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RESEARCH MEMORANDUM

SOME EFFECTS OF WING HEIGHT ON THE VERTICAL-TAIL
PRESSURE DISTRIBUTIONS OF A COMPLETE MODEL
IN SIDESLIP AT HIGH SUBSONIC SPEEDS

By Albert G. Few, Jr., and William J. Alford, Jr.

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ERRATA

NACA Research Memorandum L57D22

By Albert G. Few, Jr., and William J. Alford, Jr.
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Page 3, last line, change formula in parenthesis to read:

$$\left(0.25 - \frac{c_m, v}{c_n, v}\right)$$

Page 4, line 3:

The formula for $\frac{\bar{x}}{c_v}$ in the third line should be corrected to read:

$$0.25 - \left| \frac{\int_0^{1.0} \frac{\Delta c_n c_v}{\Delta \beta c_v, av} \left[\left(\frac{z'}{b_v} - \frac{z}{b_v} \right) \frac{b_v}{c_v} \tan \Lambda + \left(0.25 - \frac{\bar{x}}{c_v} \right) \frac{c_v}{\bar{c}_v} \right] d\left(\frac{z}{b_v}\right)}{\int_0^{1.0} \left(\frac{\Delta c_n c_v}{\Delta \beta c_v, av} \right) d\left(\frac{z}{b_v}\right)} \right]$$

where

z' spanwise distance from vertical-tail root chord to vertical-tail mean aerodynamic chord, ft

Λ sweep angle of quarter-chord line, deg

Page 97:

Replace figure 11 with corrected figure 11 attached, where the plots of \bar{x}/\bar{c}_v have been revised on the basis of the corrected formulas given in this errata.

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RESEARCH MEMORANDUM

SOME EFFECTS OF WING HEIGHT ON THE VERTICAL-TAIL
PRESSURE DISTRIBUTIONS OF A COMPLETE MODEL
IN SIDESLIP AT HIGH SUBSONIC SPEEDS

By Albert G. Few, Jr., and William J. Alford, Jr.

SUMMARY

An investigation has been made in the Langley high-speed 7- by 10-foot tunnel of some effects of wing height and angle of attack on the vertical-tail pressure distribution of a complete model in sideslip at high subsonic speeds. The 45° swept wing had an aspect ratio of 4, a taper ratio of 0.30, and NACA 65A006 airfoil sections parallel to the model plane of symmetry. The wing was located in high, middle, and low positions on a circular fuselage. Tests were made with the horizontal tail off and with the horizontal tail on the fuselage center line. Test Mach numbers ranged from 0.60 to 0.92, which corresponds to a Reynolds number range from approximately 2.7×10^6 to 3.4×10^6 based on the wing mean aerodynamic chord. The sideslip angles varied from -3.9° to 12.7° at several selected angles of attack.

The results indicated that increased wing height progressively decreased the vertical-tail load for constant angles of attack and sideslip, the largest load reductions occurring in the region near the tail root chord. Increases in angle of attack for constant sideslip angle produced increases in the vertical-tail loads for the low- and mid-wing configurations over most of the tail span except in the region of the root chord where load reductions occurred. For the high-wing configuration, increases in angle of attack produced reductions in the tail loads over the complete span, the largest reduction occurring in the region near the tail root chord. Substantial movements in the spanwise centers of pressure toward the tip of the vertical tail were caused by increases in angle of attack for all wing-height configurations. Increases in angle of attack also caused rearward movements in the chordwise locations of the centers of pressure particularly in the region of the root chord. The effects of wing height on the center-of-pressure location were considerably smaller than the effects of angle of attack. The vertical-tail center-of-pressure locations as determined from previous tail-force tests and as determined from the present pressure measurements were generally in good agreement.

[Redacted]

INTRODUCTION

The need for a better understanding of the nature of the air flow at the tail and its effects on the resulting vertical-tail loads has become increasingly important at the higher speeds of modern airplanes, inasmuch as several of these airplanes have, in maneuvering flight, been subjected to extreme vertical-tail loads while experiencing losses in directional stability. Of the many variables affecting the aerodynamic characteristics of a particular vertical-tail configuration, past research investigations (for example, refs. 1 to 3) have shown that wing height and fuselage cross-sectional shape are among the most important. Existing data on vertical-tail loads utilized configurations that are now outdated (ref. 4) or did not represent complete airplanes (ref. 5).

The purpose of this paper is to present the results of an experimental investigation made to determine the effects of changes in wing height on the chordwise pressure distributions and integrated loads on the vertical tail of a complete model in sideslip at high subsonic speeds. The complete model consisted of a 45° sweptback wing of aspect ratio 4.0 located in the low, middle, and high positions on a circular cross-section body in combination with a triangular horizontal tail of aspect ratio 4.0 and a vertical tail of aspect ratio 1.02 having a swept leading edge and an unswept trailing edge. The sideslip-angle range extended from -3.9° to 12.7° at angles of attack of approximately 0° , 9° , and 15° . The test Mach numbers varied from 0.60 to 0.92 with corresponding Reynolds number varying from 2.7×10^6 to 3.4×10^6 .

COEFFICIENTS AND SYMBOLS

c_L lift coefficient, $\frac{\text{Lift}}{qS}$

S wing area, sq ft

c_p pressure coefficient, $\frac{p_l - p_o}{q}$

p_l local static pressure, lb/sq ft

p_o free-stream static pressure, lb/sq ft

q dynamic pressure, $\frac{1}{2}\rho V_o^2$, lb/sq ft

ρ air density, slugs/cu ft

| | |
|------------------------------------|---|
| V_o | free-stream velocity, ft/sec |
| M | Mach number |
| c_v | local vertical-tail chord, ft |
| \bar{c}_v | vertical-tail mean aerodynamic chord, ft |
| $c_{v,av}$ | average vertical-tail chord, ft |
| \bar{c} | wing mean aerodynamic chord, ft |
| b_v | exposed vertical-tail span, ft |
| x | chordwise distance from leading edge of vertical-tail local chord, ft |
| z | spanwise distance from vertical-tail root chord (vertical-tail root chord 0.154 ft above fuselage center line), ft |
| $\Delta\left(\frac{x}{c_v}\right)$ | increment of vertical-tail local chord over which the pressure at a particular orifice is assumed to act (distance between points midway between adjacent orifices) |
| $c_{n,v}$ | vertical-tail section normal-force coefficient, $\sum_{\frac{x}{c_v} = 0}^1 (c_{p,L} - c_{p,R}) \Delta\left(\frac{x}{c_v}\right)$ |
| $c_{m,v}$ | vertical-tail section moment coefficient about 0.25 local vertical-tail chord, $\sum_{\frac{x}{c_v} = 0}^1 (c_{p,L} - c_{p,R}) \left(\frac{\bar{x}}{c_v} - 0.25 \right) \Delta\left(\frac{x}{c_v}\right)$ |
| $\frac{\bar{x}}{c_v}$ | local chordwise location of vertical-tail center of pressure, $\left(\frac{c_{m,v}}{c_{n,v}} - 0.25 \right)$ |

$\frac{\bar{x}}{c_v}$

chordwise center-of-pressure location of total vertical-tail load

$$\frac{\int_0^{1.0} \frac{\Delta c_n c_v}{\Delta \beta c_{v,av}} \left(\frac{\bar{x}}{c_v} - \frac{c_v}{\bar{c}_v} - 0.25 \right) d\left(\frac{z}{b_v}\right)}{\int_0^{1.0} \frac{\Delta c_n c_v}{\Delta \beta c_{v,av}} d\left(\frac{z}{b_v}\right)}$$

 $\frac{\bar{z}}{b_v}$

spanwise center-of-pressure location of total vertical-tail load

$$\frac{\int_0^{1.0} \frac{\Delta c_n c_v}{\Delta \beta c_{v,av}} \frac{z}{b_v} d\left(\frac{z}{b_v}\right)}{\int_0^{1.0} \frac{\Delta c_n c_v}{\Delta \beta c_{v,av}} d\left(\frac{z}{b_v}\right)}$$

α angle of attack, deg

β angle of sideslip, deg

i_t horizontal-tail incidence angle, deg

Subscripts:

R right side of vertical tail looking upstream

L left side of vertical tail looking upstream

MODEL AND APPARATUS

Details of the complete model as tested are given in figure 1 and a photograph of the model mounted on the sting-type support system is given as figure 2. The fuselage was of fineness ratio 10.94 and was constructed of aluminum. The physical characteristics of the fuselage including afterbody ordinates are given in figure 1(c). The 45° swept wing was made of aluminum and had an aspect ratio of 4, a taper ratio of 0.30, and NACA 65A006 airfoil sections parallel to the model plane of symmetry. The triangular horizontal tail ($i_t = 0^\circ$) located on the fuselage center line, was made of steel and covered with plastic and fiberglass; it had an aspect ratio of 4 and NACA 65A006 airfoil sections. The vertical tail was made of steel and covered with plastic and fiber-glass; it had an aspect ratio of 1.02 (based on an exposed area and span), a taper ratio of 0.46, quarter-chord sweep of 28.35° , and NACA 65A006 airfoil sections. Twenty-three chordwise pressure orifices (in rows parallel

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to fuselage center line) were located at each of the following spanwise locations: $0.11b_v$, $0.38b_v$, $0.66b_v$, and $0.93 b_v$. Details of the orifice locations are given in figure 1(b) and other details of model geometry are given in table I.

Tests were made on the sting-support system shown in figure 2. With this system the model can be remotely operated through an angle-of-attack range of approximately 26° in the plane of the vertical strut. By utilization of couplings in the sting behind the model, the model can be rolled 90° so that either angle of attack or angle of sideslip can be the remotely controlled variable. With the wings vertical, the couplings can be used to support the model at fixed angles of attack while the model is tested through the angle-of-sideslip range.

With the model at a given angle of attack and angle of sideslip, a record was taken of the pressures existing at the orifices by photographing a manometer board to which the orifices were connected. These pressures were reduced to coefficient form and are presented in tables II to VI.

TESTS AND CORRECTIONS

The tests were made in the Langley high-speed 7- by 10-foot tunnel through a Mach number range of 0.60 to 0.92, which corresponds to a Reynolds number range from approximately 2.7×10^6 to 3.4×10^6 based on the wing mean aerodynamic chord. Pressure measurements on the vertical tail were made through a sideslip-angle range from approximately -4° to 13° at angles of attack of 0° , 9° , and 15° with the horizontal tail ($i_t = 0^\circ$) on the fuselage center line and the wing in low, middle, and high positions on a circular cross-section fuselage. Pressure measurements on the vertical tail were obtained for the mid-wing configuration with the horizontal tail removed and also with the fuselage with both horizontal and vertical tails.

Blockage corrections, calculated by the method of reference 6, were applied to Mach number and dynamic pressure. Jet-boundary corrections calculated by the method of reference 7 have been applied to the angle of attack. Corrections due to sting-support deflection have been applied to the angles of attack and sideslip.

PRESENTATION OF RESULTS

All the individual pressure coefficients are given in tables II to VI and some selected results from the investigation are presented in the

following figures:

Figure

| | |
|---|--------|
| Variation of model lift coefficient with angle of attack, horizontal tail off | 3 |
| Effect of wing height on the vertical-tail chordwise pressure distributions | 4 to 6 |
| Effect of angle of sideslip on the spanwise variation of vertical-tail section normal-force coefficients | 7 |
| Effect of wing height on the spanwise variation of vertical-tail section normal-force coefficient per degree of sideslip, $\frac{\Delta c_{n,v}}{\Delta \beta}$ | 8 |
| Effect of wing height on the chordwise location of vertical-tail local centers of pressure | 9 |
| Effect of wing height on the variation of the spanwise location of the vertical-tail center of pressure with angle of attack | 10 |
| Comparison of the location of vertical-tail spanwise center of pressure as obtained from force and pressure measurements | 11 |

DISCUSSION

Vertical-Tail Loads

For a given angle of attack, increases in the section load accompany increases in the angle of sideslip for all wing positions, except at the highest sideslip angle (12.7°) where some local load reductions are in evidence. (See fig. 7.) The effect of changing the wing vertical location on the fuselage from low to mid to high is, in general, to cause a progressive reduction in the vertical-tail section loads for any of the angles of attack and sideslip investigated. (See figs. 7 and 8.)

For the low- and mid-wing locations, increasing the angle of attack, for a constant sideslip angle, generally causes increases in the vertical-tail section loads over most of the span, although there are reductions in the vicinity of the root chord. The largest increase in loading with angle of attack occurs for the low-wing position. (See figs. 7 and 8.) For the high-wing position increasing the angle of attack causes reductions in the vertical-tail loads over the complete span, the largest reduction again occurring in the region near the root chord. (See figs. 7 and 8.)

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Increases in Mach number from 0.60 to 0.92, for small angles of sideslip, generally caused some increase in the vertical-tail section loads for given angles of attack, these increases being particularly noticeable near the tip chord of the tail for the higher Mach numbers. (See fig. 8.) For the conditions investigated, however, effects of Mach number appear to be of minor importance compared with the more pronounced effects of wing height and angle of attack.

From the foregoing discussion it is evident that the losses in vertical-tail loads due to raising the wing and to increasing the angle of attack would cause undesirable losses in directional stability, inasmuch as the largest load losses occur in the regions of the root chord which, because of taper, are the largest contributors to the total tail load.

Vertical-Tail Center of Pressure

The chordwise locations of local center of pressure as affected by wing height are presented in figure 9 for various model angles of attack and angles of sideslip. These data indicate no large effects of wing height. The individual configurations, however, are affected by angle of attack, inasmuch as the local chordwise center of pressure appears to move rearward for $z/b_v = 0.11$, especially for sideslip angles of 3.9° . Examination of the chordwise loadings presented in figure 6 indicates that the section normal force for $z/b_v = 0.11$ is small compared with that farther outboard. This small load is assumed to be the result of adverse sidewash velocities near the vertical-tail fuselage juncture. (See ref. 2.)

Increasing the angle of attack produced the largest effect on the spanwise location of the center of pressure and caused a movement toward the tip for each wing-height configuration as shown in figure 10. Changes in wing height produced only small movements of the spanwise centers of pressure as compared with the effects of angle of attack. The effect of the presence of the wing on the spanwise location of the vertical-tail center of pressure was negligible except for the highest angle of attack investigated (15.9°). (See figs. 10 and 11.)

The comparison between the spanwise and chordwise locations of the vertical-tail center of pressure as obtained from the present tests and those obtained by force measurements (ref. 8), presented in figure 11 for the wing-off configuration, indicates good agreement except in the case of the chordwise centers of pressure for a Mach number of 0.92. The cause for this latter disagreement is not fully understood.

CONCLUSIONS

The results of a wind-tunnel investigation at high subsonic speeds of the effects of wing height and angle of attack on the vertical-tail pressure distributions of a complete model having a 45° swept wing indicate the following conclusions:

1. Raising the wing progressively decreased the vertical-tail load for constant angles of attack and sideslip, the largest load reductions occurring in the region near the tail root chord.
2. Increases in angle of attack, for a constant sideslip angle, produced increases in the vertical-tail loads for the low- and mid-wing configurations over most of the tail span except in the region of the root chord where load reductions occurred. For the high-wing configuration increases in angle of attack produced reductions in the tail loads over the complete span, the largest reduction occurring in the region near the tail root chord.
3. Substantial movements in the spanwise centers of pressure toward the tip of the vertical tail were caused by increases in angle of attack for all wing-height configurations. Increases in angle of attack also caused rearward movements in the chordwise locations of the centers of pressure particularly in the region of the root chord. The effects of wing height on the center-of-pressure location were considerably smaller than the effects of angle of attack.
4. The vertical-tail center-of-pressure locations as determined from previous tail-force tests and as determined from the present pressure measurements were generally in good agreement.

Langley Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va., April 3, 1957.

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TABLE I

PHYSICAL CHARACTERISTICS OF THE MODEL

Wing:

| | |
|--------------------------------------|-------------|
| Span, ft | 3.00 |
| Root chord, ft | 1.154 |
| Tip chord, ft | 0.346 |
| Mean aerodynamic chord, ft | 0.822 |
| Area, sq ft | 2.25 |
| Aspect ratio | 4.00 |
| Taper ratio | 0.30 |
| Quarter-chord sweep, deg | 45 |
| Airfoil section | NACA 65A006 |

Horizontal tail:

| | |
|--------------------------------------|-------------|
| Span, ft | 1.162 |
| Root chord, ft | 0.581 |
| Tip chord, ft | 0 |
| Mean aerodynamic chord, ft | 0.388 |
| Area, sq ft | 0.337 |
| Aspect ratio | 4.00 |
| Taper ratio | 0 |
| Quarter-chord sweep, deg | 36.85 |
| Airfoil section | NACA 65A006 |

Vertical tail:

| | |
|--|-------------|
| Span (measured from root chord), ft | 0.683 |
| Root chord (located 0.154 ft above fuselage center line), ft . . | 0.912 |
| Tip chord, ft | 0.420 |
| Mean aerodynamic chord, ft | 0.696 |
| Area, sq ft | 0.454 |
| Aspect ratio | 1.02 |
| Taper ratio | 0.46 |
| Quarter-chord sweep, deg | 28.35 |
| Airfoil section | NACA 65A006 |

TABLE II. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL

(a) $\alpha = 0^\circ$; $M = 0.60$.

| x c_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .608 | .649 | .381 | -.409 | -1.289 | .279 | .728 | .329 | -.397 | -1.179 |
| .025 | -.096 | -.535 | -1.146 | -2.274 | | .328 | -.087 | -.612 | -1.051 | -1.163 |
| .075 | -.107 | -.359 | -.673 | -1.524 | | .141 | -.130 | -.425 | -.934 | -1.105 |
| .150 | .033 | -.134 | -.293 | -.477 | -.724 | .051 | -.134 | -.309 | -.701 | -1.055 |
| .250 | .012 | -.098 | -.194 | -.298 | -.420 | -.013 | -.144 | -.259 | -.425 | -1.017 |
| .350 | -.026 | -.107 | -.162 | -.232 | -.341 | -.067 | -.162 | -.244 | -.325 | -.864 |
| .450 | -.060 | -.116 | -.144 | -.189 | -.305 | -.105 | -.171 | -.219 | -.264 | -.666 |
| .550 | -.071 | -.103 | -.112 | -.149 | -.307 | -.094 | -.139 | -.160 | -.198 | -.497 |
| .650 | -.035 | -.060 | -.063 | -.094 | -.211 | -.069 | -.098 | -.103 | -.130 | -.366 |
| .750 | -.010 | -.019 | -.015 | -.049 | -.132 | -.026 | -.040 | -.038 | -.065 | -.247 |
| .850 | .028 | .030 | .028 | .005 | -.053 | .026 | .021 | .028 | .012 | -.134 |
| .900 | .053 | .057 | .069 | .035 | -.010 | .055 | .060 | .060 | .053 | -.073 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.453 | -.033 | .317 | .607 | .830 | -.609 | -.069 | .372 | .596 | .738 |
| .075 | -.376 | -.112 | .127 | .345 | .546 | -.417 | -.123 | .146 | .360 | .524 |
| .150 | -.290 | -.125 | .051 | .213 | .373 | -.313 | -.130 | .051 | .218 | .364 |
| .250 | -.207 | -.103 | .019 | .143 | .262 | -.254 | -.141 | -.013 | .118 | .233 |
| .350 | -.173 | -.112 | -.029 | .064 | .166 | -.227 | -.153 | -.060 | .046 | .136 |
| .450 | -.159 | -.125 | -.065 | .008 | .089 | -.211 | -.157 | -.090 | -.011 | .064 |
| .550 | -.110 | -.103 | -.065 | -.011 | .048 | -.162 | -.137 | -.090 | -.033 | .021 |
| .650 | -.060 | -.058 | -.035 | -.003 | .044 | -.105 | -.094 | -.065 | -.020 | .012 |
| .750 | -.013 | -.015 | -.011 | -.019 | .046 | -.035 | -.028 | -.017 | .010 | .021 |
| .850 | .048 | .046 | .044 | .062 | .073 | .046 | .048 | .062 | .057 | .046 |
| .900 | .069 | .066 | .069 | .075 | .073 | .062 | .060 | .057 | .062 | .030 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .229 | .719 | .284 | -.373 | -.659 | .398 | .671 | .236 | -.275 | -.492 |
| .025 | .335 | -.119 | -.773 | -1.042 | -.742 | .193 | -.198 | -.678 | -.825 | -.528 |
| .075 | .148 | -.144 | -.474 | -.945 | -.724 | .021 | -.166 | -.388 | -.805 | -.535 |
| .150 | .035 | -.157 | -.361 | -.773 | -.708 | -.055 | -.144 | -.273 | -.701 | -.571 |
| .250 | -.028 | -.159 | -.284 | -.526 | -.672 | -.031 | -.089 | -.194 | -.540 | -.560 |
| .350 | -.085 | -.175 | -.244 | -.361 | -.645 | | | | | |
| .450 | -.114 | -.175 | -.214 | -.275 | -.614 | | | | | |
| .550 | -.114 | -.157 | -.176 | -.212 | -.575 | | | | | |
| .650 | -.083 | -.105 | -.112 | -.149 | -.521 | -.074 | -.071 | -.099 | -.339 | -.397 |
| .750 | -.044 | -.046 | -.054 | -.081 | -.458 | -.055 | -.040 | -.072 | -.316 | -.377 |
| .850 | .019 | .005 | .008 | -.024 | -.384 | -.031 | -.006 | -.054 | -.280 | -.350 |
| .900 | .030 | .028 | .030 | .005 | -.357 | -.013 | -.017 | -.047 | -.248 | -.337 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.710 | -.078 | .383 | .587 | .688 | -.561 | -.144 | .234 | .394 | .461 |
| .075 | -.466 | -.139 | .143 | .356 | .485 | -.378 | -.180 | .010 | .134 | .213 |
| .150 | -.324 | -.144 | .053 | .211 | .332 | -.265 | -.148 | -.060 | .003 | .062 |
| .250 | -.277 | -.162 | -.029 | .103 | .199 | | | | | |
| .350 | -.252 | -.173 | -.081 | .021 | .091 | | | | | |
| .450 | -.209 | -.173 | -.108 | -.026 | .033 | | | | | |
| .550 | -.168 | -.144 | -.101 | -.045 | -.006 | | | | | |
| .650 | -.105 | -.105 | -.072 | -.033 | -.019 | -.085 | -.071 | -.072 | -.060 | -.089 |
| .750 | -.046 | -.033 | -.029 | -.008 | -.039 | -.074 | -.046 | -.060 | -.067 | -.125 |
| .850 | .028 | .035 | .041 | .039 | -.033 | -.013 | .012 | -.006 | -.022 | -.114 |
| .900 | .060 | .060 | .062 | .053 | -.062 | -.010 | .035 | .012 | -.020 | -.134 |

