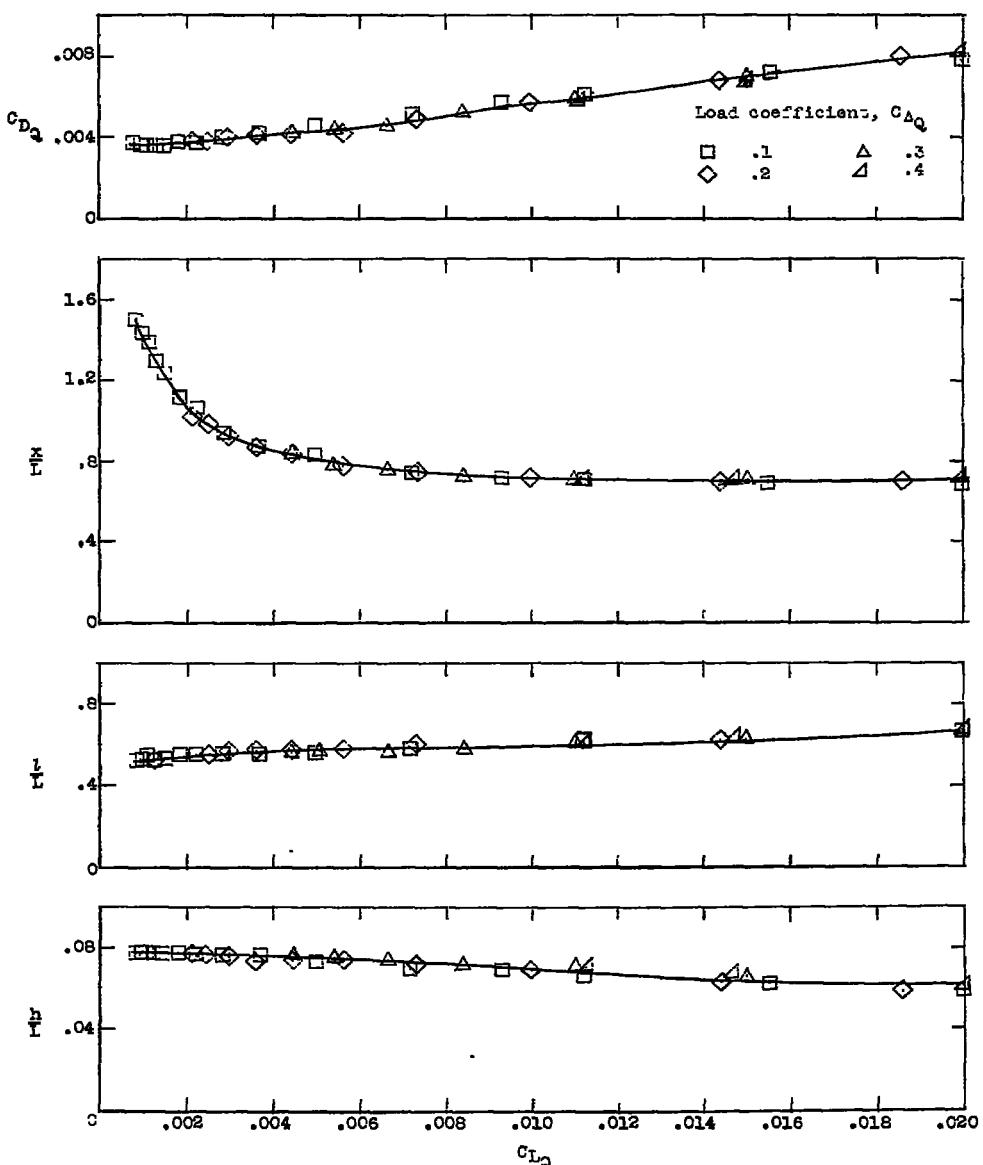
(f) Trim, 20°.

Figure 5-- Concluded.



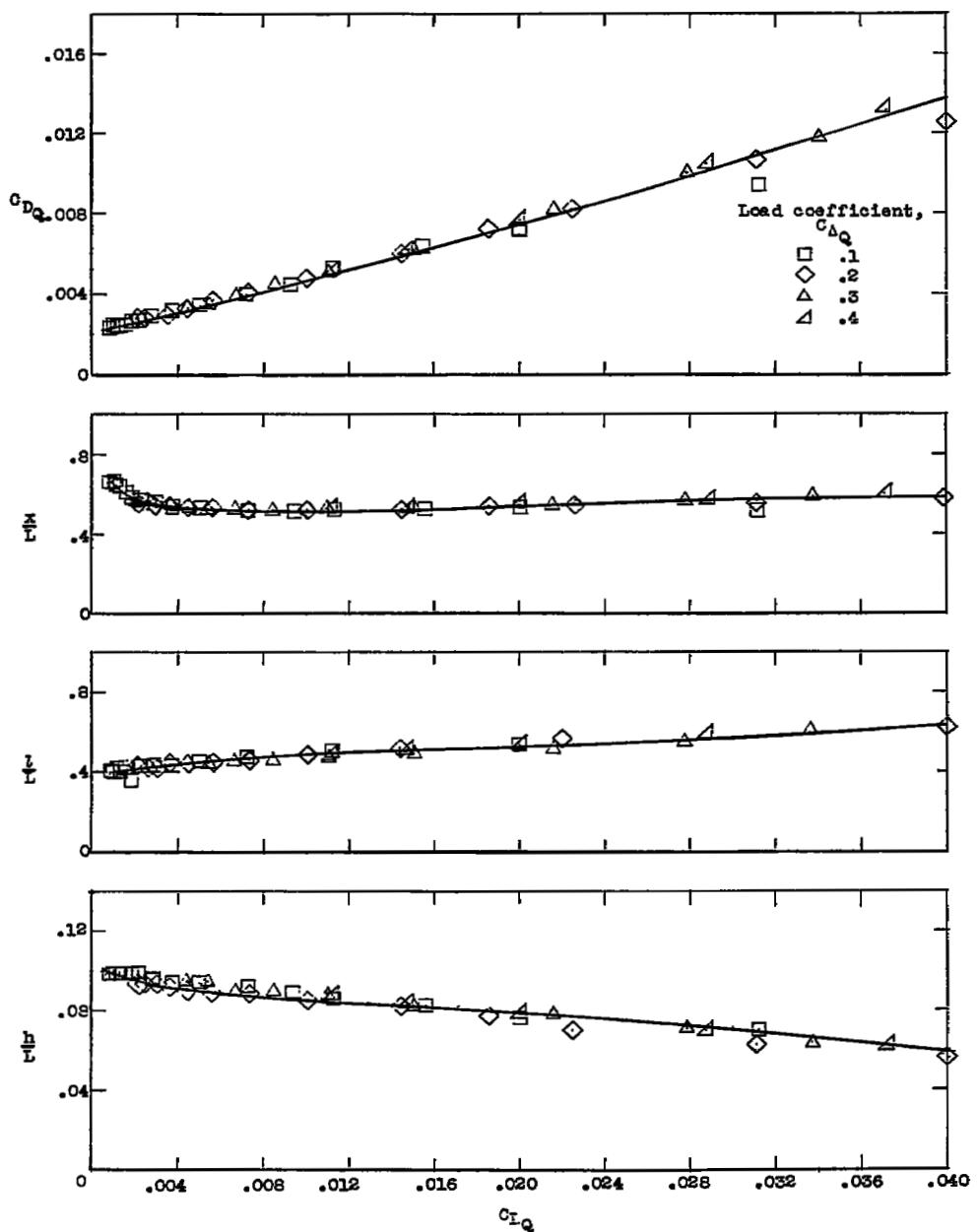
(a) Trim, 4°.

Figure 6.- Hydrodynamic characteristics of model with chine strips.
Fineness ratio 6; planing condition.



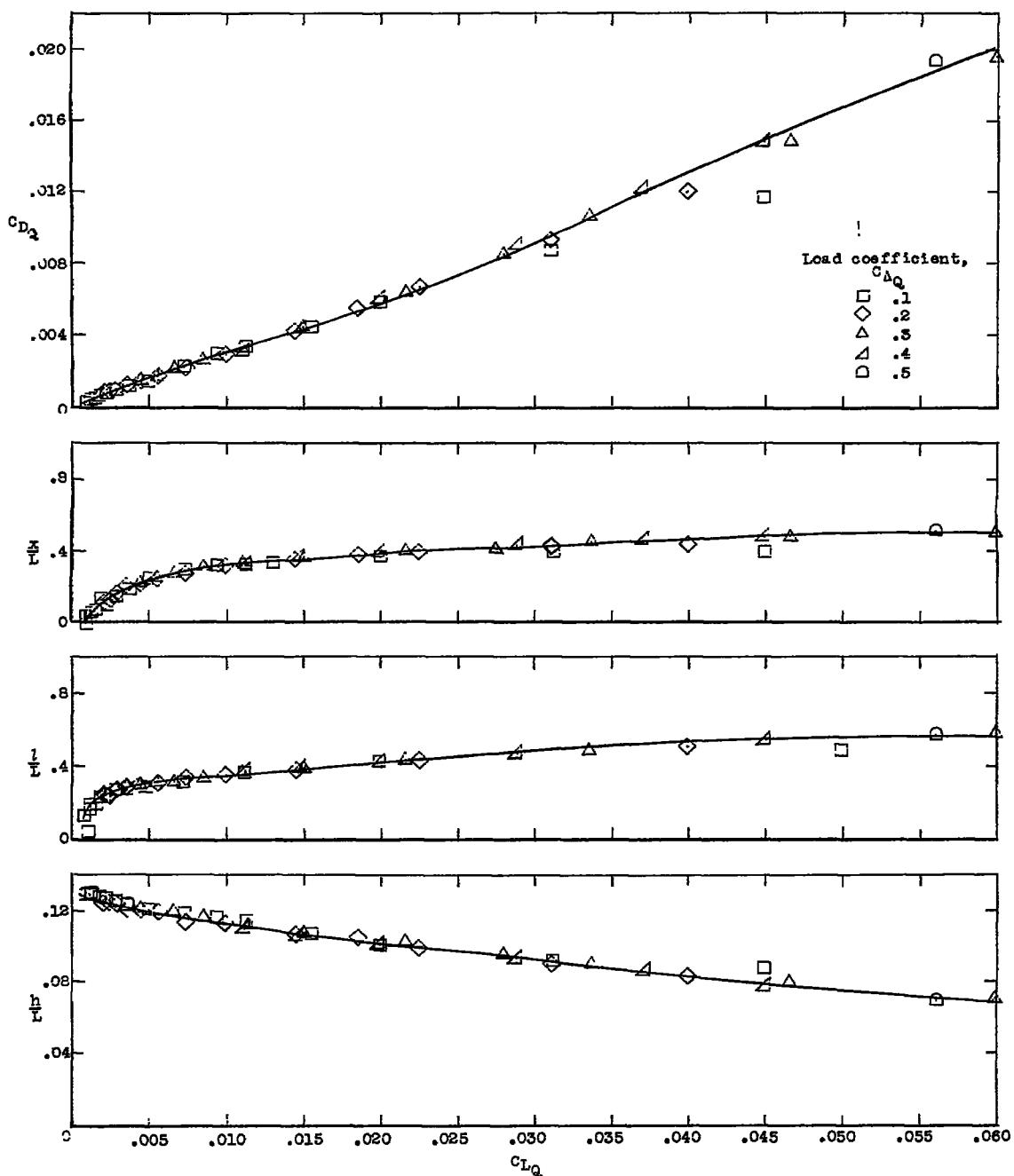
(b) Trim, 8°.

Figure 6.- Continued.



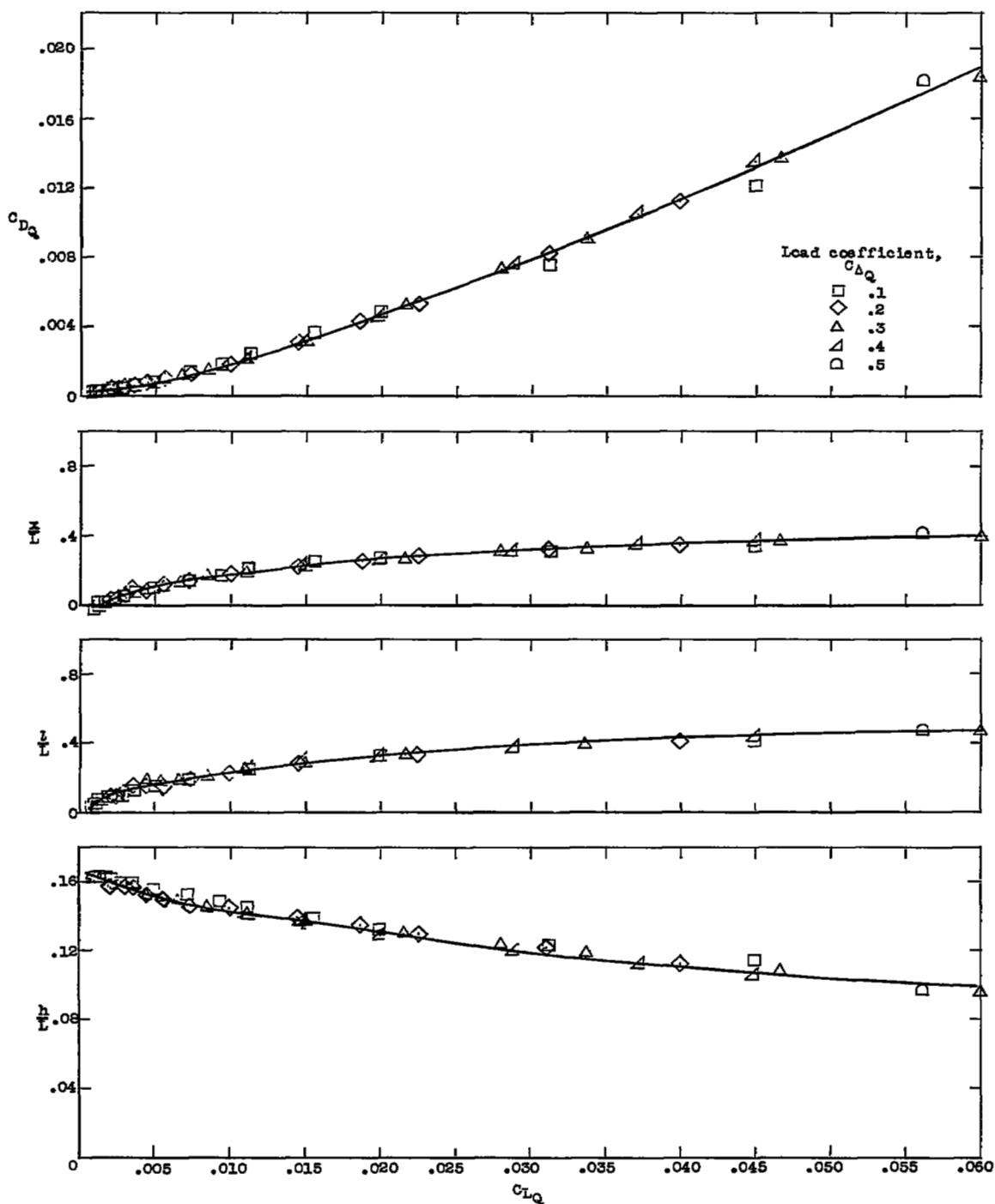
(c) Trim, 12°.

Figure 6.- Continued.



(d) Trim, 16°.

Figure 6.- Continued.



(e) Trim, 20°.

Figure 6.- Concluded.

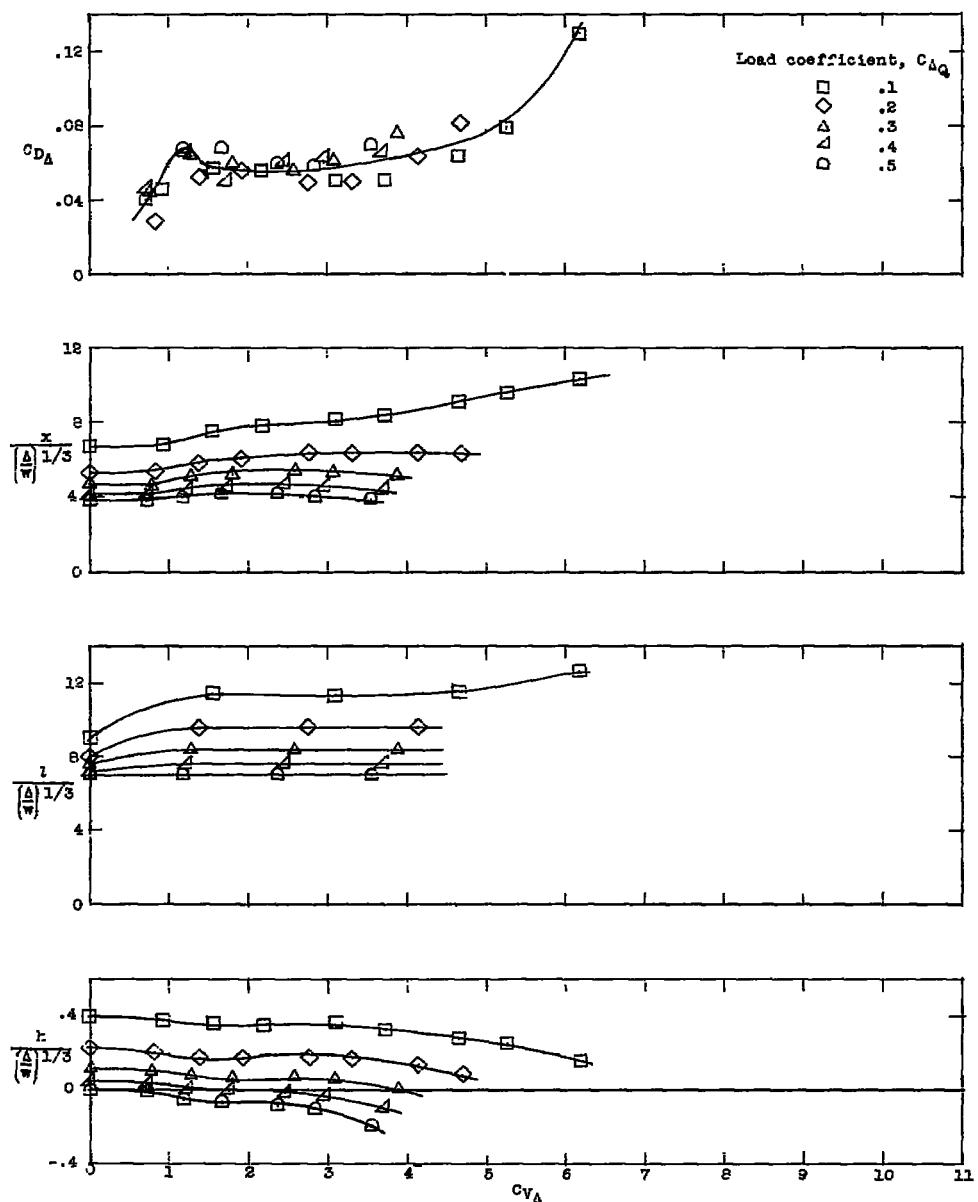
(a) Trim, 0° .

Figure 7.- Hydrodynamic characteristics of model with chine strips.
Fineness ratio 9; displacement condition.

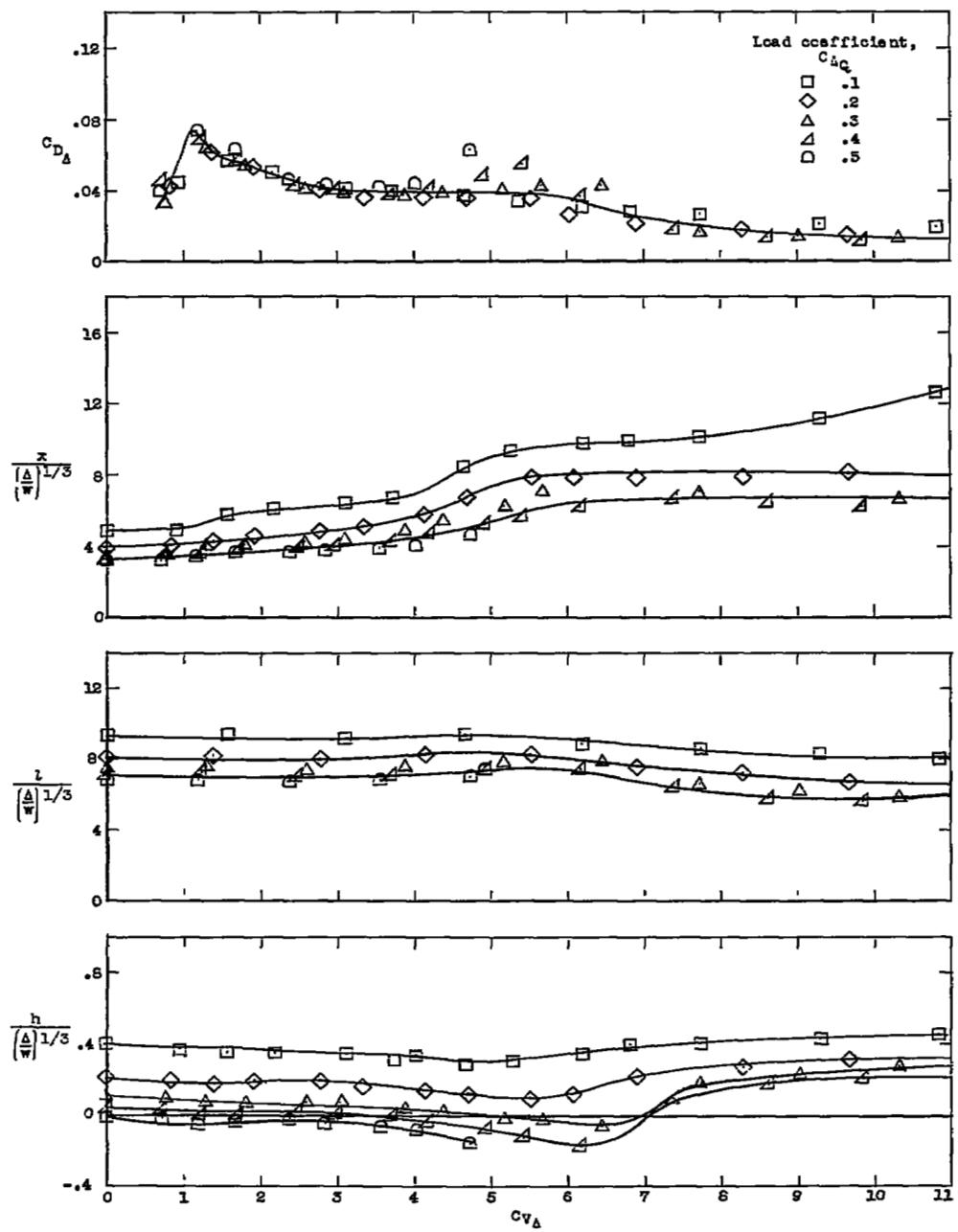
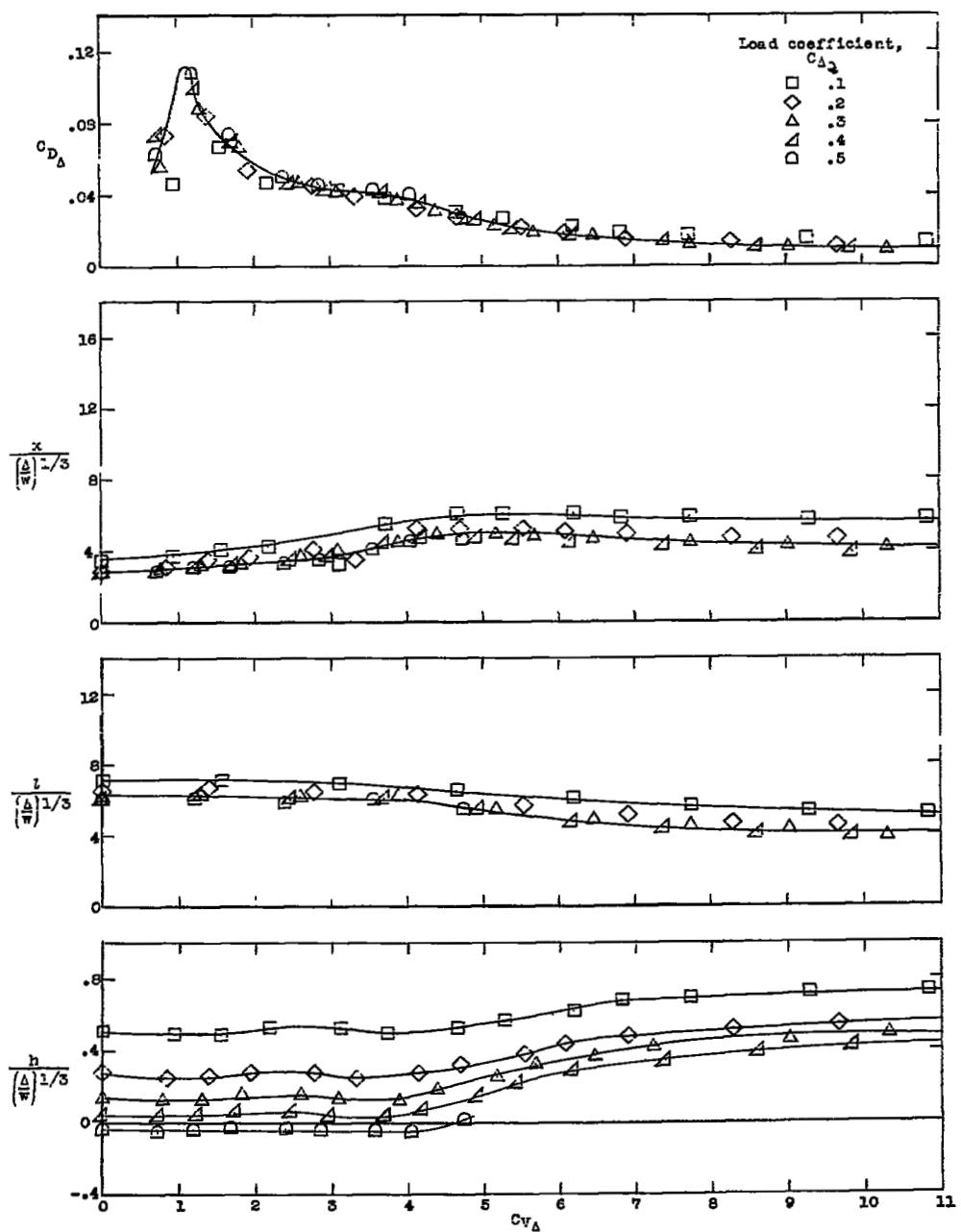
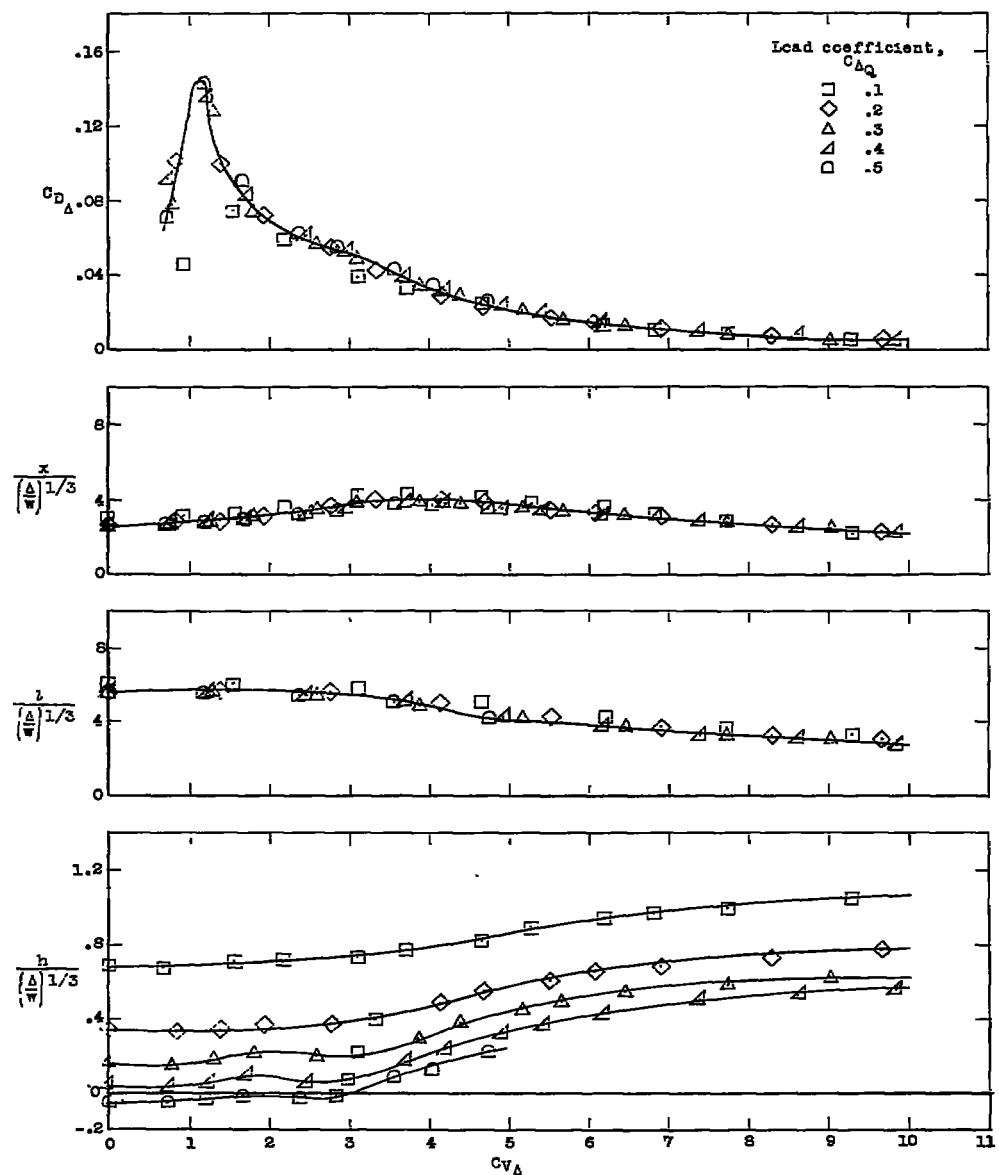
(b) Trim, 4° .

Figure 7.- Continued.



(c) Trim, 8°.

Figure 7.- Continued.



(d) Trim, 12°.

Figure 7.- Continued.

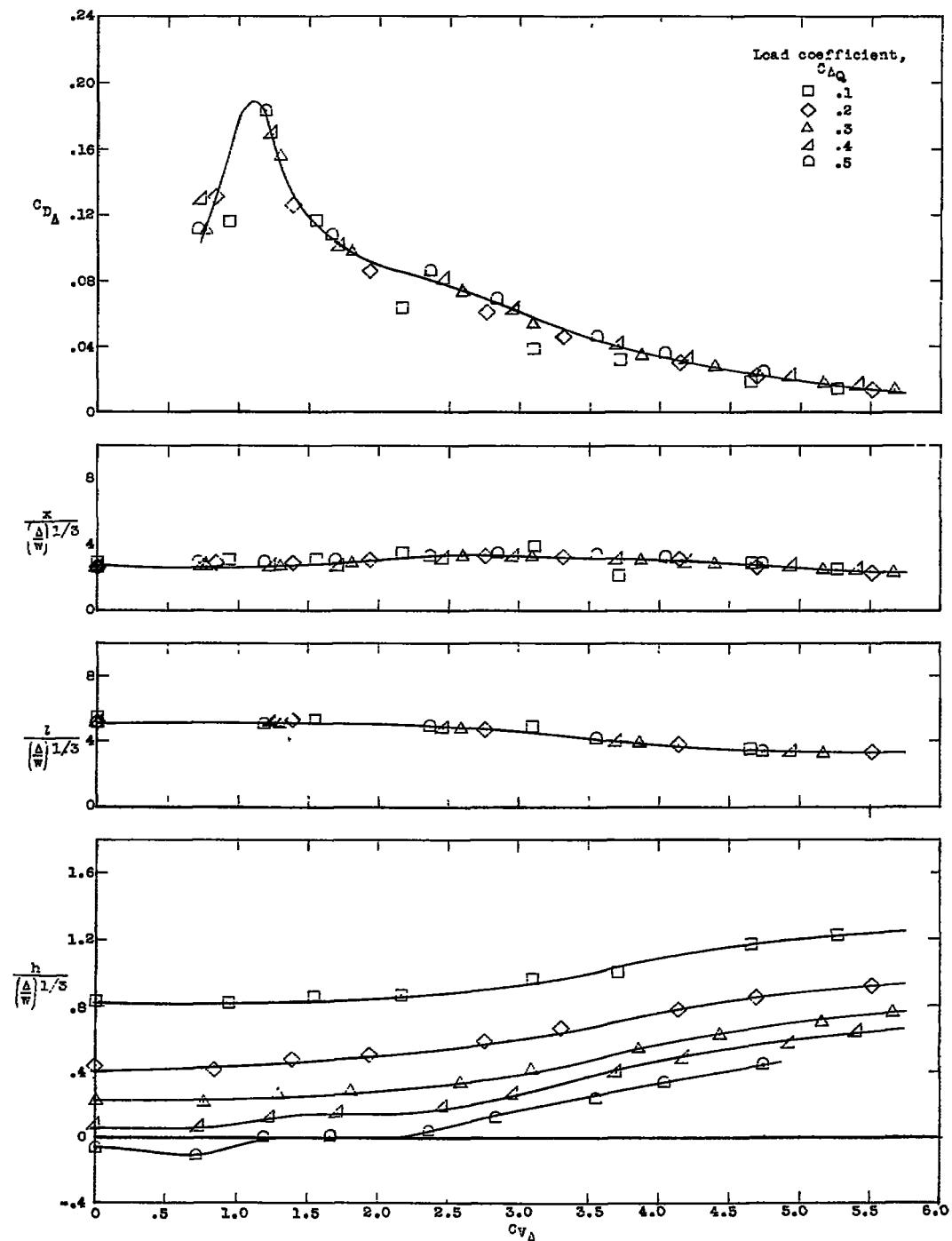
(e) Trim, 16° .