TABLE II.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Continued

(b) $\alpha = 0^\circ$; $M = 0.80$.

| $\frac{x}{C_V}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_V = 0.11$ | | | | | $z/b_V = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .715 | .677 | .553 | .205 | -.280 | .472 | .771 | .535 | .043 | -.542 |
| .025 | .278 | -.064 | -.535 | -1.094 | -.1.417 | .330 | -.078 | -1.038 | -1.716 | -1.014 |
| .075 | .143 | -.092 | -.369 | -.892 | -1.207 | .148 | -.131 | -.443 | -1.513 | -1.006 |
| .150 | .045 | -.135 | -.325 | -.539 | -1.002 | .054 | -.143 | -.336 | -.506 | -.937 |
| .250 | .020 | -.102 | -.213 | -.302 | -.694 | -.019 | -.153 | -.278 | -.361 | -.854 |
| .350 | -.025 | -.110 | -.175 | -.234 | -.456 | -.078 | -.177 | -.260 | -.325 | -.743 |
| .450 | -.069 | -.129 | -.163 | -.197 | -.352 | -.130 | -.189 | -.231 | -.270 | -.629 |
| .550 | -.086 | -.117 | -.127 | -.141 | -.268 | -.107 | -.153 | -.165 | -.179 | -.512 |
| .650 | -.050 | -.058 | -.056 | -.089 | -.174 | -.078 | -.102 | -.100 | -.103 | -.419 |
| .750 | -.018 | -.016 | -.003 | -.036 | -.123 | -.030 | -.030 | -.026 | -.024 | -.316 |
| .850 | .034 | .044 | .056 | .028 | -.058 | .043 | .047 | .051 | .053 | -.218 |
| .900 | .067 | .079 | .086 | .066 | -.012 | .075 | .083 | .090 | .090 | -.156 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.414 | .003 | .331 | .608 | .831 | -.965 | -.048 | .371 | .607 | .746 |
| .075 | -.392 | -.096 | .140 | .360 | .559 | -.426 | -.119 | .157 | .368 | .535 |
| .150 | -.307 | -.120 | .056 | .225 | .390 | -.332 | -.131 | .059 | .228 | .377 |
| .250 | -.215 | -.102 | .016 | .158 | .279 | -.268 | -.150 | -.012 | .126 | .257 |
| .350 | -.186 | -.119 | -.032 | .073 | .178 | -.242 | -.167 | -.068 | .047 | .157 |
| .450 | -.162 | -.134 | -.079 | .008 | .087 | -.216 | -.173 | -.106 | -.023 | .060 |
| .550 | -.115 | -.107 | -.079 | -.023 | .044 | -.166 | -.147 | -.110 | -.045 | .012 |
| .650 | -.048 | -.055 | -.047 | -.004 | .035 | -.091 | -.093 | -.077 | -.029 | .001 |
| .750 | .001 | -.013 | -.014 | .020 | .030 | -.012 | -.013 | -.011 | .014 | .006 |
| .850 | .070 | .061 | .051 | .066 | .060 | .070 | .071 | .065 | .070 | .025 |
| .900 | .090 | .086 | .071 | .082 | .063 | .093 | .086 | .075 | .081 | .006 |
| $z/b_V = 0.66$ | | | | | $z/b_V = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .435 | .759 | .488 | .008 | -.382 | .492 | .704 | .382 | .000 | -.322 |
| .025 | .340 | -.117 | -1.127 | -1.437 | -.710 | .190 | -.235 | -.956 | -.732 | -.470 |
| .075 | .152 | -.150 | -.544 | -1.249 | -.707 | -.001 | -.201 | -.511 | -.734 | -.482 |
| .150 | .040 | -.171 | -.399 | -.960 | -.710 | -.075 | -.156 | -.293 | -.716 | -.512 |
| .250 | -.042 | -.176 | -.305 | -.716 | -.674 | -.036 | -.083 | -.210 | -.602 | -.502 |
| .350 | -.095 | -.189 | -.257 | -.480 | -.621 | | | | | |
| .450 | -.136 | -.195 | -.230 | -.305 | -.567 | | | | | |
| .550 | -.125 | -.168 | -.178 | -.196 | -.518 | | | | | |
| .650 | -.091 | -.105 | -.109 | -.106 | -.464 | | | | | |
| .750 | -.039 | -.030 | -.035 | -.033 | -.410 | | | | | |
| .850 | .028 | .038 | .035 | .028 | -.355 | | | | | |
| .900 | .049 | .065 | .063 | .053 | -.328 | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.185 | -.058 | .383 | .599 | .705 | -.1.043 | -.150 | .220 | .397 | .500 |
| .075 | -.4500 | -.138 | .158 | .360 | .512 | -.461 | -.205 | -.017 | .123 | .248 |
| .150 | -.347 | -.143 | .057 | .224 | .358 | -.267 | -.159 | -.077 | -.013 | .078 |
| .250 | -.295 | -.174 | -.036 | .102 | .228 | | | | | |
| .350 | -.262 | -.188 | -.097 | .011 | .106 | | | | | |
| .450 | -.223 | -.183 | -.130 | -.042 | .027 | | | | | |
| .550 | -.169 | -.159 | -.123 | -.059 | -.020 | | | | | |
| .650 | -.100 | -.101 | -.082 | -.041 | -.038 | | | | | |
| .750 | -.024 | -.018 | -.029 | -.004 | -.046 | | | | | |
| .850 | .061 | .068 | .056 | .058 | -.033 | | | | | |
| .900 | .096 | .095 | .080 | .076 | -.065 | | | | | |

TABLE II.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Continued

(c) $\alpha = 0^\circ$; $M = 0.85$.

| x C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .746 | .687 | .604 | .323 | -.110 | .528 | .781 | .595 | .189 | -.359 |
| .025 | .282 | -.054 | -.518 | -1.055 | -1.175 | .336 | -.071 | -1.068 | -1.531 | -.841 |
| .075 | .152 | -.088 | -.376 | -.867 | -1.034 | .152 | -.129 | -.415 | -1.370 | -.856 |
| .150 | .050 | -.138 | -.348 | -.686 | -.912 | .059 | -.146 | -.352 | -1.202 | -.825 |
| .250 | .022 | -.107 | -.229 | -.357 | -.749 | -.022 | -.163 | -.303 | -.330 | -.796 |
| .350 | -.028 | -.120 | -.192 | -.249 | -.585 | -.088 | -.189 | -.284 | -.276 | -.733 |
| .450 | -.080 | -.142 | -.175 | -.197 | -.471 | -.146 | -.211 | -.249 | -.266 | -.644 |
| .550 | -.101 | -.129 | -.134 | -.149 | -.366 | -.129 | -.170 | -.179 | -.190 | -.551 |
| .650 | -.062 | -.073 | -.065 | -.096 | -.249 | -.095 | -.111 | -.107 | -.107 | -.461 |
| .750 | -.025 | -.019 | -.002 | -.032 | -.177 | -.040 | -.040 | -.031 | -.026 | -.365 |
| .850 | .036 | .049 | .059 | .035 | -.087 | .040 | .047 | .056 | .059 | -.267 |
| .900 | .069 | .084 | .090 | .072 | -.034 | .083 | .088 | .100 | .098 | -.211 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.381 | .006 | .335 | .609 | .842 | -.981 | -.059 | .366 | .595 | .753 |
| .075 | -.400 | -.101 | .141 | .360 | .566 | -.448 | -.127 | .152 | .358 | .542 |
| .150 | -.323 | -.128 | .054 | .220 | .396 | -.344 | -.144 | .053 | .220 | .381 |
| .250 | -.224 | -.111 | .016 | .146 | .285 | -.284 | -.158 | -.022 | .118 | .257 |
| .350 | -.199 | -.131 | -.042 | .063 | .175 | -.260 | -.180 | -.086 | .032 | .152 |
| .450 | -.170 | -.145 | -.092 | -.006 | .080 | -.231 | -.193 | -.130 | -.043 | .049 |
| .550 | -.117 | -.121 | -.099 | -.036 | .030 | -.170 | -.161 | -.134 | -.073 | -.008 |
| .650 | -.052 | -.064 | -.058 | -.022 | .019 | -.093 | -.103 | -.093 | -.049 | -.024 |
| .750 | -.002 | -.019 | -.022 | -.002 | .008 | -.009 | -.016 | -.024 | -.004 | -.017 |
| .850 | .071 | .060 | .049 | .059 | .039 | .076 | .070 | .059 | .062 | .000 |
| .900 | .100 | .090 | .066 | .073 | .042 | .101 | .088 | .076 | .078 | -.021 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .484 | .766 | .547 | .140 | -.266 | .516 | .709 | .435 | .045 | -.270 |
| .025 | .339 | -.110 | -1.167 | -1.622 | -.747 | .179 | -.251 | -1.090 | -.840 | -.474 |
| .075 | .155 | -.153 | -.594 | -1.441 | -.759 | -.022 | -.231 | -.596 | -.821 | -.497 |
| .150 | .036 | -.183 | -.415 | -1.082 | -.766 | -.098 | -.176 | -.287 | -.800 | -.539 |
| .250 | -.053 | -.192 | -.313 | -.680 | -.701 | -.045 | -.098 | -.208 | -.673 | -.521 |
| .350 | -.118 | -.214 | -.270 | -.481 | -.628 | | | | | |
| .450 | -.158 | -.216 | -.245 | -.300 | -.593 | | | | | |
| .550 | -.151 | -.187 | -.189 | -.189 | -.545 | | | | | |
| .650 | -.103 | -.117 | -.110 | -.099 | -.488 | -.074 | -.064 | -.100 | -.380 | -.407 |
| .750 | -.042 | -.035 | -.032 | -.025 | -.430 | -.039 | -.020 | -.062 | -.327 | -.382 |
| .850 | .029 | .032 | .039 | .032 | -.366 | -.001 | .029 | -.036 | -.270 | -.352 |
| .900 | .053 | .062 | .070 | .059 | -.339 | .019 | .050 | -.018 | -.234 | -.339 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.153 | -.076 | .373 | .589 | .714 | -1.151 | -.172 | .207 | .388 | .503 |
| .075 | -.409 | -.152 | .149 | .348 | .513 | -.586 | -.237 | -.048 | .099 | .248 |
| .150 | -.366 | -.155 | .046 | .212 | .359 | -.231 | -.177 | -.109 | -.056 | .061 |
| .250 | -.309 | -.193 | -.049 | .085 | .221 | | | | | |
| .350 | -.274 | -.216 | -.120 | -.011 | .095 | | | | | |
| .450 | -.230 | -.207 | -.157 | -.075 | .008 | | | | | |
| .550 | -.175 | -.170 | -.148 | -.089 | -.046 | | | | | |
| .650 | -.098 | -.103 | -.099 | -.062 | -.060 | -.073 | -.060 | -.069 | -.079 | -.111 |
| .750 | -.018 | -.029 | -.032 | -.022 | -.070 | -.056 | -.026 | -.049 | -.069 | -.143 |
| .850 | .070 | .064 | .056 | .049 | -.055 | .011 | .056 | .025 | -.012 | -.119 |
| .900 | .104 | .095 | .080 | .075 | -.085 | .023 | .070 | .034 | -.016 | -.144 |

TABLE II - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Continued

(d) $\alpha = 0^\circ$; $M = 0.90$.

| $\frac{x}{C_V}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_V = 0.11$ | | | | | $Z/b_V = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .776 | .695 | .654 | .430 | .028 | .588 | .794 | .655 | .313 | .198 |
| .025 | .289 | -.046 | -.469 | -.969 | -1.040 | .330 | -.070 | -.973 | -1.333 | .725 |
| .075 | .156 | -.083 | -.390 | -.791 | -.923 | .150 | -.142 | -.668 | -1.206 | .730 |
| .150 | .046 | -.142 | -.370 | -.684 | -.814 | .048 | -.161 | -.374 | -1.100 | .737 |
| .250 | .010 | -.115 | -.239 | -.525 | -.691 | -.031 | -.182 | -.311 | -.660 | .723 |
| .350 | -.039 | -.134 | -.200 | -.336 | -.586 | -.109 | -.217 | -.319 | -.449 | .677 |
| .450 | -.105 | -.159 | -.190 | -.258 | -.517 | -.181 | -.251 | -.252 | -.245 | .616 |
| .550 | -.141 | -.153 | -.133 | -.146 | -.436 | -.173 | -.198 | -.167 | -.112 | .545 |
| .650 | -.083 | -.087 | -.059 | -.070 | -.330 | -.129 | -.125 | -.092 | -.056 | .473 |
| .750 | -.041 | -.025 | .011 | -.009 | -.233 | -.052 | -.035 | -.012 | .006 | .392 |
| .850 | .026 | .051 | .075 | .051 | -.137 | .038 | .051 | .074 | .083 | .316 |
| .900 | .062 | .087 | .101 | .086 | -.081 | .084 | .098 | .115 | .119 | .261 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.354 | .021 | .353 | .617 | .847 | -.927 | -.055 | .373 | .593 | .759 |
| .075 | -.417 | -.094 | .159 | .364 | .576 | -.654 | -.135 | .167 | .357 | .544 |
| .150 | -.365 | -.131 | .064 | .226 | .410 | -.392 | -.174 | .048 | .198 | .253 |
| .250 | -.259 | -.121 | .026 | .149 | .295 | -.313 | -.174 | -.014 | .111 | .265 |
| .350 | -.233 | -.143 | -.041 | .057 | .186 | -.314 | -.209 | -.087 | .023 | .157 |
| .450 | -.203 | -.165 | -.096 | -.017 | .081 | -.256 | -.227 | -.148 | -.062 | .044 |
| .550 | -.131 | -.142 | -.112 | -.058 | .023 | -.179 | -.187 | -.153 | -.101 | .017 |
| .650 | -.051 | -.073 | -.063 | -.038 | .004 | -.093 | -.118 | -.103 | -.080 | .040 |
| .750 | .004 | -.022 | -.025 | -.021 | -.012 | -.006 | -.014 | -.022 | -.014 | .034 |
| .850 | .074 | .062 | .050 | .054 | .016 | .084 | .079 | .070 | .058 | .017 |
| .900 | .100 | .091 | .075 | .069 | .011 | .110 | .094 | .088 | .078 | .052 |
| $Z/b_V = 0.66$ | | | | | $Z/b_V = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .535 | .775 | .609 | .268 | -.138 | .551 | .710 | .492 | .141 | .193 |
| .025 | .331 | -.113 | -1.087 | -1.413 | -.734 | .152 | -.269 | -1.048 | -1.373 | .460 |
| .075 | .146 | -.166 | -.903 | -.1274 | -.750 | -.063 | -.323 | -.989 | -1.317 | .479 |
| .150 | .021 | -.203 | -.390 | -.190 | -.753 | -.195 | -.206 | -.370 | -1.110 | .523 |
| .250 | -.076 | -.227 | -.390 | -.118 | -.698 | -.080 | -.113 | -.143 | -.743 | .509 |
| .350 | -.181 | -.254 | -.223 | -.639 | -.596 | | | | | |
| .450 | -.211 | -.253 | -.230 | -.206 | -.574 | | | | | |
| .550 | -.193 | -.213 | -.182 | -.064 | -.545 | | | | | |
| .650 | -.128 | -.119 | -.097 | -.032 | -.508 | | | | | |
| .750 | -.031 | -.031 | -.014 | .011 | -.459 | | | | | |
| .850 | .026 | .043 | .059 | .059 | .398 | | | | | |
| .900 | .054 | .074 | .088 | .085 | -.378 | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.051 | -.074 | .381 | .577 | .719 | -1.085 | -.193 | .206 | .378 | .513 |
| .075 | -.854 | -.169 | .157 | .342 | .512 | -.979 | -.327 | -.069 | .087 | .258 |
| .150 | -.368 | -.169 | .055 | .205 | .363 | -.385 | -.214 | -.176 | -.109 | .063 |
| .250 | -.394 | -.217 | -.057 | .071 | .227 | | | | | |
| .350 | -.265 | -.257 | -.140 | -.036 | .092 | | | | | |
| .450 | -.231 | -.245 | -.182 | -.117 | -.007 | | | | | |
| .550 | -.179 | -.198 | -.163 | -.130 | -.066 | | | | | |
| .650 | -.099 | -.114 | -.108 | -.093 | -.082 | | | | | |
| .750 | -.018 | -.025 | -.026 | -.034 | -.093 | | | | | |
| .850 | .078 | .073 | .071 | .055 | -.066 | | | | | |
| .900 | .112 | .103 | .095 | .081 | -.094 | | | | | |

TABLE II.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Continued

(e) $\alpha = 0^\circ$; $M = 0.92$.

| $\frac{x}{c_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .780 | .694 | .668 | .467 | .075 | .604 | .796 | .676 | .353 | .144 |
| .025 | .282 | -.039 | -.450 | -.929 | -1.013 | .322 | -.064 | -.928 | -1.245 | .763 |
| .075 | .153 | -.080 | -.380 | -.755 | -.897 | .143 | -.137 | -.701 | -1.126 | .735 |
| .150 | .039 | -.143 | -.370 | -.664 | -.793 | .043 | -.159 | -.410 | -1.040 | .717 |
| .250 | .008 | -.119 | -.257 | -.556 | -.674 | -.035 | -.182 | -.316 | -.716 | .700 |
| .350 | -.042 | -.138 | -.212 | -.370 | -.574 | -.114 | -.226 | -.338 | -.520 | .667 |
| .450 | -.112 | -.176 | -.205 | -.298 | -.515 | -.194 | -.277 | -.296 | -.380 | .614 |
| .550 | -.150 | -.178 | -.139 | -.168 | -.455 | -.188 | -.217 | -.164 | -.103 | .553 |
| .650 | -.091 | -.094 | -.058 | -.070 | -.361 | -.131 | -.127 | -.092 | -.032 | .493 |
| .750 | -.044 | -.020 | -.009 | -.001 | -.095 | -.055 | -.026 | -.011 | .027 | .420 |
| .850 | .028 | .056 | .073 | .059 | .176 | .039 | .061 | .078 | .092 | .349 |
| .900 | .060 | .095 | .102 | .096 | .112 | .085 | .109 | .118 | .129 | .283 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.334 | .029 | .346 | .620 | .852 | -.869 | -.045 | .362 | .595 | .760 |
| .075 | -.406 | -.088 | .151 | .368 | .580 | -.650 | -.132 | .156 | .364 | .545 |
| .150 | -.368 | -.127 | .061 | .234 | .414 | | | .225 | .230 | .227 |
| .250 | -.267 | -.119 | .018 | .155 | .297 | -.314 | -.176 | -.024 | .114 | .259 |
| .350 | -.230 | -.147 | -.051 | .062 | .185 | -.326 | -.218 | -.096 | .019 | .151 |
| .450 | -.211 | -.176 | -.104 | -.020 | .080 | -.281 | -.257 | -.165 | -.065 | .042 |
| .550 | -.133 | -.160 | -.126 | -.060 | .016 | -.169 | -.209 | -.177 | -.108 | -.026 |
| .650 | -.055 | -.077 | -.079 | -.043 | -.005 | -.086 | -.119 | -.118 | -.086 | -.057 |
| .750 | .004 | -.018 | -.037 | -.022 | -.029 | .001 | -.008 | -.026 | -.020 | -.050 |
| .850 | .079 | .070 | .048 | .053 | -.001 | .087 | .082 | .067 | .063 | -.037 |
| .900 | .101 | .096 | .069 | .078 | -.008 | .113 | .102 | .086 | .081 | -.062 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .550 | .780 | .629 | .310 | -.091 | .562 | .714 | .514 | .185 | .165 |
| .025 | .325 | -.107 | -1.036 | -1.320 | -.679 | .140 | -.284 | -1.007 | -1.279 | .507 |
| .075 | .139 | -.161 | -.878 | -.198 | -.687 | -.061 | -.304 | -.969 | -1.201 | .473 |
| .150 | .018 | -.204 | -.581 | -.113 | -.699 | -.224 | -.237 | -.659 | -1.015 | .515 |
| .250 | -.078 | -.234 | -.387 | -.1068 | -.683 | -.111 | -.107 | -.138 | -.900 | .510 |
| .350 | -.175 | -.299 | -.340 | -.937 | -.625 | | | | | |
| .450 | -.228 | -.274 | -.197 | -.356 | -.562 | | | | | |
| .550 | -.204 | -.220 | -.177 | -.047 | -.526 | | | | | |
| .650 | -.135 | -.108 | -.095 | .003 | -.494 | -.081 | -.050 | -.089 | -.436 | .421 |
| .750 | -.023 | -.023 | -.011 | .040 | -.451 | -.039 | -.006 | -.051 | -.351 | .399 |
| .850 | .029 | .055 | .063 | .079 | -.406 | .005 | .047 | -.020 | -.279 | -.371 |
| .900 | .060 | .086 | .092 | .098 | -.372 | .025 | .069 | -.007 | -.234 | -.355 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.002 | -.064 | .365 | .581 | .719 | -1.042 | -.181 | .194 | .386 | .515 |
| .075 | -.831 | -.158 | .145 | .346 | .516 | -.963 | -.361 | -.083 | .095 | .258 |
| .150 | -.458 | -.164 | .046 | .212 | .364 | -.585 | -.237 | -.215 | -.108 | .057 |
| .250 | -.387 | -.227 | -.066 | .074 | .225 | | | | | |
| .350 | -.362 | -.301 | -.163 | -.041 | .089 | | | | | |
| .450 | -.192 | -.259 | -.215 | -.128 | -.015 | | | | | |
| .550 | -.173 | -.202 | -.184 | -.153 | -.081 | | | | | |
| .650 | -.097 | -.101 | -.118 | -.102 | -.096 | -.085 | -.055 | -.068 | -.075 | -.123 |
| .750 | -.010 | -.017 | -.026 | -.035 | -.106 | -.060 | -.010 | -.037 | -.064 | -.174 |
| .850 | .081 | .083 | .071 | .063 | -.076 | .009 | .069 | .039 | .011 | -.134 |
| .900 | .111 | .114 | .094 | .095 | -.106 | .018 | .089 | .051 | .014 | -.156 |