Figure 7.- Continued.

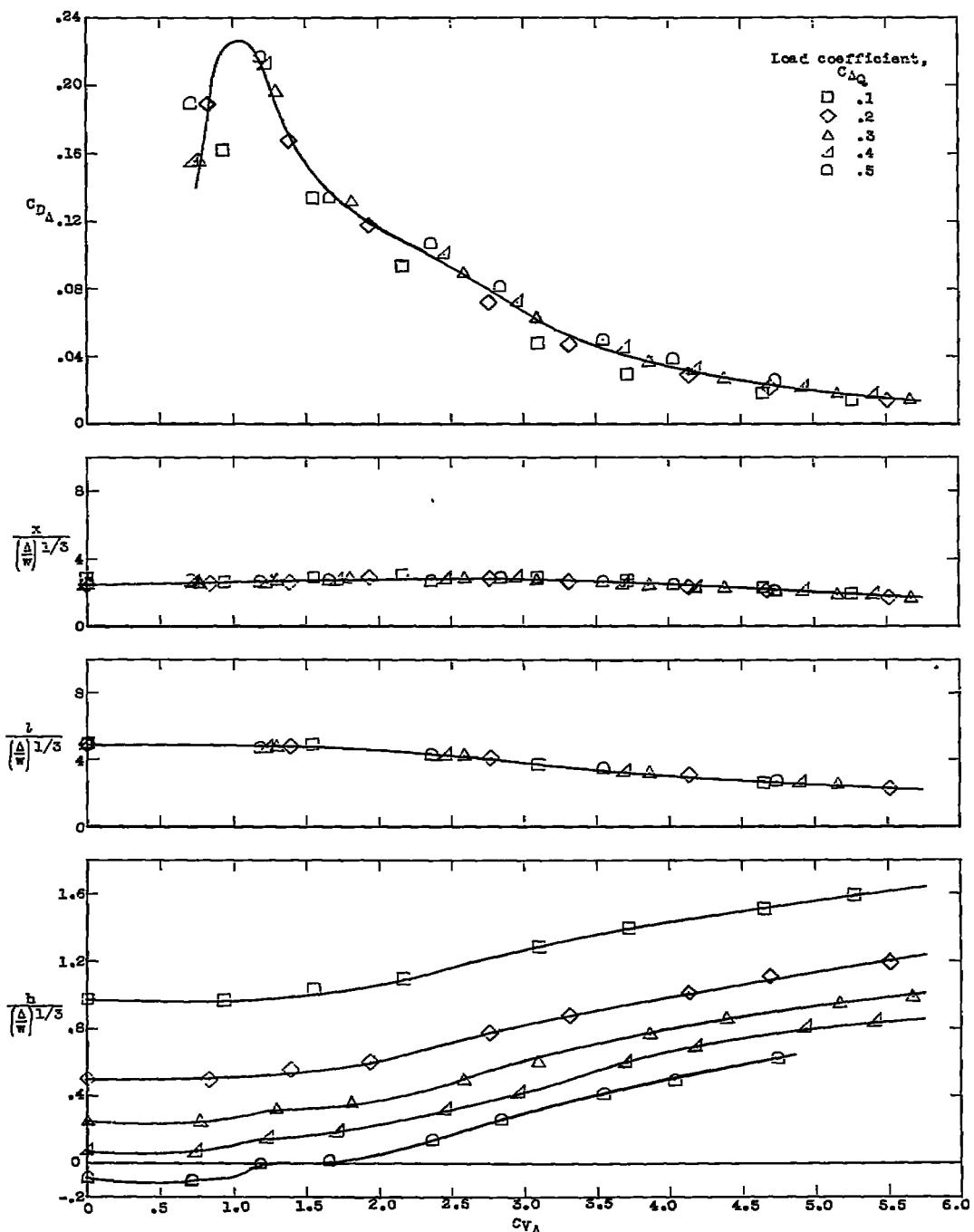
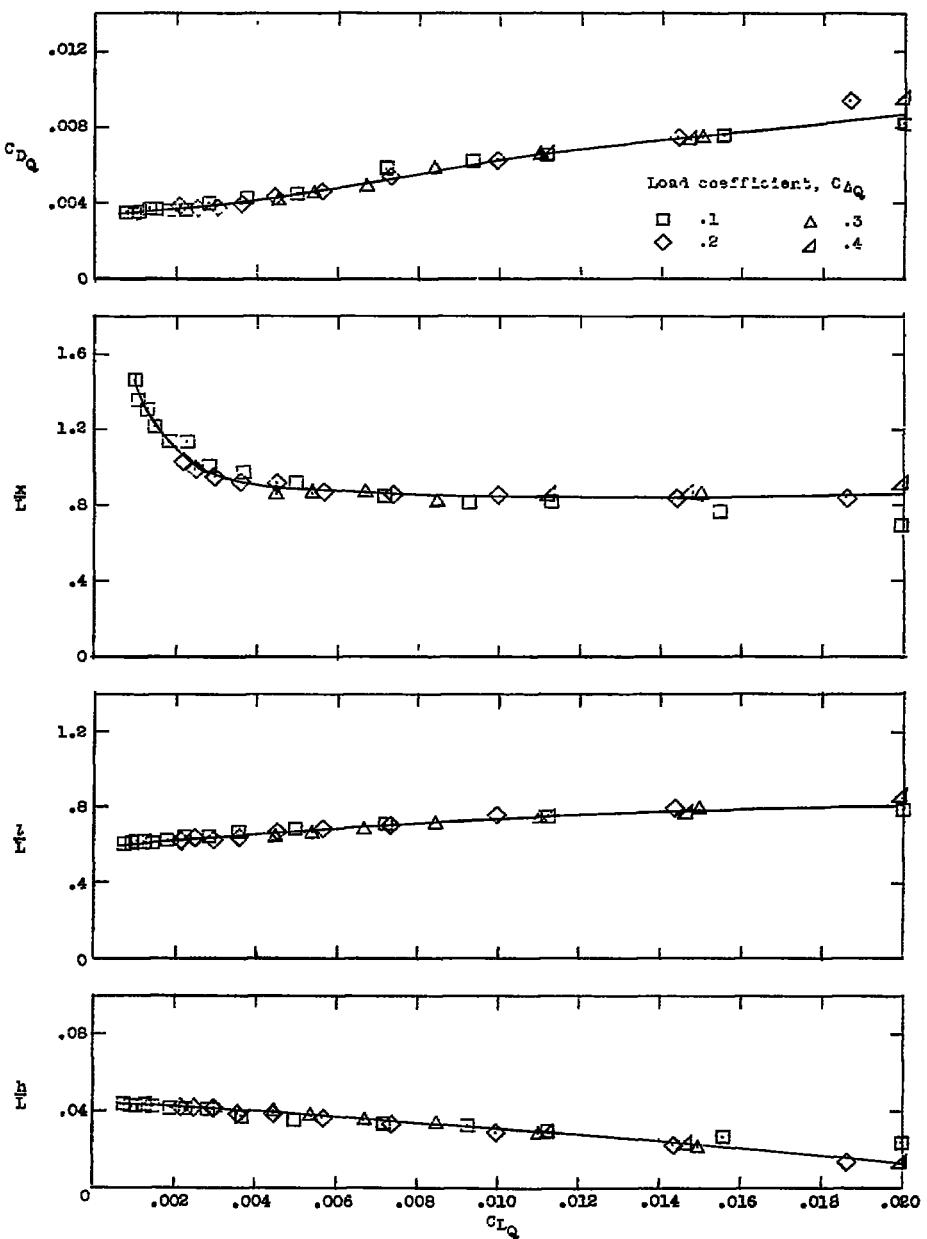
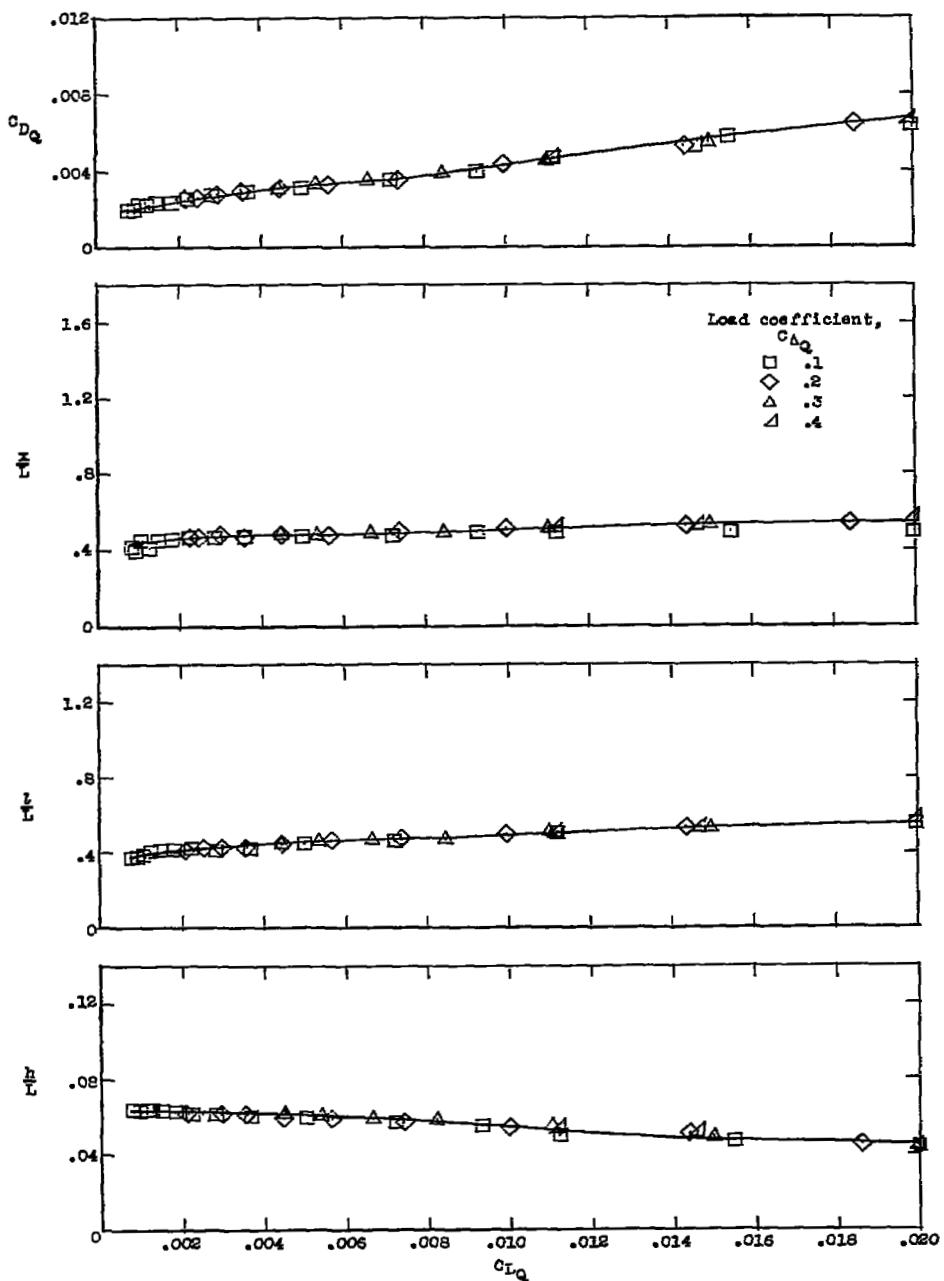
(f) Trim, 20° .

Figure 7.- Concluded.



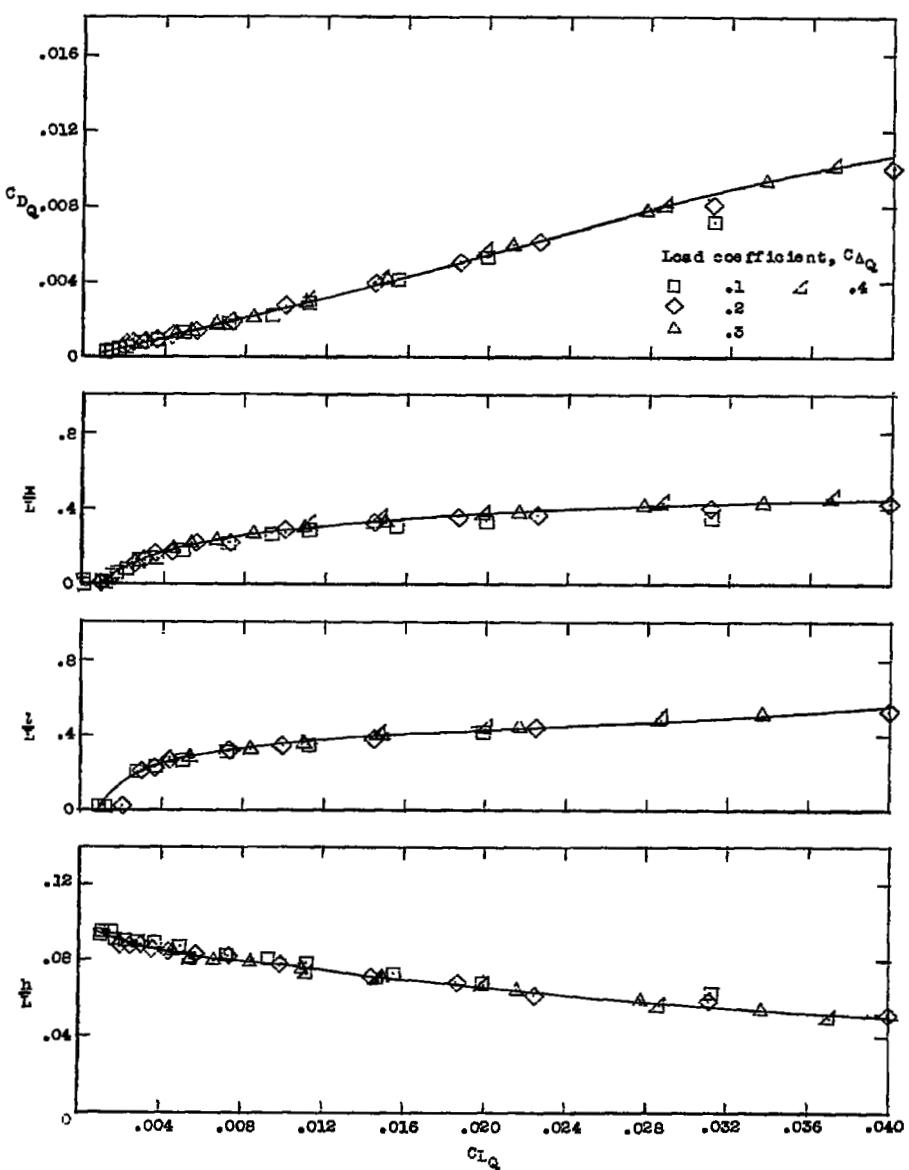
(a) Trim, 4°.

Figure 8.- Hydrodynamic characteristics of model with chine strips.
Fineness ratio 9; planing condition.



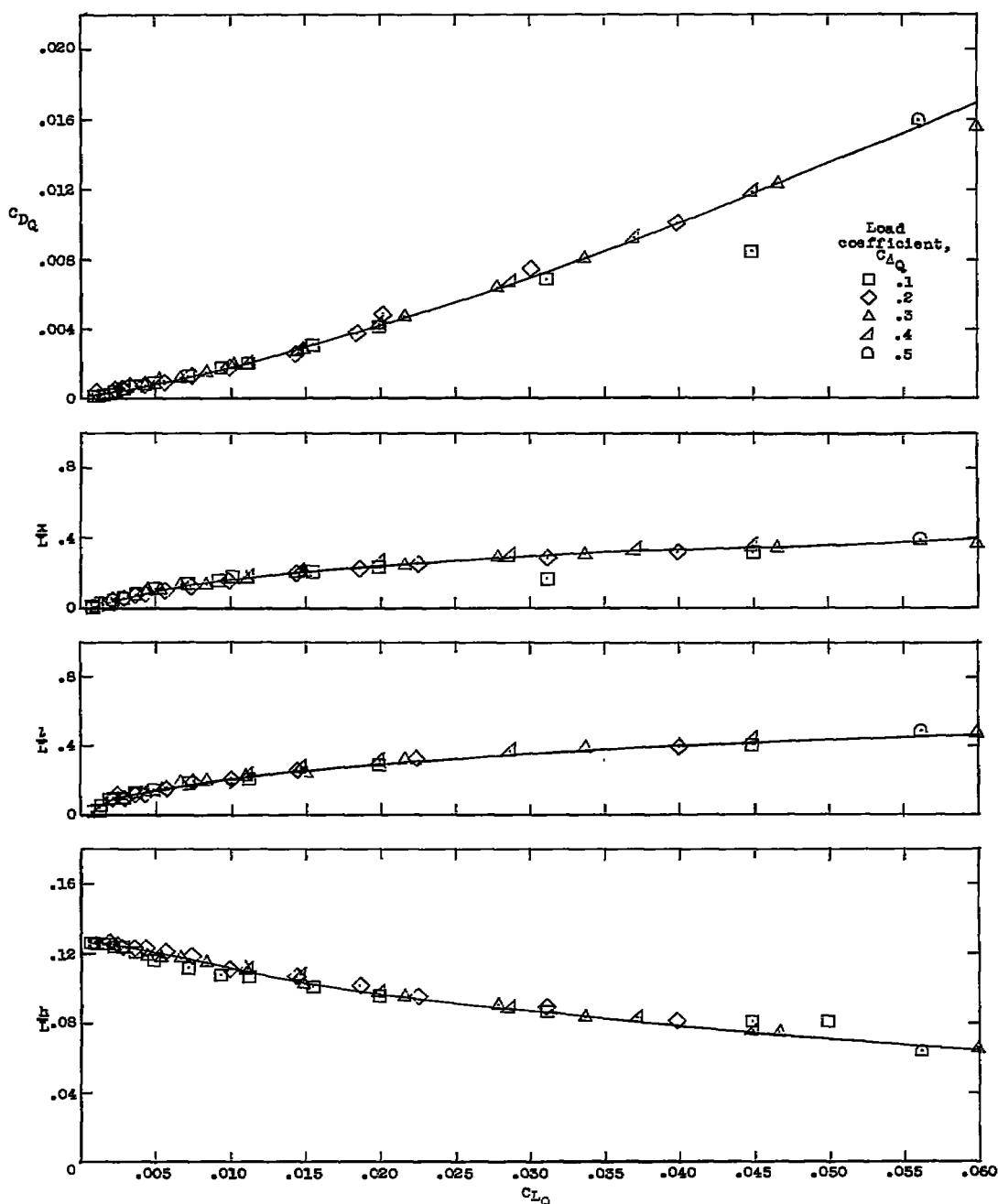
(b) Trim, 8°.

Figure 8.- Continued.



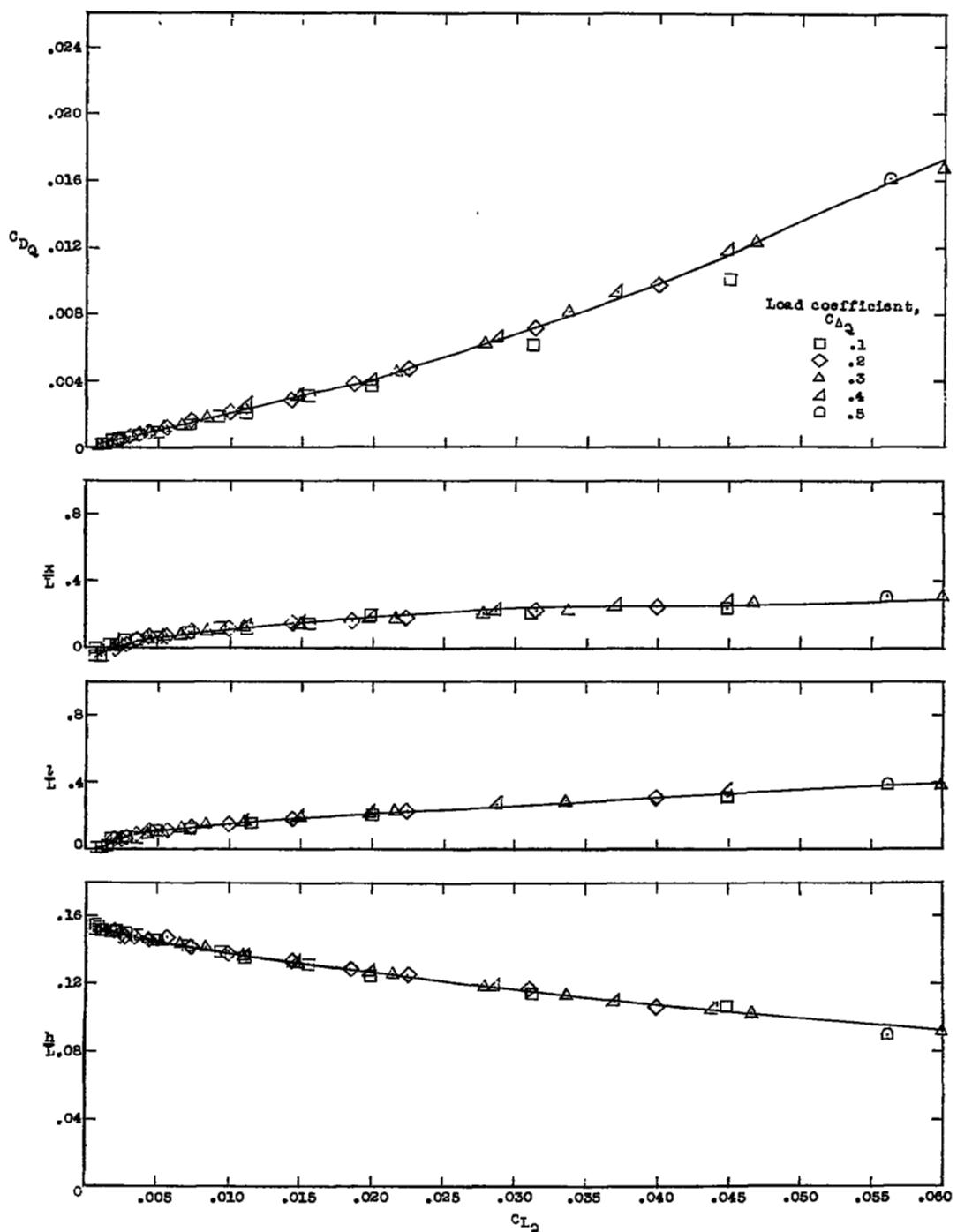
(c) Trim, 12°.

Figure 8.- Continued.



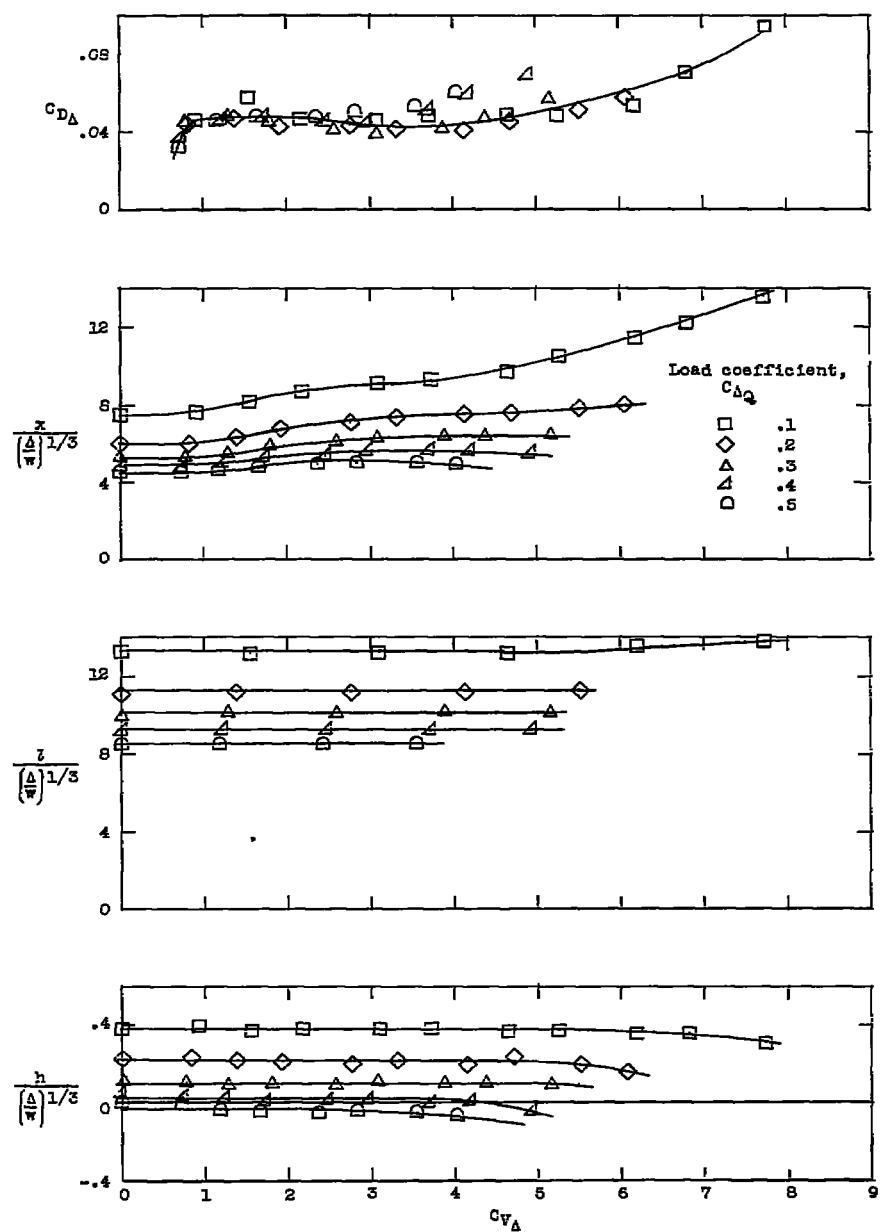
(d) Trim, 16°.

Figure 8.- Continued.



(e) Trim, 20°.

Figure 8.- Concluded.



(a) Trim, 0°.

Figure 9.- Hydrodynamic characteristics of model with chine strips.
Fineness ratio 12; displacement condition.

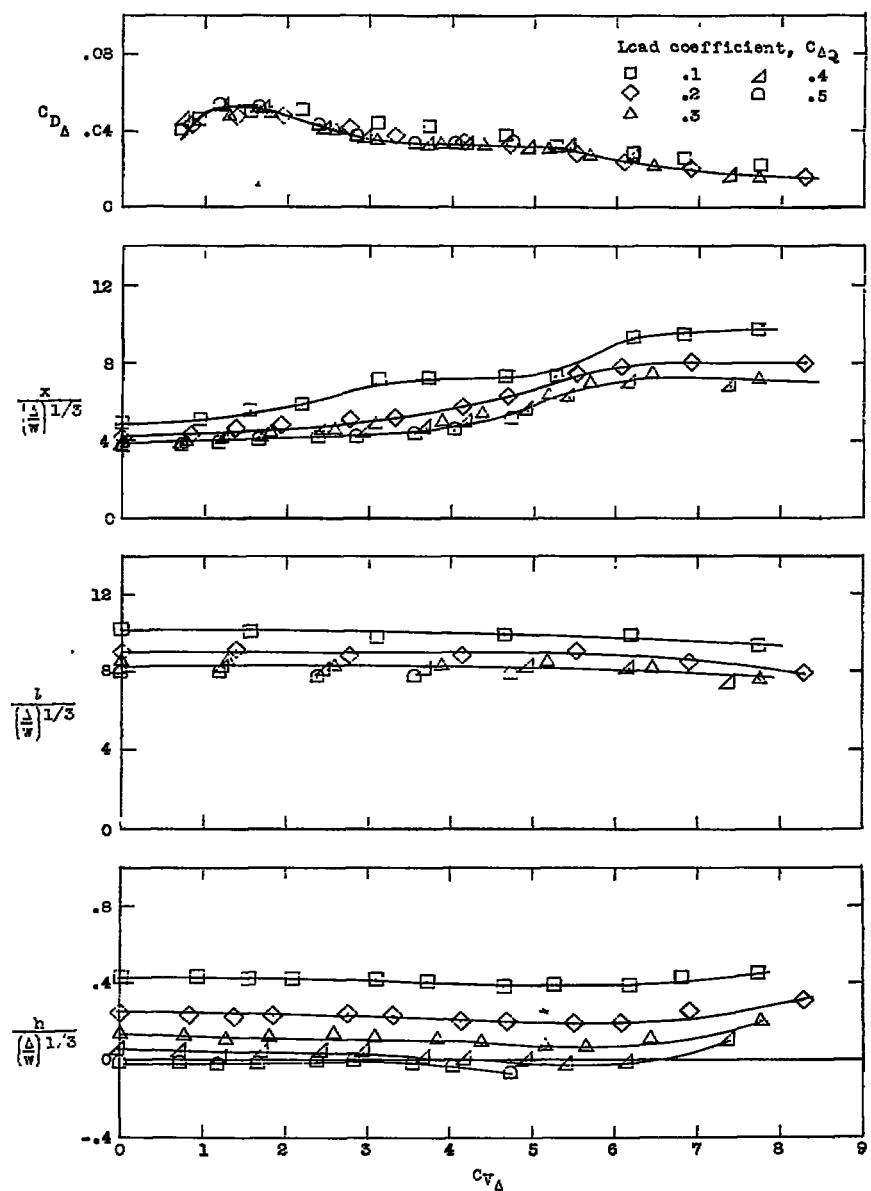
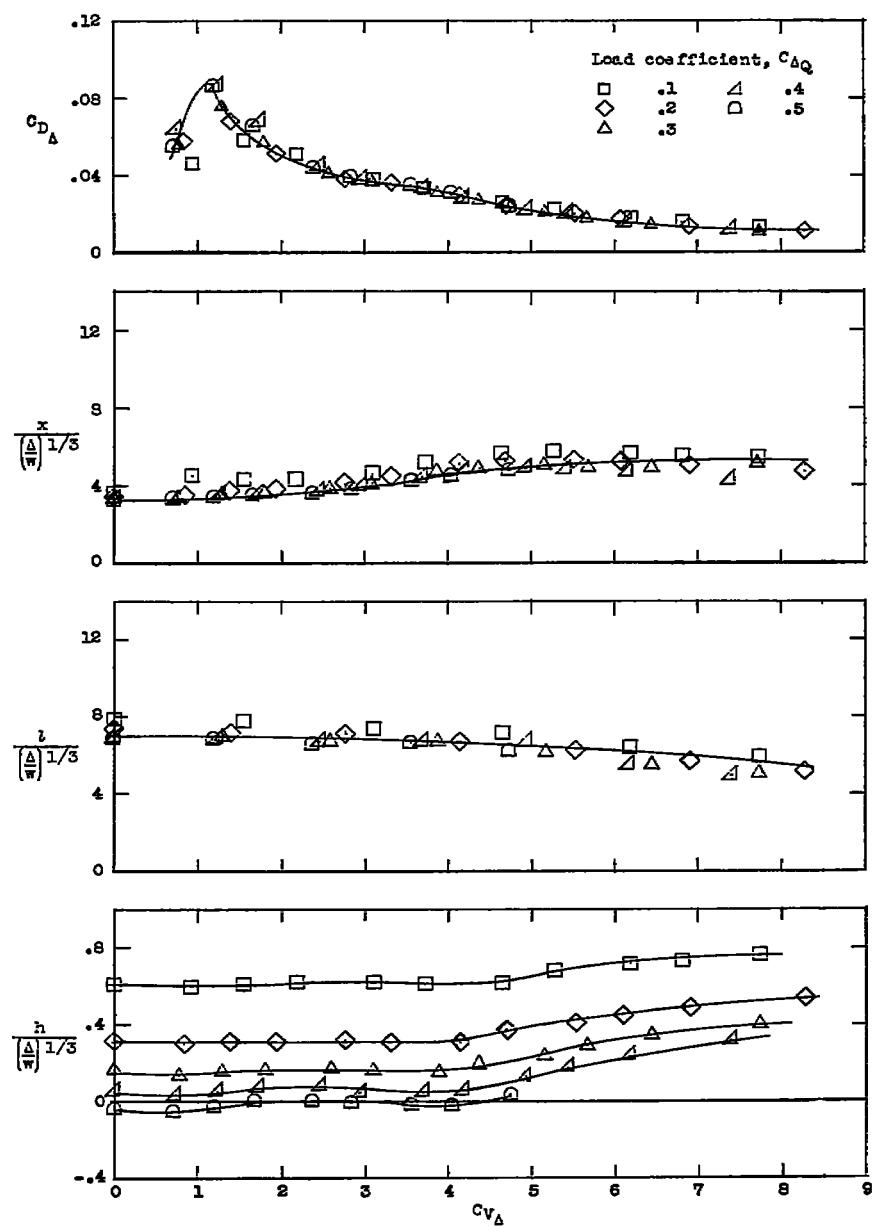
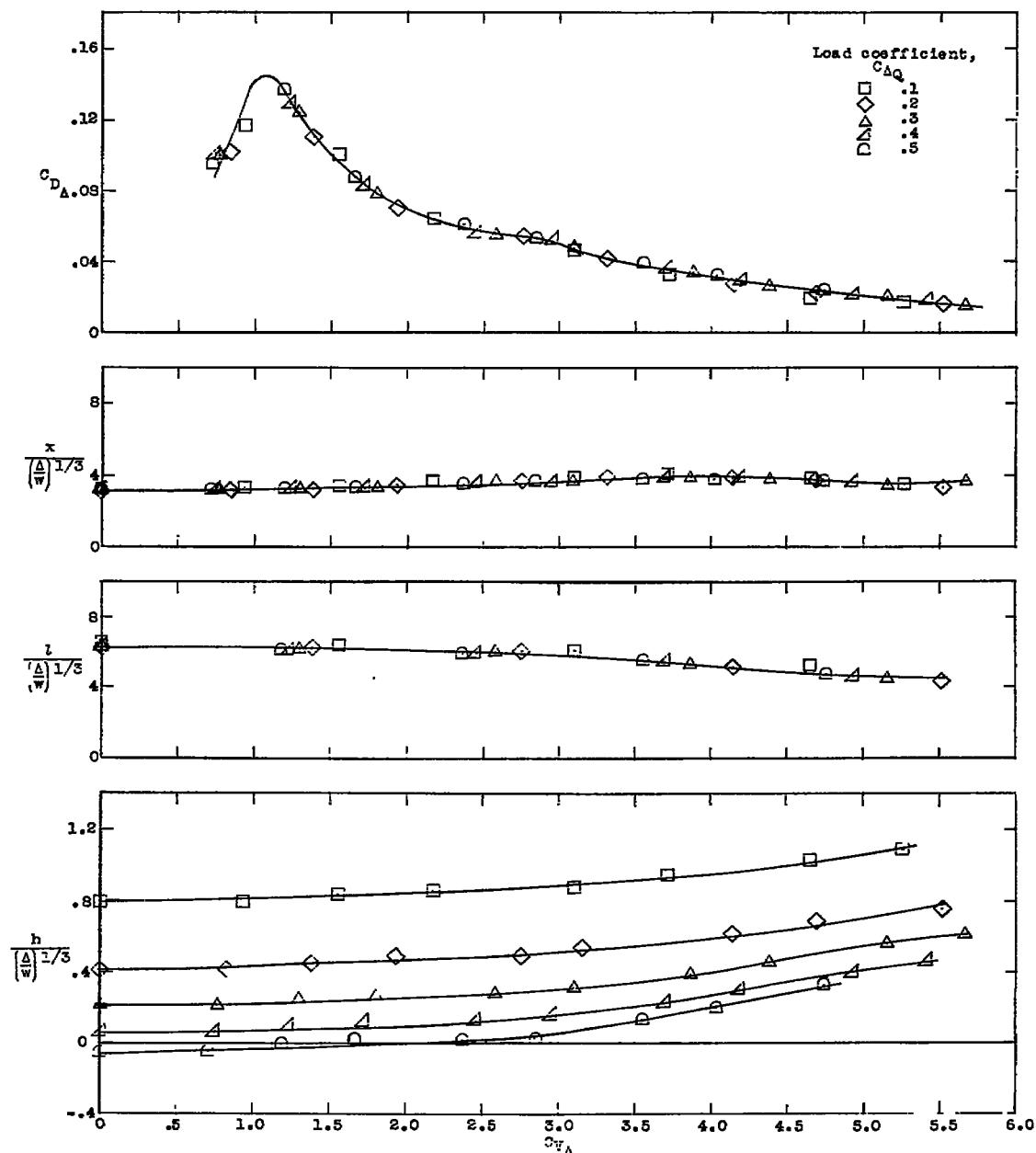
(b) Trim, 4° .

Figure 9.- Continued.



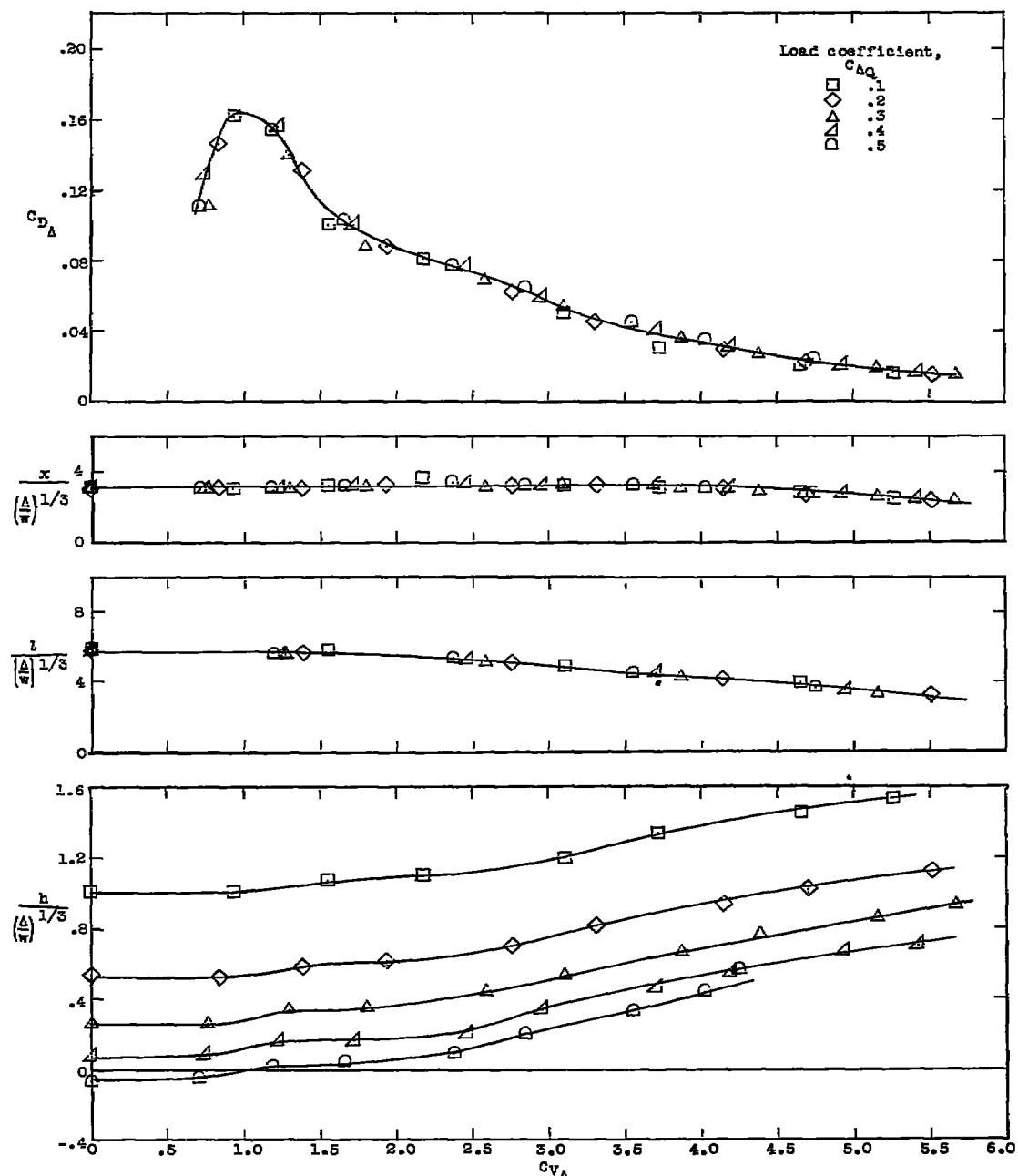
(c) Trim, 8°.

Figure 9.- Continued.



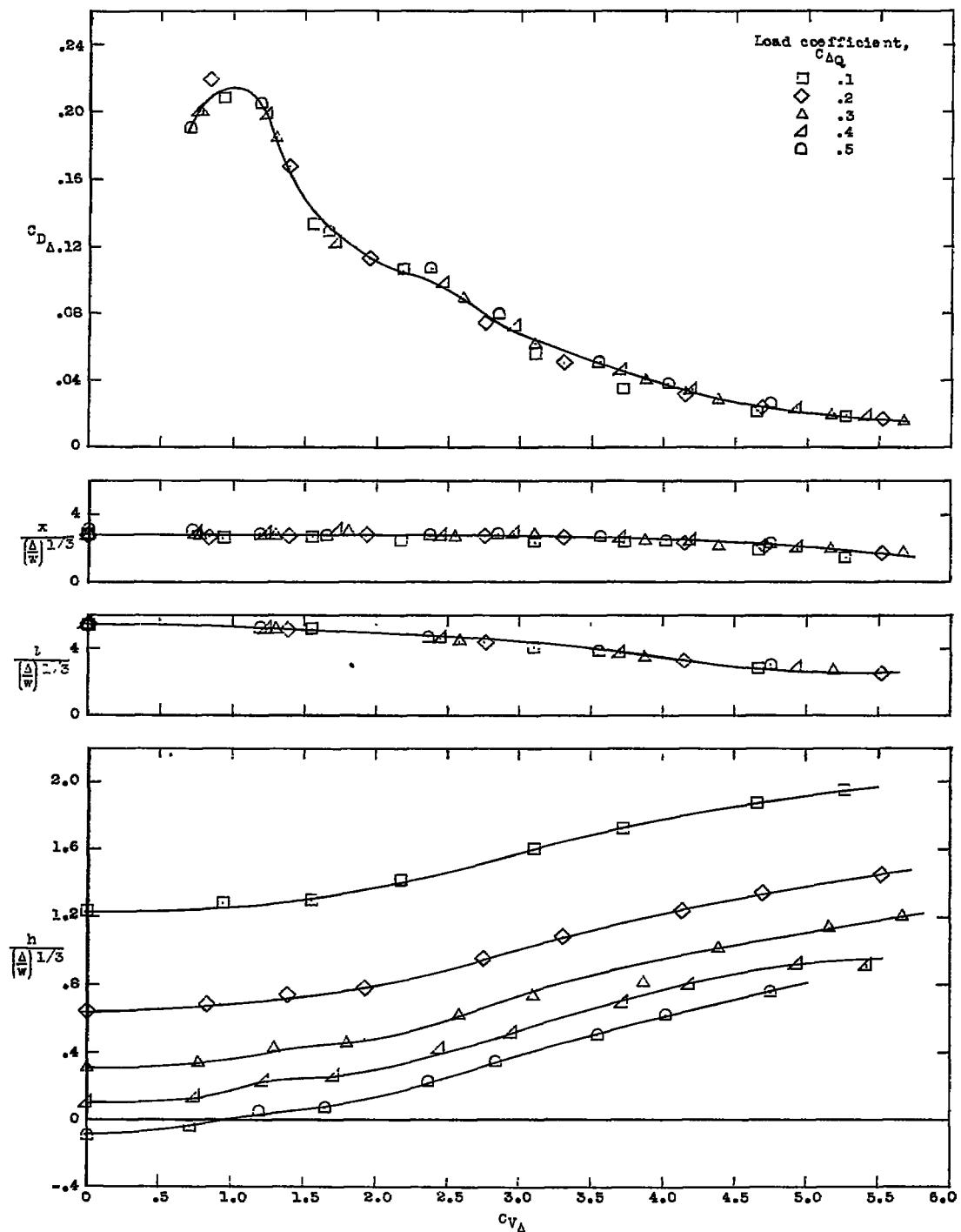
(d) Trim, 12°.

Figure 9.- Continued.



(e) Trim, 16°.

Figure 9--Continued.



(f) Trim, 20°.

Figure 9.- Concluded.

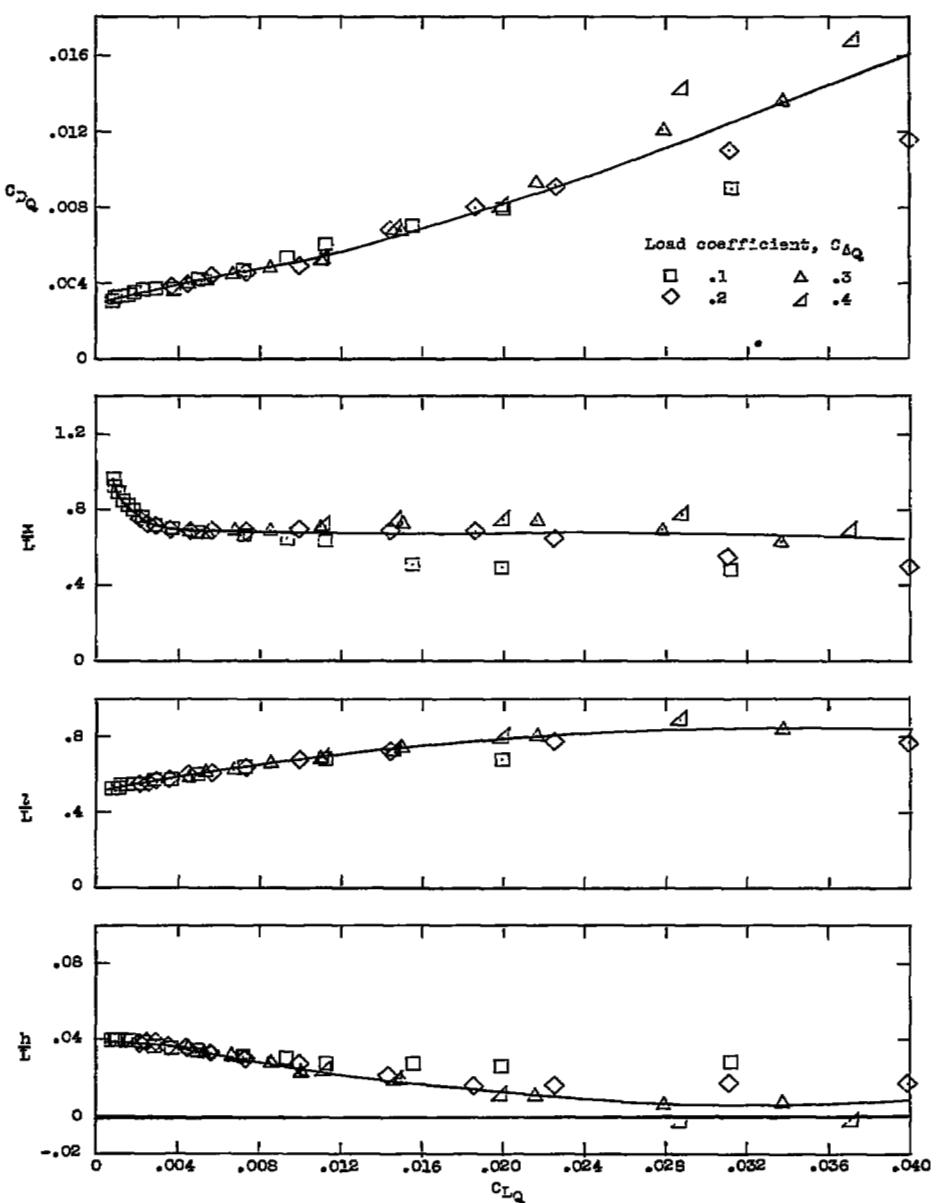
(a) Trim, 4° .

Figure 10.- Hydrodynamic characteristics of model with chine strips.
Fineness ratio 12; planing condition.

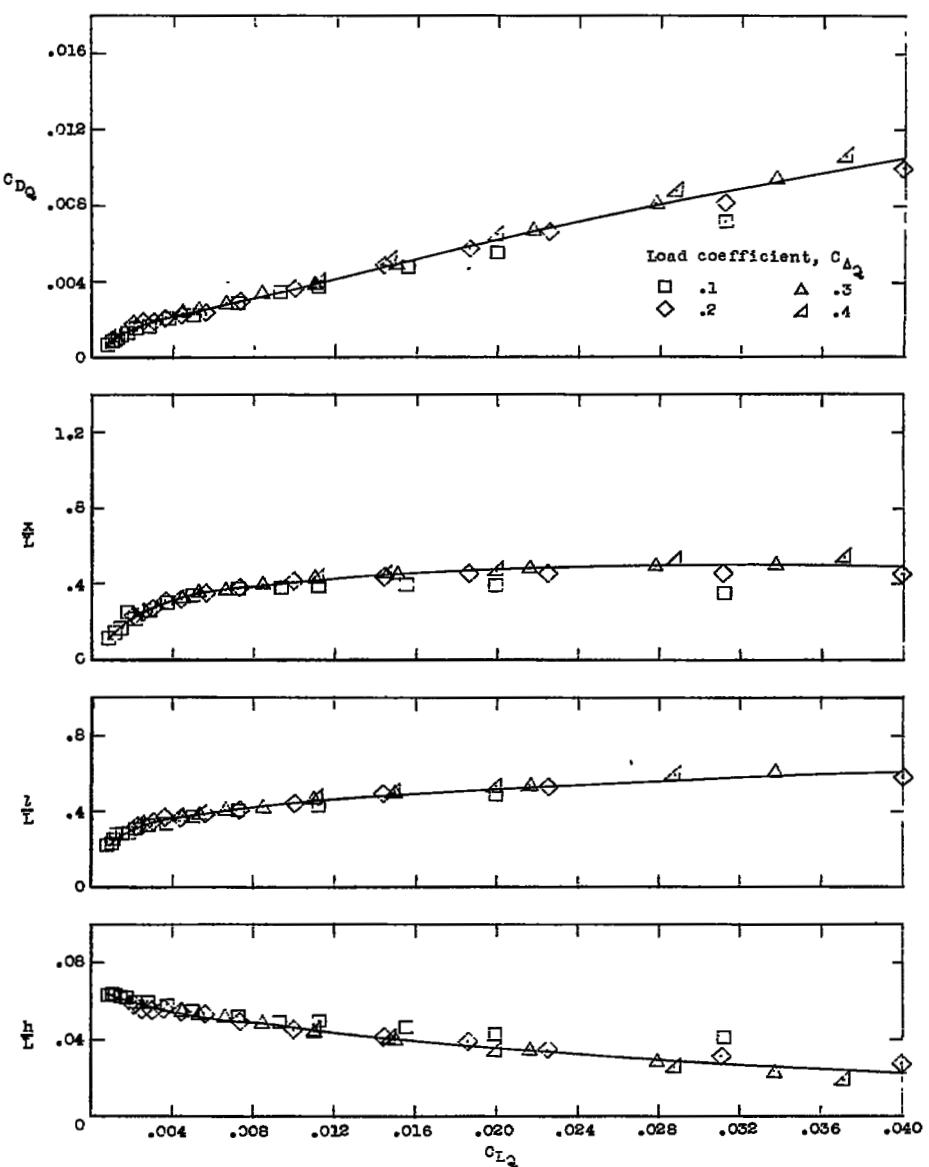
(b) Trim, 8° .

Figure 10.- Continued.

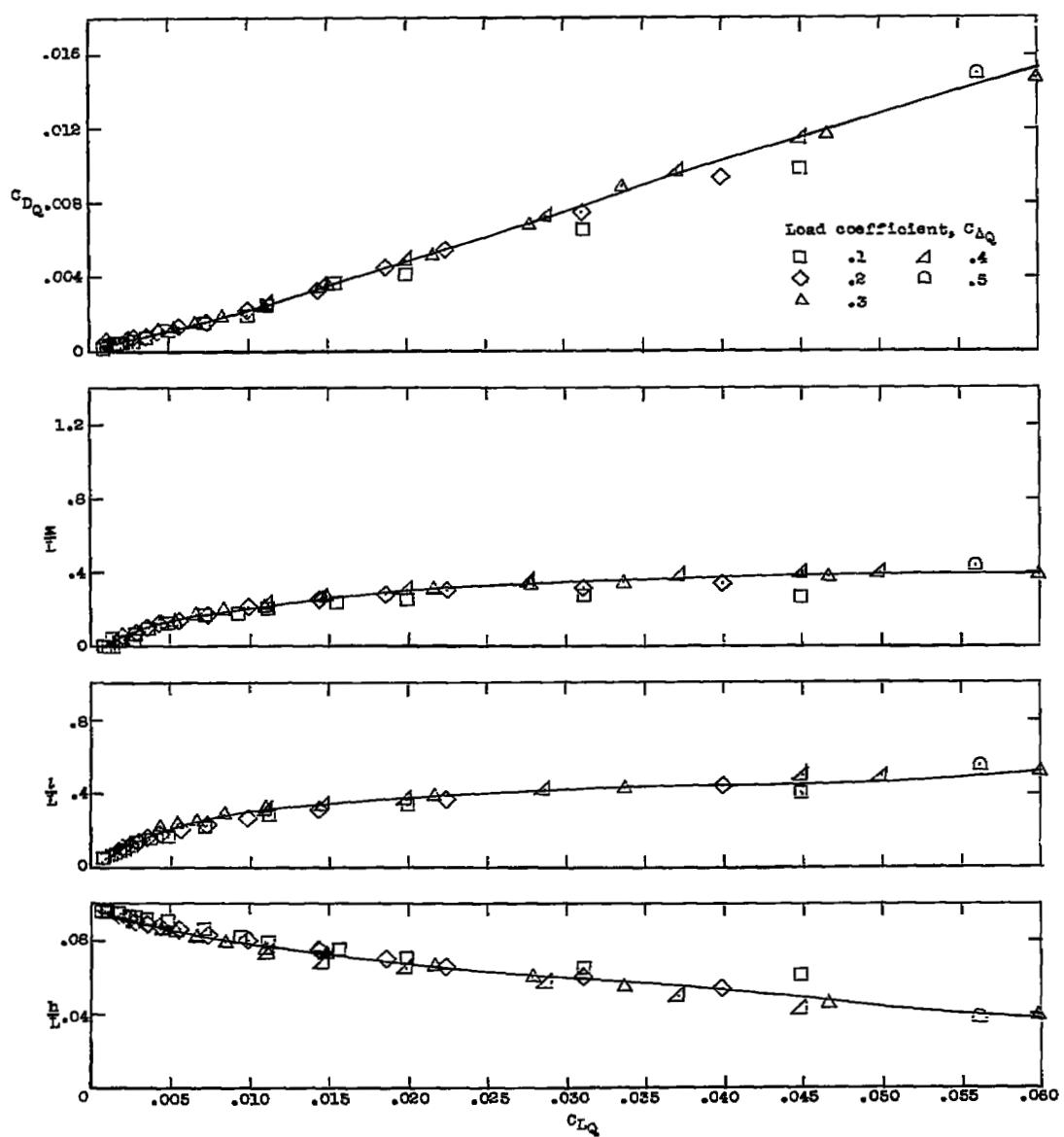
(c) Trim, 12° .

Figure 10.- Continued.

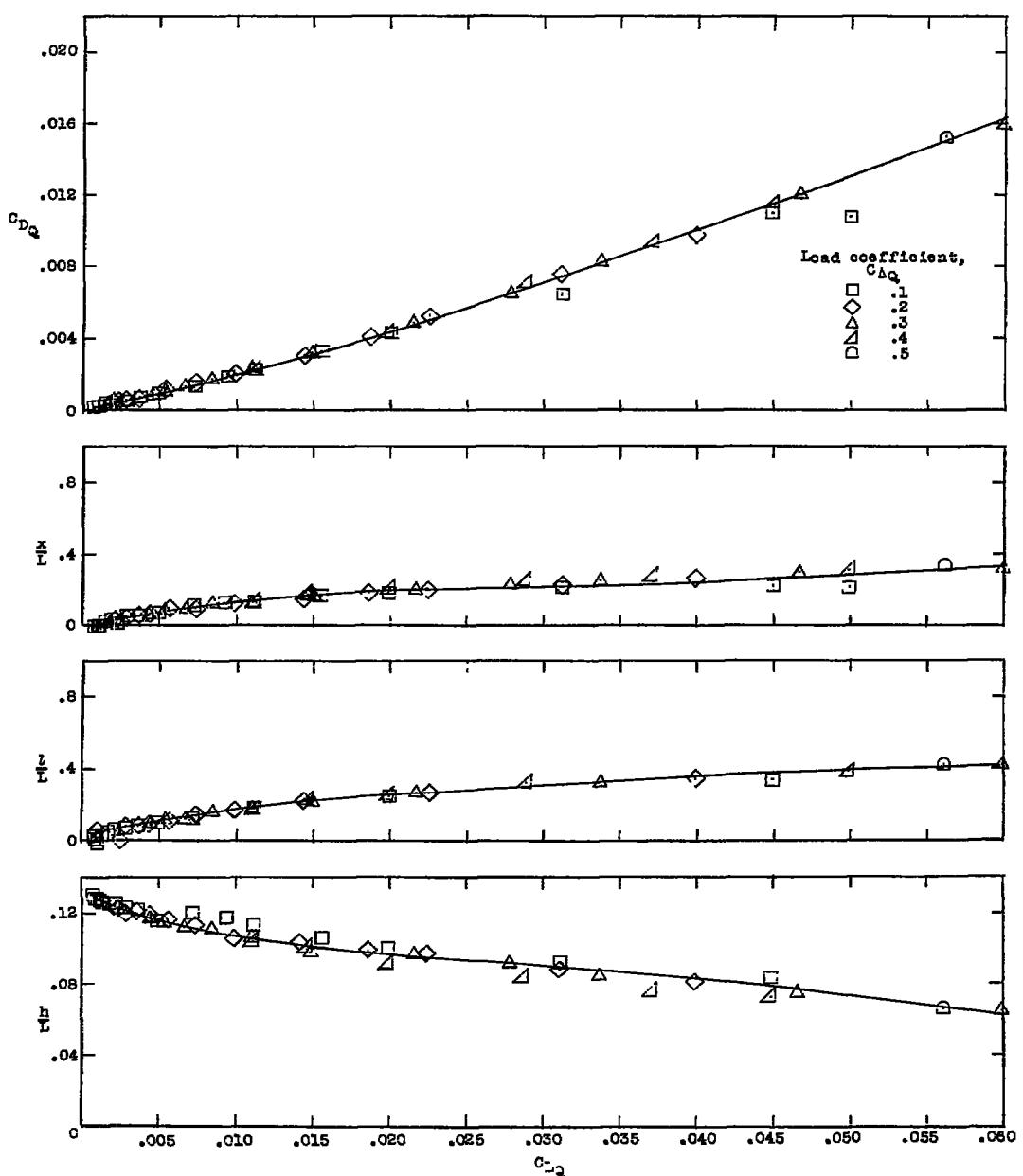
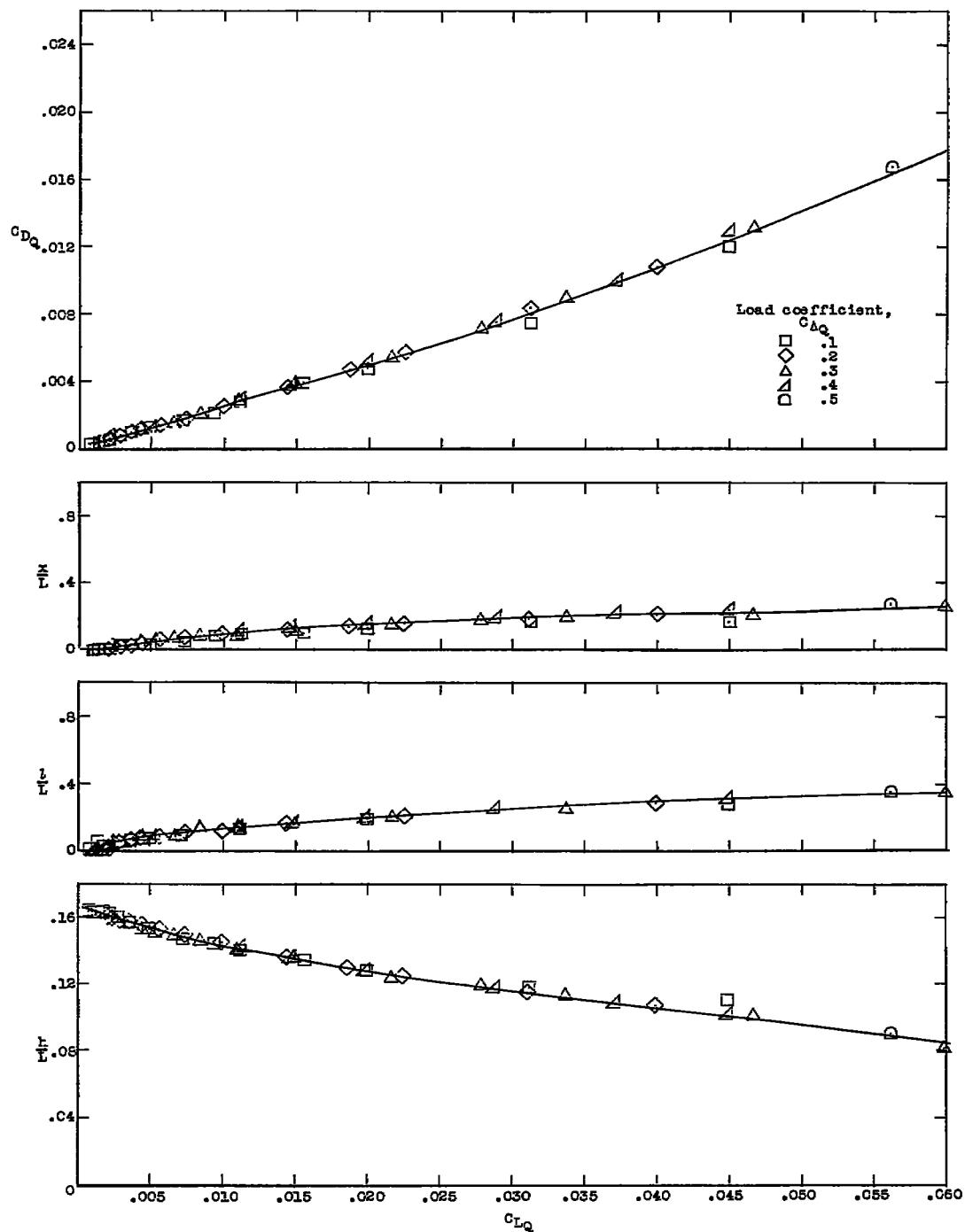
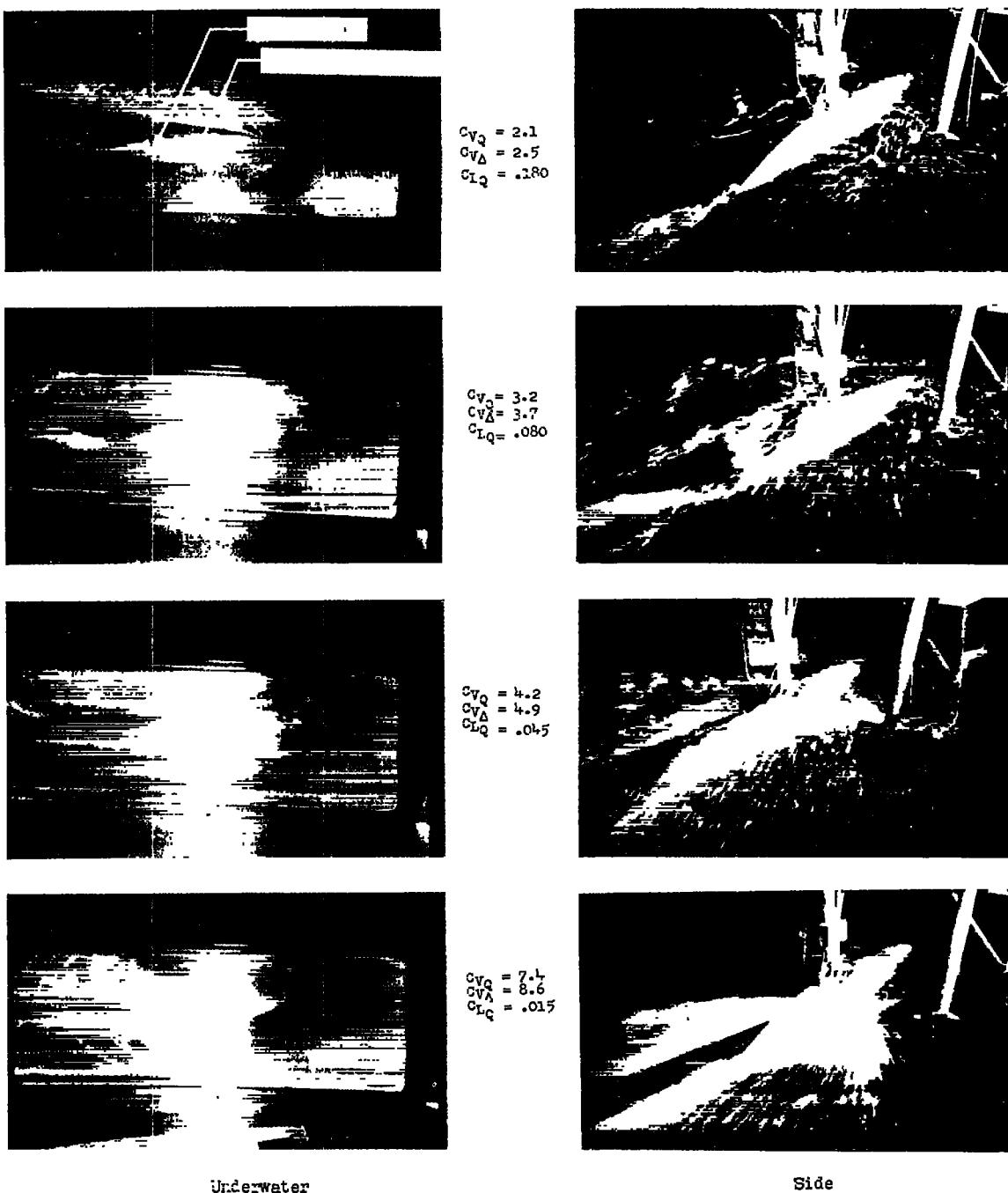
(d) Trim, 16° .