TABLE II. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Continued

(f) $\alpha = 9.4^\circ$; $M = 0.60$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|---|-------|-------|--------|----------------|---|-------|-------|--------|--------|
| | $\beta = -3.9^\circ \quad \beta = 0^\circ \quad \beta = 3.9^\circ \quad \beta = 7.9^\circ \quad \beta = 12.7^\circ$ | | | | | $\beta = -3.9^\circ \quad \beta = 0^\circ \quad \beta = 3.9^\circ \quad \beta = 7.9^\circ \quad \beta = 12.7^\circ$ | | | | |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .516 | .818 | .499 | -.393 | -1.164 | .227 | .667 | .185 | -.695 | -1.564 |
| .025 | -.028 | -.134 | -.236 | -.769 | -2.346 | .291 | -.124 | -.673 | -1.141 | -1.424 |
| .075 | .004 | -.134 | -.298 | -.507 | -.874 | .121 | -.154 | -.453 | -.976 | -1.417 |
| .150 | -.023 | -.152 | -.298 | -.407 | -.608 | .036 | -.150 | -.334 | -.753 | -1.479 |
| .250 | -.021 | -.104 | -.215 | -.286 | -.396 | -.021 | -.159 | -.277 | -.407 | -1.146 |
| .350 | -.042 | -.104 | -.193 | -.237 | -.336 | -.067 | -.168 | -.259 | -.302 | -.598 |
| .450 | -.058 | -.115 | -.181 | -.207 | -.318 | -.095 | -.179 | -.236 | -.262 | -.364 |
| .550 | -.060 | -.113 | -.156 | -.169 | -.249 | -.090 | -.143 | -.181 | -.197 | -.284 |
| .650 | -.035 | -.065 | -.099 | -.132 | -.166 | -.067 | -.104 | -.128 | -.137 | -.215 |
| .750 | -.003 | -.030 | -.048 | -.053 | -.095 | -.026 | -.046 | -.069 | -.074 | -.129 |
| .850 | .027 | .022 | .007 | .005 | -.026 | .032 | .018 | .011 | .005 | -.056 |
| .900 | .055 | .055 | .039 | .040 | -.020 | .057 | .050 | .048 | .042 | -.017 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.179 | -.021 | -.007 | .531 | .799 | -.599 | -.040 | .352 | .568 | .687 |
| .075 | -.294 | -.115 | .007 | .317 | .528 | -.402 | -.111 | .153 | .347 | .526 |
| .150 | -.273 | -.122 | -.003 | .207 | .374 | -.312 | -.127 | .057 | .214 | .376 |
| .250 | -.207 | -.097 | -.014 | .149 | .275 | -.257 | -.136 | -.003 | .124 | .257 |
| .350 | -.191 | -.106 | -.044 | .077 | .183 | -.232 | -.147 | -.048 | .059 | .167 |
| .450 | -.177 | -.118 | -.062 | .021 | .114 | -.214 | -.154 | -.080 | .000 | .091 |
| .550 | -.143 | -.101 | -.058 | .003 | .075 | -.175 | -.134 | -.083 | -.023 | .054 |
| .650 | -.092 | -.062 | -.032 | .014 | .066 | -.118 | -.090 | -.055 | -.013 | .041 |
| .750 | -.042 | -.019 | -.003 | .028 | .066 | -.046 | -.030 | -.012 | .017 | .050 |
| .850 | .020 | .038 | .041 | .070 | .089 | .032 | .043 | .043 | .061 | .073 |
| .900 | .052 | .059 | .057 | .084 | .096 | .055 | .052 | .052 | .061 | .061 |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .132 | .628 | .059 | -.751 | -1.047 | .247 | .568 | -.003 | -.798 | |
| .025 | .293 | -.163 | -.920 | -1.255 | -.907 | .151 | -.234 | -.806 | -.707 | -.594 |
| .075 | .126 | -.170 | -.511 | -1.200 | -.902 | -.017 | -.195 | -.428 | -.695 | -.603 |
| .150 | .027 | -.177 | -.385 | -.1083 | -.874 | -.092 | -.168 | -.286 | -.646 | -.603 |
| .250 | -.037 | -.173 | -.302 | -.700 | -.838 | -.067 | -.106 | -.199 | -.541 | -.571 |
| .350 | -.088 | -.179 | -.266 | -.325 | -.812 | | | | | |
| .450 | -.115 | -.182 | -.234 | -.225 | -.762 | | | | | |
| .550 | -.118 | -.163 | -.197 | -.197 | -.677 | | | | | |
| .650 | -.090 | -.108 | -.133 | -.130 | -.552 | -.083 | -.062 | -.110 | -.332 | -.449 |
| .750 | -.040 | -.051 | -.069 | -.074 | -.428 | -.062 | -.023 | -.078 | -.288 | -.424 |
| .850 | -.001 | -.003 | -.012 | -.023 | -.318 | -.030 | -.004 | -.060 | -.244 | -.398 |
| .900 | .022 | .025 | .020 | .003 | -.261 | -.005 | -.022 | -.035 | -.211 | -.382 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.705 | -.060 | .364 | .554 | .631 | -.604 | -.131 | .196 | .317 | .397 |
| .075 | -.459 | -.124 | .146 | .338 | .484 | -.386 | -.182 | -.021 | .080 | .197 |
| .150 | -.329 | -.134 | .050 | .203 | .346 | -.260 | -.166 | -.101 | -.048 | .031 |
| .250 | -.285 | -.159 | -.028 | .093 | .222 | | | | | |
| .350 | -.257 | -.166 | -.080 | .019 | .126 | | | | | |
| .450 | -.216 | -.163 | -.108 | -.023 | .061 | | | | | |
| .550 | -.177 | -.145 | -.106 | -.041 | .018 | | | | | |
| .650 | -.118 | -.111 | -.078 | -.034 | .006 | -.079 | -.067 | -.074 | -.097 | -.104 |
| .750 | -.058 | -.033 | -.039 | -.013 | -.005 | -.067 | -.037 | -.078 | -.097 | -.139 |
| .850 | .025 | .032 | .032 | .038 | .006 | -.010 | .022 | -.014 | -.041 | -.132 |
| .900 | .045 | .055 | .048 | .054 | -.003 | -.001 | .034 | -.007 | -.044 | -.162 |

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TABLE II.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Continued

(g) $\alpha = 9.6^\circ$; $M = 0.80$.

| $\frac{X}{C_v}$ | C_p for - | | | | | C_p for - | | | | | | | | | | | |
|-------------------|----------------------|-------|-------------------|--------|---------------------|---------------------|----------------------|----------------------|--------|-------------------|------|---------------------|---------------------|----------------------|--|--|--|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | | | |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | | | | | | |
| .000 | .466 | .864 | .474 | -.119 | -.126 | .414 | .704 | .442 | -.127 | -.127 | .781 | | | | | | |
| .025 | -.064 | -.116 | -.154 | -.593 | -.1593 | .288 | -.125 | -.900 | -.1389 | -.1149 | | | | | | | |
| .075 | -.003 | -.128 | -.313 | -.496 | -.051 | .119 | -.160 | -.482 | -.1160 | -.1095 | | | | | | | |
| .150 | -.035 | -.169 | -.346 | -.483 | -.648 | .036 | -.152 | -.362 | -.813 | -.1054 | | | | | | | |
| .250 | -.031 | -.119 | -.244 | -.348 | -.445 | -.028 | -.166 | -.307 | -.442 | -.968 | | | | | | | |
| .350 | -.055 | -.122 | -.215 | -.281 | -.368 | -.081 | -.192 | -.287 | -.351 | -.790 | | | | | | | |
| .450 | -.076 | -.139 | -.208 | -.243 | -.349 | -.124 | -.207 | -.256 | -.296 | -.579 | | | | | | | |
| .550 | -.080 | -.136 | -.176 | -.198 | -.283 | -.110 | -.161 | -.192 | -.221 | -.426 | | | | | | | |
| .650 | -.046 | -.076 | -.105 | -.145 | -.216 | -.083 | -.111 | -.130 | -.154 | -.338 | | | | | | | |
| .750 | -.014 | -.031 | -.052 | -.060 | -.139 | -.038 | -.042 | -.055 | -.070 | -.249 | | | | | | | |
| .850 | .032 | .031 | .013 | .012 | -.060 | .035 | .036 | .030 | .012 | -.149 | | | | | | | |
| .900 | -.065 | -.070 | -.056 | -.053 | -.014 | -.068 | -.077 | -.074 | -.061 | -.091 | | | | | | | |
| <i>Right side</i> | | | | | | | | | | | | | | | | | |
| .025 | -.083 | .005 | -.038 | .481 | .754 | -.881 | -.028 | .347 | .568 | .703 | | | | | | | |
| .075 | -.308 | -.111 | .000 | .311 | .511 | -.427 | -.108 | .143 | .350 | .520 | | | | | | | |
| .150 | -.310 | -.130 | -.012 | .213 | .363 | -.337 | -.126 | .053 | .222 | .377 | | | | | | | |
| .250 | -.233 | -.102 | -.031 | .152 | .268 | -.285 | -.142 | -.011 | .125 | .259 | | | | | | | |
| .350 | -.218 | -.122 | -.058 | .076 | .175 | -.262 | -.164 | -.063 | .056 | .170 | | | | | | | |
| .450 | -.208 | -.139 | -.076 | .012 | .091 | -.241 | -.175 | -.101 | -.019 | .076 | | | | | | | |
| .550 | -.165 | -.122 | -.072 | -.014 | .050 | -.192 | -.154 | -.108 | -.041 | .036 | | | | | | | |
| .650 | -.098 | -.069 | -.043 | .000 | .039 | -.121 | -.101 | -.070 | -.029 | .012 | | | | | | | |
| .750 | -.047 | -.028 | -.011 | .015 | .035 | -.040 | -.023 | -.015 | .009 | .018 | | | | | | | |
| .850 | .033 | .042 | .050 | .064 | .059 | .047 | .055 | .058 | .059 | .039 | | | | | | | |
| .900 | -.061 | -.066 | -.065 | -.082 | -.062 | -.074 | -.070 | -.070 | -.070 | -.024 | | | | | | | |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | | | | | | |
| .000 | .318 | .657 | .314 | -.200 | -.669 | .335 | .584 | .193 | -.188 | -.607 | | | | | | | |
| .025 | .297 | -.172 | -.1098 | -.1035 | -.776 | .146 | -.292 | -.848 | -.622 | -.539 | | | | | | | |
| .075 | .126 | -.181 | -.628 | -.996 | -.755 | -.041 | -.245 | -.627 | -.618 | -.542 | | | | | | | |
| .150 | .020 | -.201 | -.422 | -.962 | -.726 | -.125 | -.184 | -.336 | -.616 | -.549 | | | | | | | |
| .250 | -.052 | -.192 | -.320 | -.868 | -.700 | -.073 | -.107 | -.227 | -.551 | -.546 | | | | | | | |
| .350 | -.108 | -.204 | -.275 | -.650 | -.675 | | | | | | | | | | | | |
| .450 | -.140 | -.205 | -.244 | -.424 | -.649 | | | | | | | | | | | | |
| .550 | -.145 | -.181 | -.197 | -.270 | -.607 | | | | | | | | | | | | |
| .650 | -.098 | -.110 | -.125 | -.154 | -.562 | -.081 | -.046 | -.101 | -.336 | -.446 | | | | | | | |
| .750 | -.041 | -.037 | -.049 | -.061 | -.501 | -.043 | -.001 | -.066 | -.297 | -.420 | | | | | | | |
| .850 | .013 | .024 | .017 | .003 | -.425 | -.002 | -.039 | -.023 | -.250 | -.390 | | | | | | | |
| .900 | -.039 | -.054 | -.052 | -.036 | -.384 | -.018 | -.058 | -.005 | -.221 | -.371 | | | | | | | |
| <i>Right side</i> | | | | | | | | | | | | | | | | | |
| .025 | -.977 | -.043 | .353 | .558 | .656 | -.948 | -.146 | .184 | .346 | .429 | | | | | | | |
| .075 | -.514 | -.123 | .146 | .347 | .499 | -.479 | -.213 | -.047 | .100 | .222 | | | | | | | |
| .150 | -.365 | -.137 | .055 | .218 | .358 | -.272 | -.178 | -.131 | -.055 | .039 | | | | | | | |
| .250 | -.310 | -.172 | -.038 | .100 | .229 | | | | | | | | | | | | |
| .350 | -.279 | -.189 | -.096 | .012 | .120 | | | | | | | | | | | | |
| .450 | -.237 | -.190 | -.133 | -.043 | .042 | | | | | | | | | | | | |
| .550 | -.188 | -.164 | -.127 | -.064 | -.010 | | | | | | | | | | | | |
| .650 | -.115 | -.114 | -.084 | -.047 | -.030 | -.052 | -.049 | -.067 | -.080 | -.123 | | | | | | | |
| .750 | -.043 | -.025 | -.034 | -.020 | -.040 | -.049 | -.016 | -.055 | -.087 | -.164 | | | | | | | |
| .850 | .044 | .051 | .042 | .042 | -.033 | .013 | .051 | .012 | -.043 | -.150 | | | | | | | |
| .900 | -.073 | -.077 | -.065 | -.061 | -.057 | .024 | .069 | .029 | -.051 | -.176 | | | | | | | |

TABLE II.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Continued

(h) $\alpha = 9.7^\circ$; $M = 0.85$.

| $\frac{X}{C_V}$ | C_p for - | | | | | | C_p for - | | | | | |
|-------------------|----------------------|-------|--------|-------------------|-------|----------------|---------------------|-------|-------|---------------------|--------|--|
| | $\beta = -3.9^\circ$ | | | $\beta = 0^\circ$ | | | $\beta = 3.9^\circ$ | | | $\beta = 7.9^\circ$ | | |
| | $z/b_V = 0.11$ | | | $z/b_V = 0.38$ | | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | .436 | .875 | .448 | -.129 | .009 | | .478 | .707 | .510 | .013 | -.636 | |
| .025 | -.101 | -.116 | -.108 | -.543 | -.149 | | .273 | -.130 | -.103 | -.1524 | -.1167 | |
| .075 | -.019 | -.142 | -.314 | -.505 | -.022 | | .105 | -.174 | -.472 | -.1188 | -.1107 | |
| .150 | -.051 | -.191 | -.389 | -.547 | -.711 | | .022 | -.174 | -.387 | -.752 | -.041 | |
| .250 | -.048 | -.137 | -.271 | -.415 | -.493 | | -.042 | -.190 | -.337 | -.520 | -.920 | |
| .350 | -.075 | -.140 | -.242 | -.328 | -.402 | | -.099 | -.224 | -.320 | -.387 | -.774 | |
| .450 | -.099 | -.173 | -.232 | -.274 | -.380 | | -.146 | -.242 | -.287 | -.340 | -.621 | |
| .550 | -.101 | -.163 | -.202 | -.222 | -.319 | | -.134 | -.194 | -.214 | -.251 | -.507 | |
| .650 | -.062 | -.101 | -.122 | -.159 | -.251 | | -.102 | -.135 | -.144 | -.165 | -.415 | |
| .750 | -.025 | -.048 | -.063 | -.070 | -.179 | | -.051 | -.061 | -.063 | -.080 | -.318 | |
| .850 | .025 | .022 | .011 | .009 | -.094 | | .032 | .028 | .025 | .009 | -.208 | |
| .900 | .062 | .062 | .053 | .049 | -.048 | | .070 | .070 | .068 | .055 | -.144 | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | -.035 | -.003 | -.066 | .447 | .749 | | -.875 | -.068 | .336 | .561 | .700 | |
| .075 | -.309 | -.136 | -.016 | .301 | .501 | | -.462 | -.139 | .131 | .341 | .511 | |
| .150 | -.336 | -.157 | -.022 | .203 | .354 | | -.355 | -.154 | .040 | .212 | .372 | |
| .250 | -.253 | -.128 | -.043 | .144 | .258 | | -.308 | -.171 | -.033 | .113 | .250 | |
| .350 | -.241 | -.146 | -.072 | .061 | .158 | | -.291 | -.197 | -.082 | .041 | .157 | |
| .450 | -.231 | -.166 | -.098 | -.008 | .080 | | -.265 | -.208 | -.126 | -.040 | .061 | |
| .550 | -.181 | -.150 | -.093 | -.035 | .035 | | -.208 | -.185 | -.131 | -.068 | .012 | |
| .650 | -.109 | -.094 | -.059 | -.022 | .023 | | -.128 | -.126 | -.093 | -.056 | -.009 | |
| .750 | -.049 | -.050 | -.028 | -.005 | .015 | | -.038 | -.043 | -.035 | -.012 | -.007 | |
| .850 | .030 | .033 | .040 | .048 | .041 | | .050 | .048 | .046 | .047 | .015 | |
| .900 | .062 | .057 | .060 | .069 | .036 | | .080 | .066 | .060 | .058 | -.006 | |
| $z/b_V = 0.66$ | | | | | | $z/b_V = 0.93$ | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | .376 | .662 | .378 | -.112 | -.601 | | .366 | .589 | .233 | .235 | .578 | |
| .025 | .280 | -.176 | -.1221 | -.1566 | -.784 | | .125 | -.297 | -.086 | .817 | .556 | |
| .075 | .115 | -.200 | -.628 | -.1347 | -.756 | | -.071 | -.314 | -.675 | .793 | .550 | |
| .150 | .006 | -.221 | -.472 | -.1054 | -.720 | | -.158 | -.217 | -.370 | .784 | .559 | |
| .250 | -.072 | -.228 | -.360 | -.783 | -.695 | | -.094 | -.135 | -.230 | .660 | .563 | |
| .350 | -.134 | -.242 | -.298 | -.520 | -.675 | | | | | | | |
| .450 | -.169 | -.239 | -.4265 | -.337 | -.650 | | | | | | | |
| .550 | -.162 | -.212 | -.218 | -.231 | -.612 | | | | | | | |
| .650 | -.118 | -.129 | -.139 | -.136 | -.578 | | -.087 | -.067 | -.105 | .356 | .473 | |
| .750 | -.049 | -.053 | -.059 | -.053 | -.528 | | -.045 | -.019 | -.063 | .300 | .447 | |
| .850 | .013 | .017 | .014 | .009 | -.454 | | -.002 | .031 | -.025 | .239 | .419 | |
| .900 | .045 | .048 | .046 | .044 | -.425 | | .020 | .046 | -.002 | .203 | .405 | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | -1.129 | -.077 | .342 | .545 | .652 | | -1.141 | -.193 | .176 | .341 | .428 | |
| .075 | -.472 | -.157 | .143 | .334 | .488 | | -.557 | -.279 | -.071 | .085 | .218 | |
| .150 | -.395 | -.168 | .046 | .207 | .348 | | -.273 | -.218 | -.164 | -.099 | .022 | |
| .250 | -.343 | -.208 | -.053 | .084 | .218 | | | | | | | |
| .350 | -.293 | -.229 | -.118 | -.008 | .107 | | | | | | | |
| .450 | -.251 | -.228 | -.157 | -.073 | .020 | | | | | | | |
| .550 | -.198 | -.195 | -.148 | -.096 | -.039 | | | | | | | |
| .650 | -.121 | -.120 | -.099 | -.076 | -.061 | | -.071 | -.067 | -.078 | -.101 | -.154 | |
| .750 | -.041 | -.048 | -.046 | -.041 | -.071 | | -.052 | -.027 | -.058 | -.104 | -.196 | |
| .850 | .050 | .048 | .044 | .034 | -.059 | | .016 | .049 | .015 | -.047 | -.176 | |
| .900 | .088 | .076 | .070 | .051 | -.090 | | .033 | .062 | .027 | -.045 | -.205 | |

TABLE II.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Continued

(i) $\alpha = 9.7^\circ$; $M = 0.90$.