Figure 10.- Continued.



(e) Trim, 20°.

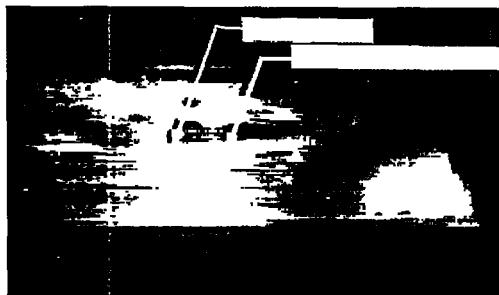
Figure 10.- Concluded.



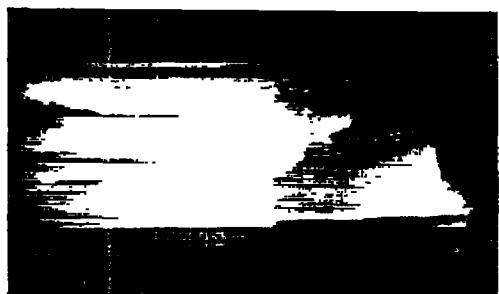
(a) Fineness ratio 6.

L-86475

Figure 11.- Spray characteristics of model with chine strips. Trim, 8° ;
load coefficient $C_{\Delta Q} = 0.4$.



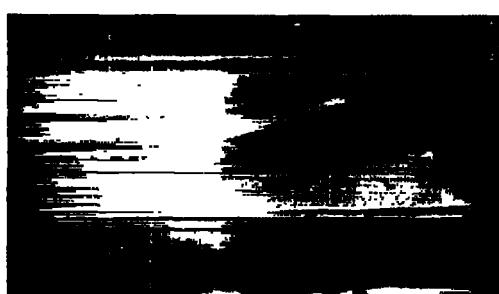
$C_{VQ} = 2.1$
 $C_{V\Delta} = 2.5$
 $C_{LQ} = .180$



$C_{VQ} = 3.2$
 $C_{V\Delta} = 3.7$
 $C_{LQ} = .060$



$C_{VQ} = 4.2$
 $C_{V\Delta} = 4.9$
 $C_{LQ} = -.045$



$C_{VQ} = 7.4$
 $C_{V\Delta} = 6.6$
 $C_{LQ} = .015$



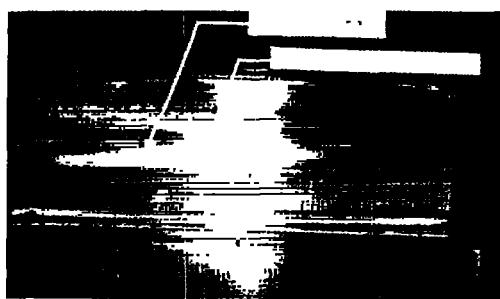
Underwater

Side

(b) Fineness ratio 9.

L-86476

Figure 11.- Continued.



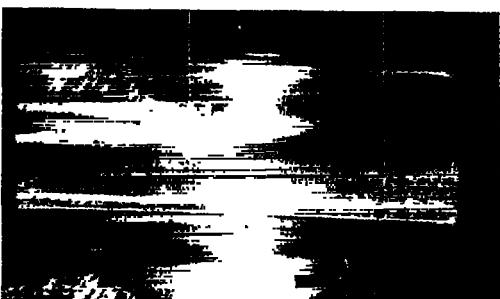
$C_{VQ} = 2.1$
 $C_{VA} = 2.5$
 $C_{LQ} = .120$



$C_{VQ} = 3.2$
 $C_{VA} = 3.7$
 $C_{LQ} = .090$



$C_{VQ} = 4.2$
 $C_{VA} = 4.9$
 $C_{LQ} = .045$



$C_{VQ} = 7.4$
 $C_{VA} = 8.6$
 $C_{LQ} = .015$



(c) Fineness ratio 12.

L-86477

Figure 11.- Concluded.

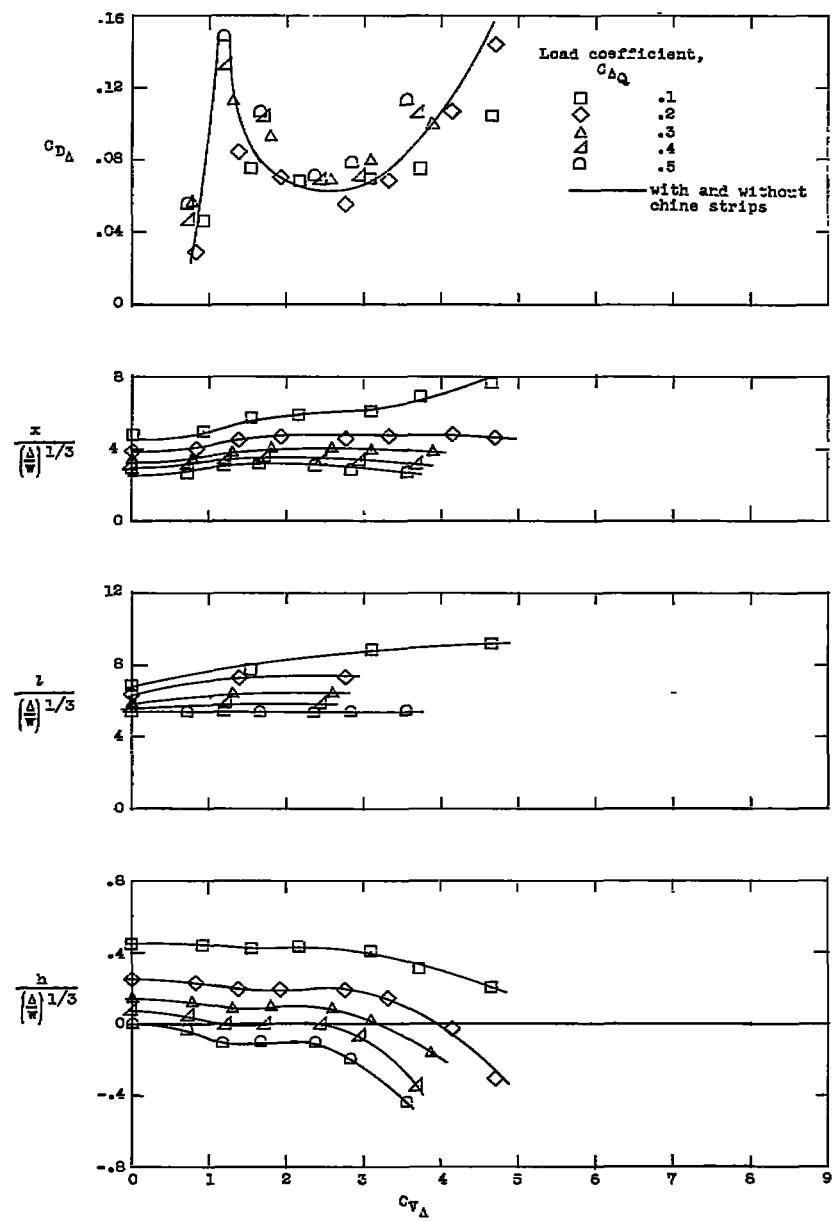
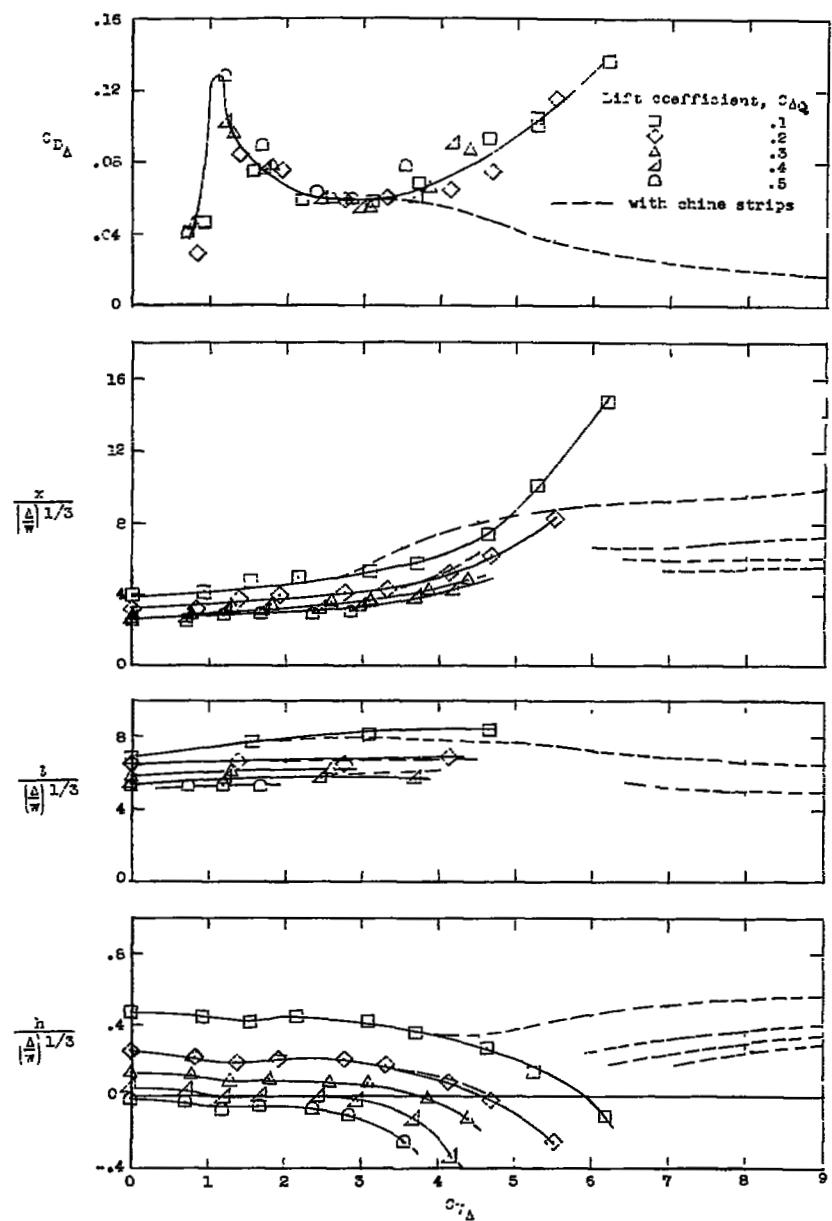
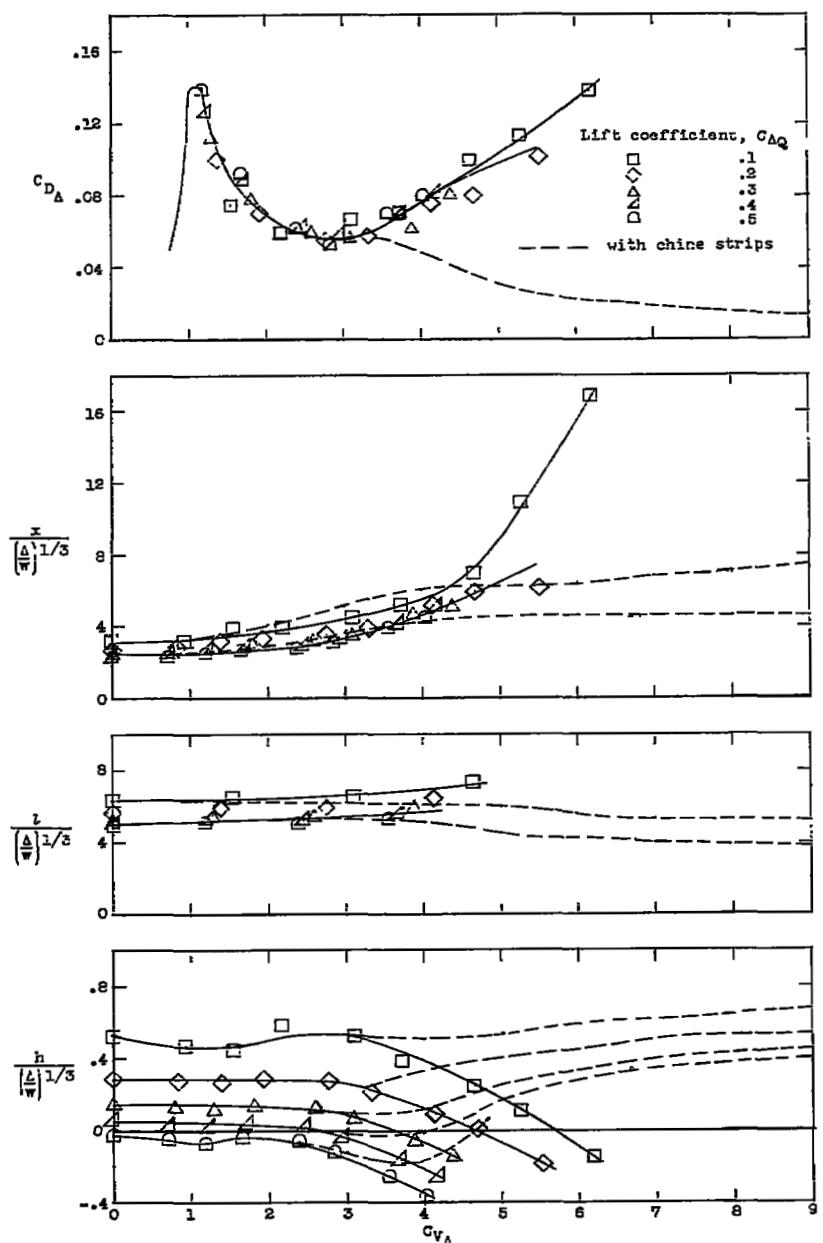
(a) Trim, 0° .

Figure 12.- Hydrodynamic characteristics of models without chine strips.
Fineness ratio 6; displacement condition.



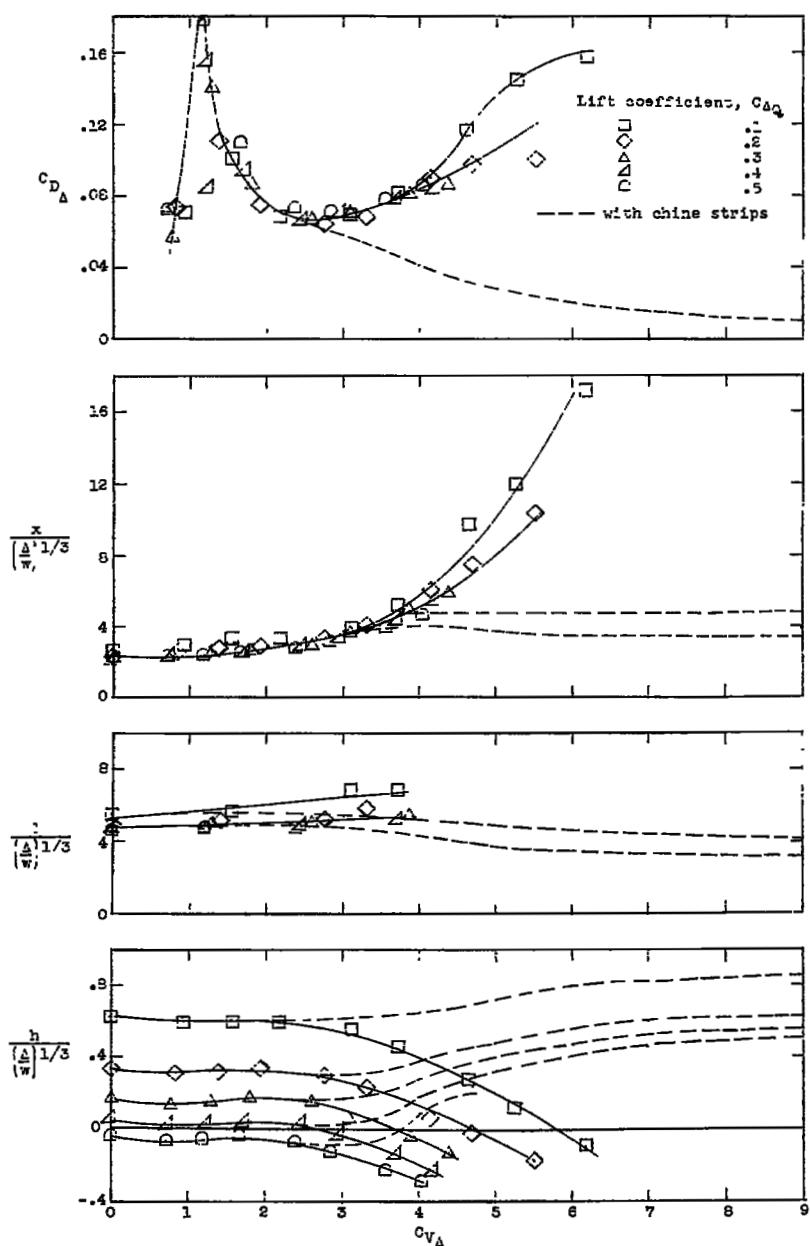
(b) Trim, 4°.

Figure 12.- Continued.



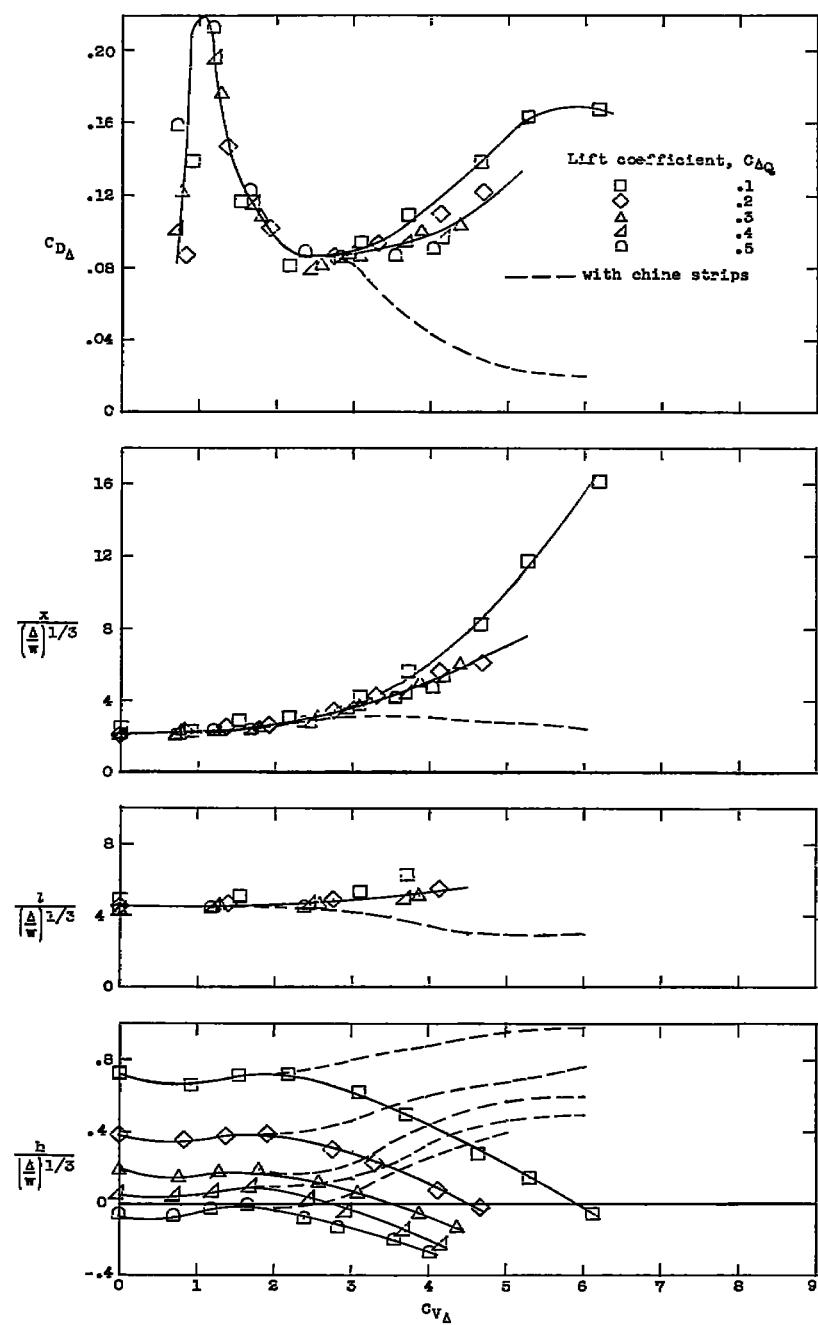
(c) Trim, 8°.

Figure 12.- Continued.



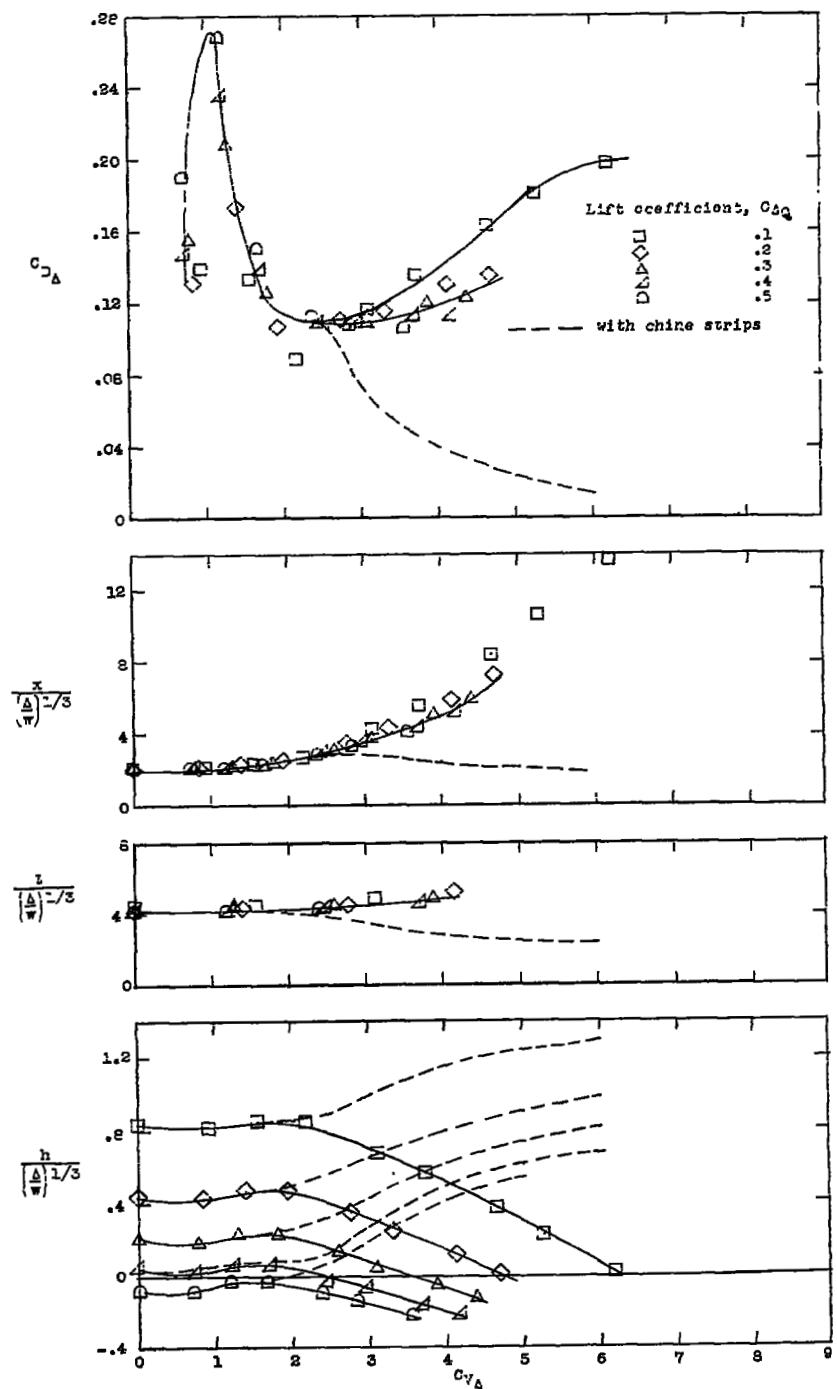
(d) Trim, 12°.

Figure 12.- Continued.



(e) Trim, 16°.

Figure 12.- Continued.



(r) Trim, 20°.

Figure 12.- Concluded.

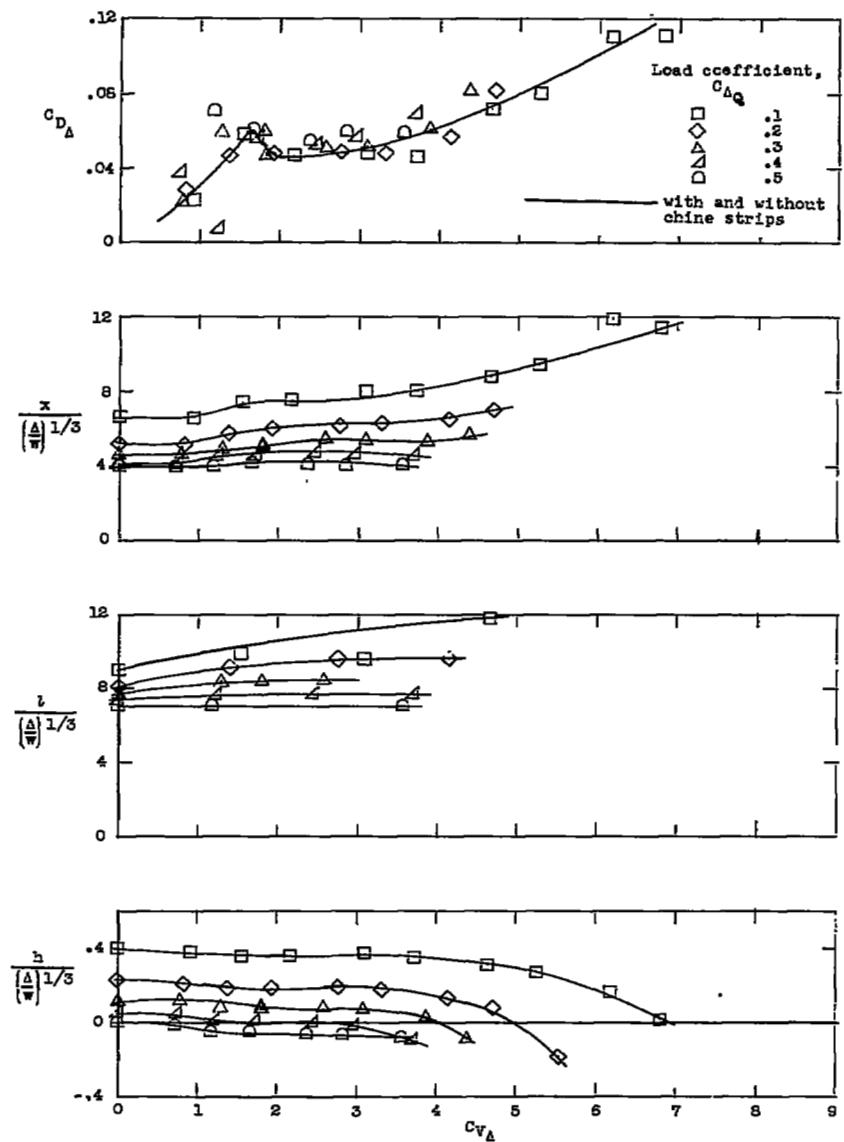
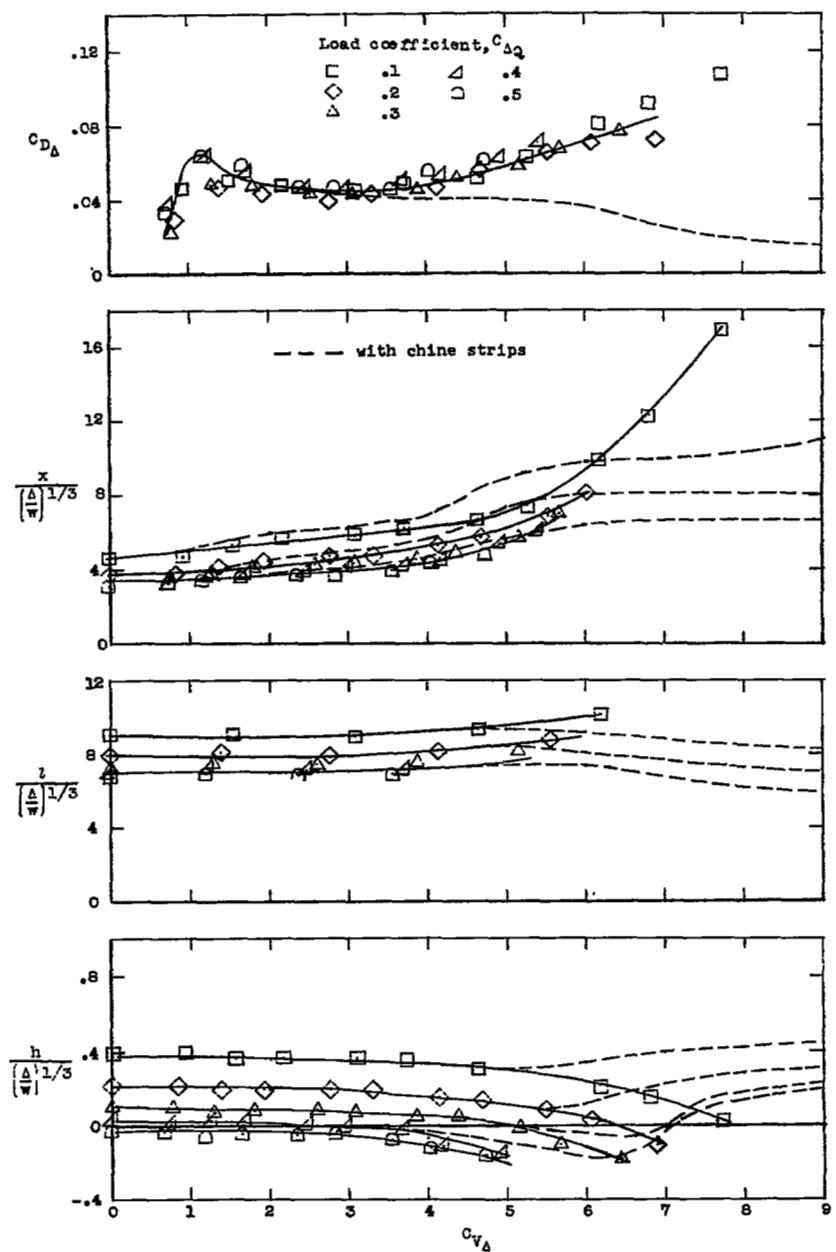
(a) Trim, 0° .

Figure 13.- Hydrodynamic characteristics of models without chine strips.
Fineness ratio 9; displacement condition.



(o) Trim, 4°.

Figure 13.- Continued.