| x c_v | C_p for - | | | | | C_p for - | | | | |
|----------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| Left side | | | | | | | | | | |
| .000 | .340 | .896 | .413 | | | .528 | .714 | .568 | | |
| .025 | -.140 | -.108 | .000 | | | .266 | -.136 | -.1001 | | |
| .075 | -.030 | -.140 | -.239 | | | .096 | -.186 | -.484 | | |
| .150 | -.050 | -.207 | -.397 | | | .011 | -.191 | -.466 | | |
| .250 | -.057 | -.151 | -.291 | | | -.052 | -.207 | -.353 | | |
| .350 | -.092 | -.159 | -.264 | | | -.116 | -.240 | -.369 | | |
| .450 | -.117 | -.196 | -.266 | | | -.183 | -.282 | -.343 | | |
| .550 | -.119 | -.196 | -.223 | | | -.171 | -.220 | -.210 | | |
| .650 | -.077 | -.111 | -.121 | | | -.131 | -.140 | -.136 | | |
| .750 | -.042 | -.052 | -.055 | | | -.061 | -.057 | -.054 | | |
| .850 | .019 | .020 | .020 | | | .026 | .036 | .039 | | |
| .900 | .058 | .067 | .062 | | | .073 | .083 | .088 | | |
| Right side | | | | | | | | | | |
| .025 | .075 | .007 | -.087 | | | -.852 | -.060 | .330 | | |
| .075 | -.256 | -.140 | -.009 | | | -.534 | -.144 | .129 | | |
| .150 | -.378 | -.170 | -.011 | | | -.425 | -.159 | .034 | | |
| .250 | -.293 | -.141 | -.039 | | | -.339 | -.183 | -.031 | | |
| .350 | -.277 | -.163 | -.073 | | | -.359 | -.219 | -.089 | | |
| .450 | -.277 | -.187 | -.102 | | | -.334 | -.244 | -.144 | | |
| .550 | -.214 | -.175 | -.099 | | | -.213 | -.214 | -.153 | | |
| .650 | -.120 | -.104 | -.069 | | | -.132 | -.143 | -.105 | | |
| .750 | -.056 | -.051 | -.031 | | | -.038 | -.033 | -.036 | | |
| .850 | -.032 | -.034 | -.038 | | | .053 | .055 | .047 | | |
| .900 | .065 | .064 | .063 | | | .088 | .075 | .065 | | |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| Left side | | | | | | | | | | |
| .000 | .413 | .667 | .440 | | | .382 | .590 | .280 | | |
| .025 | .272 | -.183 | -.157 | | | .113 | -.347 | -.153 | | |
| .075 | .105 | -.211 | -.965 | | | -.089 | -.330 | -.073 | | |
| .150 | -.009 | -.234 | -.459 | | | -.295 | -.258 | -.502 | | |
| .250 | -.092 | -.251 | -.443 | | | -.140 | -.121 | -.156 | | |
| .350 | -.170 | -.294 | -.385 | | | | | | | |
| .450 | -.221 | -.274 | -.229 | | | | | | | |
| .550 | -.202 | -.227 | -.202 | | | | | | | |
| .650 | -.136 | -.127 | -.126 | | | | | | | |
| .750 | -.056 | -.043 | -.043 | | | | | | | |
| .850 | .011 | .028 | .028 | | | | | | | |
| .900 | .045 | .060 | .065 | | | | | | | |
| Right side | | | | | | | | | | |
| .025 | -.1070 | -.073 | .333 | | | -.131 | -.196 | .166 | | |
| .075 | -.809 | -.164 | .128 | | | -.972 | -.338 | -.091 | | |
| .150 | -.407 | -.178 | .034 | | | -.391 | -.256 | -.285 | | |
| .250 | -.434 | -.234 | -.067 | | | | | | | |
| .350 | -.409 | -.274 | -.148 | | | | | | | |
| .450 | -.232 | -.259 | -.198 | | | | | | | |
| .550 | -.198 | -.220 | -.175 | | | | | | | |
| .650 | -.119 | -.109 | -.114 | | | | | | | |
| .750 | -.038 | -.037 | -.047 | | | | | | | |
| .850 | .056 | .059 | .046 | | | | | | | |
| .900 | .091 | .090 | .071 | | | | | | | |

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TABLE II.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Continued

(j) $\alpha = 15.6^\circ$; $M = 0.60$.

| x c_v | C_p for - | | | | | | C_p for - | | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|--|--|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | | |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | .785 | .809 | .833 | .170 | -.458 | .235 | .676 | .293 | -.651 | -.1487 | | |
| .025 | -.303 | -.160 | -.176 | -.412 | -.149 | .316 | -.124 | -.673 | -.1487 | -.1941 | | |
| .075 | -.141 | -.155 | -.267 | -.385 | -.739 | .127 | -.158 | -.471 | -.974 | -.2067 | | |
| .150 | -.109 | -.182 | -.303 | -.390 | -.566 | .030 | -.164 | -.353 | -.507 | -.1473 | | |
| .250 | -.073 | -.135 | -.222 | -.290 | -.394 | -.039 | -.167 | -.297 | -.401 | -.521 | | |
| .350 | -.087 | -.133 | -.199 | -.252 | -.333 | -.089 | -.182 | -.281 | -.351 | -.498 | | |
| .450 | -.105 | -.144 | -.194 | -.232 | -.297 | -.123 | -.191 | -.260 | -.304 | -.435 | | |
| .550 | -.107 | -.133 | -.165 | -.182 | -.253 | -.107 | -.164 | -.206 | -.236 | -.340 | | |
| .650 | -.073 | -.088 | -.108 | -.121 | -.185 | -.087 | -.124 | -.147 | -.175 | -.267 | | |
| .750 | -.046 | -.050 | -.061 | -.069 | -.124 | -.055 | -.070 | -.086 | -.107 | -.188 | | |
| .850 | -.003 | .004 | -.002 | -.004 | -.054 | .006 | .002 | -.009 | -.042 | -.104 | | |
| .900 | .026 | .037 | .032 | .033 | -.011 | .037 | .033 | .028 | -.008 | -.058 | | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | -.071 | -.077 | -.201 | .245 | .561 | -.686 | -.102 | .345 | .536 | .699 | | |
| .075 | -.285 | -.164 | -.156 | .109 | .298 | -.472 | -.155 | .125 | .308 | .477 | | |
| .150 | -.296 | -.169 | -.104 | .062 | .157 | -.361 | -.162 | .035 | .173 | .307 | | |
| .250 | -.235 | -.133 | -.074 | .035 | .089 | -.296 | -.167 | -.027 | .078 | .175 | | |
| .350 | -.220 | -.135 | -.088 | -.006 | .030 | -.274 | -.171 | -.074 | .005 | .089 | | |
| .450 | -.208 | -.151 | -.106 | -.044 | -.015 | -.253 | -.182 | -.104 | -.055 | .010 | | |
| .550 | -.166 | -.126 | -.097 | -.049 | -.024 | -.211 | -.162 | -.104 | -.076 | -.031 | | |
| .650 | -.114 | -.086 | -.067 | -.033 | -.015 | -.152 | -.115 | -.077 | -.062 | -.038 | | |
| .750 | -.060 | -.043 | -.036 | -.008 | -.002 | -.078 | -.054 | -.029 | -.033 | -.029 | | |
| .850 | .008 | .020 | .014 | .033 | .028 | .003 | .017 | .030 | .014 | .005 | | |
| .900 | .028 | .042 | .032 | .046 | .035 | .024 | .035 | .037 | .019 | -.006 | | |
| $z/b_v = 0.66$ | | | | | | $z/b_v = 0.93$ | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | -.026 | .616 | .003 | -.805 | -.1317 | .098 | .544 | -.111 | -.566 | -.845 | | |
| .025 | .339 | -.142 | -.1038 | -.1320 | -.131 | .175 | -.218 | .868 | -.746 | -.741 | | |
| .075 | .148 | -.169 | -.555 | -.1295 | -.140 | -.015 | -.200 | -.462 | -.724 | -.739 | | |
| .150 | .030 | -.182 | -.410 | -.1225 | -.108 | -.116 | -.178 | -.308 | -.679 | -.725 | | |
| .250 | -.037 | -.178 | -.315 | -.807 | -.077 | -.091 | -.108 | -.219 | -.590 | -.689 | | |
| .350 | -.100 | -.196 | -.285 | -.329 | -.1009 | | | | | | | |
| .450 | -.136 | -.198 | -.256 | -.245 | -.866 | | | | | | | |
| .550 | -.143 | -.180 | -.215 | -.220 | -.693 | | | | | | | |
| .650 | -.114 | -.137 | -.151 | -.159 | -.505 | -.123 | -.081 | -.133 | -.403 | -.575 | | |
| .750 | -.073 | -.072 | -.088 | -.094 | -.335 | -.091 | -.046 | -.104 | -.351 | -.553 | | |
| .850 | -.028 | -.021 | -.029 | -.033 | -.208 | -.055 | -.007 | -.074 | -.293 | -.521 | | |
| .900 | -.008 | .002 | .005 | -.008 | -.156 | -.033 | .011 | -.049 | -.254 | -.494 | | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | -.1037 | -.115 | .359 | .556 | .665 | -.828 | -.178 | .196 | .321 | .397 | | |
| .075 | -.569 | -.164 | .137 | .346 | .518 | -.503 | -.216 | -.033 | .087 | .207 | | |
| .150 | -.393 | -.162 | .044 | .204 | .366 | -.328 | -.185 | -.120 | -.060 | .032 | | |
| .250 | -.337 | -.182 | -.045 | .087 | .230 | | | | | | | |
| .350 | -.301 | -.189 | -.090 | .001 | .130 | | | | | | | |
| .450 | -.258 | -.189 | -.129 | -.051 | .057 | | | | | | | |
| .550 | -.215 | -.167 | -.124 | -.074 | .010 | | | | | | | |
| .650 | -.154 | -.122 | -.102 | -.065 | -.006 | -.114 | -.084 | -.097 | -.110 | -.113 | | |
| .750 | -.093 | -.066 | -.061 | -.042 | -.018 | -.116 | -.050 | -.090 | -.119 | -.147 | | |
| .850 | -.017 | .011 | .012 | .012 | .010 | -.060 | .011 | -.031 | -.071 | -.131 | | |
| .900 | .019 | .033 | .032 | .028 | .003 | -.037 | .022 | -.015 | -.069 | -.163 | | |

TABLE II. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Continued

(k) $\alpha = 15.8^\circ$; $M = 0.80$.

| x c_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .332 | .837 | .665 | .540 | -.437 | .436 | .729 | .497 | .156 | -1.503 |
| .025 | -.033 | -.195 | .270 | -.101 | -1.153 | .299 | -.148 | -1.180 | -1.651 | -1.970 |
| .075 | -.308 | -.203 | -.109 | -.265 | -.724 | .109 | -.201 | -.551 | -.954 | -2.095 |
| .150 | -.131 | -.242 | -.353 | -.457 | -.548 | .021 | -.207 | -.430 | -.688 | -1.489 |
| .250 | -.089 | -.191 | -.282 | -.353 | -.367 | -.050 | -.215 | -.365 | -.460 | -.501 |
| .350 | -.092 | -.171 | -.258 | -.306 | -.301 | -.118 | -.237 | -.339 | -.427 | -.480 |
| .450 | -.118 | -.192 | -.256 | -.290 | -.268 | -.158 | -.251 | -.309 | -.370 | -.409 |
| .550 | -.127 | -.181 | -.218 | -.247 | -.224 | -.145 | -.210 | -.239 | -.294 | -.315 |
| .650 | -.098 | -.117 | -.137 | -.180 | -.151 | -.119 | -.153 | -.171 | -.211 | -.233 |
| .750 | -.071 | -.064 | -.078 | -.104 | -.092 | -.066 | -.083 | -.085 | -.122 | -.153 |
| .850 | -.027 | -.002 | -.014 | -.018 | -.020 | .002 | -.000 | -.005 | -.042 | -.067 |
| .900 | -.009 | .042 | .030 | .022 | .034 | .036 | .042 | .040 | .004 | -.015 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .359 | -.088 | -.979 | -.100 | .619 | -.1.167 | -.129 | .346 | .493 | .762 |
| .075 | -.116 | -.212 | -.303 | -.088 | .347 | -.529 | -.194 | .116 | .252 | .530 |
| .150 | -.324 | -.224 | -.118 | -.054 | .201 | -.422 | -.201 | .019 | .121 | .358 |
| .250 | -.276 | -.186 | -.081 | -.045 | .131 | -.351 | -.204 | -.041 | .035 | .222 |
| .350 | -.264 | -.181 | -.093 | -.057 | .067 | -.321 | -.218 | -.093 | -.036 | .124 |
| .450 | -.246 | -.195 | -.123 | -.082 | .025 | -.290 | -.234 | -.143 | -.101 | .048 |
| .550 | -.196 | -.168 | -.123 | -.076 | .016 | -.232 | -.204 | -.144 | -.119 | .006 |
| .650 | -.127 | -.109 | -.097 | -.048 | .027 | -.155 | -.139 | -.111 | -.100 | .006 |
| .750 | -.068 | -.059 | -.064 | -.030 | .032 | -.069 | -.064 | -.053 | -.063 | .013 |
| .850 | -.011 | .016 | -.003 | .025 | .067 | .017 | .021 | .019 | -.006 | .041 |
| .900 | .032 | .047 | .019 | .037 | .077 | .042 | .041 | .034 | -.005 | .034 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .234 | .655 | .269 | -.213 | -1.322 | .229 | .563 | .083 | -.400 | -.834 |
| .025 | .332 | -.160 | -1.365 | -1.385 | -1.130 | .169 | -.280 | -1.073 | -.740 | -.726 |
| .075 | .151 | -.197 | -.760 | -1.302 | -1.135 | -.035 | -.265 | -.758 | -.746 | -.724 |
| .150 | .026 | -.218 | -.504 | -1.104 | -1.106 | -.152 | -.218 | -.451 | -.725 | -.710 |
| .250 | -.054 | -.219 | -.377 | -.898 | -.1078 | -.099 | -.124 | -.294 | -.657 | -.672 |
| .350 | -.122 | -.239 | -.327 | -.651 | -1.001 | | | | | |
| .450 | -.169 | -.246 | -.289 | -.412 | -.853 | | | | | |
| .550 | -.179 | -.219 | -.239 | -.281 | -.677 | | | | | |
| .650 | -.137 | -.151 | -.168 | -.180 | -.480 | | | | | |
| .750 | -.078 | -.076 | -.088 | -.097 | -.301 | | | | | |
| .850 | -.024 | -.014 | -.017 | -.027 | -.175 | | | | | |
| .900 | -.000 | .021 | .016 | .001 | -.123 | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.468 | -.135 | .367 | .554 | .729 | -.900 | -.224 | .198 | .349 | .450 |
| .075 | -.652 | -.203 | .149 | .337 | .574 | -.724 | -.278 | -.066 | .099 | .255 |
| .150 | -.452 | -.195 | .043 | .200 | .419 | -.452 | -.227 | -.164 | -.079 | .072 |
| .250 | -.379 | -.218 | -.053 | .083 | .281 | | | | | |
| .350 | -.329 | -.246 | -.121 | -.015 | .170 | | | | | |
| .450 | -.279 | -.234 | -.161 | -.079 | .095 | | | | | |
| .550 | -.231 | -.204 | -.162 | -.110 | .051 | | | | | |
| .650 | -.157 | -.139 | -.125 | -.100 | .034 | | | | | |
| .750 | -.075 | -.076 | -.072 | -.066 | .020 | | | | | |
| .850 | -.014 | .018 | .010 | -.003 | .046 | | | | | |
| .900 | .044 | .048 | .031 | .014 | .044 | | | | | |

~~CONFIDENTIAL~~

TABLE II.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
AND VERTICAL TAIL - Concluded

(l) $\alpha = 15.9^\circ$; $M = 0.85$.

| x C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| 000 | .384 | .852 | .699 | .482 | | .487 | .736 | .552 | .251 | |
| 025 | -1.035 | -0.220 | .301 | .155 | | .273 | .183 | -1.230 | -1.497 | |
| 075 | -0.535 | -0.238 | -0.073 | -0.289 | | .078 | -0.244 | -0.614 | -0.922 | |
| 150 | -0.160 | -0.292 | -0.379 | -0.474 | | -0.015 | -0.245 | -0.493 | -0.806 | |
| 250 | -0.118 | -0.234 | -0.323 | -0.450 | | -0.087 | -0.248 | -0.399 | -0.592 | |
| 350 | -0.123 | -0.202 | -0.291 | -0.359 | | -0.161 | -0.281 | -0.388 | -0.416 | |
| 450 | -0.142 | -0.231 | -0.294 | -0.310 | | -0.206 | -0.303 | -0.341 | -0.423 | |
| 550 | -0.143 | -0.219 | -0.247 | -0.264 | | -0.189 | -0.248 | -0.257 | -0.317 | |
| 650 | -0.108 | -0.141 | -0.155 | -0.191 | | -0.153 | -0.183 | -0.182 | -0.226 | |
| 750 | -0.071 | -0.090 | -0.094 | -0.120 | | -0.092 | -0.103 | -0.098 | -0.131 | |
| 850 | -0.021 | -0.022 | -0.021 | -0.039 | | -0.016 | -0.013 | -0.010 | -0.043 | |
| 900 | 0.017 | 0.029 | 0.023 | 0.009 | | 0.027 | 0.033 | 0.037 | 0.005 | |
| <i>Right side</i> | | | | | | | | | | |
| 025 | .393 | -0.101 | -0.982 | -0.073 | | -1.108 | -0.145 | .319 | .462 | |
| 075 | -0.064 | -0.254 | -0.465 | -0.094 | | -0.635 | -0.223 | .091 | .227 | |
| 150 | -0.371 | -0.268 | -0.131 | -0.076 | | -0.535 | -0.230 | -0.010 | .098 | |
| 250 | -0.350 | -0.227 | -0.105 | -0.070 | | -0.406 | -0.240 | -0.075 | .013 | |
| 350 | -0.324 | -0.217 | -0.115 | -0.087 | | -0.379 | -0.260 | -0.128 | .059 | |
| 450 | -0.296 | -0.228 | -0.135 | -0.107 | | -0.327 | -0.274 | -0.179 | .130 | |
| 550 | -0.237 | -0.202 | -0.129 | -0.099 | | -0.260 | -0.238 | -0.178 | .147 | |
| 650 | -0.154 | -0.131 | -0.098 | -0.070 | | -0.173 | -0.169 | -0.136 | .124 | |
| 750 | -0.094 | -0.083 | -0.064 | -0.046 | | -0.083 | -0.087 | -0.073 | .075 | |
| 850 | -0.007 | 0.001 | -0.002 | 0.006 | | 0.005 | 0.006 | 0.006 | -0.017 | |
| 900 | 0.020 | 0.035 | 0.027 | 0.023 | | 0.037 | 0.033 | 0.024 | -0.009 | |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| 000 | .306 | .654 | .348 | .086 | | .254 | .552 | .131 | -.365 | |
| 025 | .299 | -0.200 | -1.402 | -1.388 | | .134 | -0.343 | -1.332 | -0.831 | |
| 075 | .116 | -0.233 | -1.168 | -1.283 | | -0.077 | -0.344 | -0.915 | -0.838 | |
| 150 | -0.009 | -0.258 | -0.520 | -1.127 | | -0.249 | -0.260 | -0.531 | -0.800 | |
| 250 | -0.092 | -0.268 | -0.422 | -0.881 | | -0.136 | -0.146 | -0.276 | -0.735 | |
| 350 | -0.174 | -0.291 | -0.340 | -0.712 | | | | | | |
| 450 | -0.223 | -0.292 | -0.311 | -0.504 | | | | | | |
| 550 | -0.226 | -0.255 | -0.263 | -0.337 | | | | | | |
| 650 | -0.173 | -0.176 | -0.182 | -0.209 | | -0.139 | -0.103 | -0.162 | -.440 | |
| 750 | -0.102 | -0.094 | -0.098 | -0.110 | | -0.095 | -0.053 | -0.115 | -.376 | |
| 850 | -0.038 | -0.028 | -0.023 | -0.034 | | -0.053 | -0.006 | -0.078 | -.304 | |
| 900 | -0.008 | 0.011 | 0.014 | 0.000 | | -0.028 | 0.021 | 0.050 | -.267 | |
| <i>Right side</i> | | | | | | | | | | |
| 025 | -1.374 | -0.149 | .332 | .537 | | -1.403 | -0.254 | .166 | .342 | |
| 075 | -1.137 | -0.226 | .114 | .313 | | -0.981 | -0.344 | -0.104 | .084 | |
| 150 | -0.472 | -0.220 | .011 | .179 | | -0.564 | -0.267 | -0.247 | -.119 | |
| 250 | -0.443 | -0.260 | -0.087 | .056 | | | | | | |
| 350 | -0.347 | -0.293 | -0.165 | -.051 | | | | | | |
| 450 | -0.308 | -0.278 | -0.206 | -.116 | | | | | | |
| 550 | -0.251 | -0.235 | -0.200 | -.144 | | | | | | |
| 650 | -0.173 | -0.163 | -0.152 | -.126 | | -0.144 | -0.104 | -0.124 | -.151 | |
| 750 | -0.091 | -0.090 | -0.097 | -.087 | | -0.121 | -0.064 | -0.102 | -.150 | |
| 850 | 0.005 | 0.009 | -0.004 | -0.017 | | -0.050 | 0.016 | -0.026 | -.089 | |
| 900 | 0.037 | 0.039 | 0.025 | 0.003 | | -0.032 | 0.032 | -0.014 | -.092 | |

TABLE III. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL

(a) $\alpha = 0^\circ$; $M = 0.60$.