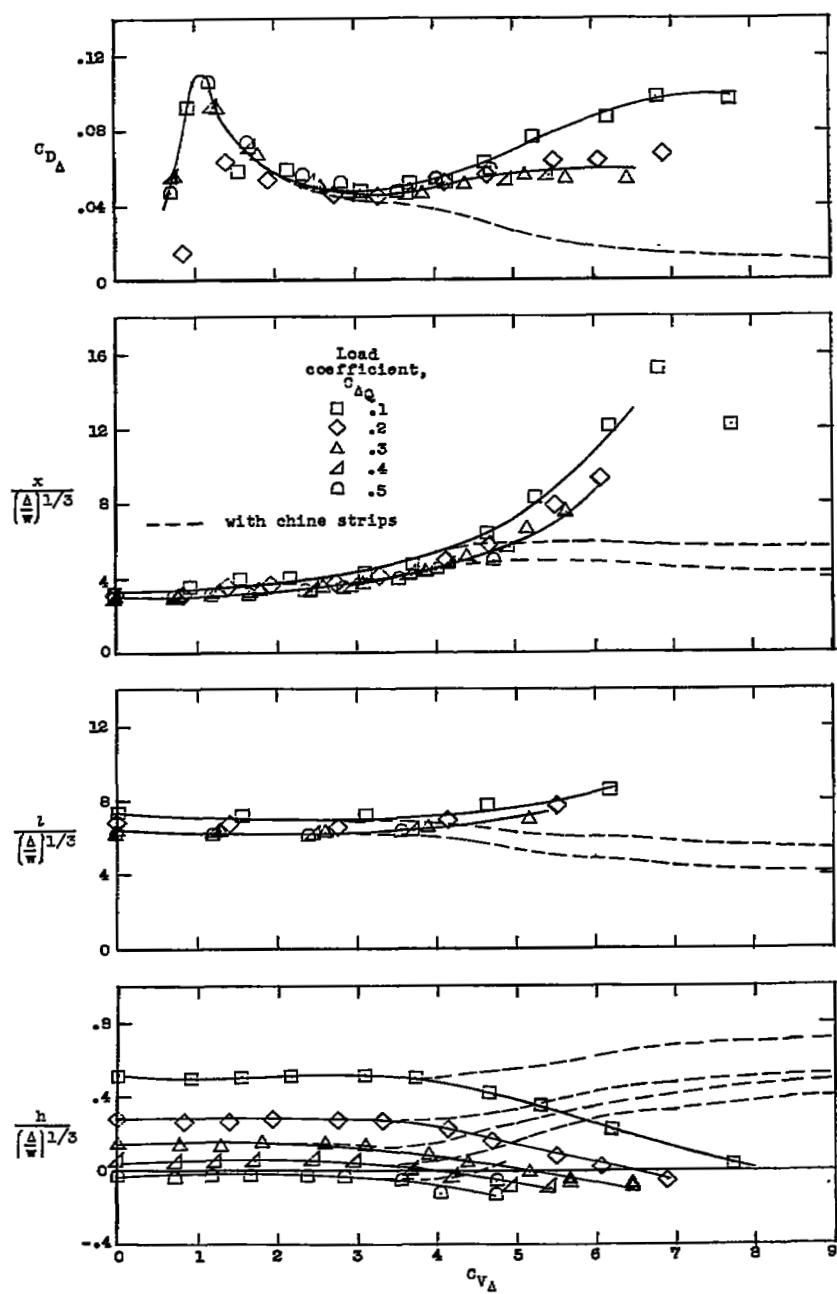
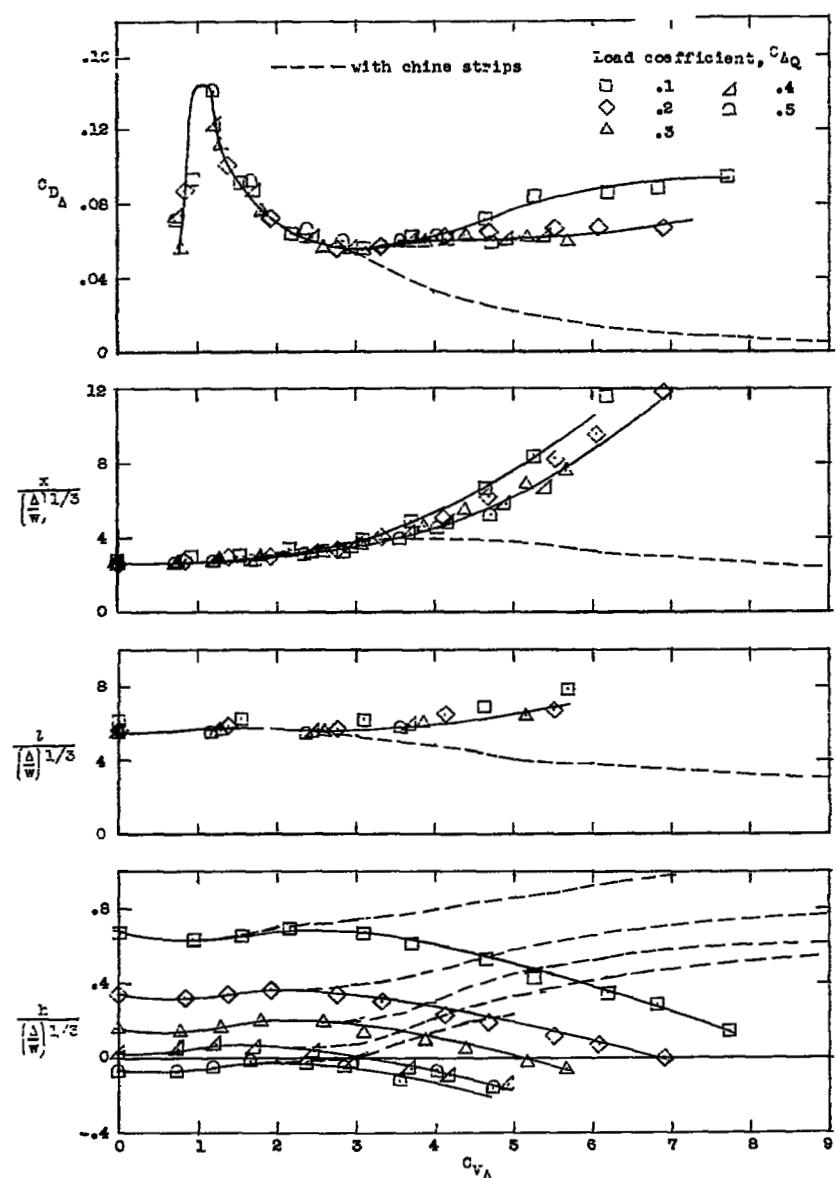
(c) Trim, 8° .

Figure 13.- Continued.



(d) Trim, 12°.

Figure 13.- Continued.

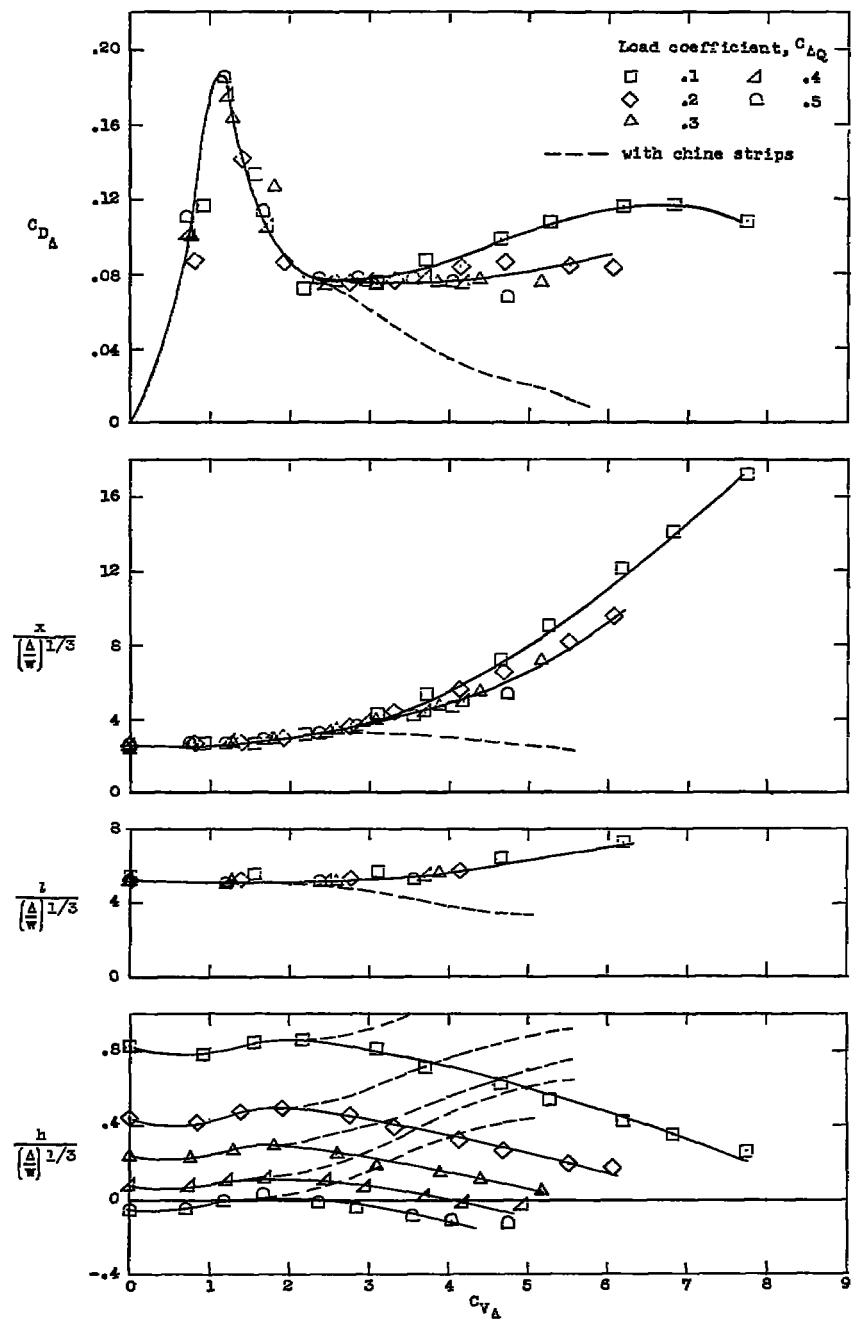
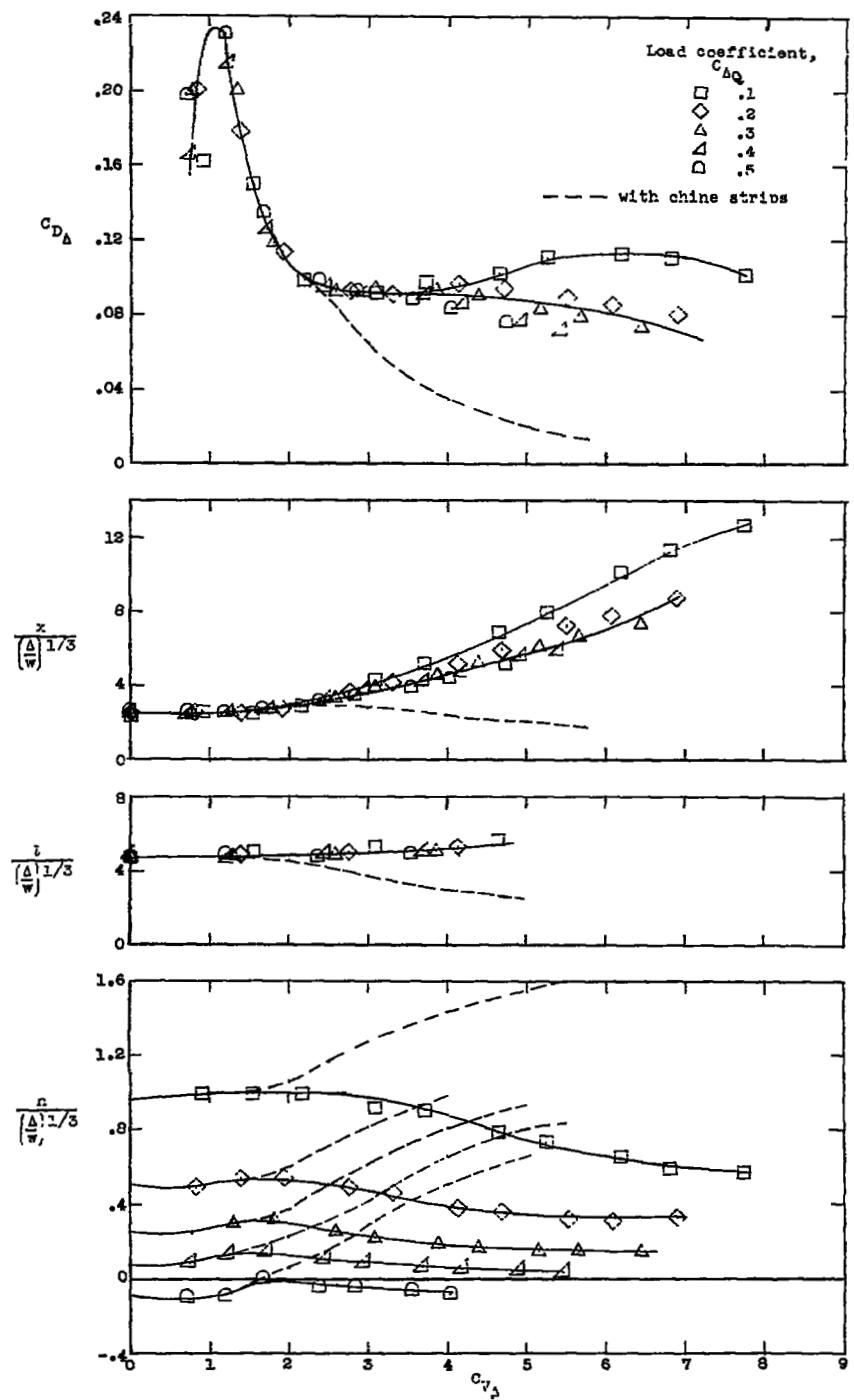
(e) Trim, 16° .

Figure 13.- Continued.



(f) Trim, 20°.

Figure 13.- Concluded.

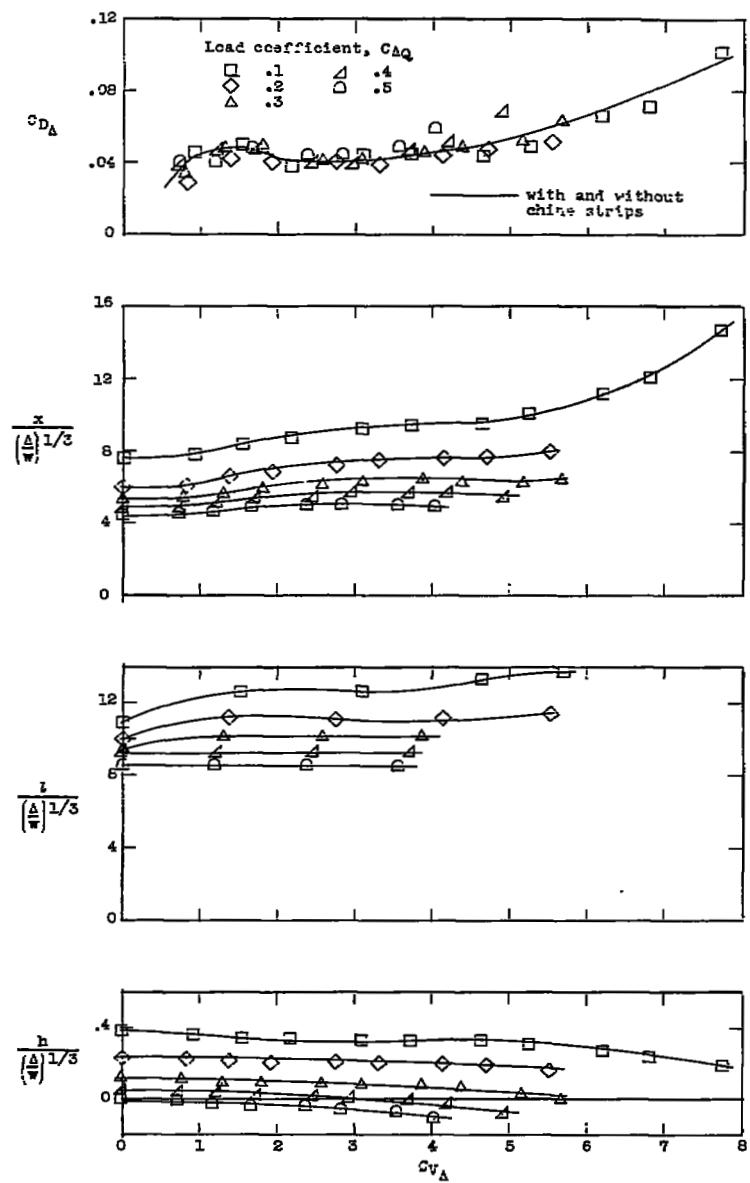
(a) Trim, 0° .

Figure 14.- Hydrodynamic characteristics of models without chine strips.
Fineness ratio 12; displacement condition.

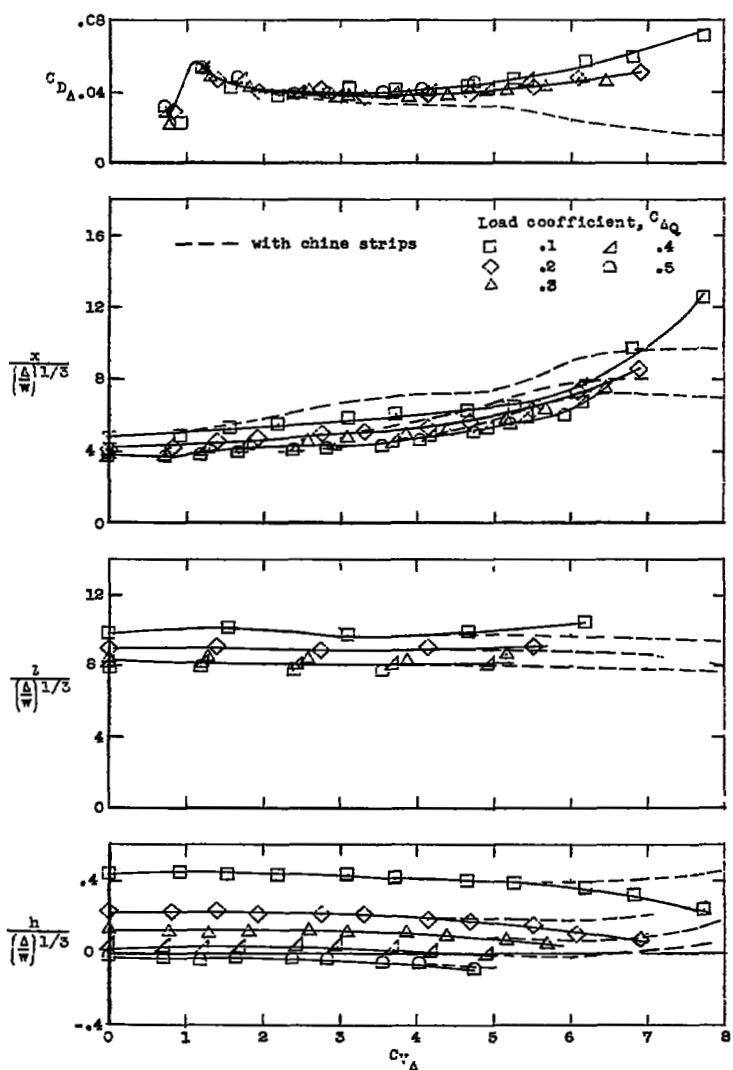
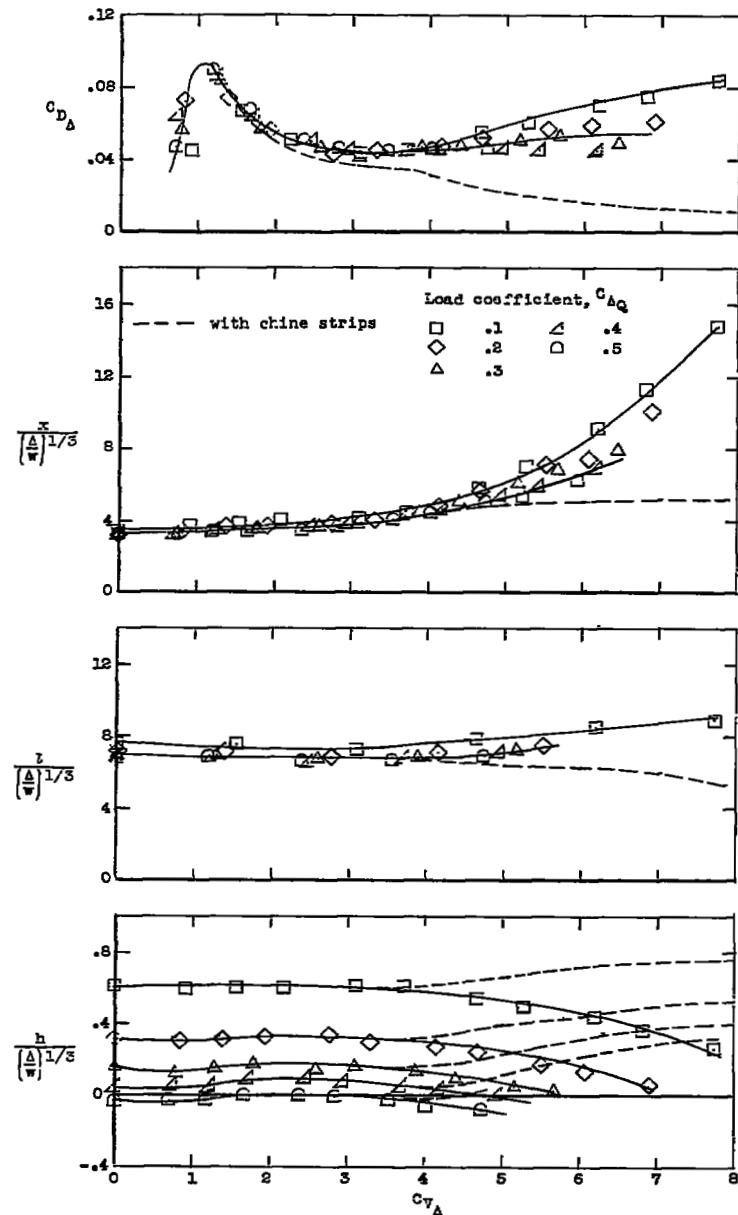
(b) Trim, 4° .

Figure 14.- Continued.



(c) Trim, 8°.

Figure 14.- Continued.

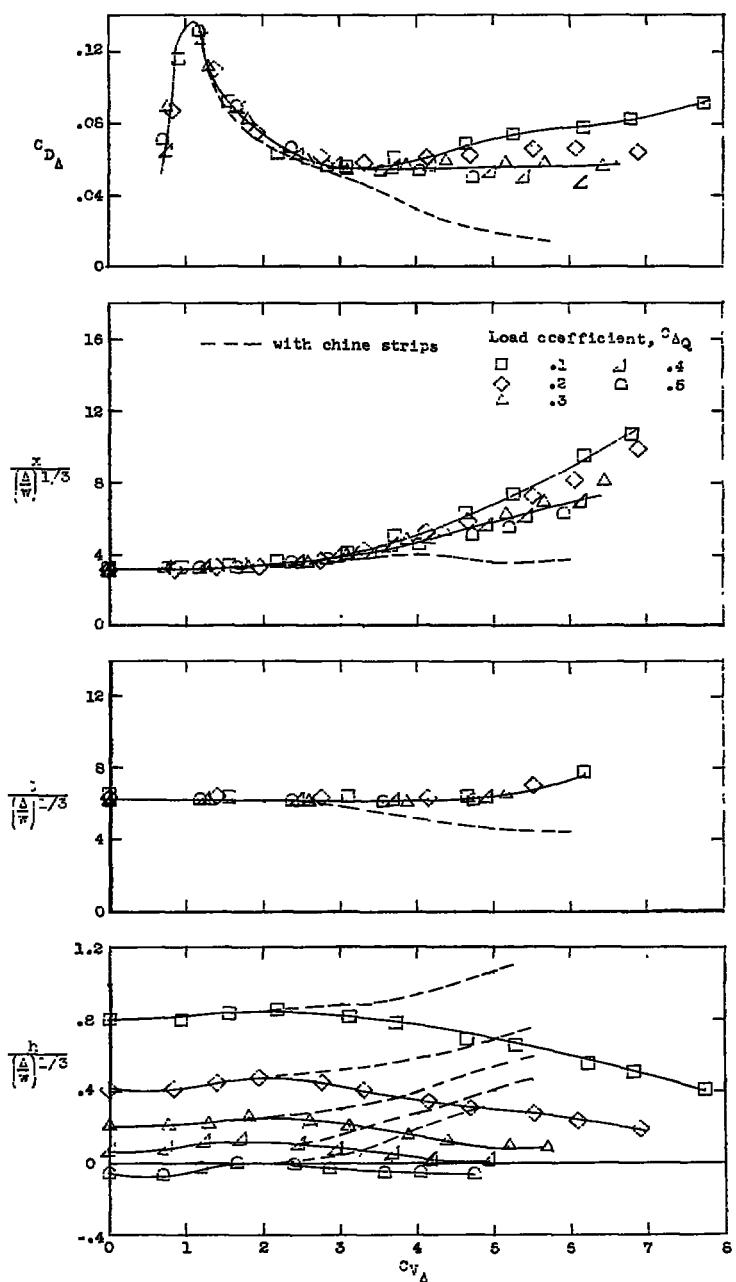
(d) Trim, 12° .

Figure 14.- Continued.

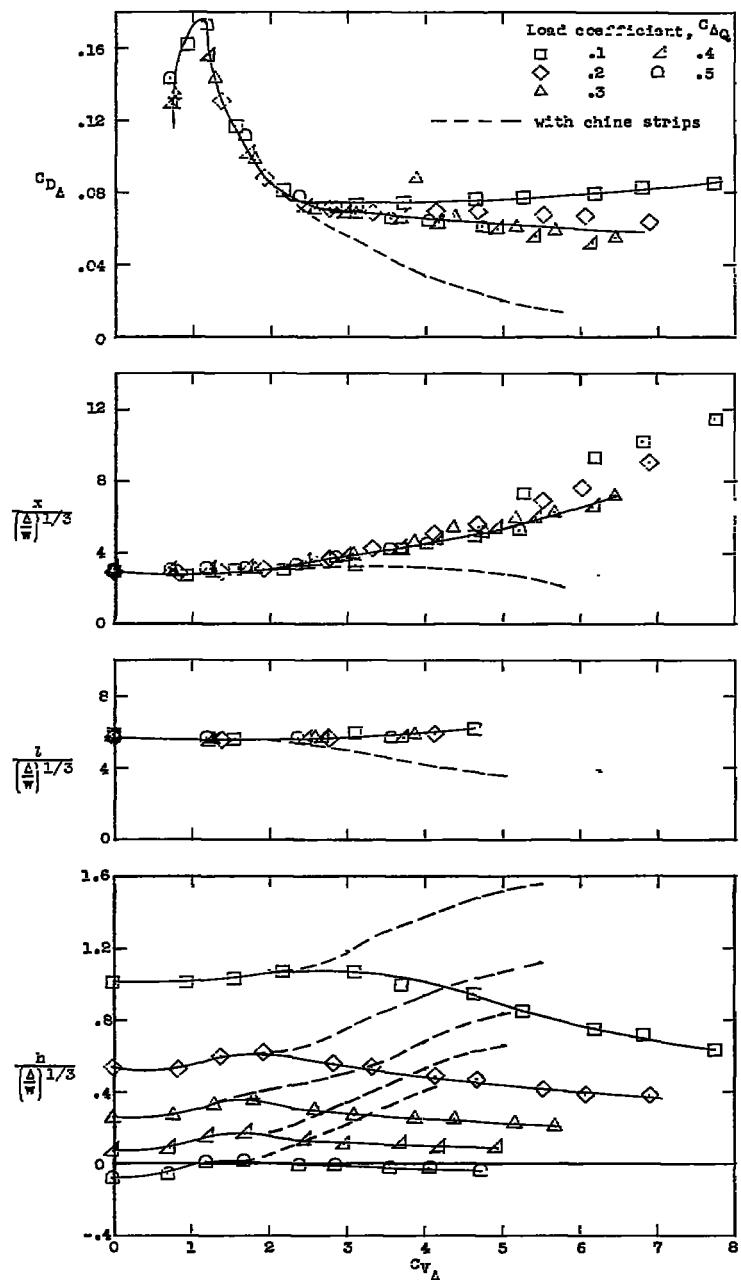
(e) Trim, 16° .

Figure 14.- Continued.

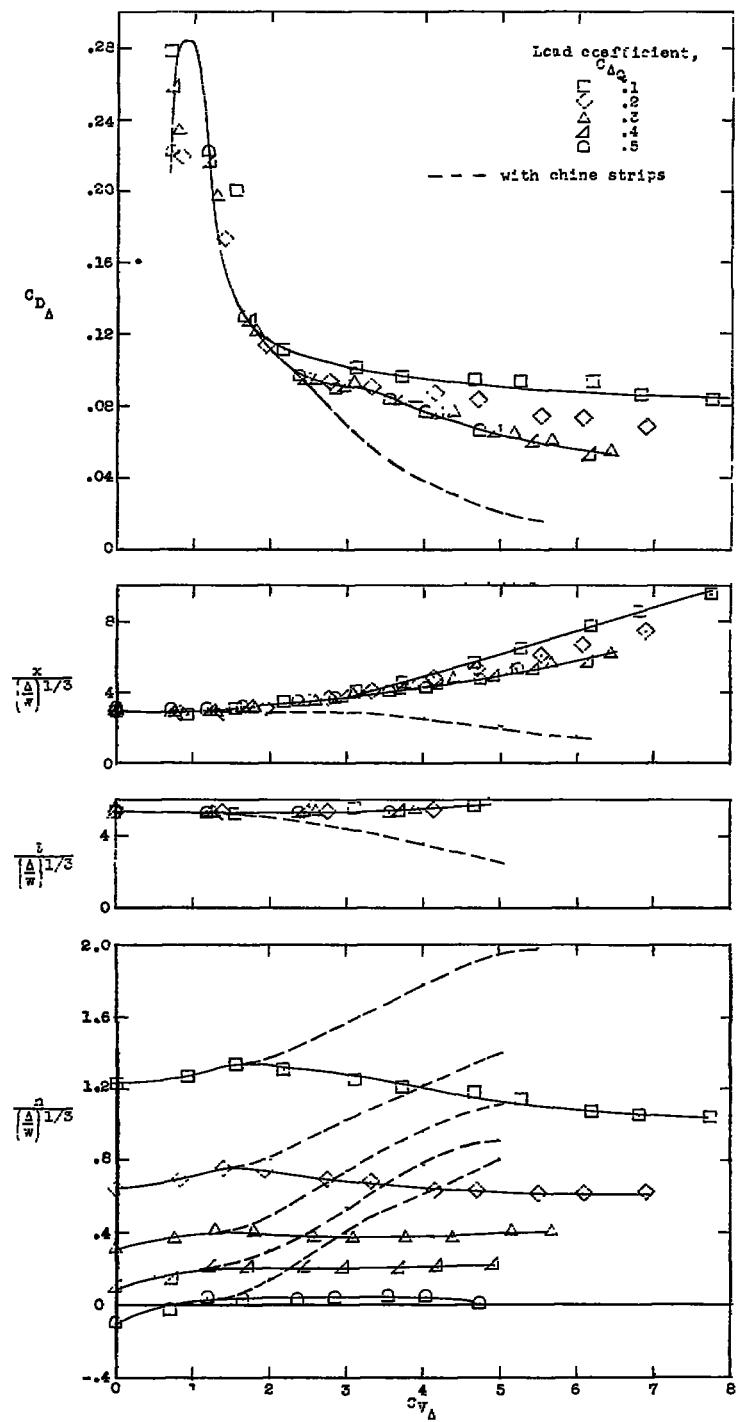
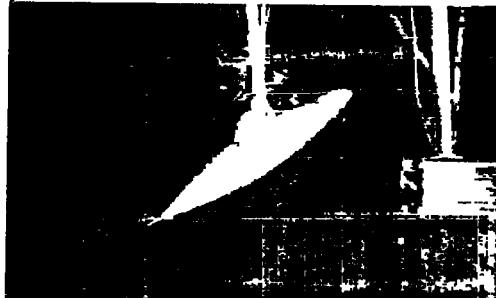


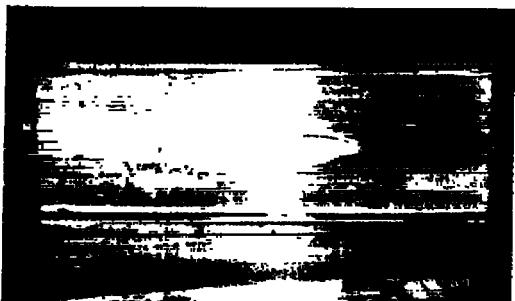
Figure 14.- Concluded.



$C_{VQ} = 1.1$
 $C_{V\Delta} = 1.2$
 $C_{LQ} = .72$



$C_{VQ} = 2.1$
 $C_{V\Delta} = 2.5$
 $C_{LQ} = .18$



$C_{VQ} = 3.2$
 $C_{V\Delta} = 3.7$
 $C_{LQ} = .08$



Underwater

Side

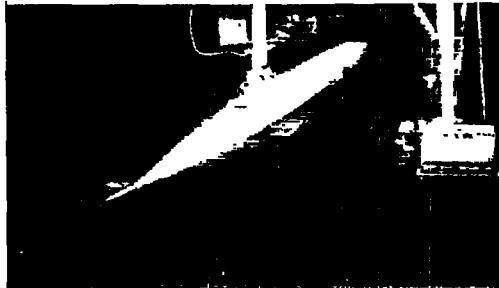
(a) Fineness ratio 6.

L-86478

Figure 15.- Spray characteristics of models without chine strips.
 Trim, 8° ; load coefficient $C_{\Delta Q} = 0.4$.



$C_{VQ} = 1.1$
 $C_{V\Delta} = 1.2$
 $C_{LQ} = .72$



$C_{VQ} = 2.1$
 $C_{V\Delta} = 2.5$
 $C_{LQ} = .18$



$C_{VQ} = 3.2$
 $C_{V\Delta} = 3.7$
 $C_{LQ} = .08$



Underwater

Side

(b) Fineness ratio 9.

L-86479

Figure 15.- Continued.