| X C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .559 | .657 | .242 | -.658 | -1.359 | .171 | .736 | .197 | -.642 | -1.274 |
| .025 | .317 | -.106 | -.632 | -1.400 | -1.573 | .374 | -.090 | -.771 | -1.297 | -1.021 |
| .075 | .169 | -.110 | -.422 | -.797 | -1.518 | .178 | -.130 | -.483 | -1.256 | -1.009 |
| .150 | .068 | -.130 | -.334 | -.555 | -1.267 | .078 | -.140 | -.348 | -1.158 | -.989 |
| .250 | .043 | -.094 | -.224 | -.343 | -.783 | .002 | -.142 | -.283 | -.731 | -.950 |
| .350 | -.005 | -.106 | -.186 | -.260 | -.498 | -.053 | -.160 | -.260 | -.352 | -.872 |
| .450 | -.041 | -.117 | -.168 | -.219 | -.370 | -.103 | -.176 | -.233 | -.256 | -.749 |
| .550 | -.055 | -.103 | -.136 | -.176 | -.290 | -.085 | -.144 | -.179 | -.196 | -.619 |
| .650 | -.028 | -.069 | -.084 | -.130 | -.256 | -.069 | -.108 | -.123 | -.146 | -.512 |
| .750 | -.016 | -.026 | -.039 | -.087 | -.206 | -.028 | -.049 | -.060 | -.082 | -.397 |
| .850 | .020 | .019 | .017 | -.028 | -.142 | .025 | .019 | .017 | .000 | -.283 |
| .900 | .050 | .051 | .044 | .004 | -.094 | .057 | .057 | .055 | .039 | -.215 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.553 | -.035 | .366 | .669 | .877 | -.703 | -.069 | .413 | .635 | .753 |
| .075 | -.429 | -.119 | .163 | .395 | .591 | -.464 | -.124 | .188 | .390 | .550 |
| .150 | -.322 | -.121 | .082 | .253 | .422 | -.352 | -.135 | .080 | .240 | .390 |
| .250 | -.224 | -.097 | .044 | .167 | .297 | -.272 | -.137 | .010 | .128 | .256 |
| .350 | -.199 | -.108 | -.006 | .089 | .196 | -.247 | -.149 | -.037 | .062 | .162 |
| .450 | -.171 | -.117 | -.039 | .036 | .119 | -.222 | -.160 | -.073 | .000 | .089 |
| .550 | -.130 | -.094 | -.039 | .016 | .082 | -.180 | -.137 | -.080 | -.023 | .039 |
| .650 | -.073 | -.058 | -.017 | .030 | .066 | -.117 | -.092 | -.053 | -.012 | .018 |
| .750 | -.030 | -.017 | -.001 | .034 | .055 | -.048 | -.031 | -.010 | .014 | .014 |
| .850 | .027 | .035 | .042 | .064 | .066 | .032 | .041 | .051 | .059 | .020 |
| .900 | .055 | .055 | .057 | .057 | .059 | .057 | .060 | .057 | .059 | -.007 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .151 | .718 | .172 | -.295 | -.731 | .347 | .675 | .154 | -.142 | -.525 |
| .025 | .379 | -.126 | -1.003 | -.877 | -.724 | .230 | -.176 | -.837 | -.662 | -.528 |
| .075 | .178 | -.151 | -.528 | -.845 | -.715 | .048 | -.167 | -.420 | -.651 | -.548 |
| .150 | .062 | -.162 | .393 | -.806 | -.715 | -.046 | -.146 | -.292 | -.639 | -.580 |
| .250 | -.016 | -.164 | -.301 | -.735 | -.687 | -.028 | -.094 | -.213 | -.566 | -.573 |
| .350 | -.073 | -.178 | -.262 | -.628 | -.667 | | | | | |
| .450 | -.105 | -.180 | -.235 | -.507 | -.637 | | | | | |
| .550 | -.105 | -.160 | -.193 | -.375 | -.594 | | | | | |
| .650 | -.080 | -.119 | -.129 | -.270 | -.543 | -.085 | -.074 | -.118 | -.388 | -.436 |
| .750 | -.039 | -.047 | -.064 | -.171 | -.486 | -.064 | -.042 | -.082 | -.356 | -.416 |
| .850 | .009 | .005 | .001 | .089 | .425 | -.032 | -.011 | -.073 | -.315 | -.391 |
| .900 | .036 | .028 | .028 | -.059 | -.386 | -.009 | .014 | -.060 | -.283 | -.379 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.868 | -.087 | .416 | .598 | .689 | -.630 | -.146 | .251 | .363 | .457 |
| .075 | -.507 | -.149 | .179 | .356 | .507 | -.407 | -.183 | .019 | .116 | .224 |
| .150 | -.356 | -.146 | .073 | .215 | .347 | -.283 | -.158 | -.055 | -.009 | .073 |
| .250 | -.299 | -.162 | -.010 | .105 | .210 | | | | | |
| .350 | -.263 | -.171 | -.069 | .020 | .107 | | | | | |
| .450 | -.222 | -.176 | -.093 | -.028 | .039 | | | | | |
| .550 | -.174 | -.153 | -.100 | -.059 | -.009 | | | | | |
| .650 | -.110 | -.106 | -.073 | -.043 | -.032 | -.053 | -.063 | -.073 | -.087 | -.110 |
| .750 | -.053 | -.031 | -.046 | -.025 | -.055 | -.085 | -.051 | -.071 | -.096 | -.153 |
| .850 | -.023 | .030 | .044 | .023 | -.059 | -.032 | .010 | -.010 | -.062 | -.142 |
| .900 | .057 | .060 | .060 | .030 | -.103 | -.028 | -.028 | -.006 | -.073 | -.174 |

TABLE III.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(b) $\alpha = 0^\circ$; $M = 0.80$.

| x C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .701 | .682 | .465 | .090 | -.399 | .412 | .771 | .483 | -.073 | -.642 |
| .025 | .328 | -.067 | -.633 | -1.441 | -1.116 | .371 | -.073 | -1.211 | -1.769 | -1.572 |
| .075 | .180 | -.096 | -.428 | -1.067 | -1.054 | .180 | -.131 | -.484 | -.830 | -.863 |
| .150 | .077 | -.132 | -.363 | -.703 | -.992 | .079 | -.141 | -.362 | -.801 | -.830 |
| .250 | .044 | -.102 | -.240 | -.320 | -.857 | .007 | -.156 | -.300 | -.437 | -.798 |
| .350 | -.002 | -.112 | -.193 | -.259 | -.687 | -.062 | -.173 | -.277 | -.352 | -.749 |
| .450 | -.048 | -.132 | -.179 | -.228 | -.511 | -.118 | -.203 | -.247 | -.298 | -.684 |
| .550 | -.065 | -.118 | -.143 | -.181 | -.373 | -.100 | -.161 | -.182 | -.222 | -.604 |
| .650 | -.041 | -.072 | -.087 | -.137 | -.313 | -.077 | -.115 | -.124 | -.145 | -.531 |
| .750 | -.025 | -.038 | -.036 | -.082 | -.181 | -.034 | -.047 | -.047 | -.065 | -.443 |
| .850 | .018 | .016 | .024 | -.009 | -.176 | .028 | .030 | .033 | .020 | -.364 |
| .900 | .044 | .052 | .060 | .026 | -.126 | .063 | .077 | .077 | .064 | -.302 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.513 | -.005 | .374 | .659 | .869 | -.1.216 | -.059 | .407 | .627 | .764 |
| .075 | -.459 | -.105 | .175 | .399 | .605 | -.481 | -.126 | .189 | .393 | .566 |
| .150 | -.343 | -.118 | .091 | .263 | .433 | -.363 | -.135 | .091 | .253 | .404 |
| .250 | -.236 | -.103 | .047 | .183 | .317 | -.287 | -.144 | .014 | .145 | .275 |
| .350 | -.203 | -.115 | -.004 | .097 | .207 | -.256 | -.155 | -.044 | .062 | .174 |
| .450 | -.170 | -.129 | -.045 | .037 | .119 | -.229 | -.174 | -.092 | .003 | .078 |
| .550 | -.126 | -.100 | -.045 | .015 | .077 | -.177 | -.152 | -.093 | -.029 | .024 |
| .650 | -.070 | -.055 | -.021 | .027 | .057 | -.106 | -.099 | -.063 | -.023 | -.001 |
| .750 | -.024 | -.023 | -.010 | .024 | .034 | -.028 | -.026 | -.009 | .006 | -.013 |
| .850 | .036 | .037 | .039 | .055 | .031 | .054 | .052 | .057 | .058 | -.017 |
| .900 | .063 | .065 | .054 | .062 | .016 | .074 | .077 | .075 | .067 | -.057 |
| $z/b_v = 0.66$ | | | | | | $z/b_v = 0.93$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .385 | .745 | .434 | -.058 | -.430 | .456 | .703 | .350 | -.033 | -.310 |
| .025 | .371 | -.111 | -.175 | -.131 | -.670 | .207 | -.221 | -.986 | -.729 | -.443 |
| .075 | .183 | -.149 | -.661 | -.081 | -.655 | .016 | -.200 | -.578 | -.717 | -.458 |
| .150 | .057 | -.168 | -.425 | -.970 | -.651 | -.073 | -.164 | -.320 | -.723 | -.483 |
| .250 | -.027 | -.182 | -.315 | -.794 | -.626 | -.034 | -.091 | -.225 | -.635 | -.495 |
| .350 | -.089 | -.194 | -.270 | -.627 | -.605 | | | | | |
| .450 | -.131 | -.203 | -.241 | -.470 | -.573 | | | | | |
| .550 | -.128 | -.171 | -.191 | -.336 | -.539 | | | | | |
| .650 | -.092 | -.120 | -.118 | -.221 | -.511 | -.079 | -.067 | -.109 | -.399 | -.407 |
| .750 | -.042 | -.026 | -.044 | -.126 | -.478 | -.047 | -.020 | -.071 | -.349 | -.390 |
| .850 | .021 | .030 | .027 | -.049 | -.434 | -.013 | .018 | -.054 | -.295 | -.366 |
| .900 | .039 | .051 | .059 | -.015 | -.419 | .005 | .043 | -.039 | -.263 | -.357 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.1.250 | -.066 | .413 | .607 | .717 | -.1.148 | -.156 | .243 | .396 | .499 |
| .075 | -.576 | -.144 | .190 | .378 | .525 | -.527 | -.206 | .002 | .125 | .254 |
| .150 | -.378 | -.140 | .082 | .234 | .374 | -.282 | -.167 | -.071 | -.026 | .080 |
| .250 | -.313 | -.168 | -.017 | .108 | .233 | | | | | |
| .350 | -.274 | -.193 | -.080 | .020 | .119 | | | | | |
| .450 | -.235 | -.190 | -.116 | -.046 | .031 | | | | | |
| .550 | -.187 | -.159 | -.115 | -.068 | -.026 | | | | | |
| .650 | -.115 | -.109 | -.077 | -.049 | -.051 | -.089 | -.062 | -.066 | -.082 | -.110 |
| .750 | -.041 | -.025 | -.029 | -.020 | -.075 | -.074 | -.026 | -.054 | -.090 | -.160 |
| .850 | .048 | .057 | .054 | .035 | -.081 | -.015 | .045 | .011 | -.040 | -.146 |
| .900 | .077 | .086 | .080 | .044 | -.120 | -.013 | .057 | .021 | -.055 | -.175 |

TABLE III.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(c) $\alpha = 0^\circ$; $M = 0.85$.

| x | C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|--------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | | |
| .000 | .742 | .688 | .528 | .217 | .237 | | .483 | .787 | .555 | .088 | .500 |
| .025 | .334 | -.061 | -.596 | -1.290 | -1.076 | | .369 | -.072 | -1.174 | -1.556 | .848 |
| .075 | .183 | -.093 | -.457 | -.980 | -.988 | | .183 | -.137 | -.393 | -.823 | .847 |
| .150 | .075 | -.140 | -.386 | -.844 | -.926 | | .078 | -.152 | -.360 | -1.273 | .815 |
| .250 | .044 | -.109 | -.252 | -.420 | -.833 | | -.002 | -.166 | -.312 | -.439 | .781 |
| .350 | -.007 | -.122 | -.208 | -.260 | -.707 | | -.077 | -.193 | -.293 | -.255 | .736 |
| .450 | -.062 | -.145 | -.192 | -.204 | -.565 | | -.134 | -.225 | -.263 | -.281 | .679 |
| .550 | -.077 | -.129 | -.154 | -.179 | -.436 | | -.124 | -.180 | -.198 | -.220 | .613 |
| .650 | -.050 | -.084 | -.092 | -.141 | -.362 | | -.099 | -.132 | -.126 | -.149 | .547 |
| .750 | -.039 | -.049 | -.042 | -.081 | -.296 | | -.052 | -.057 | -.057 | -.069 | .460 |
| .850 | .010 | .014 | .026 | .010 | .207 | | .027 | .030 | .038 | .025 | .387 |
| .900 | .039 | .054 | .063 | .033 | -.154 | | .068 | .075 | .080 | .068 | .330 |
| <i>Right side</i> | | | | | | | | | | | |
| .025 | -.485 | -.001 | .374 | .659 | .873 | | -1.154 | -.058 | .401 | .624 | .769 |
| .075 | -.498 | -.105 | .173 | .404 | .608 | | -.427 | -.129 | .186 | .388 | .567 |
| .150 | -.370 | -.123 | .088 | .263 | .439 | | -.369 | -.145 | .083 | .246 | .405 |
| .250 | -.256 | -.109 | .043 | .177 | .318 | | -.302 | -.157 | .003 | .139 | .274 |
| .350 | -.217 | -.126 | -.015 | .094 | .210 | | -.272 | -.174 | -.059 | .057 | .176 |
| .450 | -.188 | -.140 | -.062 | .025 | .116 | | -.241 | -.193 | -.108 | -.016 | .074 |
| .550 | -.130 | -.109 | -.064 | .005 | .068 | | -.185 | -.163 | -.111 | -.048 | .017 |
| .650 | -.074 | -.064 | -.035 | .015 | .047 | | -.111 | -.106 | -.075 | -.038 | -.016 |
| .750 | -.032 | -.037 | -.021 | .013 | .014 | | -.032 | -.032 | -.025 | -.002 | -.027 |
| .850 | .044 | .038 | .033 | .047 | .010 | | .057 | .053 | .053 | .056 | -.037 |
| .900 | .071 | .060 | .052 | .053 | -.009 | | .084 | .077 | .069 | .061 | -.074 |
| $z/b_v = 0.66$ | | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | | |
| .000 | .443 | .759 | .501 | .064 | -.333 | | .483 | .711 | .403 | .004 | -.279 |
| .025 | .371 | -.113 | -1.253 | -1.599 | -.692 | | .196 | -.254 | -1.108 | -.864 | -.467 |
| .075 | .183 | -.160 | -.988 | -1.436 | -.689 | | -.010 | -.240 | -.654 | -.814 | -.474 |
| .150 | .055 | -.187 | -.403 | -1.076 | -.695 | | -.101 | -.188 | -.340 | -.813 | -.500 |
| .250 | -.040 | -.203 | -.318 | -.757 | -.665 | | -.050 | -.112 | -.225 | -.689 | -.518 |
| .350 | -.108 | -.218 | -.279 | -.606 | -.631 | | | | | | |
| .450 | -.151 | -.227 | -.255 | -.436 | -.589 | | | | | | |
| .550 | -.148 | -.196 | -.205 | -.283 | -.557 | | | | | | |
| .650 | -.110 | -.137 | -.129 | -.162 | -.525 | | | | | | |
| .750 | -.053 | -.031 | -.047 | -.071 | -.490 | | | | | | |
| .850 | .024 | .027 | .026 | -.002 | -.444 | | | | | | |
| .900 | .042 | .058 | .056 | .025 | -.424 | | | | | | |
| <i>Right side</i> | | | | | | | | | | | |
| .025 | -1.272 | -.074 | .403 | .604 | .719 | | -1.237 | -.177 | .223 | .394 | .507 |
| .075 | -.968 | -.156 | .173 | .369 | .526 | | -.770 | -.248 | -.039 | .113 | .257 |
| .150 | -.357 | -.154 | .072 | .227 | .371 | | -.244 | -.186 | -.108 | -.052 | .069 |
| .250 | -.313 | -.191 | -.032 | .103 | .224 | | | | | | |
| .350 | -.282 | -.218 | -.105 | .004 | .103 | | | | | | |
| .450 | -.248 | -.211 | -.145 | -.068 | .012 | | | | | | |
| .550 | -.191 | -.180 | -.141 | -.088 | -.046 | | | | | | |
| .650 | -.114 | -.116 | -.095 | -.065 | -.074 | | | | | | |
| .750 | -.040 | .038 | -.044 | -.032 | -.094 | | | | | | |
| .850 | .052 | .057 | .052 | .035 | -.094 | | | | | | |
| .900 | .085 | .082 | .078 | .051 | -.128 | | | | | | |

TABLE III.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(d) $\alpha = 0^\circ$; $M = 0.90$.

| x C_v | C_p for - | | | | | C_p for - | | | | |
|----------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| Left side | | | | | | | | | | |
| .000 | .773 | .700 | .586 | .342 | -.084 | .546 | .796 | .625 | .233 | -.347 |
| .025 | .340 | -.047 | -.520 | -1.149 | -1.034 | .372 | -.067 | -1.037 | -1.151 | -1.130 |
| .075 | .198 | -.088 | -.449 | -.873 | -.908 | .187 | -.141 | -.406 | -.487 | -.584 |
| .150 | .084 | -.144 | -.425 | -.806 | -.844 | .083 | -.160 | -.429 | -.182 | -.753 |
| .250 | .048 | -.120 | -.282 | -.650 | -.771 | .002 | -.183 | -.322 | -.1065 | -.738 |
| .350 | -.006 | -.137 | -.223 | -.376 | -.673 | -.079 | -.219 | -.341 | -.455 | -.702 |
| .450 | -.071 | -.165 | -.215 | -.259 | -.578 | -.156 | -.271 | -.275 | -.221 | -.646 |
| .550 | -.091 | -.156 | -.159 | -.165 | -.475 | -.144 | -.216 | -.194 | -.147 | -.593 |
| .650 | -.063 | -.103 | -.095 | -.119 | -.404 | -.117 | -.149 | -.124 | -.100 | -.536 |
| .750 | -.049 | -.064 | -.040 | -.063 | -.339 | -.055 | -.063 | -.044 | -.039 | -.464 |
| .850 | .004 | .004 | .028 | -.001 | -.239 | .026 | .032 | .046 | .042 | -.400 |
| .900 | .038 | .050 | .068 | .035 | -.183 | .075 | .080 | .092 | .084 | -.348 |
| Right side | | | | | | | | | | |
| .025 | -.425 | .005 | .377 | .662 | .882 | -1.035 | -.064 | .392 | .623 | .782 |
| .075 | -.488 | -.108 | .179 | .409 | .622 | -.835 | -.141 | .181 | .390 | .577 |
| .150 | -.418 | -.131 | .087 | .271 | .459 | -.408 | -.155 | .076 | .249 | .416 |
| .250 | -.278 | -.123 | .036 | .187 | .337 | -.310 | -.173 | -.004 | .143 | .287 |
| .350 | -.232 | -.145 | -.022 | .097 | .219 | -.298 | -.201 | -.073 | .047 | .185 |
| .450 | -.195 | -.161 | -.071 | .023 | .124 | -.236 | -.232 | -.131 | -.033 | .076 |
| .550 | -.128 | -.131 | -.080 | -.001 | .069 | -.179 | -.195 | -.141 | -.064 | .015 |
| .650 | -.067 | -.077 | -.047 | .008 | .049 | -.103 | -.125 | -.100 | -.052 | -.020 |
| .750 | -.020 | -.045 | -.039 | -.001 | .009 | -.016 | -.039 | -.037 | -.012 | -.037 |
| .850 | .047 | .028 | .026 | .045 | -.005 | .068 | .050 | .050 | .051 | -.049 |
| .900 | .079 | .057 | .042 | .051 | -.032 | .097 | .080 | .068 | .061 | -.086 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| Left side | | | | | | | | | | |
| .000 | .503 | .769 | .574 | .203 | -.219 | .523 | .712 | .474 | .103 | -.211 |
| .025 | .371 | -.104 | -1.133 | -1.454 | -.678 | .182 | -.276 | -1.073 | -1.185 | -.447 |
| .075 | .181 | -.165 | -.976 | -1.321 | -.686 | -.029 | .325 | -1.037 | -1.053 | -.460 |
| .150 | .051 | -.208 | -.795 | -1.236 | -.698 | -.175 | -.215 | -.572 | -.996 | -.487 |
| .250 | -.044 | -.239 | -.369 | -.1068 | -.659 | -.071 | -.117 | -.155 | -.880 | -.501 |
| .350 | -.129 | -.265 | -.226 | -.708 | -.622 | | | | | |
| .450 | -.182 | -.264 | -.234 | -.455 | -.584 | | | | | |
| .550 | -.178 | -.229 | -.207 | -.232 | -.549 | | | | | |
| .650 | -.123 | -.165 | -.127 | -.098 | -.525 | -.087 | -.076 | -.117 | -.467 | -.435 |
| .750 | -.060 | -.023 | -.039 | -.028 | -.493 | -.039 | -.019 | -.077 | -.403 | -.420 |
| .850 | .031 | .032 | .038 | .033 | -.451 | .002 | .028 | -.061 | -.398 | -.396 |
| .900 | .054 | .062 | .066 | .053 | -.428 | .020 | .053 | -.044 | -.305 | -.383 |
| Right side | | | | | | | | | | |
| .025 | -.1.151 | -.077 | .391 | .596 | .731 | -1.162 | -.203 | .203 | .390 | .517 |
| .075 | -.969 | -.168 | .166 | .363 | .536 | -1.049 | -.346 | -.069 | .104 | .270 |
| .150 | -.663 | -.169 | .062 | .224 | .382 | -.448 | -.216 | -.194 | -.094 | .071 |
| .250 | -.350 | -.221 | -.052 | .094 | .238 | | | | | |
| .350 | -.234 | -.268 | -.137 | -.020 | .117 | | | | | |
| .450 | -.223 | -.253 | -.186 | -.099 | .017 | | | | | |
| .550 | -.183 | -.208 | -.172 | -.126 | -.054 | | | | | |
| .650 | -.108 | -.128 | -.117 | -.090 | -.080 | -.087 | -.073 | -.083 | -.108 | -.134 |
| .750 | -.024 | -.037 | -.053 | -.044 | -.102 | -.079 | -.028 | -.060 | -.096 | -.186 |
| .850 | .068 | .062 | .059 | .039 | -.090 | -.020 | .052 | .023 | -.031 | -.156 |
| .900 | .101 | .094 | .079 | .058 | -.128 | -.014 | .069 | .031 | -.041 | -.185 |