$C_{VQ} = 1.1$
 $C_{V\Delta} = 1.2$
 $C_{LQ} = .72$



$C_{VQ} = 2.1$
 $C_{V\Delta} = 2.5$
 $C_{LQ} = .18$



$C_{VQ} = 3.2$
 $C_{V\Delta} = 3.7$
 $C_{LQ} = .08$



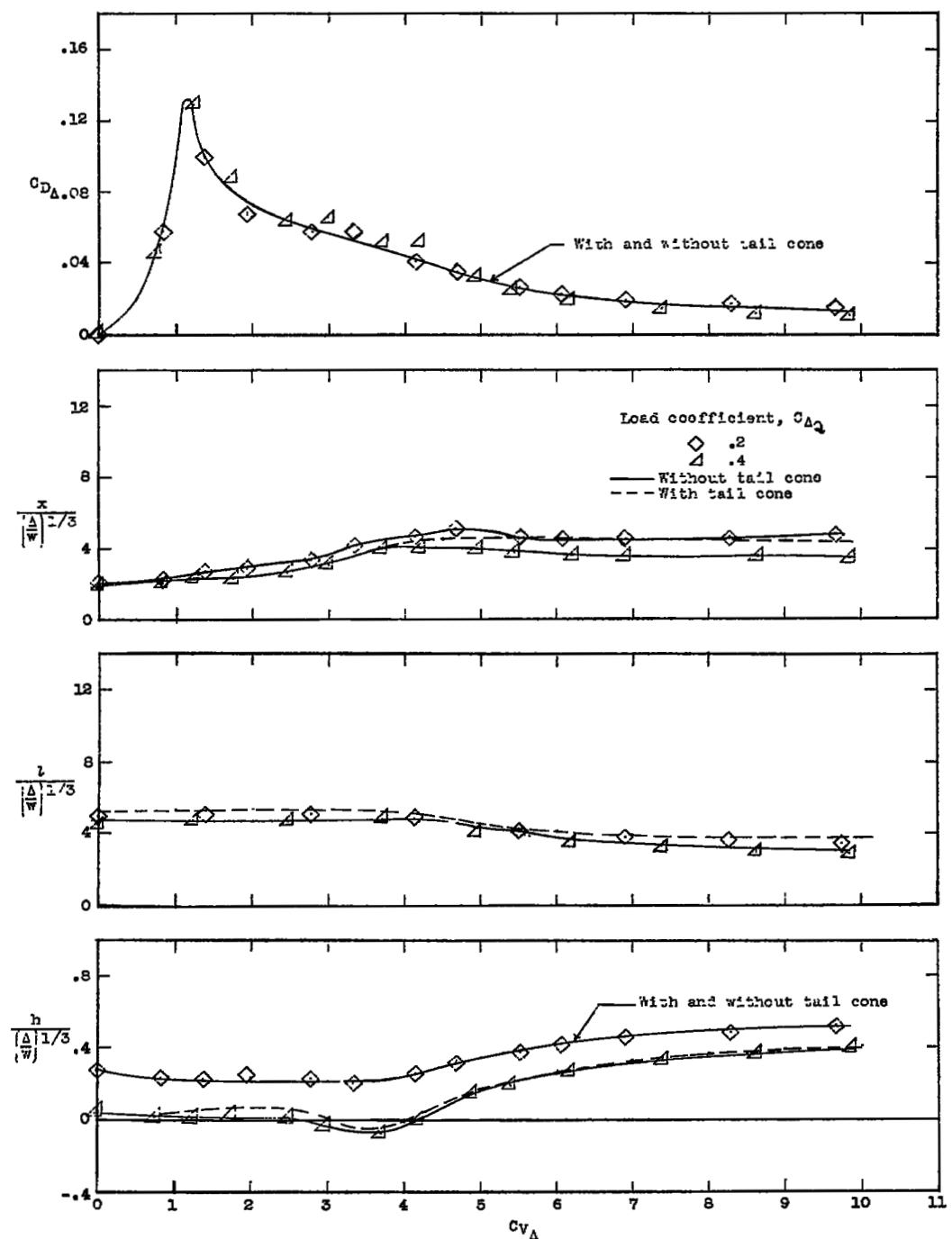
Underwater

Side

(c) Fineness ratio 12.

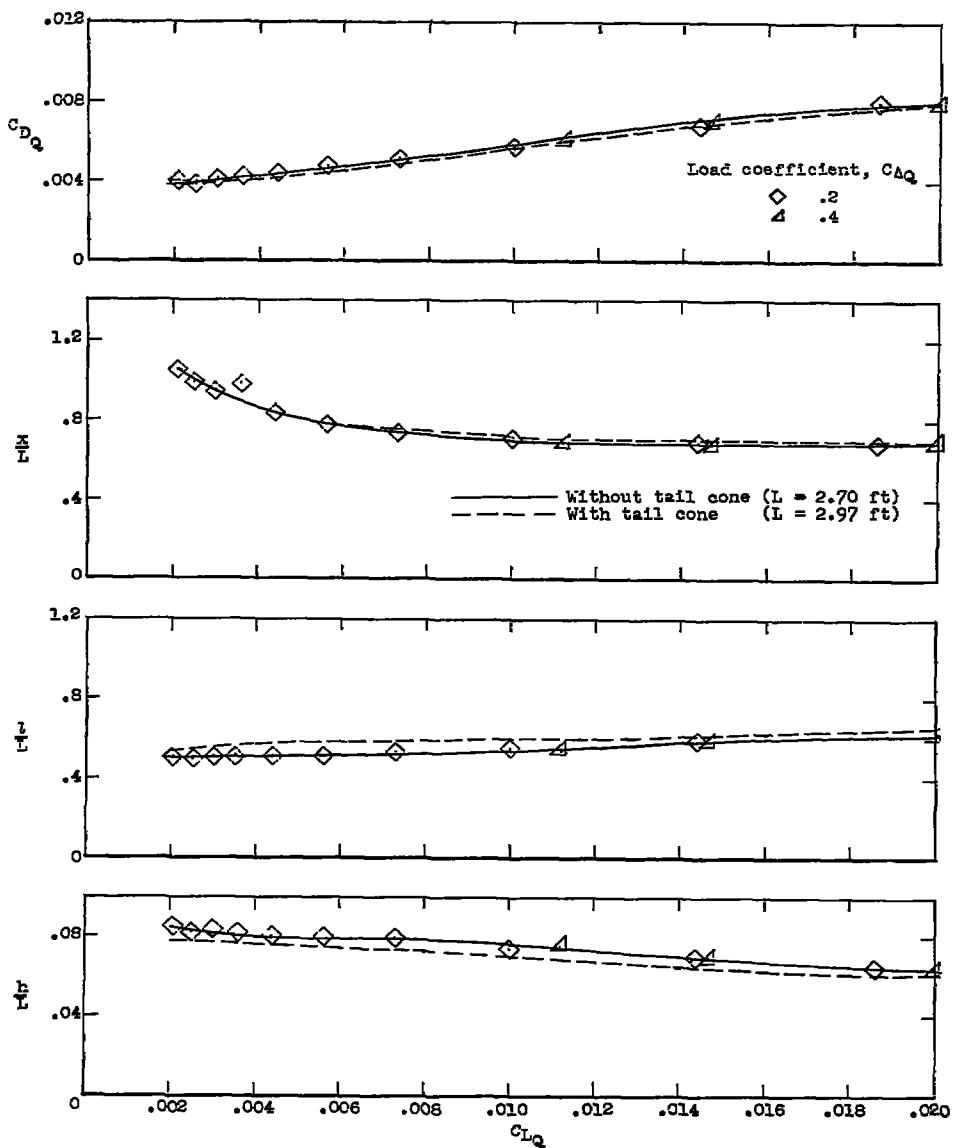
L-86480

Figure 15.- Concluded.



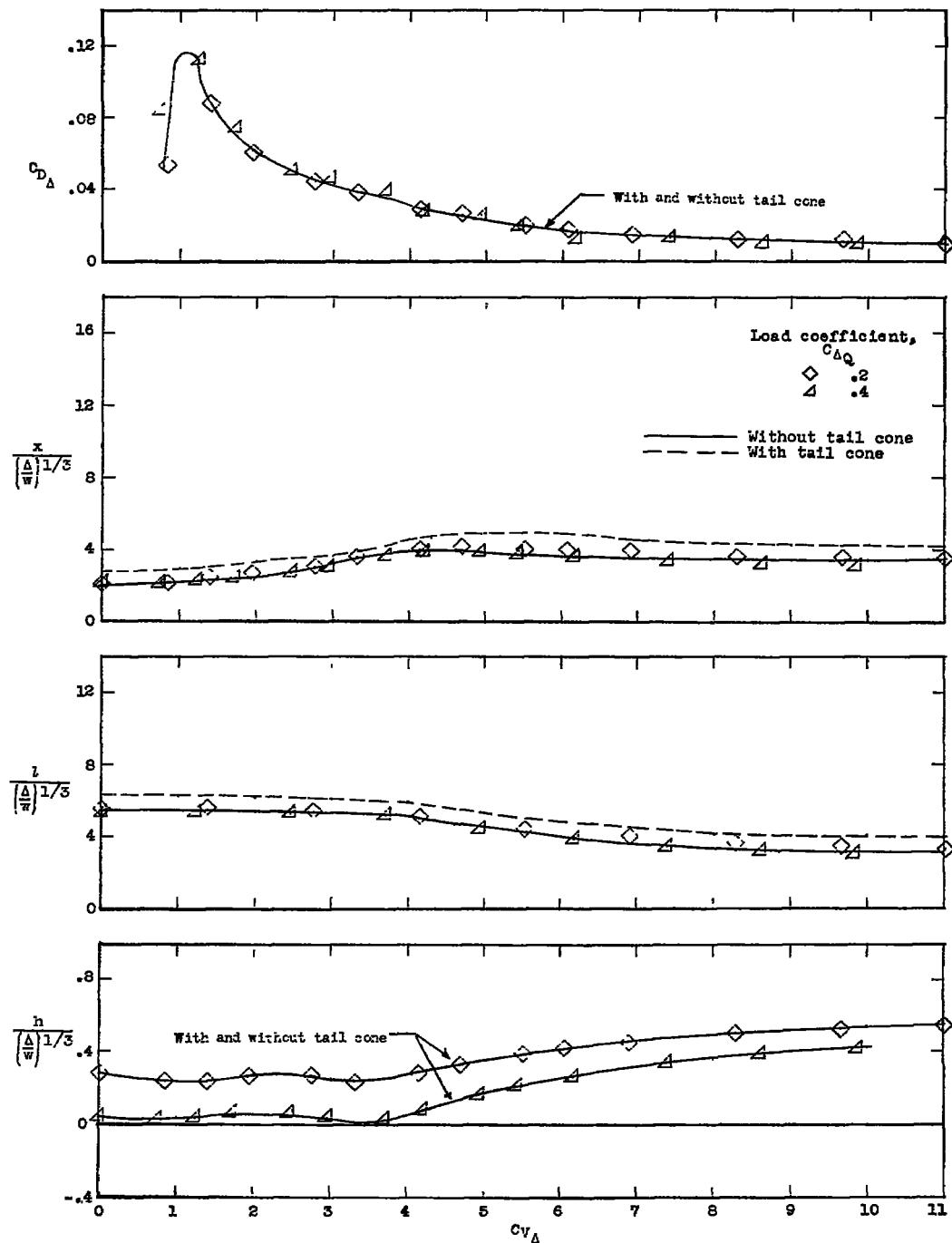
(a) Displacement condition.

Figure 16.- Hydrodynamic characteristics of models with chine strips but with the tail cones removed. Fineness ratio 6; trim, 8° .



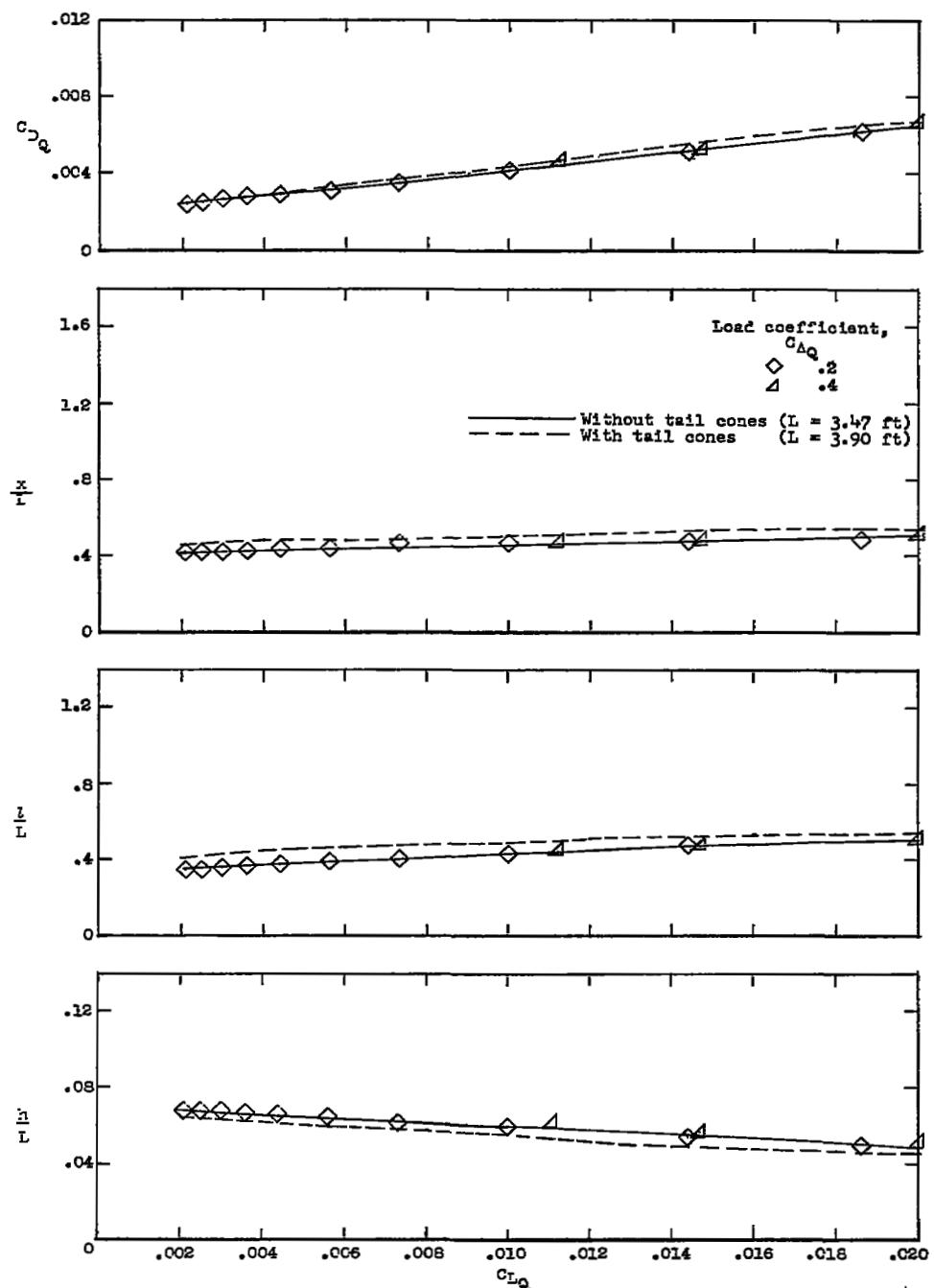
(b) Planing condition.

Figure 16.- Concluded.



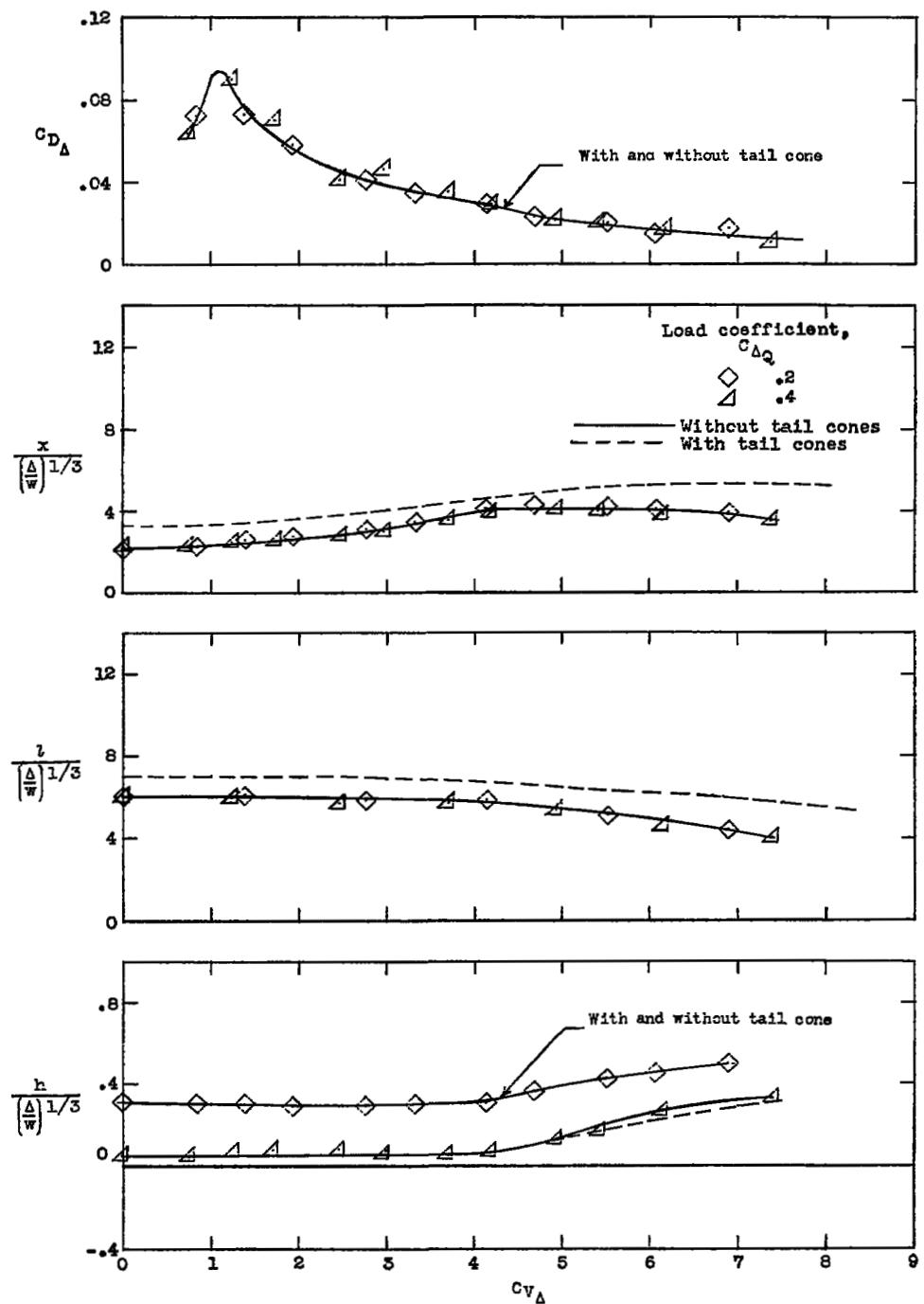
(a) Displacement condition.

Figure 17.- Hydrodynamic characteristics of models with chine strips but with the tail cones removed. Fineness ratio 9; trim, 8° .



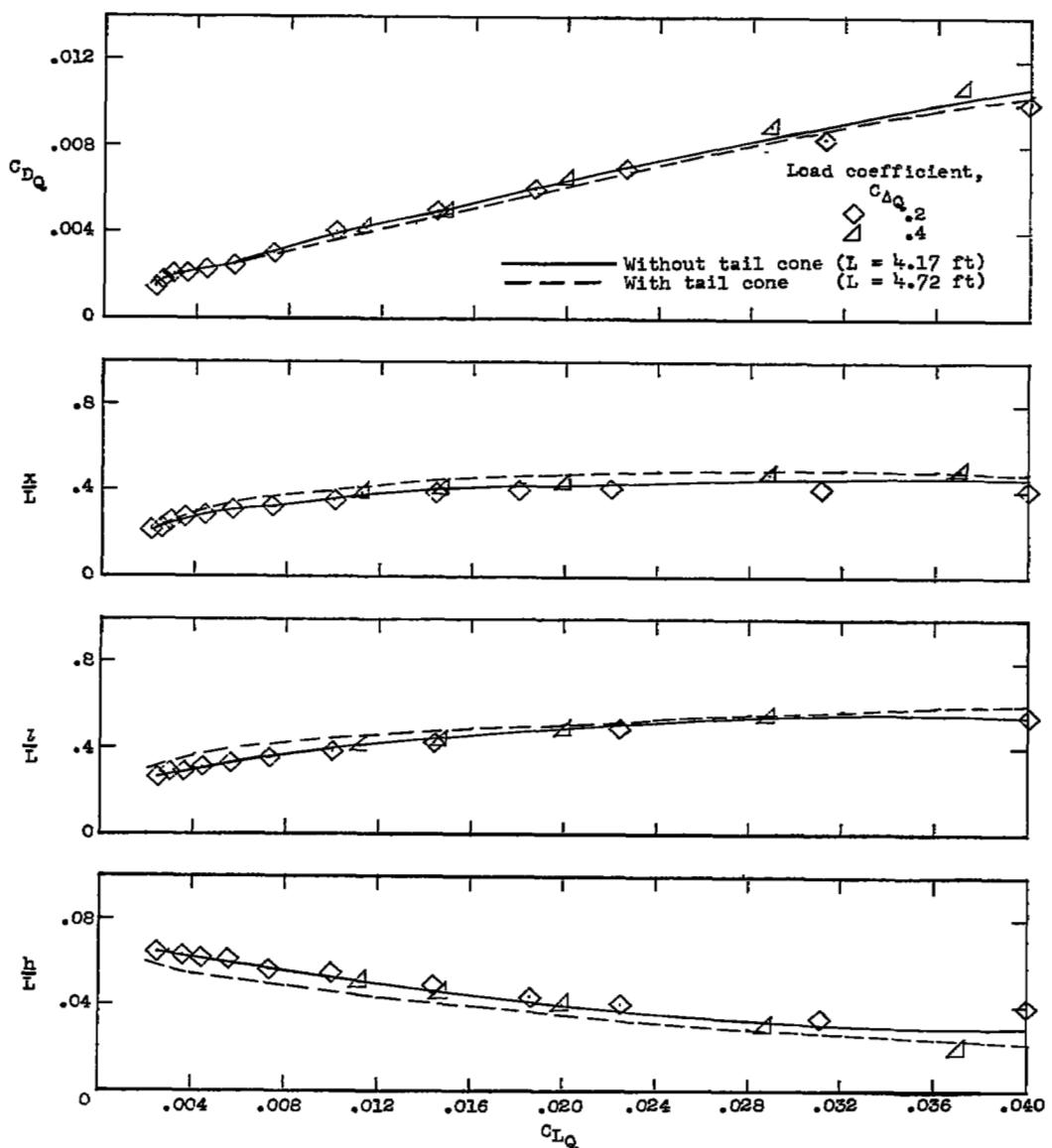
(b) Planing condition.

Figure 17.- Concluded.



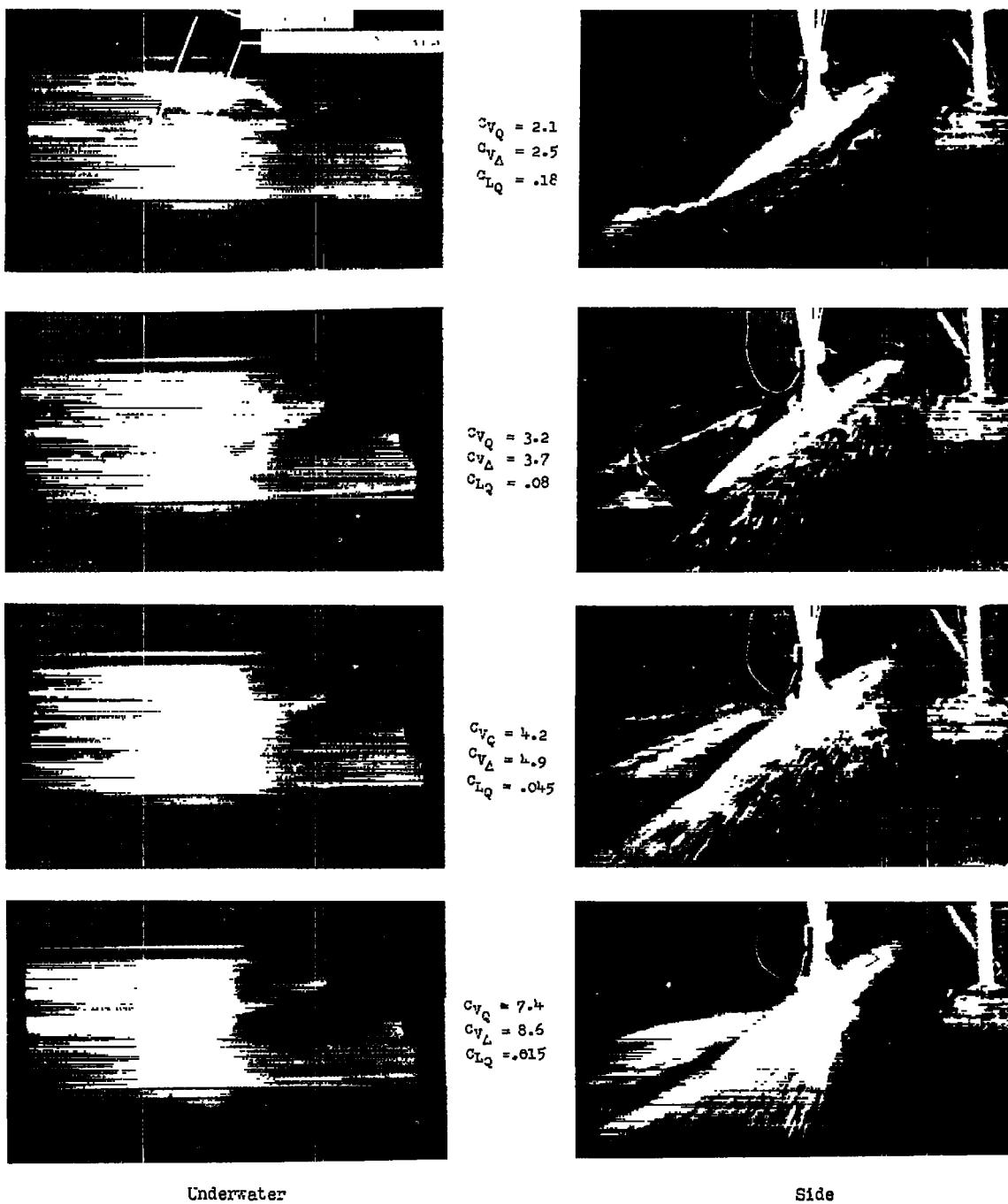
(a) Displacement condition.

Figure 18.. Hydrodynamic characteristics of models with chine strips but with the tail cone removed. Fineness ratio 12; trim, 8° .



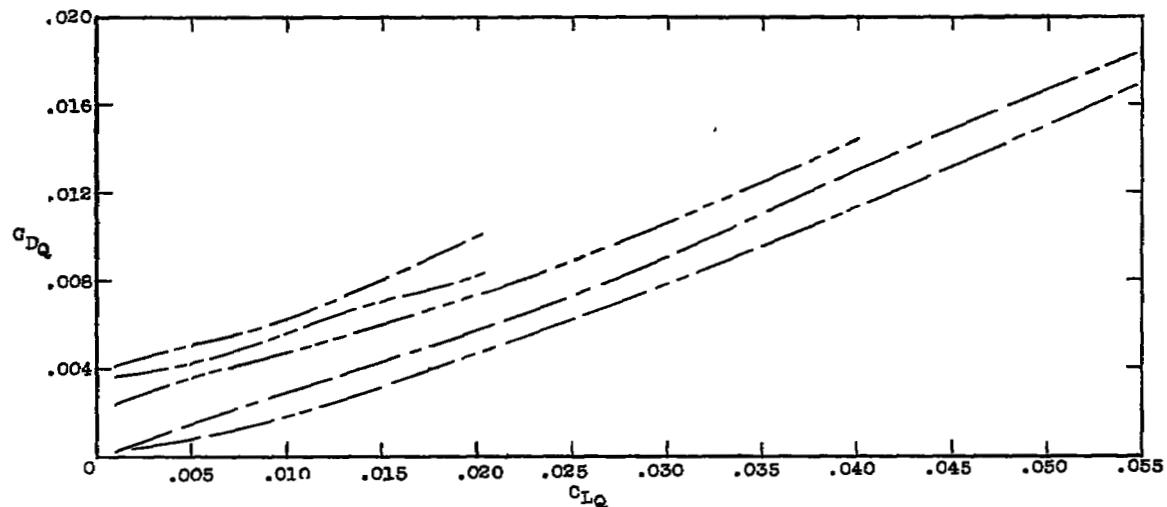
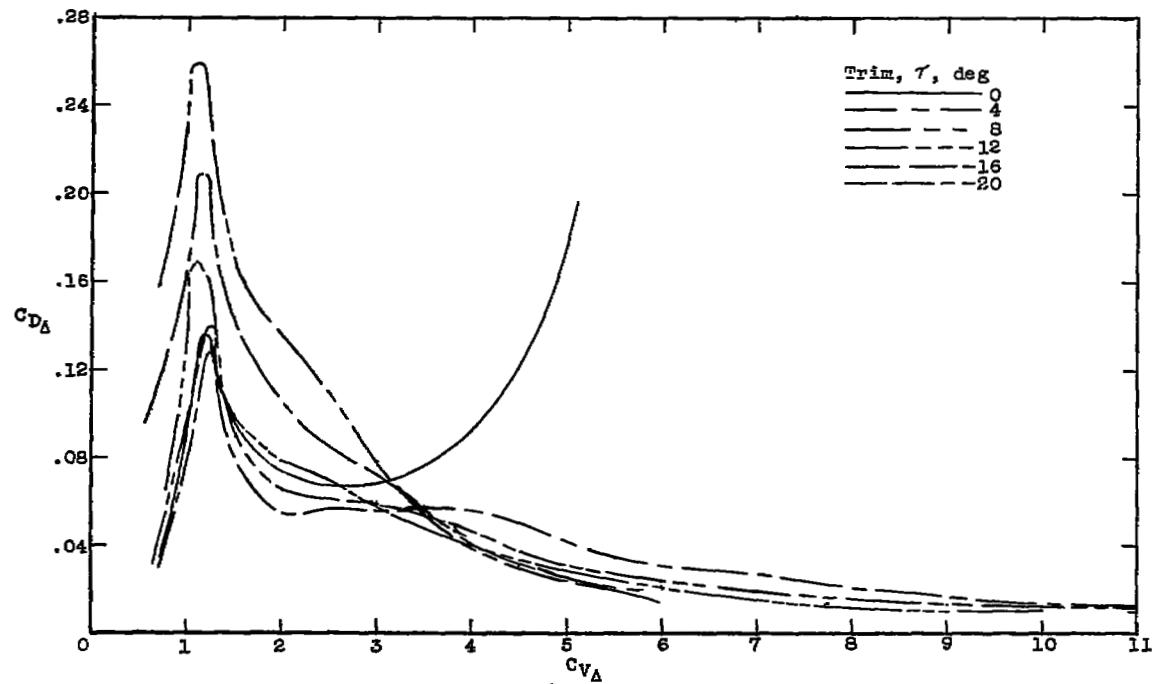
(b) Planing condition.

Figure 18.- Concluded.



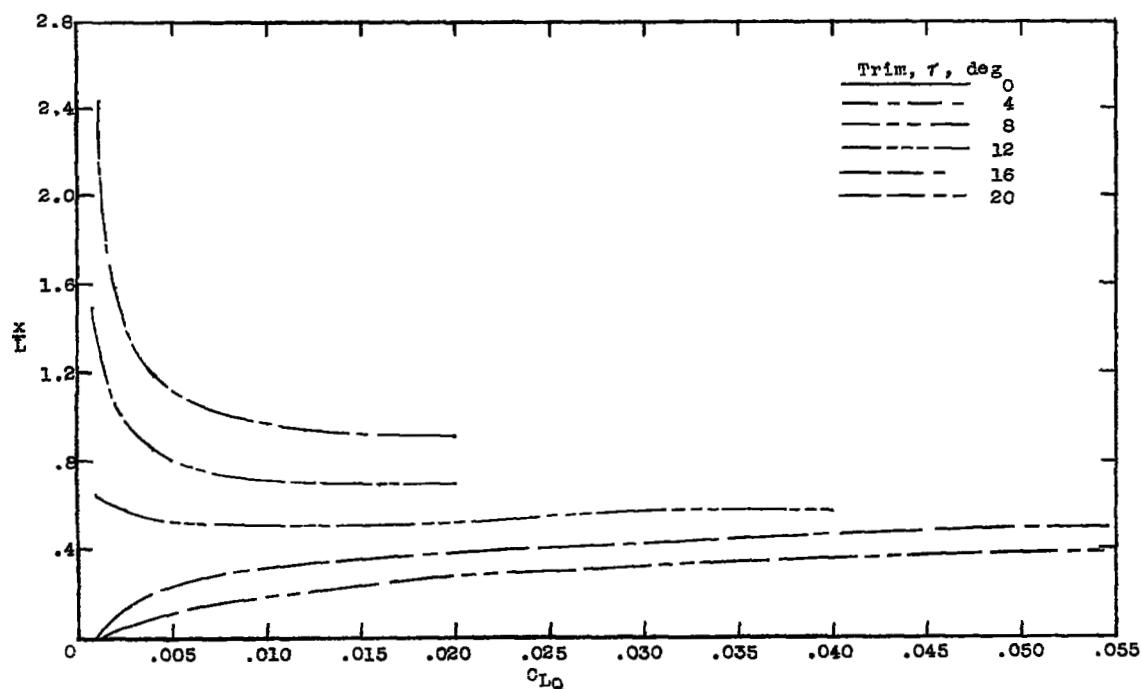
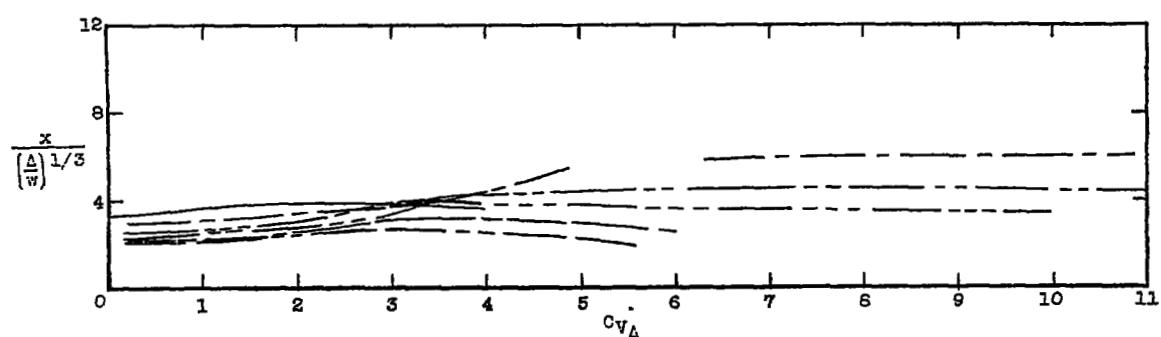
L-86481

Figure 19.- Spray characteristics of model with chine strips but with the tail cone removed. Fineness ratio, 9; trim, 8° ; load coefficient $C_{\Delta Q} = 0.4$.



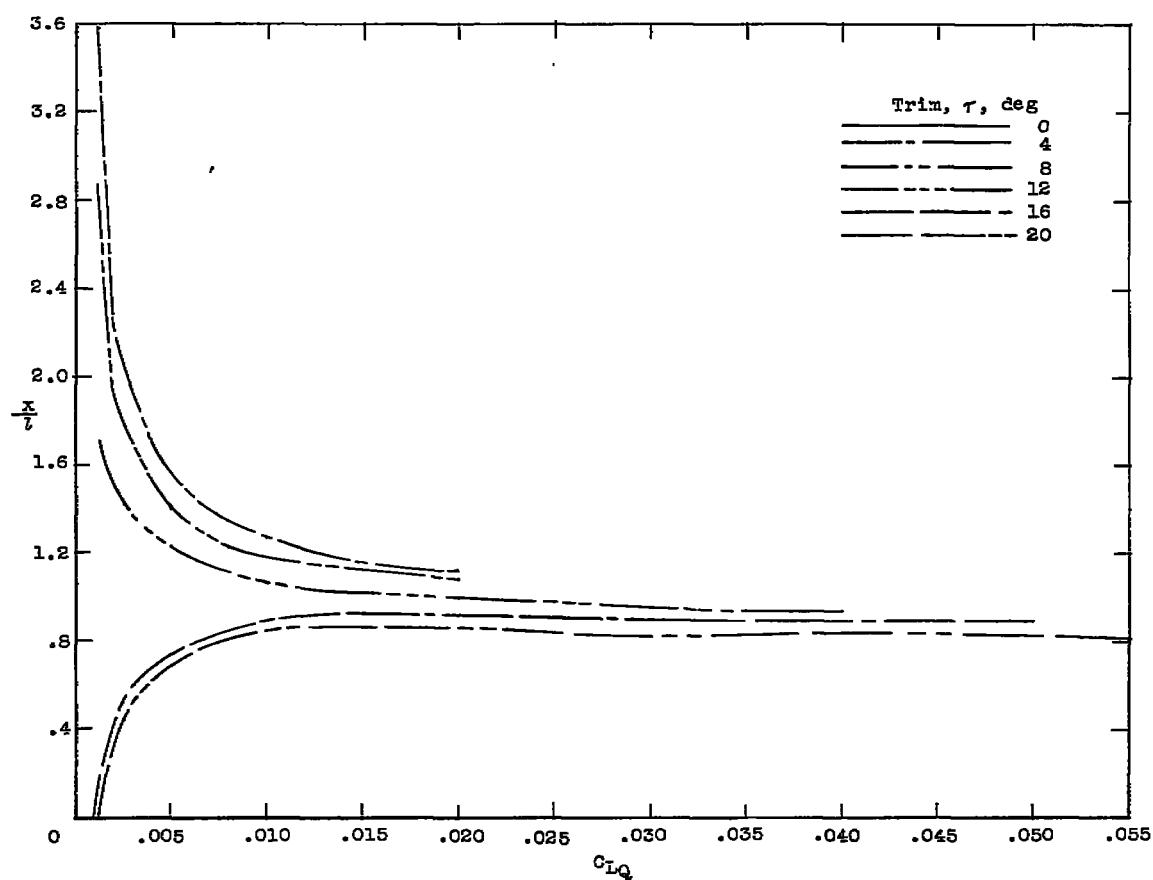
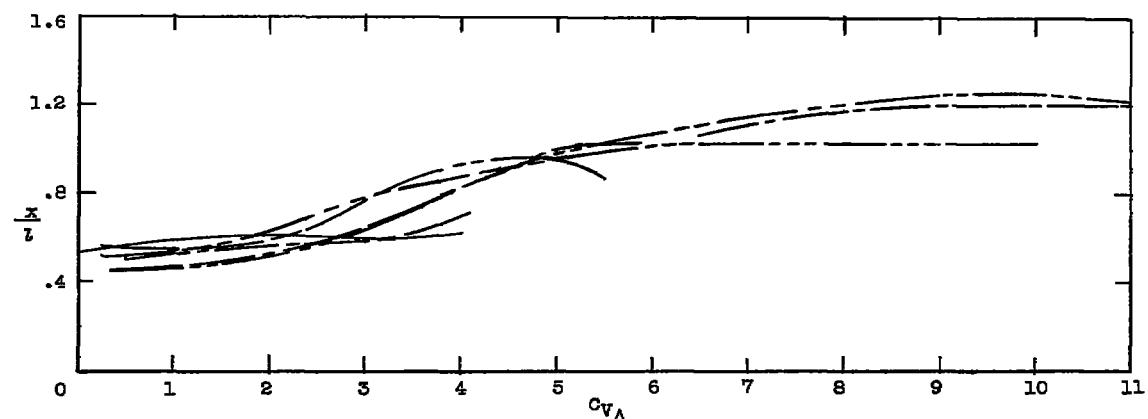
(a) Resistance.

Figure 20.- Effect of trim on hydrodynamic characteristics of model with chine strips. Fineness ratio 6.



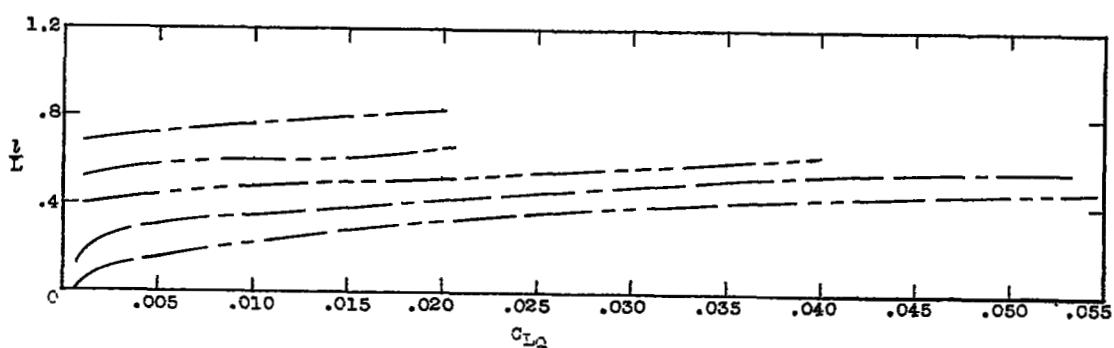
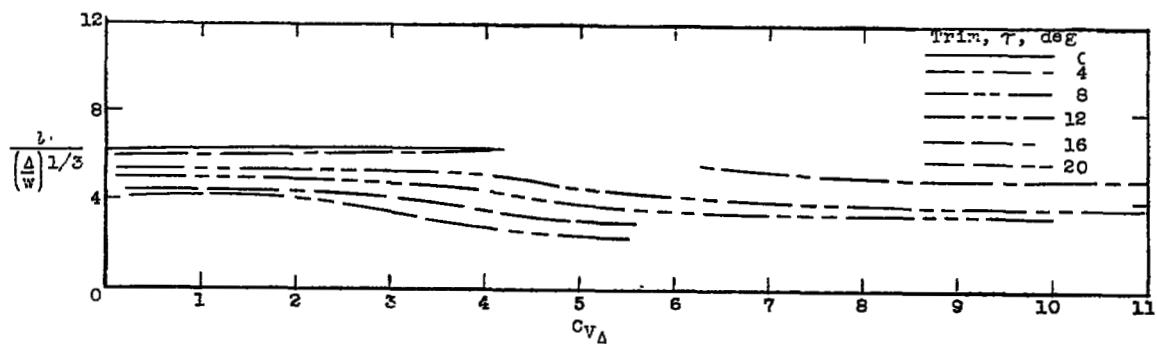
(b) Distance of center of pressure from rear end.

Figure 20.- Continued.



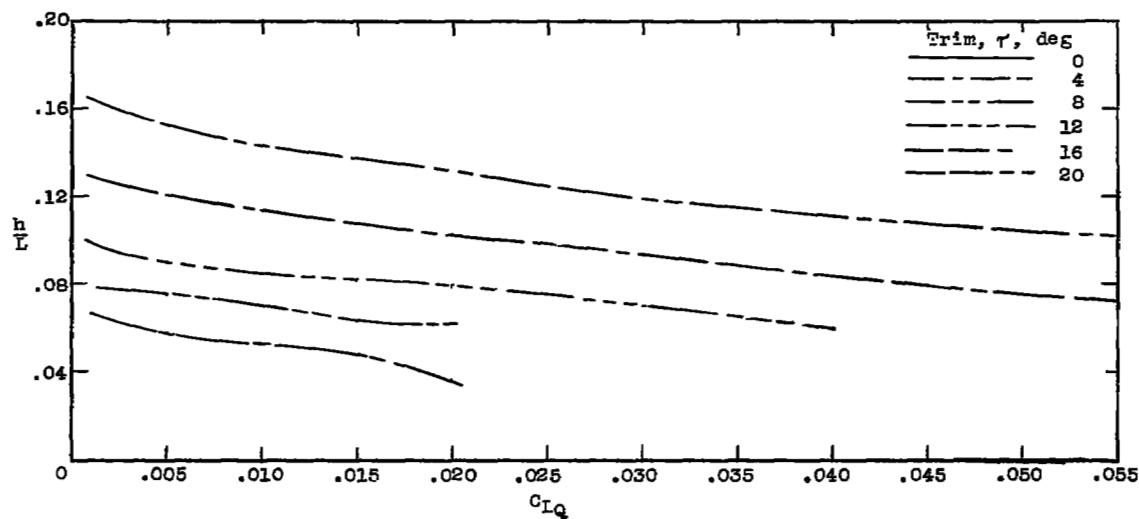
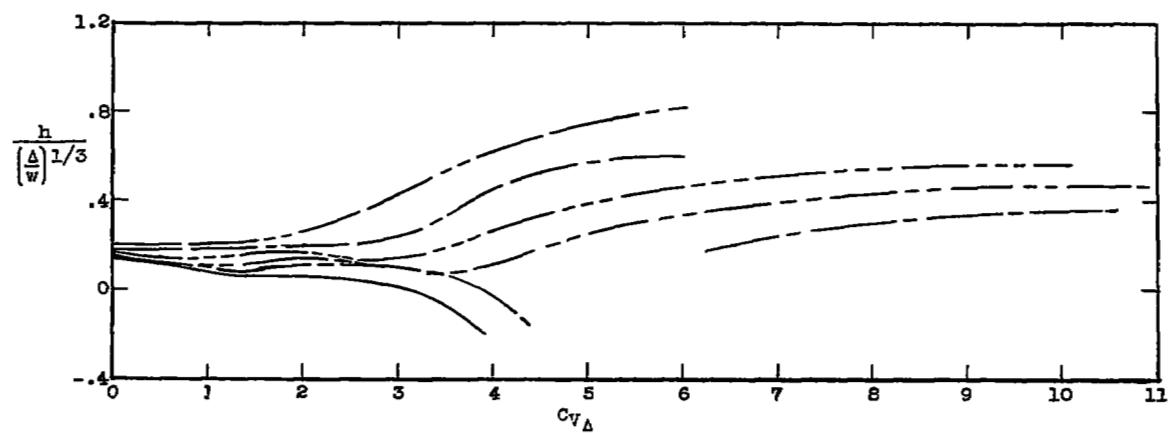
(c) Ratio of center of pressure to wetted length.

Figure 20.- Continued.



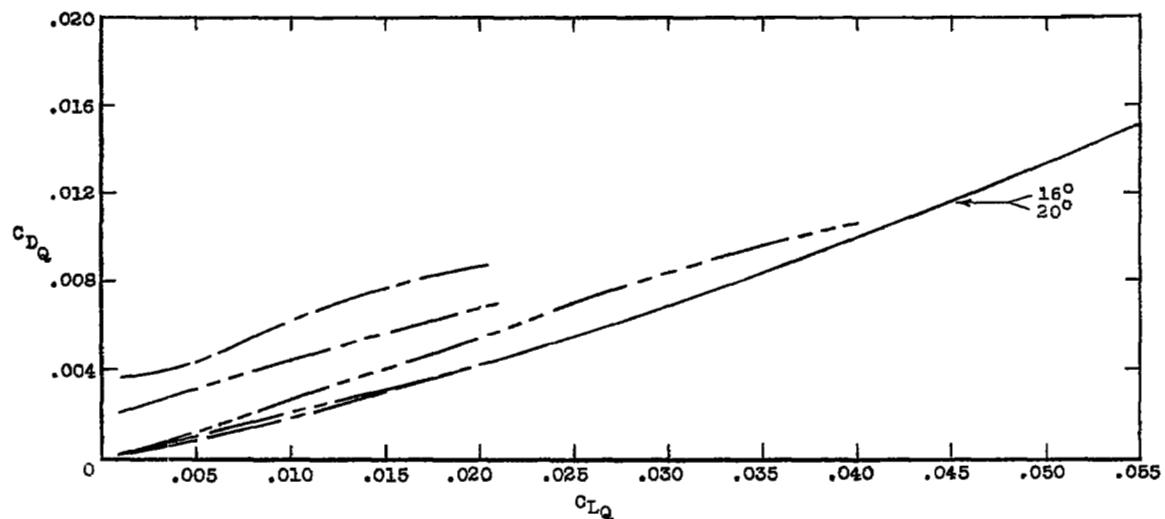
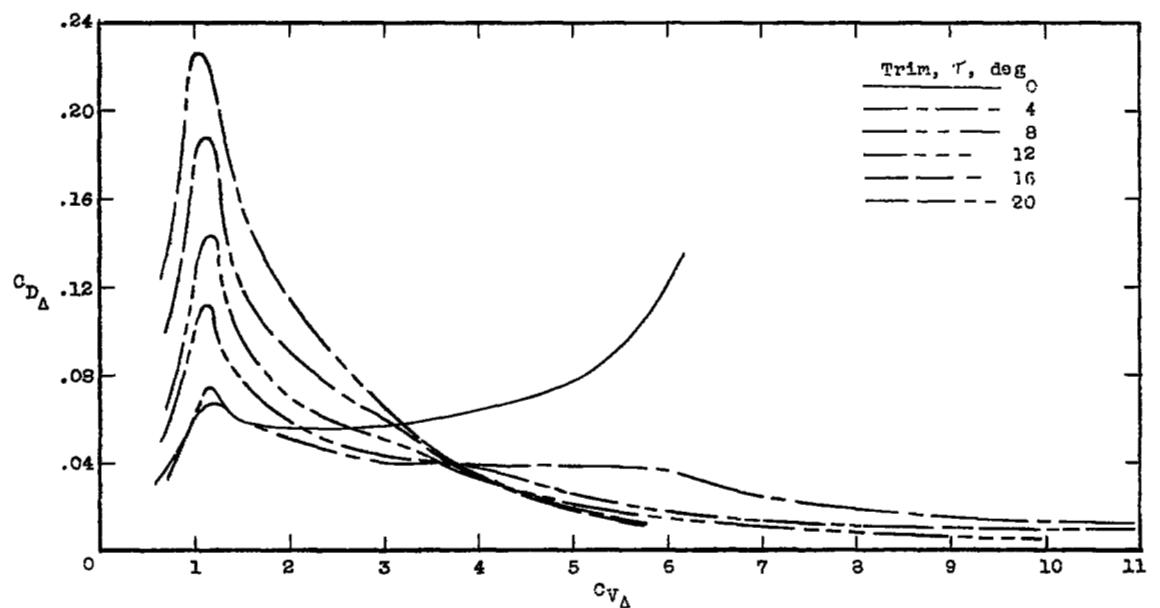
(d) Wetted length.

Figure 20.- Continued.



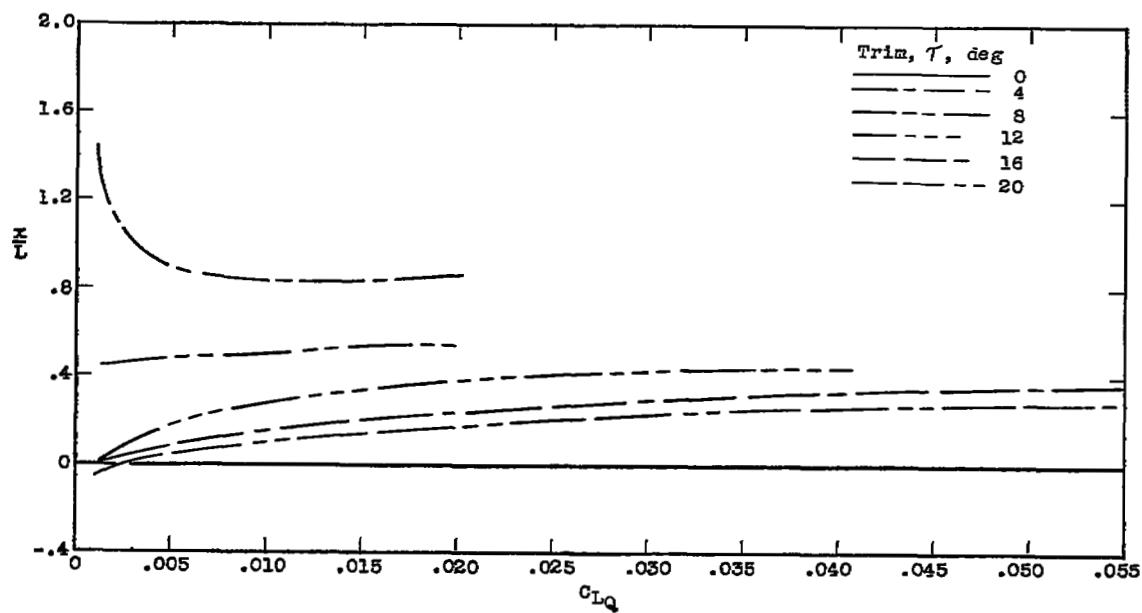
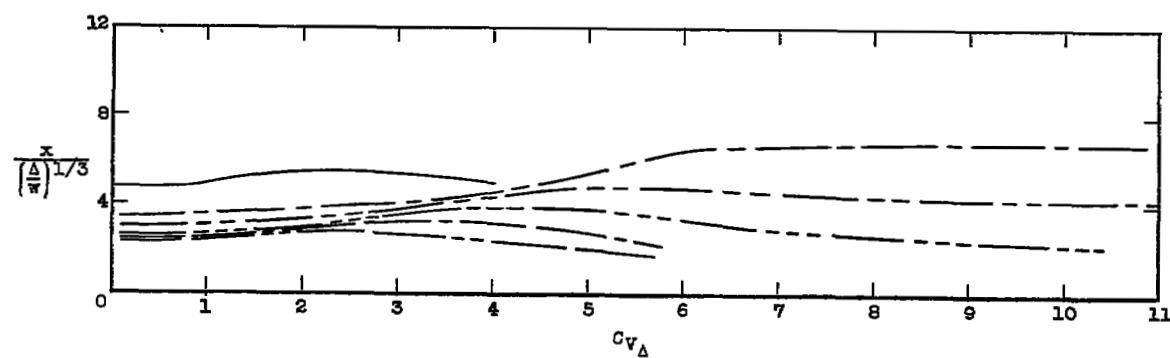
(e) Height of center-line midpoint.

Figure 20.- Concluded.



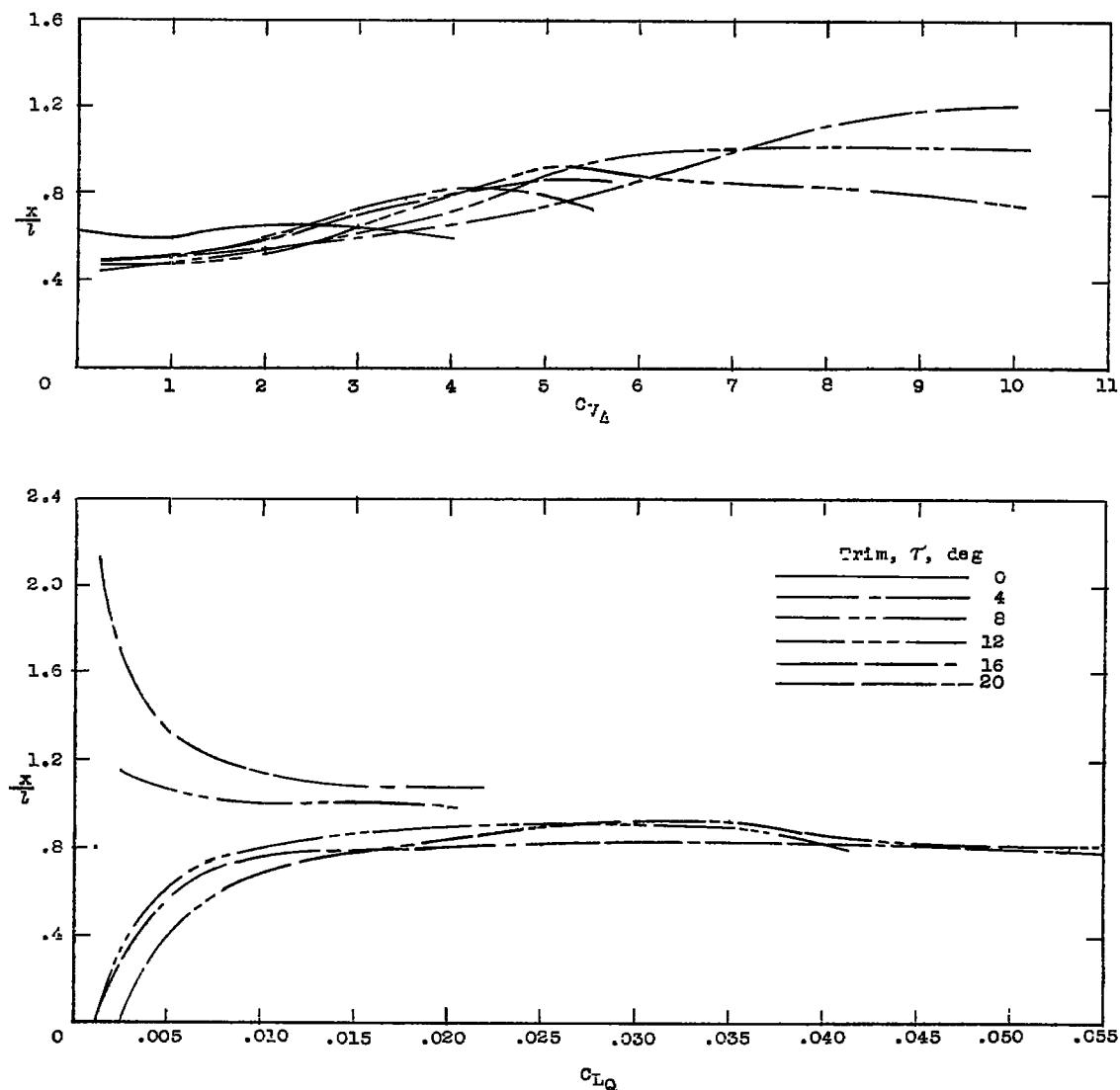
(a) Resistance.

Figure 21.- Effect of trim on hydrodynamic characteristics of model with chine strips. Fineness ratio 9.



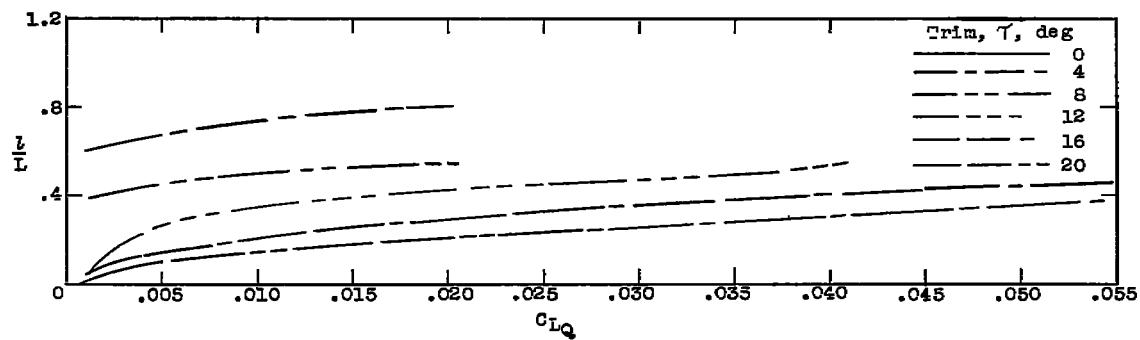
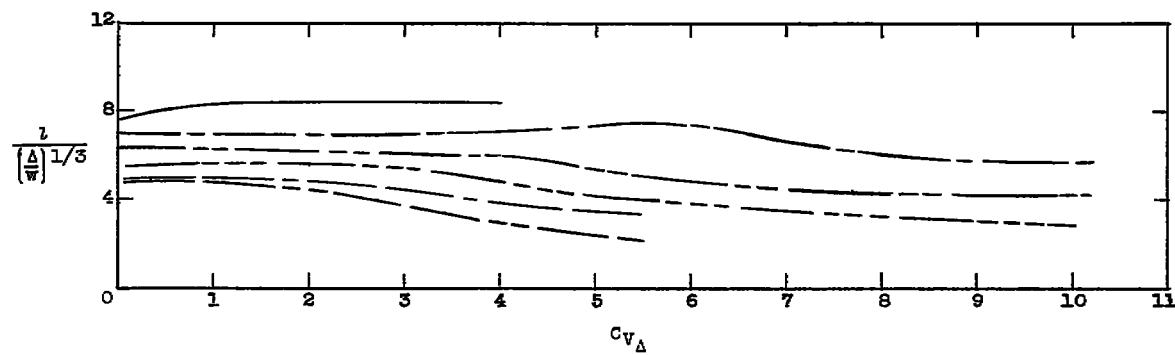
(b) Distance of center of pressure from rear end.

Figure 21.- Continued.



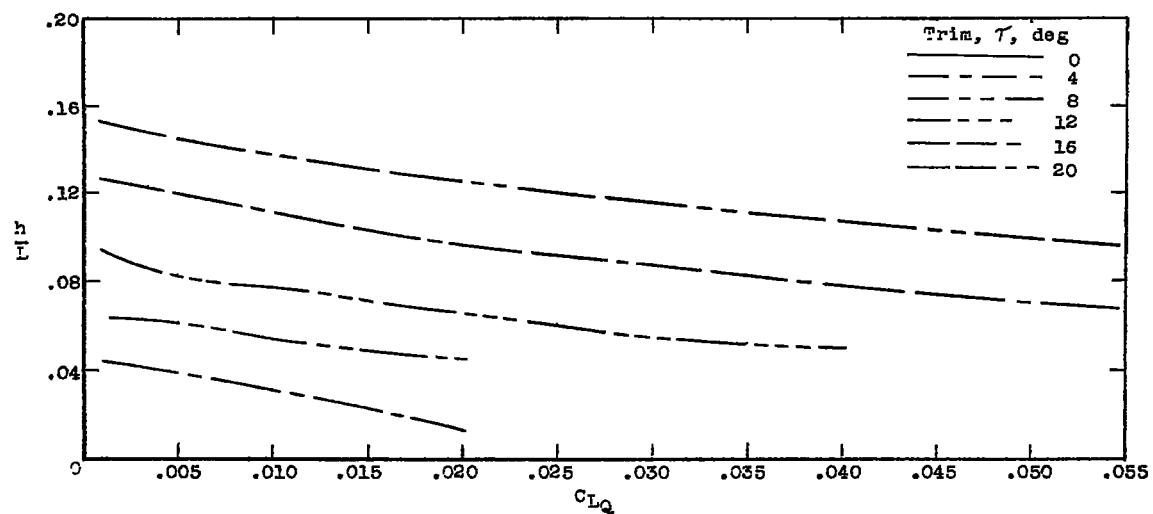
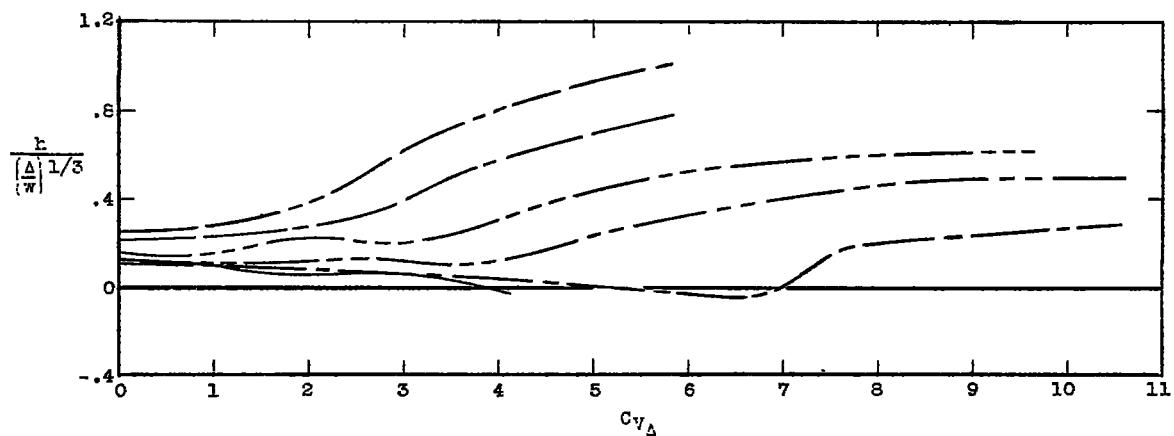
(c) Ratio of center of pressure to wetted length.

Figure 21.- Continued.