TABLE III.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued
(e) $\alpha = 0^\circ$; $M = 0.92$.

| X C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .785 | .690 | .604 | .383 | -.063 | .569 | .799 | .648 | .283 | -.327 |
| .025 | .331 | -.044 | -.491 | -.098 | -1.057 | .361 | -.070 | -.970 | -1.315 | -.763 |
| .075 | .190 | -.087 | -.442 | -.830 | -.928 | .176 | -.144 | -.775 | -1.075 | -.784 |
| .150 | .076 | -.152 | -.429 | -.775 | -.860 | .073 | -.169 | -.444 | -1.124 | -.767 |
| .250 | .036 | -.127 | -.342 | -.683 | -.787 | -.015 | -.188 | -.379 | -1.041 | -.754 |
| .350 | -.024 | -.147 | -.247 | -.436 | -.688 | -.102 | -.236 | -.361 | -.654 | -.716 |
| .450 | -.092 | -.187 | -.238 | -.343 | -.598 | -.192 | -.300 | -.361 | -.427 | -.668 |
| .550 | -.122 | -.190 | -.182 | -.218 | -.500 | -.190 | -.255 | -.175 | -.140 | -.611 |
| .650 | -.089 | -.122 | -.095 | -.128 | -.425 | -.152 | -.173 | -.112 | -.070 | -.557 |
| .750 | -.072 | -.075 | -.040 | -.061 | -.360 | -.072 | -.063 | -.046 | -.018 | -.484 |
| .850 | -.016 | -.002 | .025 | .002 | -.273 | .015 | .030 | .046 | .055 | -.425 |
| .900 | .023 | .043 | .064 | .044 | -.212 | .067 | .081 | .093 | .093 | -.368 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.399 | .008 | .372 | .657 | .886 | -.946 | -.069 | .383 | .620 | .784 |
| .075 | -.480 | -.113 | .175 | .409 | .623 | -.806 | -.152 | .172 | .387 | .578 |
| .150 | -.447 | -.138 | .085 | .269 | .457 | -.490 | -.166 | .068 | .248 | .418 |
| .250 | -.339 | -.132 | .037 | .183 | .336 | -.344 | -.187 | .017 | .192 | .282 |
| .350 | -.266 | -.158 | -.036 | .085 | .213 | -.349 | -.221 | -.085 | .040 | .173 |
| .450 | -.226 | -.182 | -.087 | .009 | .113 | -.306 | -.274 | .153 | -.042 | .066 |
| .550 | -.147 | -.157 | -.100 | -.020 | .062 | -.168 | -.229 | -.175 | -.087 | .000 |
| .650 | -.070 | -.089 | -.066 | -.007 | .039 | -.101 | -.136 | -.127 | -.078 | -.035 |
| .750 | -.031 | -.054 | -.058 | -.016 | -.004 | -.019 | -.040 | -.050 | -.033 | -.055 |
| .850 | .043 | .021 | .008 | .028 | -.026 | .062 | .048 | .041 | .042 | -.066 |
| .900 | .071 | .052 | .030 | .043 | -.055 | .091 | .078 | .061 | .057 | -.110 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .528 | .769 | .597 | .249 | -.208 | .536 | .712 | .498 | .150 | -.218 |
| .025 | .345 | -.109 | -1.063 | -1.376 | -.692 | .160 | -.282 | -1.013 | -1.327 | -.473 |
| .075 | .164 | -.169 | -.926 | -.246 | -.700 | -.046 | -.309 | -.992 | -1.108 | -.478 |
| .150 | .036 | -.213 | -.827 | -.187 | -.710 | -.229 | -.282 | -.832 | -1.024 | -.506 |
| .250 | -.065 | -.255 | -.399 | -.128 | -.692 | -.142 | -.136 | -.414 | -.947 | -.522 |
| .350 | -.168 | -.310 | -.412 | -.020 | -.647 | | | | | |
| .450 | -.241 | -.317 | -.178 | -.529 | -.601 | | | | | |
| .550 | -.229 | -.261 | -.171 | -.287 | -.573 | | | | | |
| .650 | -.156 | -.167 | -.115 | -.081 | -.554 | -.100 | -.075 | -.115 | -.560 | -.461 |
| .750 | -.050 | -.030 | -.039 | .010 | -.523 | -.046 | -.023 | -.084 | -.461 | -.442 |
| .850 | .022 | .028 | .038 | .060 | -.478 | -.010 | .029 | -.067 | -.373 | -.420 |
| .900 | .045 | .063 | .071 | .080 | -.461 | .019 | .052 | -.048 | -.326 | -.408 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.065 | -.083 | .379 | .591 | .729 | -1.089 | -.209 | .197 | .391 | .520 |
| .075 | -.916 | -.180 | .158 | .362 | .530 | -1.008 | -.375 | -.079 | .101 | .264 |
| .150 | -.777 | -.183 | .051 | .223 | .379 | -.819 | -.275 | -.235 | -.105 | .059 |
| .250 | -.380 | -.242 | -.062 | .086 | .232 | | | | | |
| .350 | -.401 | -.320 | -.164 | -.029 | .104 | | | | | |
| .450 | -.168 | -.294 | -.236 | -.112 | .000 | | | | | |
| .550 | -.168 | -.229 | -.216 | -.151 | -.074 | | | | | |
| .650 | -.110 | -.126 | -.144 | -.109 | -.103 | -.106 | -.076 | -.082 | -.109 | -.160 |
| .750 | -.032 | -.035 | -.046 | -.057 | -.133 | -.093 | -.031 | -.057 | -.099 | -.210 |
| .850 | .065 | .063 | .056 | .043 | -.111 | -.029 | .052 | .021 | -.028 | -.178 |
| .900 | .096 | .098 | .081 | .066 | -.148 | -.020 | .069 | .032 | -.033 | -.207 |

TABLE III.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(f) $\alpha = 9.4^\circ$; $M = 0.60$.

| $\frac{C_p}{C_v}$ | C_p for - | | | | | C_p for - | | | | | | |
|-------------------|----------------------|-------|-------------------|---------------------|---------------------|----------------------|----------------------|--------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | .385 | .806 | -.650 | -1.449 | .002 | .661 | -1.036 | -1.512 | | | | |
| .025 | | -.130 | -.972 | -2.578 | .349 | -.109 | -1.368 | -1.289 | | | | |
| .075 | .037 | -.127 | -.622 | -1.446 | .169 | -.143 | -1.318 | -1.273 | | | | |
| .150 | .021 | -.155 | -.472 | -.695 | .068 | -.150 | -1.159 | -1.285 | | | | |
| .250 | .009 | -.114 | -.325 | -.501 | -.002 | -.162 | -.384 | -1.253 | | | | |
| .350 | -.025 | -.118 | -.270 | -.433 | -.059 | -.184 | -.288 | -.959 | | | | |
| .450 | -.057 | -.139 | -.241 | -.346 | -.100 | -.205 | -.295 | -.631 | | | | |
| .550 | -.073 | -.150 | -.218 | -.280 | -.096 | -.178 | -.245 | -.442 | | | | |
| .650 | -.068 | -.123 | -.186 | -.239 | -.084 | -.141 | -.193 | -.346 | | | | |
| .750 | -.055 | -.105 | -.138 | -.196 | -.055 | -.091 | -.120 | -.269 | | | | |
| .850 | -.016 | -.043 | -.061 | -.114 | -.002 | -.018 | -.036 | -.173 | | | | |
| .900 | .011 | -.014 | -.027 | -.059 | .025 | -.016 | .007 | -.118 | | | | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | -.155 | -.057 | .589 | .870 | -.761 | -.068 | .589 | .677 | | | | |
| .075 | -.319 | -.132 | .373 | .590 | -.483 | -.125 | .378 | .535 | | | | |
| .150 | -.305 | -.134 | .259 | .426 | -.364 | -.137 | .239 | .390 | | | | |
| .250 | -.225 | -.109 | .187 | .317 | -.287 | -.146 | .137 | .269 | | | | |
| .350 | -.209 | -.114 | .109 | .214 | -.255 | -.164 | .064 | .180 | | | | |
| .450 | -.203 | -.137 | .041 | .135 | -.241 | -.178 | .003 | .098 | | | | |
| .550 | -.173 | -.132 | .016 | .096 | -.200 | -.164 | -.022 | .048 | | | | |
| .650 | -.127 | -.107 | .005 | .078 | -.146 | -.125 | -.022 | .025 | | | | |
| .750 | -.096 | -.084 | .000 | .062 | -.077 | -.066 | .000 | .023 | | | | |
| .850 | -.023 | -.018 | .037 | .075 | -.002 | -.005 | .037 | .039 | | | | |
| .900 | .007 | .005 | .050 | .071 | .030 | .027 | .041 | .018 | | | | |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | -.039 | .613 | -.732 | -1.141 | .137 | .549 | -.434 | -.822 | | | | |
| .025 | .335 | -.155 | -.072 | -.856 | .176 | -.241 | -.632 | -.601 | | | | |
| .075 | .155 | -.171 | -.045 | -.840 | -.009 | -.205 | -.629 | -.606 | | | | |
| .150 | .043 | -.182 | -.000 | -.818 | -.100 | -.182 | -.602 | -.615 | | | | |
| .250 | -.030 | -.184 | -.904 | -.790 | -.077 | -.116 | -.536 | -.601 | | | | |
| .350 | -.084 | -.196 | -.702 | -.786 | | | | | | | | |
| .450 | -.118 | -.203 | -.488 | -.761 | | | | | | | | |
| .550 | -.134 | -.187 | -.325 | -.706 | | | | | | | | |
| .650 | -.100 | -.141 | -.213 | -.629 | -.102 | -.082 | -.379 | -.487 | | | | |
| .750 | -.055 | -.077 | -.129 | -.544 | -.075 | -.041 | -.338 | -.465 | | | | |
| .850 | -.014 | -.023 | -.068 | -.465 | -.052 | -.011 | -.309 | -.437 | | | | |
| .900 | .000 | .000 | -.038 | -.426 | -.027 | -.002 | -.268 | -.412 | | | | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | -.998 | -.086 | .548 | .611 | -.717 | -.159 | .318 | .371 | | | | |
| .075 | -.537 | -.146 | .353 | .476 | -.435 | -.198 | .087 | .178 | | | | |
| .150 | -.371 | -.153 | .214 | .340 | -.291 | -.178 | -.057 | .005 | | | | |
| .250 | -.317 | -.173 | .103 | .214 | | | | | | | | |
| .350 | -.285 | -.182 | .021 | .112 | | | | | | | | |
| .450 | -.241 | -.182 | -.022 | .041 | | | | | | | | |
| .550 | -.203 | -.164 | -.057 | -.007 | | | | | | | | |
| .650 | -.146 | -.125 | -.047 | -.030 | -.107 | -.075 | -.116 | -.157 | | | | |
| .750 | -.084 | -.064 | -.029 | -.057 | -.091 | -.059 | -.127 | -.194 | | | | |
| .850 | -.004 | .002 | .018 | -.055 | -.032 | -.007 | -.088 | -.184 | | | | |
| .900 | .037 | .032 | .030 | -.082 | -.016 | -.025 | -.097 | -.209 | | | | |

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TABLE III. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(g) $\alpha = 9.6^\circ$; $M = 0.80$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | | C_p for - | | | | | | | | | | | | | | | | |
|-----------------|----------------------|-------|-------------------|-------|---------------------|----------------|---------------------|-------|----------------------|--------|----------------------|--|-------------------|--|---------------------|----------------|---------------------|--|----------------------|--|--|--|--|--|--|--|--|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | | $\beta = 7.9^\circ$ | | $\beta = 12.7^\circ$ | | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | | $\beta = 7.9^\circ$ | | $\beta = 12.7^\circ$ | | | | | | | | |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | | | | | | | | |
| Left side | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .000 | .350 | .856 | .414 | -.228 | -.308 | | .284 | .689 | .329 | -.357 | | | | | | | | | | | | | | | | | |
| .025 | | -.113 | -.153 | -.745 | -1.646 | | .341 | -.109 | -1.110 | -1.477 | -1.059 | | | | | | | | | | | | | | | | |
| .075 | .019 | -.127 | -.330 | -.599 | -1.326 | | .161 | -.154 | -.554 | -1.419 | -1.026 | | | | | | | | | | | | | | | | |
| .150 | .003 | -.162 | -.369 | -.545 | -.834 | | .069 | -.157 | -.387 | -1.194 | -.981 | | | | | | | | | | | | | | | | |
| .250 | -.004 | -.115 | -.256 | -.371 | -.557 | | -.001 | -.168 | -.320 | -.259 | -.941 | | | | | | | | | | | | | | | | |
| .350 | -.041 | -.124 | -.224 | -.293 | -.474 | | -.071 | -.197 | -.305 | -.325 | -.854 | | | | | | | | | | | | | | | | |
| .450 | -.073 | -.151 | -.221 | -.262 | -.365 | | -.121 | -.231 | -.282 | -.326 | -.715 | | | | | | | | | | | | | | | | |
| .550 | -.091 | -.163 | -.208 | -.240 | -.335 | | -.121 | -.206 | -.230 | -.280 | -.592 | | | | | | | | | | | | | | | | |
| .650 | -.079 | -.139 | -.163 | -.219 | -.318 | | -.111 | -.163 | -.171 | -.225 | -.498 | | | | | | | | | | | | | | | | |
| .750 | -.074 | -.124 | -.127 | -.160 | -.294 | | -.071 | -.106 | -.102 | -.150 | -.407 | | | | | | | | | | | | | | | | |
| .850 | -.027 | -.061 | -.054 | -.082 | -.191 | | -.003 | -.020 | -.011 | -.057 | -.303 | | | | | | | | | | | | | | | | |
| .900 | -.005 | -.008 | -.006 | -.033 | -.131 | | .031 | .030 | .035 | -.006 | -.238 | | | | | | | | | | | | | | | | |
| Right side | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .025 | -.077 | -.020 | -.041 | .524 | .836 | | -.1.214 | -.056 | .388 | .583 | .697 | | | | | | | | | | | | | | | | |
| .075 | -.339 | -.130 | .027 | .361 | .590 | | -.500 | -.120 | .178 | .374 | .540 | | | | | | | | | | | | | | | | |
| .150 | -.348 | -.141 | .023 | .257 | .437 | | -.386 | -.135 | .082 | .247 | .400 | | | | | | | | | | | | | | | | |
| .250 | -.261 | -.109 | .001 | .195 | .329 | | -.314 | -.150 | .015 | .146 | .281 | | | | | | | | | | | | | | | | |
| .350 | -.237 | -.123 | -.031 | .112 | .230 | | -.282 | -.172 | -.043 | .069 | .190 | | | | | | | | | | | | | | | | |
| .450 | -.220 | -.144 | -.060 | .046 | .145 | | -.266 | -.201 | -.090 | -.003 | .096 | | | | | | | | | | | | | | | | |
| .550 | -.185 | -.138 | -.069 | .014 | .096 | | -.219 | -.184 | -.108 | -.040 | .042 | | | | | | | | | | | | | | | | |
| .650 | -.144 | -.113 | -.060 | -.004 | -.066 | | -.155 | -.139 | -.084 | -.039 | .012 | | | | | | | | | | | | | | | | |
| .750 | -.111 | -.100 | -.047 | -.008 | -.036 | | -.077 | -.071 | -.040 | -.014 | .001 | | | | | | | | | | | | | | | | |
| .850 | -.030 | -.023 | -.004 | -.027 | -.040 | | -.012 | -.012 | -.029 | -.029 | .000 | | | | | | | | | | | | | | | | |
| .900 | -.005 | -.004 | -.024 | -.040 | -.028 | | -.041 | -.036 | -.042 | -.032 | -.026 | | | | | | | | | | | | | | | | |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | | | | | | | | | | | | | | | | | | |
| Left side | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .000 | .205 | .634 | .212 | -.320 | -.808 | | .253 | .562 | .123 | -.253 | -.669 | | | | | | | | | | | | | | | | |
| .025 | -.330 | -.151 | -.120 | -.928 | -.746 | | .154 | -.295 | -.807 | -.596 | -.541 | | | | | | | | | | | | | | | | |
| .075 | .157 | -.177 | -.735 | -.890 | -.727 | | -.035 | -.254 | -.691 | -.585 | -.541 | | | | | | | | | | | | | | | | |
| .150 | .038 | -.197 | -.451 | -.857 | -.705 | | -.140 | -.209 | -.439 | -.590 | -.547 | | | | | | | | | | | | | | | | |
| .250 | -.039 | -.203 | -.343 | -.842 | -.681 | | -.088 | -.127 | -.272 | -.542 | -.550 | | | | | | | | | | | | | | | | |
| .350 | -.103 | -.221 | -.301 | -.774 | -.665 | | | | | | | | | | | | | | | | | | | | | | |
| .450 | -.149 | -.233 | -.272 | -.626 | -.645 | | | | | | | | | | | | | | | | | | | | | | |
| .550 | -.158 | -.213 | -.227 | -.465 | -.615 | | | | | | | | | | | | | | | | | | | | | | |
| .650 | -.120 | -.148 | -.156 | -.326 | -.583 | | -.105 | -.071 | -.130 | -.359 | -.480 | | | | | | | | | | | | | | | | |
| .750 | -.065 | -.073 | -.076 | -.208 | -.545 | | -.068 | -.027 | -.096 | -.331 | -.457 | | | | | | | | | | | | | | | | |
| .850 | -.010 | -.008 | -.009 | -.113 | -.498 | | -.030 | -.015 | -.060 | -.302 | -.433 | | | | | | | | | | | | | | | | |
| .900 | -.011 | -.025 | -.024 | -.074 | -.483 | | -.009 | -.038 | -.032 | -.283 | -.418 | | | | | | | | | | | | | | | | |
| Right side | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .025 | -.150 | -.073 | .378 | .552 | .627 | | -.980 | -.177 | .193 | .327 | .407 | | | | | | | | | | | | | | | | |
| .075 | -.661 | -.145 | .166 | .352 | .490 | | -.585 | -.242 | -.044 | .084 | .207 | | | | | | | | | | | | | | | | |
| .150 | -.404 | -.153 | .067 | .220 | .357 | | -.313 | -.203 | -.145 | -.071 | .016 | | | | | | | | | | | | | | | | |
| .250 | -.333 | -.189 | -.028 | .103 | .228 | | | | | | | | | | | | | | | | | | | | | | |
| .350 | -.298 | -.212 | -.090 | .014 | .118 | | | | | | | | | | | | | | | | | | | | | | |
| .450 | -.258 | -.216 | -.128 | -.051 | .033 | | | | | | | | | | | | | | | | | | | | | | |
| .550 | -.203 | -.188 | -.134 | -.080 | -.025 | | | | | | | | | | | | | | | | | | | | | | |
| .650 | -.143 | -.139 | -.101 | -.071 | -.055 | | -.108 | -.067 | -.089 | -.125 | -.171 | | | | | | | | | | | | | | | | |
| .750 | -.068 | -.064 | -.052 | -.050 | -.081 | | -.082 | -.038 | -.072 | -.140 | -.220 | | | | | | | | | | | | | | | | |
| .850 | -.023 | -.027 | -.026 | -.004 | -.084 | | -.009 | -.036 | -.003 | -.103 | -.214 | | | | | | | | | | | | | | | | |
| .900 | -.055 | -.054 | -.047 | -.018 | -.123 | | -.006 | -.050 | -.007 | -.117 | -.233 | | | | | | | | | | | | | | | | |

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TABLE III. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(h) $\alpha = 9.7^\circ$; $M = 0.85$.

| $\frac{X}{C_V}$ | C_p for - | | | | | C_p for - | | | | |
|-----------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_V = 0.11$ | | | | | $Z/b_V = 0.38$ | | | | |
| Left side | | | | | | | | | | |
| .000 | .311 | .877 | .390 | -.245 | -.143 | .349 | .702 | .417 | -.180 | -.861 |
| .025 | -.106 | -.112 | -.633 | -1.521 | .335 | -.107 | -1.227 | -1.658 | -1.011 | |
| .075 | .013 | -.124 | -.323 | -.587 | -1.248 | .157 | -.155 | -.503 | -1.315 | .984 |
| .150 | .000 | -.172 | -.418 | -.609 | -.831 | .063 | -.163 | -.401 | -.856 | .936 |
| .250 | -.016 | -.126 | -.282 | -.447 | -.574 | -.013 | -.178 | -.350 | -.580 | .900 |
| .350 | -.050 | -.130 | -.249 | -.345 | -.480 | -.088 | -.215 | -.336 | -.457 | .833 |
| .450 | -.081 | -.164 | -.247 | -.298 | -.394 | -.142 | -.254 | -.309 | -.395 | .716 |
| .550 | -.103 | -.184 | -.230 | -.266 | -.356 | -.148 | -.225 | -.257 | -.321 | .613 |
| .650 | -.098 | -.160 | -.188 | -.254 | -.346 | -.135 | -.181 | -.194 | -.248 | .530 |
| .750 | -.096 | -.140 | -.150 | -.177 | -.348 | -.096 | -.117 | -.116 | -.159 | .440 |
| .850 | -.046 | -.069 | -.072 | -.095 | -.230 | -.018 | -.020 | -.021 | -.062 | .347 |
| .900 | -.008 | -.013 | -.020 | -.049 | -.160 | .025 | -.028 | -.031 | -.011 | -.281 |
| Right side | | | | | | | | | | |
| .025 | -.049 | -.016 | -.066 | .465 | .826 | -1.182 | -.076 | .375 | .569 | .706 |
| .075 | -.341 | -.136 | -.013 | .333 | .593 | -.475 | -.133 | .168 | .361 | .546 |
| .150 | -.386 | -.150 | -.007 | .247 | .442 | -.401 | -.150 | .070 | .231 | .404 |
| .250 | -.285 | -.118 | -.014 | .179 | .333 | -.340 | -.164 | -.001 | .135 | .284 |
| .350 | -.261 | -.136 | -.048 | .098 | .232 | -.313 | -.191 | -.057 | .051 | .193 |
| .450 | -.245 | -.158 | -.076 | .031 | .143 | -.290 | -.221 | -.108 | -.028 | .099 |
| .550 | -.204 | -.154 | -.089 | -.001 | .093 | -.242 | -.204 | -.133 | -.066 | .036 |
| .650 | -.165 | -.126 | -.081 | -.014 | .063 | -.175 | -.158 | -.113 | -.069 | -.001 |
| .750 | -.129 | -.113 | -.071 | -.033 | .026 | -.088 | -.086 | -.058 | -.041 | -.011 |
| .850 | -.045 | -.033 | -.015 | .011 | .024 | -.004 | -.011 | -.016 | -.011 | -.017 |
| .900 | -.005 | .001 | .010 | .018 | .012 | .038 | .035 | .029 | .011 | -.051 |
| $Z/b_V = 0.66$ | | | | | $Z/b_V = 0.93$ | | | | | |
| Left side | | | | | | | | | | |
| .000 | .256 | .644 | .291 | -.254 | -.726 | .272 | .561 | .152 | -.332 | -.646 |
| .025 | .322 | -.153 | -1.326 | -1.438 | -.764 | .141 | -.289 | -1.218 | -.824 | -.544 |
| .075 | .152 | -.184 | -.815 | -1.315 | -.733 | -.058 | -.303 | -.779 | -.803 | -.541 |
| .150 | .028 | -.207 | -.498 | -1.137 | -.701 | -.185 | -.231 | -.444 | -.788 | -.547 |
| .250 | -.056 | -.221 | -.380 | -.876 | -.680 | -.108 | -.150 | -.255 | -.694 | -.557 |
| .350 | -.125 | -.246 | -.315 | -.716 | -.664 | | | | | |
| .450 | -.177 | -.258 | -.292 | -.500 | -.644 | | | | | |
| .550 | -.189 | -.239 | -.249 | -.335 | -.616 | | | | | |
| .650 | -.145 | -.167 | -.170 | -.215 | -.588 | -.119 | -.080 | -.137 | -.421 | -.493 |
| .750 | -.082 | -.077 | -.086 | -.121 | -.553 | -.076 | -.035 | -.098 | -.367 | -.473 |
| .850 | -.019 | -.012 | -.013 | -.052 | -.510 | -.033 | -.012 | -.059 | -.313 | -.448 |
| .900 | .011 | 1.098 | .029 | -.020 | -.496 | -.008 | -.034 | -.031 | -.285 | -.434 |
| Right side | | | | | | | | | | |
| .025 | -.350 | -.093 | .362 | .536 | .637 | -1.320 | -.215 | .180 | .328 | .417 |
| .075 | -.629 | -.167 | .155 | .338 | .492 | -.702 | -.291 | -.074 | .073 | .219 |
| .150 | -.430 | -.170 | .058 | .208 | .359 | -.338 | -.228 | -.193 | -.122 | .014 |
| .250 | -.371 | -.212 | -.042 | .085 | .230 | | | | | |
| .350 | -.323 | -.238 | -.118 | -.011 | .117 | | | | | |
| .450 | -.281 | -.244 | -.162 | -.083 | .029 | | | | | |
| .550 | -.232 | -.215 | -.162 | -.117 | -.040 | | | | | |
| .650 | -.155 | -.158 | -.125 | -.105 | -.068 | -.111 | -.084 | -.099 | -.156 | -.198 |
| .750 | -.072 | -.070 | -.068 | -.073 | -.097 | -.091 | -.040 | -.086 | -.151 | -.237 |
| .850 | .018 | .025 | .019 | -.005 | -.098 | -.022 | .037 | -.008 | -.096 | -.227 |
| .900 | .054 | .055 | .047 | .008 | -.140 | .000 | .052 | .007 | -.107 | -.253 |

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TABLE III. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(1) $\alpha = 9.7^\circ$; $M = 0.90$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | | C_p for - | | | | | C_p for - | | | | | | | | | | | | | | | |
|-----------------|----------------------|-------|-------------------|--------|---------------------|----------------|---------------------|--|----------------------|--|----------------------|-------|-------------------|--------|---------------------|----------------|---------------------|--|----------------------|--|--|--|--|--|--|--|--|--|--|--|--|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | | $\beta = 7.9^\circ$ | | $\beta = 12.7^\circ$ | | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | | $\beta = 7.9^\circ$ | | $\beta = 12.7^\circ$ | | | | | | | | | | | | |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | | | | | | | | | | | | |
| Left side | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .000 | .281 | .895 | .394 | -.229 | | | | | | | .417 | .704 | .489 | .016 | | | | | | | | | | | | | | | | | |
| .025 | -.105 | -.039 | -.464 | | | | | | | | .321 | -.109 | -1.078 | -1.413 | | | | | | | | | | | | | | | | | |
| .075 | .014 | -.126 | -.258 | -.458 | | | | | | | .147 | -.167 | -.642 | -1.275 | | | | | | | | | | | | | | | | | |
| .150 | .001 | -.193 | -.421 | -.547 | | | | | | | .054 | -.177 | -.506 | -.796 | | | | | | | | | | | | | | | | | |
| .250 | -.013 | -.142 | -.318 | -.499 | | | | | | | -.021 | -.195 | -.357 | -.686 | | | | | | | | | | | | | | | | | |
| .350 | -.049 | -.149 | -.265 | -.414 | | | | | | | -.096 | -.237 | -.363 | -.537 | | | | | | | | | | | | | | | | | |
| .450 | -.088 | -.190 | -.270 | -.345 | | | | | | | -.164 | -.302 | -.375 | -.357 | | | | | | | | | | | | | | | | | |
| .550 | -.117 | -.233 | -.263 | -.277 | | | | | | | -.185 | -.283 | -.269 | -.337 | | | | | | | | | | | | | | | | | |
| .650 | -.125 | -.199 | -.209 | -.272 | | | | | | | -.178 | -.243 | -.201 | -.357 | | | | | | | | | | | | | | | | | |
| .750 | -.120 | -.187 | -.171 | -.256 | | | | | | | -.120 | -.140 | -.119 | -.217 | | | | | | | | | | | | | | | | | |
| .850 | -.060 | -.094 | -.077 | -.124 | | | | | | | -.027 | -.029 | -.017 | -.078 | | | | | | | | | | | | | | | | | |
| .900 | -.014 | -.032 | -.021 | -.058 | | | | | | | -.022 | -.027 | -.039 | -.020 | | | | | | | | | | | | | | | | | |
| Right side | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .025 | .025 | -.016 | -.062 | .417 | | | | | | | -.991 | -.081 | .371 | .567 | | | | | | | | | | | | | | | | | |
| .075 | -.277 | -.152 | .018 | .331 | | | | | | | -.662 | -.153 | .170 | .362 | | | | | | | | | | | | | | | | | |
| .150 | -.413 | -.173 | .022 | .250 | | | | | | | -.487 | -.165 | .073 | .238 | | | | | | | | | | | | | | | | | |
| .250 | -.319 | -.142 | -.001 | .192 | | | | | | | -.364 | -.186 | -.001 | .140 | | | | | | | | | | | | | | | | | |
| .350 | -.295 | -.157 | -.041 | .101 | | | | | | | -.363 | -.222 | -.063 | .053 | | | | | | | | | | | | | | | | | |
| .450 | -.276 | -.183 | -.075 | .028 | | | | | | | -.353 | -.265 | -.123 | -.035 | | | | | | | | | | | | | | | | | |
| .550 | -.234 | -.194 | -.087 | -.012 | | | | | | | -.258 | -.266 | -.159 | -.083 | | | | | | | | | | | | | | | | | |
| .650 | -.182 | -.161 | -.086 | -.029 | | | | | | | -.186 | -.203 | -.139 | -.099 | | | | | | | | | | | | | | | | | |
| .750 | -.154 | -.152 | -.079 | -.057 | | | | | | | -.093 | -.104 | -.071 | -.070 | | | | | | | | | | | | | | | | | |
| .850 | -.056 | -.058 | -.022 | -.012 | | | | | | | -.002 | -.003 | -.007 | -.010 | | | | | | | | | | | | | | | | | |
| .900 | -.015 | -.016 | .006 | .000 | | | | | | | -.041 | -.032 | -.029 | -.001 | | | | | | | | | | | | | | | | | |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Left side | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .000 | .320 | .640 | .363 | -.066 | | | | | | | .320 | .560 | .218 | -.179 | | | | | | | | | | | | | | | | | |
| .025 | .309 | -.152 | -1.209 | -1.357 | | | | | | | .114 | -.344 | -1.194 | -.775 | | | | | | | | | | | | | | | | | |
| .075 | .141 | -.195 | -1.030 | -1.276 | | | | | | | -.066 | -.315 | -1.119 | -.783 | | | | | | | | | | | | | | | | | |
| .150 | .019 | -.223 | -.550 | -1.124 | | | | | | | -.309 | -.330 | -.674 | -.803 | | | | | | | | | | | | | | | | | |
| .250 | -.074 | -.250 | -.426 | -.746 | | | | | | | -.201 | -.129 | -.209 | -.762 | | | | | | | | | | | | | | | | | |
| .350 | -.160 | -.314 | -.449 | -.603 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .450 | -.236 | -.331 | -.249 | -.559 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .550 | -.242 | -.303 | -.239 | -.515 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .650 | -.172 | -.187 | -.166 | -.371 | | | | | | | -.122 | -.086 | -.137 | -.459 | | | | | | | | | | | | | | | | | |
| .750 | -.093 | -.085 | -.081 | -.223 | | | | | | | -.078 | -.034 | -.097 | -.397 | | | | | | | | | | | | | | | | | |
| .850 | -.022 | -.008 | -.003 | -.109 | | | | | | | -.030 | -.021 | -.057 | -.329 | | | | | | | | | | | | | | | | | |
| .900 | -.014 | .025 | .038 | -.057 | | | | | | | -.003 | -.039 | -.030 | -.297 | | | | | | | | | | | | | | | | | |
| Right side | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .025 | -1.154 | -.106 | .353 | .528 | | | | | | | -1.201 | -.234 | .174 | .330 | | | | | | | | | | | | | | | | | |
| .075 | -.965 | -.181 | .153 | .330 | | | | | | | -1.078 | -.374 | -.081 | -.077 | | | | | | | | | | | | | | | | | |
| .150 | -.417 | -.189 | .053 | .209 | | | | | | | -.619 | -.308 | -.299 | -.152 | | | | | | | | | | | | | | | | | |
| .250 | -.432 | -.243 | -.054 | .088 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .350 | -.447 | -.303 | -.142 | -.024 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .450 | -.246 | -.303 | -.206 | -.114 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .550 | -.226 | -.263 | -.203 | -.163 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .650 | -.158 | -.171 | -.142 | -.144 | | | | | | | -.114 | -.082 | -.103 | -.160 | | | | | | | | | | | | | | | | | |
| .750 | -.074 | -.073 | -.075 | -.102 | | | | | | | -.090 | -.041 | -.081 | -.168 | | | | | | | | | | | | | | | | | |
| .850 | -.026 | -.028 | -.019 | -.020 | | | | | | | -.017 | -.044 | -.002 | -.113 | | | | | | | | | | | | | | | | | |
| .900 | -.062 | -.059 | -.047 | -.004 | | | | | | | -.003 | -.056 | -.011 | -.115 | | | | | | | | | | | | | | | | | |

TABLE III.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(j) $\alpha = 9.7^\circ$; $M = 0.92$.

| X C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .297 | .912 | .408 | -.254 | | .437 | .678 | .512 | -.033 | |
| .025 | | -.123 | -.003 | -.430 | | .318 | -.139 | -.1018 | -.1388 | |
| .075 | .008 | -.154 | -.215 | -.440 | | .148 | -.205 | -.566 | -.1244 | |
| .150 | .010 | -.230 | -.391 | -.532 | | .054 | -.212 | -.507 | -.796 | |
| .250 | -.007 | -.183 | -.360 | -.506 | | -.022 | -.225 | -.433 | -.711 | |
| .350 | -.045 | -.187 | -.302 | -.441 | | -.099 | -.268 | -.392 | -.591 | |
| .450 | -.088 | -.239 | -.306 | -.374 | | -.175 | -.322 | -.408 | -.391 | |
| .550 | -.126 | -.268 | -.307 | -.295 | | -.209 | -.340 | -.390 | -.328 | |
| .650 | -.147 | -.248 | -.264 | -.273 | | -.243 | -.364 | -.247 | -.371 | |
| .750 | -.154 | -.329 | -.215 | -.279 | | -.167 | -.288 | -.123 | -.256 | |
| .850 | -.086 | -.157 | -.092 | -.148 | | -.039 | -.046 | -.021 | -.099 | |
| .900 | -.031 | -.067 | -.035 | -.074 | | -.016 | -.022 | -.028 | -.032 | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .058 | -.033 | -.084 | .418 | | -.976 | -.106 | .351 | .575 | |
| .075 | -.235 | -.179 | .005 | .340 | | -.631 | -.183 | .153 | .366 | |
| .150 | .394 | -.213 | .015 | .258 | | -.507 | -.195 | .057 | .244 | |
| .250 | -.345 | -.184 | -.006 | .191 | | -.393 | -.213 | -.012 | .142 | |
| .350 | -.316 | -.195 | -.048 | .104 | | -.393 | -.255 | -.078 | .050 | |
| .450 | -.304 | -.217 | -.089 | .026 | | -.393 | -.301 | -.144 | -.040 | |
| .550 | -.271 | -.240 | -.108 | -.019 | | -.355 | -.314 | -.189 | -.093 | |
| .650 | -.222 | -.218 | -.118 | -.041 | | -.201 | -.338 | -.206 | -.119 | |
| .750 | -.179 | -.277 | -.123 | -.077 | | -.091 | -.201 | -.119 | -.091 | |
| .850 | -.071 | -.114 | -.055 | -.036 | | -.002 | -.015 | -.011 | -.029 | |
| .900 | -.024 | -.059 | -.019 | -.020 | | -.040 | -.024 | -.011 | -.018 | |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .340 | .623 | .396 | -.048 | | .331 | .549 | .250 | -.163 | |
| .025 | .305 | -.175 | -.147 | -.367 | | .132 | -.369 | -.173 | -.771 | |
| .075 | .140 | -.222 | -.980 | -.279 | | -.058 | -.309 | -.076 | -.780 | |
| .150 | .021 | -.248 | -.649 | -.115 | | -.312 | -.424 | -.914 | -.792 | |
| .250 | -.071 | -.273 | -.489 | -.744 | | -.260 | -.295 | -.433 | -.746 | |
| .350 | -.166 | -.330 | -.472 | -.614 | | | | | | |
| .450 | -.268 | -.413 | -.485 | -.561 | | | | | | |
| .550 | -.341 | -.443 | -.247 | -.528 | | | | | | |
| .650 | -.256 | -.342 | -.140 | -.416 | | | | | | |
| .750 | -.092 | -.096 | -.068 | -.277 | | | | | | |
| .850 | -.018 | -.001 | -.003 | -.157 | | | | | | |
| .900 | .014 | .038 | .035 | -.101 | | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.133 | -.123 | .331 | .531 | | -1.180 | -.251 | .164 | .332 | |
| .075 | -.951 | -.201 | .135 | .335 | | -1.064 | -.364 | -.083 | .081 | |
| .150 | -.545 | -.212 | .041 | .209 | | -.874 | -.411 | -.310 | -.155 | |
| .250 | -.451 | -.266 | -.061 | .087 | | | | | | |
| .350 | -.486 | -.330 | -.165 | -.027 | | | | | | |
| .450 | -.456 | -.403 | -.255 | -.120 | | | | | | |
| .550 | -.207 | -.408 | -.314 | -.185 | | | | | | |
| .650 | -.133 | -.309 | -.216 | -.168 | | | | | | |
| .750 | -.062 | -.066 | -.089 | -.127 | | | | | | |
| .850 | .029 | .035 | .015 | -.043 | | | | | | |
| .900 | .063 | .061 | .043 | -.027 | | | | | | |

TABLE III.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(k) $\alpha = 15.6^\circ$; $M = 0.60$.

| X C_V | C_p for - | | | | | C_p for - | | | | | C_p for - | | | | | | | | | | | | | | | | |
|-------------------|----------------------|-------|-------------------|--------|---------------------|----------------|---------------------|-------|----------------------|--------|----------------------|-------|-------------------|--------|---------------------|----------------|---------------------|-------|----------------------|--------|--------|--|--|--|--|--|--|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | | $\beta = 7.9^\circ$ | | $\beta = 12.7^\circ$ | | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | | $\beta = 7.9^\circ$ | | $\beta = 12.7^\circ$ | | | | | | | | |
| | $Z/b_V = 0.11$ | | | | | $Z/b_V = 0.38$ | | | | | $Z/b_V = 0.11$ | | | | | $Z/b_V = 0.38$ | | | | | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .000 | .621 | .807 | .829 | .123 | -1.083 | .002 | .659 | .105 | -1.228 | -1.884 | .025 | -.450 | -.151 | -.119 | -.430 | -2.349 | .383 | -.104 | -.845 | -1.868 | -1.755 | | | | | | |
| .075 | -.176 | -.151 | -.262 | -.421 | -.866 | .180 | -.146 | -.520 | -1.467 | -1.834 | .150 | -.110 | -.178 | -.309 | -.430 | -.646 | .075 | -.160 | -.386 | -.505 | -1.761 | | | | | | |
| .250 | -.073 | -.137 | -.237 | -.308 | -.451 | -.002 | -.173 | -.321 | -.448 | -1.006 | .350 | -.096 | -.137 | -.216 | -.263 | -.383 | -.064 | -.196 | -.309 | -.408 | -.560 | | | | | | |
| .450 | -.126 | -.169 | -.219 | -.247 | -.358 | -.107 | -.220 | -.296 | -.353 | -.503 | .550 | -.149 | -.182 | -.214 | -.228 | -.335 | -.114 | -.200 | -.246 | -.308 | -.444 | | | | | | |
| .650 | -.144 | -.155 | -.185 | -.192 | -.306 | -.107 | -.169 | -.201 | -.269 | -.383 | .750 | -.139 | -.142 | -.155 | -.156 | -.256 | -.080 | -.117 | -.137 | -.222 | -.287 | | | | | | |
| .850 | -.103 | -.093 | -.101 | -.095 | -.163 | -.025 | -.048 | -.065 | -.158 | -.192 | .900 | -.078 | -.048 | -.058 | -.052 | -.106 | -.180 | -.178 | -.160 | -.176 | -.170 | | | | | | |
| <i>Right side</i> | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .025 | .046 | -.075 | -.287 | .180 | .774 | -.881 | -.104 | .399 | .533 | .640 | .075 | -.258 | -.164 | -.169 | -.125 | -.531 | -.546 | -.153 | .173 | .345 | .518 | | | | | | |
| .150 | -.308 | -.169 | -.108 | .114 | .377 | -.407 | -.158 | .066 | .209 | .381 | .250 | -.251 | -.140 | -.081 | -.093 | -.284 | -.327 | -.169 | -.002 | .116 | .259 | | | | | | |
| .350 | -.238 | -.151 | -.092 | .050 | .186 | -.285 | -.207 | -.097 | -.024 | .082 | .450 | -.238 | -.169 | -.124 | -.002 | .103 | -.285 | -.207 | -.097 | -.024 | .082 | | | | | | |
| .550 | -.210 | -.162 | -.137 | -.024 | .046 | -.247 | -.193 | -.110 | -.054 | .030 | .650 | -.171 | -.144 | -.124 | -.045 | .014 | -.192 | -.155 | -.097 | -.058 | .005 | | | | | | |
| .750 | -.142 | -.124 | -.110 | -.056 | -.011 | -.119 | -.104 | -.058 | -.038 | -.004 | .850 | -.075 | -.063 | -.069 | -.018 | .010 | -.037 | -.028 | .001 | .005 | .016 | | | | | | |
| .900 | -.053 | -.039 | -.049 | -.006 | .003 | -.014 | -.014 | .008 | .001 | -.002 | $Z/b_V = 0.66$ | | | | | $Z/b_V = 0.93$ | | | | | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .000 | -.169 | .578 | -.137 | -1.063 | -1.126 | .062 | .508 | -.235 | -.646 | -.777 | .025 | .356 | -.128 | -1.063 | -.1294 | -1.020 | -.153 | -.227 | -1.029 | -.721 | -.757 | | | | | | |
| .075 | .169 | -.164 | -.683 | -.1272 | -.1027 | -.023 | -.211 | -.477 | -.702 | -.764 | .150 | -.048 | -.189 | -.449 | -.1272 | -.013 | -.130 | -.193 | -.318 | -.664 | -.752 | | | | | | |
| .250 | .148 | -.046 | -.273 | -.920 | -.031 | -.091 | -.115 | -.235 | -.585 | -.707 | .350 | -.094 | -.207 | -.305 | -.612 | -.1020 | | | | | | | | | | | |
| .450 | -.137 | -.216 | -.275 | -.287 | -.925 | | | | | | .550 | -.149 | -.202 | -.241 | -.240 | -.791 | | | | | | | | | | | |
| .650 | -.123 | -.167 | -.185 | -.192 | -.625 | -.130 | -.095 | -.155 | -.435 | -.587 | .750 | -.080 | -.086 | -.117 | -.131 | -.469 | -.098 | -.061 | -.121 | -.408 | -.560 | | | | | | |
| .850 | -.041 | -.050 | -.060 | -.072 | -.337 | -.066 | -.023 | -.092 | -.358 | -.521 | .900 | -.028 | -.023 | -.033 | -.047 | -.278 | -.046 | -.001 | -.069 | -.321 | -.494 | | | | | | |
| <i>Right side</i> | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| .025 | -.1238 | -.128 | .370 | .527 | .576 | -.804 | -.198 | .186 | .291 | .325 | .075 | -.758 | -.176 | .159 | .343 | .477 | -.607 | -.229 | -.049 | .064 | .152 | | | | | | |
| .150 | -.418 | -.169 | .055 | .207 | .343 | -.391 | -.202 | -.135 | -.086 | -.020 | .250 | -.349 | -.191 | -.029 | .093 | .218 | | | | | | | | | | | |
| .350 | -.317 | -.207 | -.087 | .007 | .121 | | | | | | .450 | -.279 | -.214 | -.126 | -.045 | .046 | | | | | | | | | | | |
| .550 | -.240 | -.193 | -.137 | -.077 | -.004 | | | | | | .650 | -.180 | -.151 | -.108 | -.072 | -.024 | -.128 | -.088 | -.106 | -.133 | -.158 | | | | | | |
| .750 | -.117 | -.086 | -.074 | -.054 | -.040 | -.128 | -.063 | -.106 | -.147 | -.194 | .850 | -.032 | -.014 | -.008 | -.002 | -.027 | -.066 | -.004 | -.038 | -.108 | -.188 | | | | | | |
| .900 | -.005 | .011 | .019 | .016 | -.047 | -.046 | -.017 | -.026 | -.115 | -.208 | | | | | | | | | | | | | | | | | |