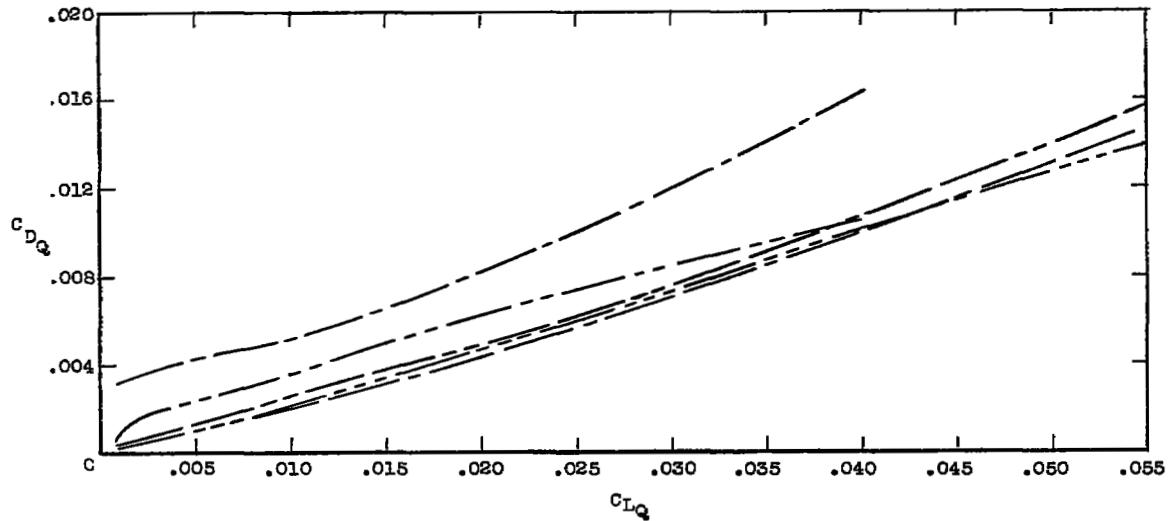
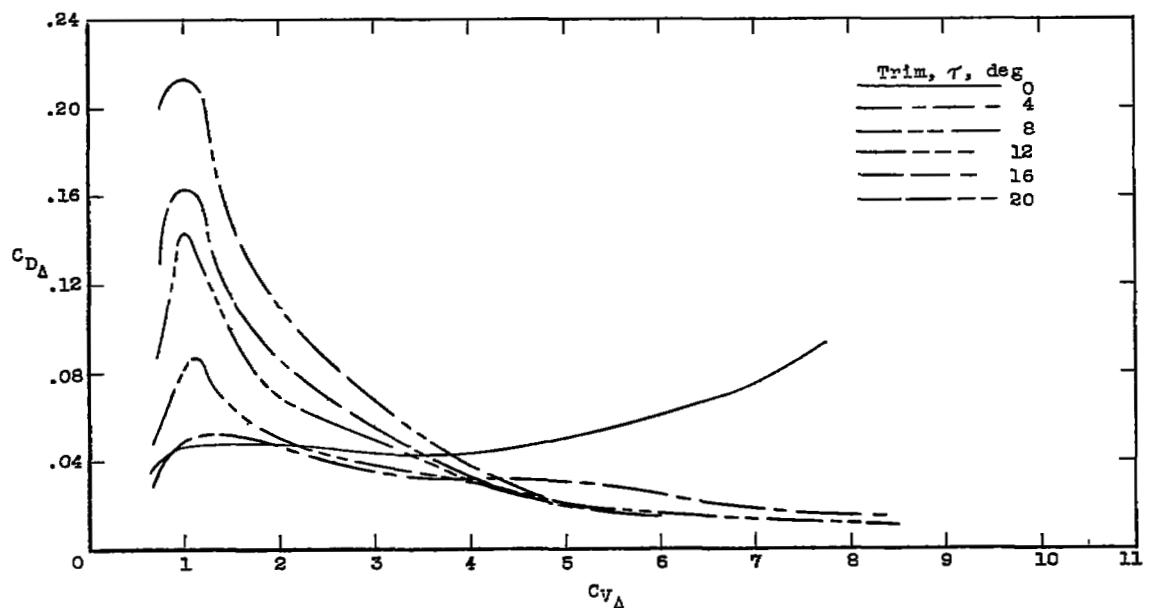
(d) Wetted length.

Figure 21.- Continued.



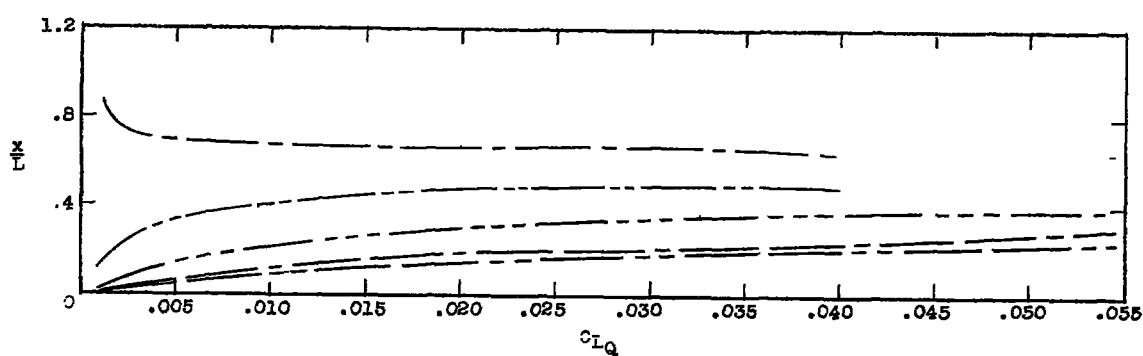
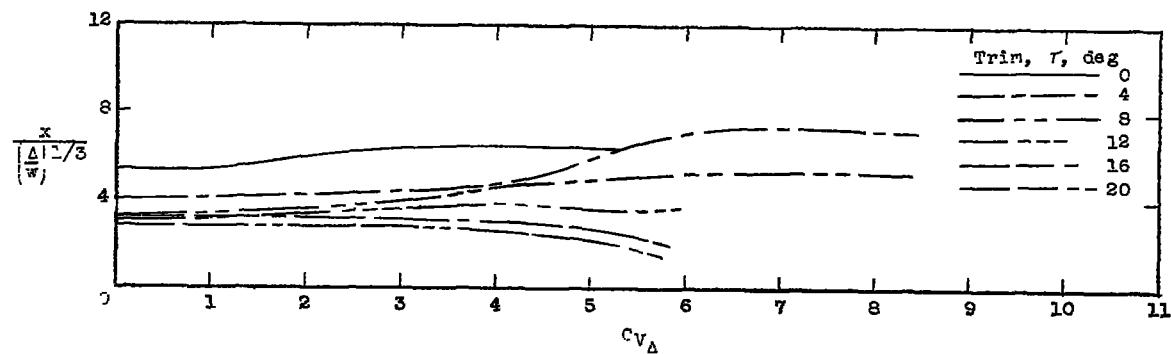
(e) Height of center-line midpoint.

Figure 21.- Concluded.



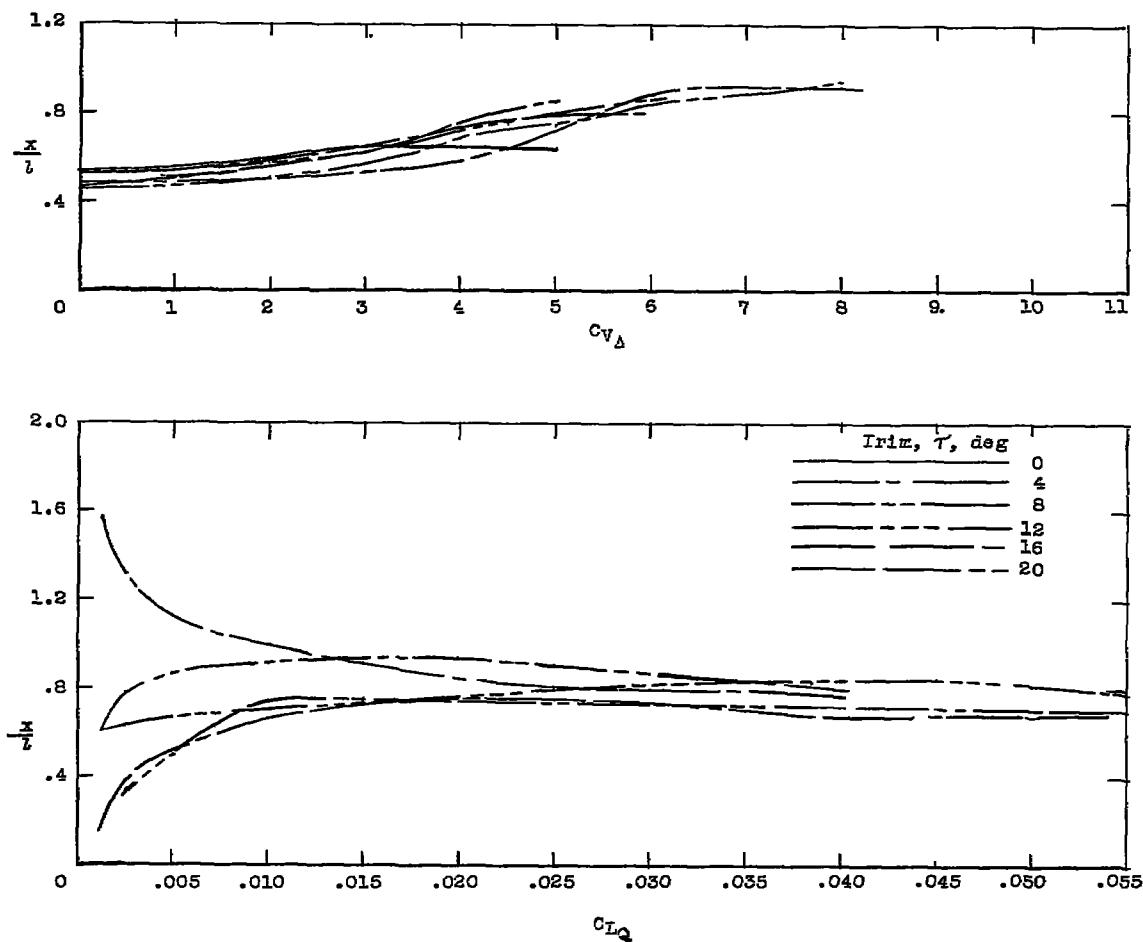
(a) Resistance.

Figure 22.- Effect of trim on hydrodynamic characteristics of model with chine strips. Fineness ratio 12.



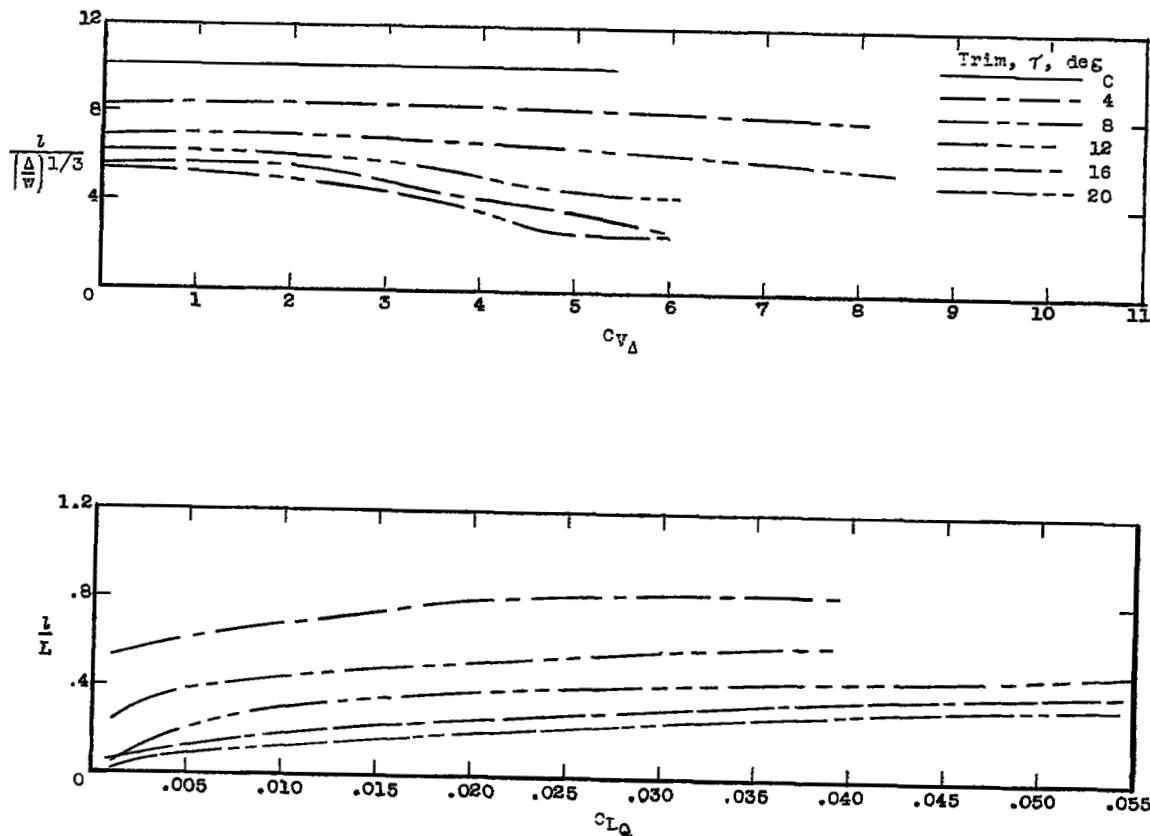
(b) Distance of center of pressure from rear end.

Figure 22.- Continued.



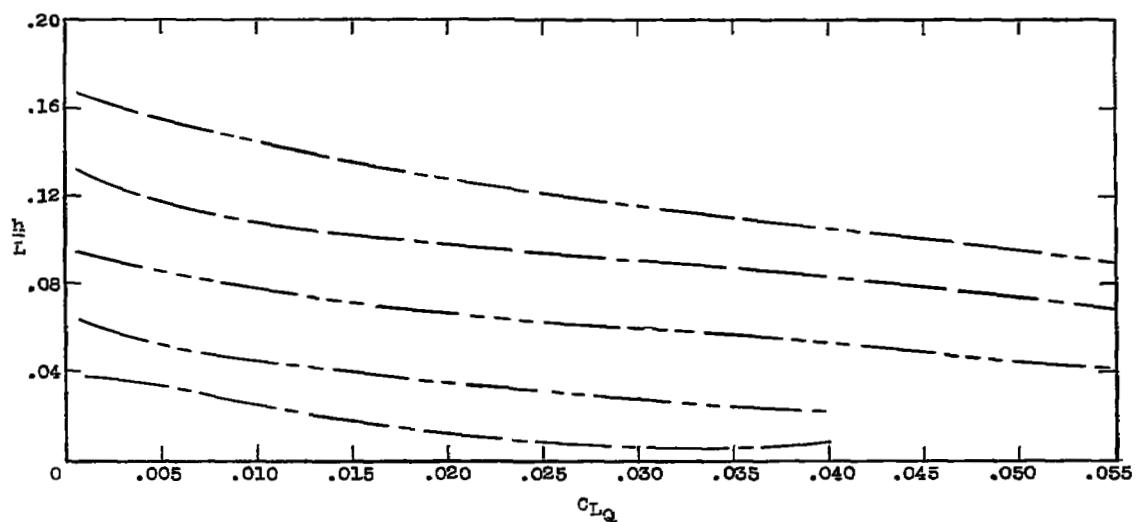
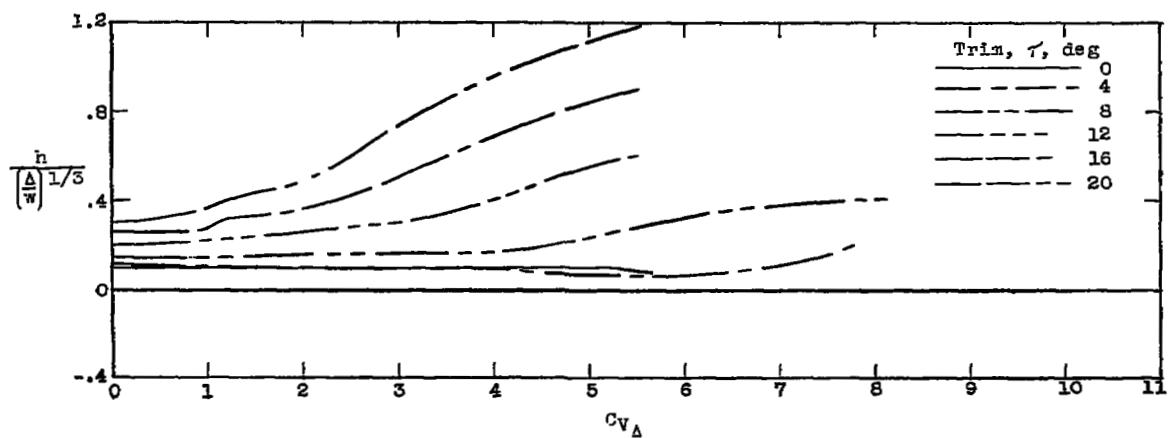
(c) Ratio of center of pressure to wetted length.

Figure 22.- Continued.



(d) Wetted length.

Figure 22.- Continued.

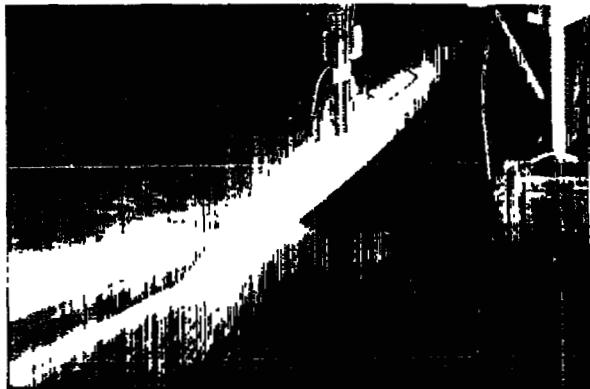


(e) Height of center-line midpoint.

Figure 22.- Concluded.

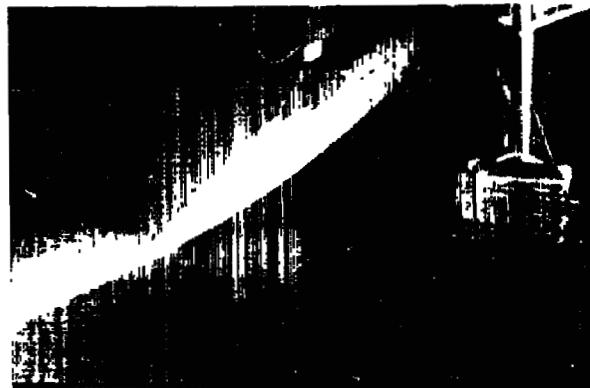


$C_{V_Q} = 7.4$
 $C_{\Delta Q} = 0.4$
 $C_{V_\Delta} = 8.6$
 $C_{L_Q} = .015$



$C_{V_Q} = 13.7$
 $C_{\Delta Q} = 0.2$
 $C_{V_\Delta} = 17.9$
 $C_{L_Q} = .002$

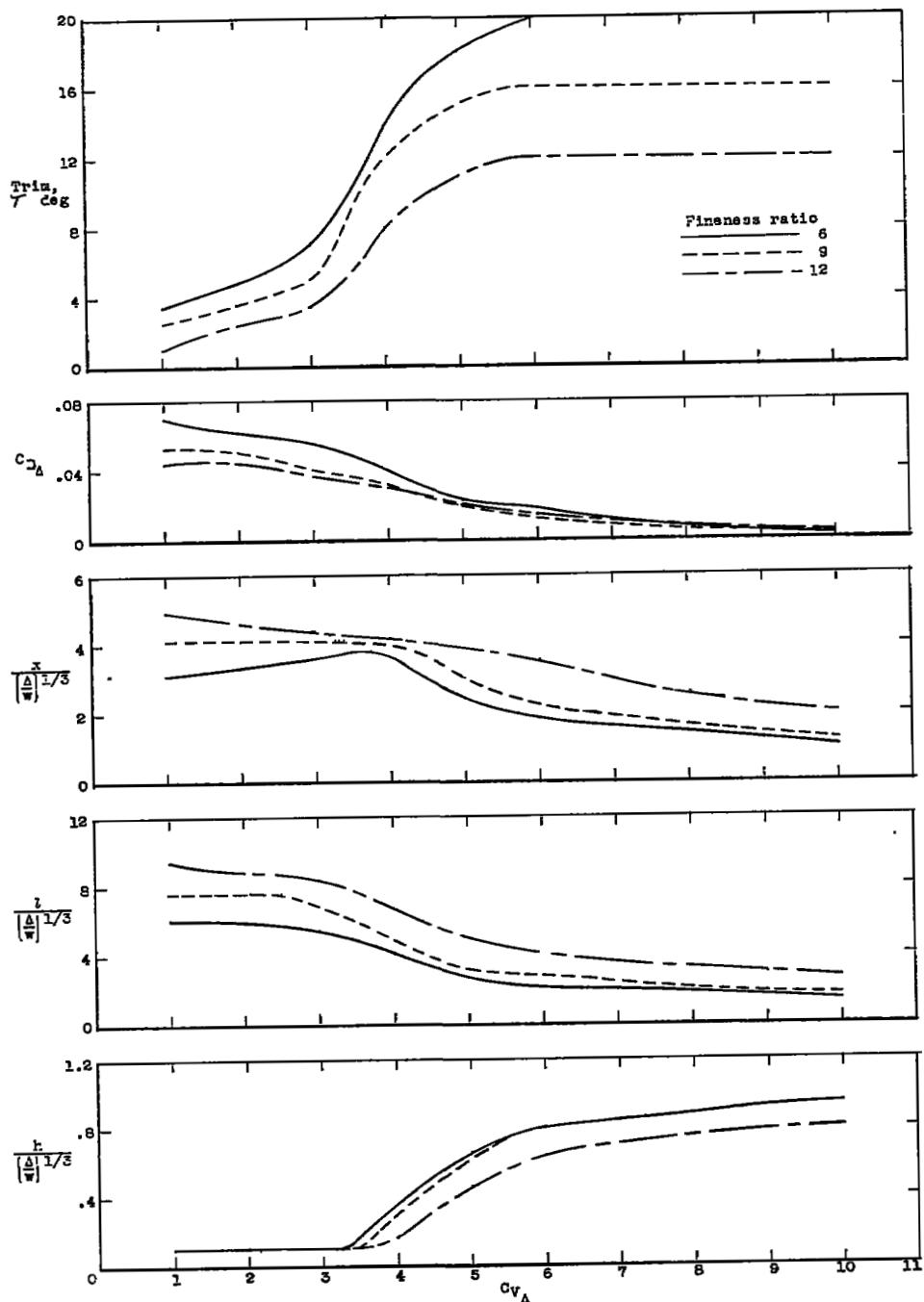
Trim, 8°



Trim, 16°

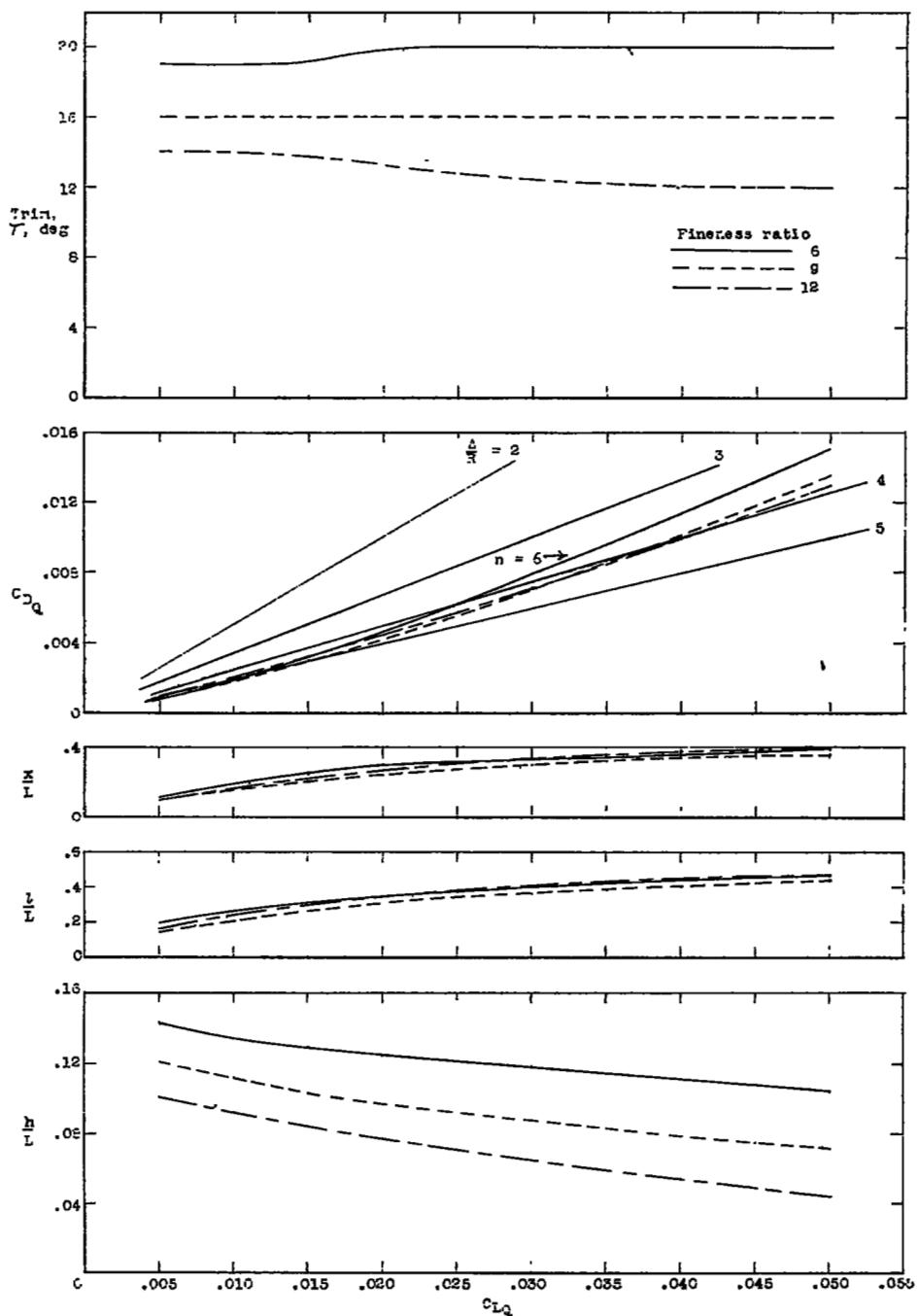
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Figure 23.- Effect of trim on the spray characteristics of model with chine strips. Fineness ratio 9.



(a) Displacement speed range. $C_{DQ} = 0.3$.

Figure 24.- Effect of fineness ratio on the hydrodynamic characteristics of the models with chine strips at best trim (trim for minimum hydrodynamic resistance).



(b) Planing speed range.

Figure 24.- Concluded.

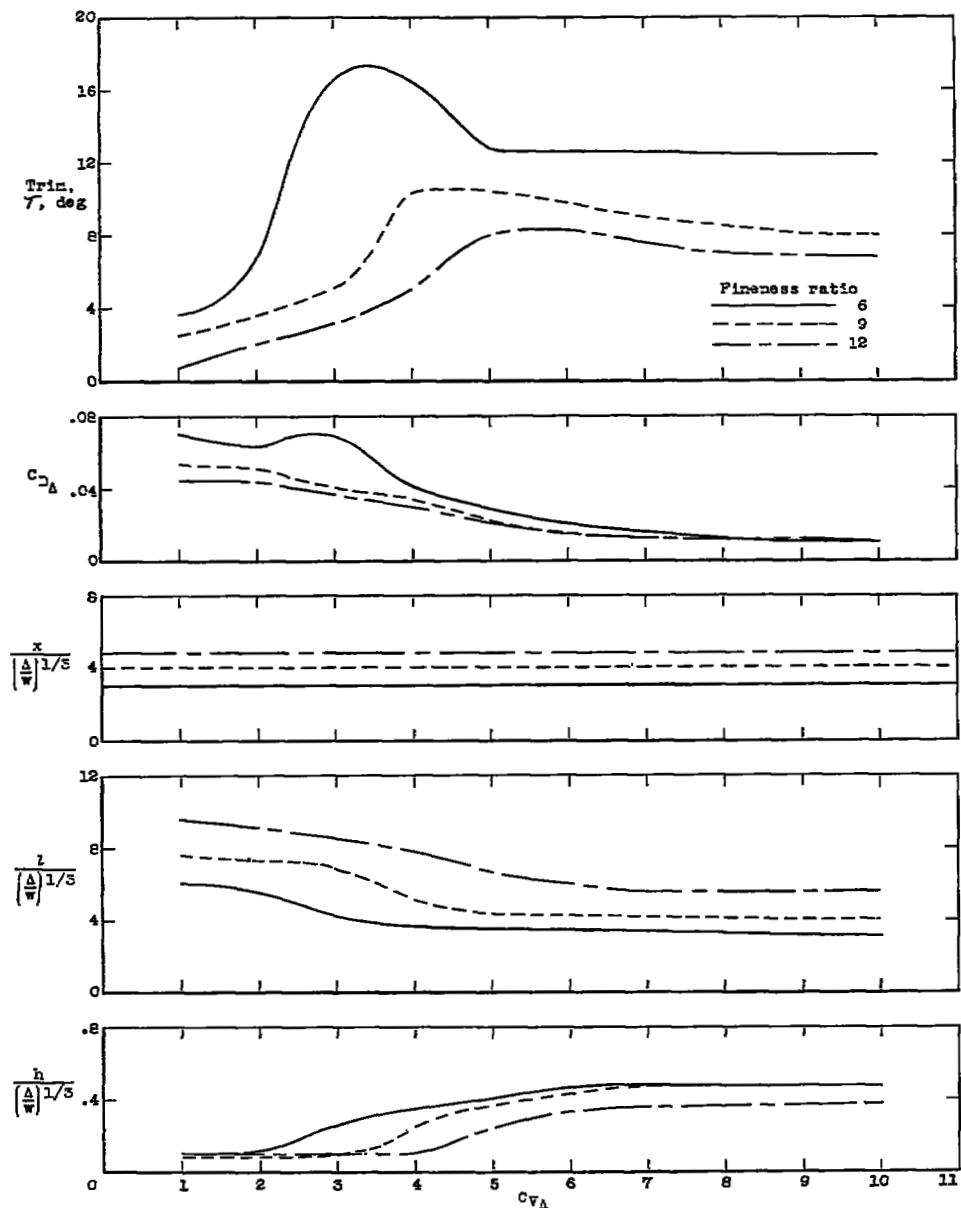
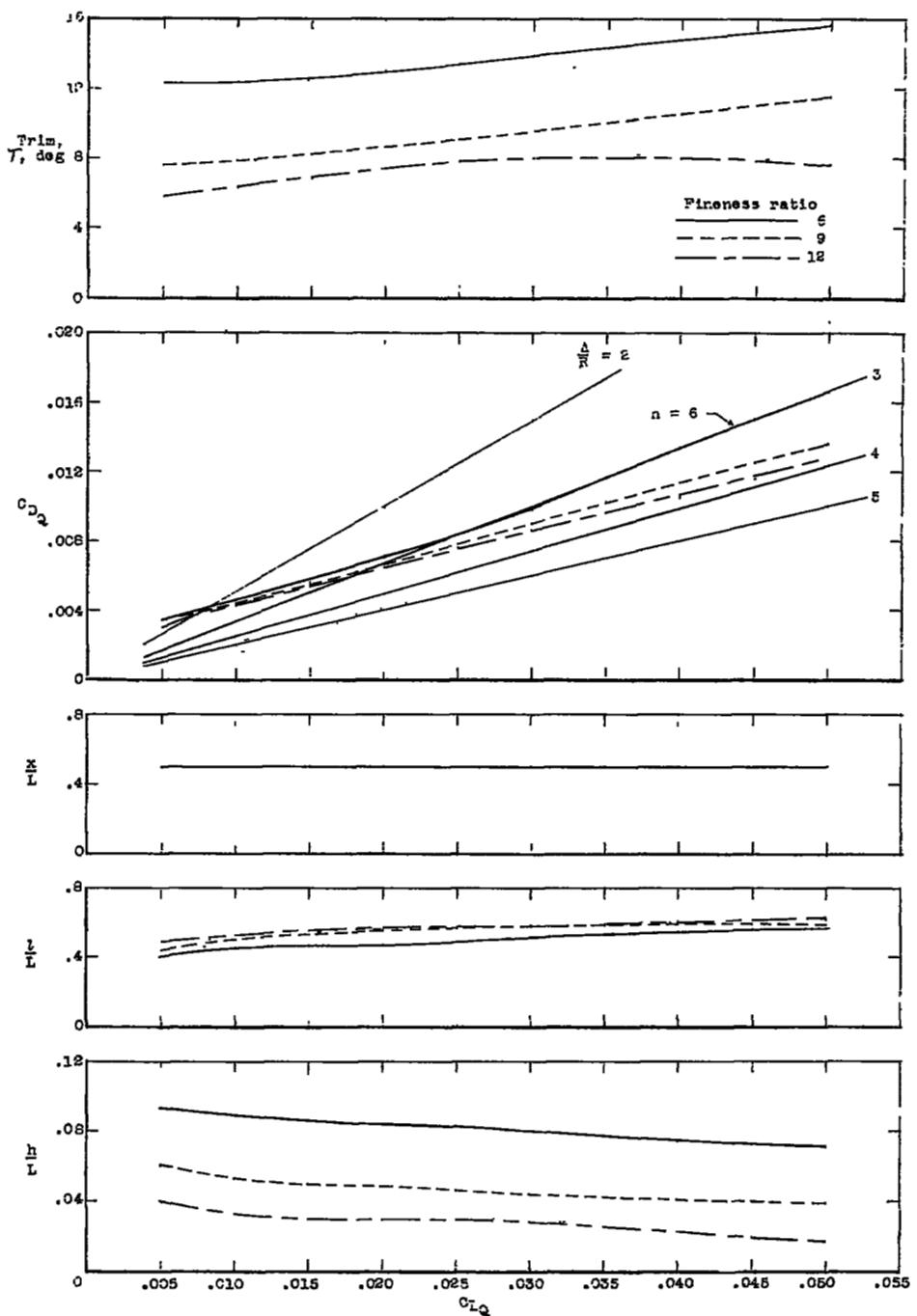
(a) Displacement speed range. $C_{\Delta Q} = 0.3$.

Figure 25.- Effect of fineness ratio on the hydrodynamic characteristics of the models with chine strips for $M = 0$ (hydrodynamic trimming moment about the midpoint of the center line equals zero).



(b) Planing speed range.

Figure 25.- Concluded.

Fineness ratio 6



Fineness ratio 9



Fineness ratio 12


 $(C_{V_Q} = 7.4; C_{\Delta_Q} = .1; C_{V_\Delta} = 8.6; C_{L_Q} = .015)$

 $(C_{V_Q} = 13.7; C_{\Delta_Q} = .2; C_{V_\Delta} = 17.9; C_{L_Q} = .002)$

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Figure 26.- Effect of fineness ratio on spray characteristics of models with chine strips. Trim, 8° .

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