TABLE III.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(l) $\alpha = 15.8^\circ$; $M = 0.80$.

| $\frac{x}{C_V}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_V = 0.11$ | | | | | $z/b_V = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .370 | .849 | .728 | .166 | -.237 | .308 | .703 | .377 | -.450 | -.158 |
| .025 | -.842 | -.178 | .181 | -.294 | -.468 | .377 | -.115 | -.429 | -.638 | -.272 |
| .075 | -.204 | -.185 | -.189 | -.367 | -.761 | .175 | -.170 | -.582 | -.361 | -.279 |
| .150 | -.110 | -.225 | -.388 | -.497 | -.689 | .080 | -.185 | -.449 | -.741 | -.264 |
| .250 | -.092 | -.190 | -.293 | -.389 | -.456 | -.003 | -.201 | -.375 | -.523 | -.113 |
| .350 | -.122 | -.167 | -.263 | -.320 | -.402 | -.087 | -.241 | -.363 | -.462 | -.786 |
| .450 | -.157 | -.201 | -.268 | -.286 | -.375 | .146 | -.273 | -.343 | -.418 | -.576 |
| .550 | -.188 | -.229 | -.262 | -.257 | -.374 | .158 | -.256 | -.292 | -.385 | -.506 |
| .650 | -.187 | -.204 | -.225 | -.221 | -.389 | .157 | -.229 | -.239 | -.352 | -.455 |
| .750 | -.198 | -.198 | -.204 | -.201 | -.338 | .119 | -.163 | -.165 | -.297 | -.359 |
| .850 | -.152 | -.133 | -.133 | -.121 | -.215 | -.050 | -.077 | -.071 | -.230 | -.252 |
| .900 | -.110 | -.080 | -.079 | -.069 | -.140 | -.170 | -.187 | -.160 | -.145 | -.143 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .293 | -.078 | -.807 | .192 | .715 | -.1369 | -.124 | .411 | .516 | .667 |
| .075 | -.195 | -.205 | -.197 | .120 | .505 | -.578 | -.182 | .184 | .336 | .521 |
| .150 | -.377 | -.219 | -.098 | .107 | .380 | -.454 | -.185 | .078 | .221 | .386 |
| .250 | -.302 | -.176 | -.094 | .093 | .295 | -.377 | -.195 | .004 | .120 | .274 |
| .350 | -.285 | -.179 | -.120 | .051 | .190 | -.348 | -.223 | -.058 | .048 | .181 |
| .450 | -.270 | -.204 | -.154 | -.006 | .102 | -.330 | -.256 | -.117 | -.033 | .081 |
| .550 | -.240 | -.207 | -.175 | -.043 | .043 | -.288 | -.246 | -.142 | -.077 | .016 |
| .650 | -.207 | -.182 | -.172 | -.066 | .000 | -.228 | -.204 | -.130 | -.089 | -.015 |
| .750 | -.188 | -.175 | -.174 | -.086 | -.042 | -.145 | -.136 | -.085 | -.065 | -.030 |
| .850 | -.112 | -.099 | -.117 | -.046 | -.030 | -.054 | -.045 | -.017 | -.022 | -.017 |
| .900 | -.075 | -.065 | -.088 | -.031 | -.026 | -.017 | -.023 | -.006 | -.021 | -.039 |
| $z/b_V = 0.66$ | | | | | $z/b_V = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .083 | .600 | .118 | -.594 | -.141 | .154 | .514 | -.044 | -.524 | -.746 |
| .025 | -.350 | -.143 | -.1292 | -.1241 | -.948 | .152 | -.282 | -.325 | -.734 | -.659 |
| .075 | .169 | -.187 | -.891 | -.198 | -.930 | -.048 | -.285 | -.784 | -.713 | -.654 |
| .150 | .045 | -.217 | -.546 | -.191 | .900 | -.188 | -.238 | -.410 | -.685 | -.651 |
| .250 | -.101 | -.163 | -.339 | -.826 | -.871 | -.112 | -.134 | -.305 | -.626 | -.639 |
| .350 | -.119 | -.258 | -.354 | -.820 | -.849 | | | | | |
| .450 | -.176 | -.274 | -.319 | -.491 | -.795 | | | | | |
| .550 | -.195 | -.262 | -.280 | -.329 | -.726 | | | | | |
| .650 | -.164 | -.199 | -.207 | -.241 | -.644 | | | | | |
| .750 | -.107 | -.119 | -.132 | -.165 | -.561 | | | | | |
| .850 | -.050 | -.051 | -.056 | -.086 | -.473 | | | | | |
| .900 | -.024 | -.020 | -.020 | -.054 | -.431 | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.305 | -.145 | .377 | .526 | .601 | -.863 | -.246 | .180 | .315 | .374 |
| .075 | -.882 | -.201 | .172 | .345 | .490 | -.754 | -.296 | -.073 | .082 | .200 |
| .150 | -.517 | -.195 | .063 | .218 | .367 | -.550 | -.252 | -.194 | -.106 | .003 |
| .250 | -.398 | -.231 | -.039 | .098 | .238 | | | | | |
| .350 | -.354 | -.264 | -.113 | -.006 | .132 | | | | | |
| .450 | -.309 | -.262 | -.162 | -.072 | .045 | | | | | |
| .550 | -.261 | -.237 | -.165 | -.110 | -.012 | | | | | |
| .650 | -.193 | -.181 | -.138 | -.106 | -.044 | | | | | |
| .750 | -.116 | -.115 | -.095 | -.086 | -.069 | | | | | |
| .850 | -.023 | -.018 | -.015 | -.028 | -.063 | | | | | |
| .900 | -.011 | -.012 | -.015 | -.012 | -.090 | | | | | |

TABLE III.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE LOW WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Concluded

(m) $\alpha = 15.9^\circ$; $M = 0.85$.

| x/c_v | C_p for - | | | | | C_p for - | | | | | | |
|-------------------|----------------------|-------|-------------------|---------------------|---------------------|----------------------|----------------------|--------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | .290 | .880 | .687 | .128 | | .379 | .723 | .471 | .279 | | | |
| .025 | -.963 | -.193 | .289 | -.208 | | .360 | -.144 | -.1276 | -.1512 | | | |
| .075 | -.379 | -.216 | -.119 | -.290 | | .163 | -.204 | -.612 | -.137 | | | |
| .150 | -.143 | -.267 | -.403 | -.467 | | .064 | -.209 | -.557 | -.856 | | | |
| .250 | -.092 | -.220 | -.334 | -.491 | | -.021 | -.220 | -.397 | -.677 | | | |
| .350 | -.120 | -.189 | -.297 | -.385 | | -.105 | -.268 | -.409 | -.519 | | | |
| .450 | -.157 | -.223 | -.310 | -.320 | | -.170 | -.312 | -.385 | -.474 | | | |
| .550 | -.188 | -.252 | -.303 | -.284 | | -.187 | -.293 | -.335 | -.457 | | | |
| .650 | -.198 | -.228 | -.263 | -.262 | | -.188 | -.264 | -.284 | -.419 | | | |
| .750 | -.213 | -.234 | -.265 | -.259 | | -.149 | -.189 | -.200 | -.348 | | | |
| .850 | -.162 | -.153 | -.174 | -.145 | | -.069 | -.087 | -.096 | -.270 | | | |
| .900 | -.118 | -.095 | -.112 | -.085 | | -.179 | -.192 | -.171 | -.147 | | | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | .387 | -.103 | -.975 | .139 | | -.1257 | -.112 | .381 | .481 | | | |
| .075 | -.129 | -.247 | -.376 | .076 | | -.632 | -.186 | .151 | .306 | | | |
| .150 | -.425 | -.250 | -.149 | .080 | | -.502 | -.196 | .048 | .193 | | | |
| .250 | -.339 | -.204 | -.113 | .068 | | -.394 | -.206 | -.030 | .102 | | | |
| .350 | -.308 | -.192 | -.146 | .029 | | -.374 | -.240 | -.092 | .022 | | | |
| .450 | -.289 | -.220 | -.187 | -.026 | | -.350 | -.279 | -.161 | -.060 | | | |
| .550 | -.259 | -.226 | -.209 | -.062 | | -.308 | -.277 | -.197 | -.110 | | | |
| .650 | -.223 | -.203 | -.209 | -.097 | | -.245 | -.237 | -.184 | -.126 | | | |
| .750 | -.215 | -.211 | -.219 | -.124 | | -.156 | -.156 | -.132 | -.104 | | | |
| .850 | -.126 | -.121 | -.149 | -.077 | | -.061 | -.062 | -.053 | -.055 | | | |
| .900 | -.089 | -.081 | -.120 | -.060 | | -.023 | -.030 | -.036 | -.046 | | | |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | .156 | .608 | .224 | -.413 | | .152 | .509 | .038 | .532 | | | |
| .025 | .331 | -.180 | -.1440 | -.1324 | | .136 | -.357 | -.1351 | -.808 | | | |
| .075 | .152 | -.217 | -.1214 | -.1293 | | -.072 | -.364 | -.1040 | -.787 | | | |
| .150 | .026 | -.241 | -.531 | -.1157 | | -.257 | -.277 | -.594 | -.753 | | | |
| .250 | -.332 | -.275 | -.386 | -.796 | | -.129 | -.152 | -.265 | -.695 | | | |
| .350 | -.145 | -.299 | -.363 | -.852 | | | | | | | | |
| .450 | -.213 | -.320 | -.355 | -.640 | | | | | | | | |
| .550 | -.240 | -.301 | -.318 | -.430 | | | | | | | | |
| .650 | -.194 | -.223 | -.239 | -.289 | | -.157 | -.118 | -.191 | -.494 | | | |
| .750 | -.129 | -.138 | -.152 | -.191 | | -.120 | -.070 | -.143 | -.447 | | | |
| .850 | -.064 | -.056 | -.067 | -.111 | | -.071 | -.016 | -.096 | -.396 | | | |
| .900 | -.035 | -.022 | -.030 | -.077 | | -.042 | -.006 | -.070 | -.364 | | | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | -.478 | -.131 | .344 | .512 | | -.360 | -.251 | .152 | .305 | | | |
| .075 | -.235 | -.203 | .138 | .329 | | -.940 | -.356 | -.113 | .066 | | | |
| .150 | -.479 | -.209 | .029 | .197 | | -.583 | -.281 | -.304 | -.150 | | | |
| .250 | -.427 | -.252 | -.075 | .077 | | | | | | | | |
| .350 | -.367 | -.293 | -.160 | -.032 | | | | | | | | |
| .450 | -.335 | -.303 | -.222 | -.117 | | | | | | | | |
| .550 | -.288 | -.274 | -.231 | -.158 | | | | | | | | |
| .650 | -.214 | -.207 | -.187 | -.153 | | -.153 | -.105 | -.139 | -.194 | | | |
| .750 | -.129 | -.129 | -.126 | -.127 | | -.137 | -.081 | -.128 | -.209 | | | |
| .850 | -.030 | -.022 | -.033 | -.058 | | -.061 | -.006 | -.047 | -.155 | | | |
| .900 | -.007 | .011 | -.006 | -.043 | | -.038 | -.022 | -.030 | -.161 | | | |

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TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL

(a) $\alpha = 0^\circ$; $M = 0.60$.

| $\frac{C_p}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .608 | .653 | .363 | -.424 | -1.296 | .279 | .732 | .320 | -.426 | -1.210 |
| .025 | .273 | -.089 | -.541 | -1.138 | -2.278 | .334 | -.087 | -.628 | -1.067 | -1.158 |
| .075 | .134 | -.105 | -.369 | -.680 | -1.585 | .148 | -.125 | -.437 | -.943 | -1.112 |
| .150 | .039 | -.128 | -.299 | -.478 | -.662 | .053 | -.132 | -.321 | -.716 | -1.060 |
| .250 | .021 | -.092 | -.199 | -.301 | -.425 | -.011 | -.141 | -.263 | -.439 | -1.011 |
| .350 | -.013 | -.098 | -.167 | -.235 | -.341 | -.058 | -.157 | -.251 | -.335 | -.868 |
| .450 | -.047 | -.110 | -.156 | -.201 | -.311 | -.104 | -.177 | -.228 | -.278 | -.669 |
| .550 | -.061 | -.103 | -.131 | -.163 | -.321 | -.081 | -.141 | -.174 | -.217 | -.508 |
| .650 | -.031 | -.067 | -.077 | -.122 | -.239 | -.063 | -.101 | -.122 | -.151 | -.391 |
| .750 | -.013 | -.035 | -.045 | -.090 | -.137 | -.027 | -.051 | -.063 | -.083 | -.271 |
| .850 | .021 | .010 | .010 | -.033 | -.090 | .030 | .019 | .016 | -.006 | -.151 |
| .900 | .044 | .046 | .035 | .005 | -.042 | .055 | .060 | .055 | .037 | -.085 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.451 | -.028 | .320 | .611 | .840 | -.612 | -.060 | .370 | .601 | .750 |
| .075 | -.371 | -.107 | .125 | .347 | .566 | -.417 | -.116 | .159 | .366 | .541 |
| .150 | -.283 | -.119 | .048 | .214 | .392 | -.312 | -.128 | .053 | .225 | .383 |
| .250 | -.197 | -.096 | .025 | .146 | .284 | -.253 | -.139 | -.004 | .128 | .256 |
| .350 | -.176 | -.107 | -.022 | .082 | .186 | -.226 | -.141 | -.049 | .057 | .168 |
| .450 | -.154 | -.114 | -.052 | .030 | .121 | -.208 | -.153 | -.086 | .003 | .098 |
| .550 | -.113 | -.094 | -.052 | .016 | .093 | -.172 | -.132 | -.083 | -.011 | .053 |
| .650 | -.072 | -.053 | -.024 | .037 | .089 | -.115 | -.089 | -.058 | -.006 | .039 |
| .750 | -.029 | -.026 | .001 | .039 | .084 | -.045 | -.031 | -.018 | .023 | .039 |
| .850 | .025 | .030 | .044 | .075 | .100 | .032 | .039 | .048 | .066 | .057 |
| .900 | .048 | .055 | .050 | .073 | .089 | .057 | .055 | .053 | .066 | .044 |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .239 | .721 | .261 | -.430 | -.678 | .393 | .676 | .223 | -.260 | -.472 |
| .025 | .345 | -.114 | -.836 | -1.120 | -.737 | .202 | -.202 | -.693 | -.800 | -.524 |
| .075 | .159 | -.139 | -.492 | -1.040 | -.714 | .028 | -.168 | -.394 | -.775 | -.533 |
| .150 | .039 | -.155 | -.374 | -.886 | -.707 | -.049 | -.139 | -.274 | -.702 | -.569 |
| .250 | -.022 | -.159 | -.285 | -.609 | -.671 | -.027 | -.083 | -.199 | -.560 | -.558 |
| .350 | -.079 | -.171 | -.253 | -.389 | -.642 | | | | | |
| .450 | -.108 | -.171 | -.228 | -.281 | -.615 | | | | | |
| .550 | -.111 | -.153 | -.192 | -.217 | -.569 | | | | | |
| .650 | -.079 | -.110 | -.129 | -.154 | -.520 | -.074 | -.069 | -.113 | -.371 | -.407 |
| .750 | -.045 | -.044 | -.061 | -.088 | -.461 | -.047 | -.035 | -.072 | -.337 | -.384 |
| .850 | .012 | .010 | .001 | -.029 | -.388 | -.024 | -.004 | -.056 | -.299 | -.352 |
| .900 | .030 | .028 | .030 | -.002 | -.352 | -.015 | .021 | -.049 | -.263 | -.341 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.709 | -.074 | .388 | .588 | .698 | -.566 | -.130 | .239 | .388 | .469 |
| .075 | -.471 | -.137 | .152 | .357 | .508 | -.380 | -.173 | .016 | .128 | .229 |
| .150 | -.331 | -.134 | .048 | .211 | .354 | -.267 | -.146 | -.054 | .003 | .073 |
| .250 | -.278 | -.155 | -.020 | .096 | .225 | | | | | |
| .350 | -.249 | -.168 | -.081 | .016 | .121 | | | | | |
| .450 | -.217 | -.164 | -.104 | -.024 | .053 | | | | | |
| .550 | -.174 | -.139 | -.099 | -.047 | .012 | | | | | |
| .650 | -.111 | -.103 | -.077 | -.027 | -.006 | -.083 | -.069 | -.072 | -.077 | -.081 |
| .750 | -.049 | -.033 | -.029 | -.006 | -.024 | -.070 | -.040 | -.061 | -.074 | -.119 |
| .850 | .028 | .033 | .037 | .041 | -.026 | -.020 | .019 | -.009 | -.031 | -.115 |
| .900 | .055 | .062 | .057 | .053 | -.060 | -.011 | .035 | .005 | -.033 | -.142 |

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TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(b) $\alpha = 0^\circ$; $M = 0.80$.

| X C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .721 | .677 | .550 | .198 | -.299 | .472 | .773 | .534 | .028 | -.591 |
| .025 | .284 | -.066 | -.541 | -1.146 | -1.535 | .341 | -.073 | -1.067 | -1.715 | -1.029 |
| .075 | .151 | -.096 | -.369 | -.897 | -1.278 | .158 | -.129 | -.445 | -1.511 | -1.009 |
| .150 | .052 | -.134 | -.319 | -.541 | -1.012 | .063 | -.140 | -.337 | -.534 | -.947 |
| .250 | .030 | -.100 | -.209 | -.305 | -.665 | -.010 | -.152 | -.282 | -.385 | -.869 |
| .350 | -.013 | -.108 | -.174 | -.244 | -.433 | -.072 | -.174 | -.264 | -.348 | -.775 |
| .450 | -.059 | -.129 | -.164 | -.216 | -.351 | -.123 | -.197 | -.240 | -.293 | -.662 |
| .550 | -.072 | -.117 | -.133 | -.180 | -.299 | -.106 | -.159 | -.179 | -.218 | -.551 |
| .650 | -.037 | -.073 | -.083 | -.137 | -.222 | -.079 | -.112 | -.118 | -.148 | -.460 |
| .750 | -.019 | -.040 | -.038 | -.094 | -.097 | -.032 | -.044 | -.048 | -.068 | -.360 |
| .850 | .024 | .021 | .022 | -.028 | -.129 | .037 | .034 | .034 | .019 | -.267 |
| .900 | .049 | .057 | .053 | .021 | -.076 | .072 | .075 | .078 | .059 | -.208 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.413 | .000 | .338 | .612 | .839 | -.978 | -.052 | .379 | .605 | .753 |
| .075 | -.391 | -.099 | .145 | .357 | .569 | -.426 | -.120 | .166 | .365 | .549 |
| .150 | -.303 | -.115 | .063 | .221 | .402 | -.326 | -.132 | .069 | .229 | .391 |
| .250 | -.209 | -.097 | .028 | .152 | .292 | -.265 | -.144 | .000 | .128 | .262 |
| .350 | -.184 | -.111 | -.018 | .077 | .190 | -.244 | -.161 | -.057 | .051 | .175 |
| .450 | -.162 | -.123 | -.053 | .022 | .116 | -.221 | -.170 | -.092 | -.010 | .084 |
| .550 | -.117 | -.099 | -.051 | .008 | .087 | -.173 | -.146 | -.095 | -.034 | .037 |
| .650 | -.067 | -.055 | -.018 | .027 | .085 | -.105 | -.097 | -.059 | -.021 | .023 |
| .750 | -.029 | -.023 | -.001 | .036 | .070 | -.026 | -.022 | -.009 | .011 | .022 |
| .850 | -.034 | .040 | .047 | .068 | .076 | -.057 | -.059 | .061 | .062 | .026 |
| .900 | .069 | .062 | .061 | .074 | .066 | -.083 | -.074 | .070 | .068 | -.003 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .446 | .748 | .482 | -.013 | -.427 | .487 | .702 | .386 | -.016 | -.311 |
| .025 | .348 | -.112 | -1.117 | -1.334 | -.699 | .193 | -.221 | -1.056 | -.781 | -.483 |
| .075 | .163 | -.150 | -.556 | -1.201 | -.697 | .006 | -.197 | -.504 | -.753 | -.481 |
| .150 | .048 | -.173 | -.401 | -.982 | -.697 | -.070 | -.159 | -.298 | -.735 | -.507 |
| .250 | -.032 | -.182 | -.305 | -.771 | -.665 | -.037 | -.090 | -.214 | -.623 | -.509 |
| .350 | -.096 | -.194 | -.267 | -.556 | -.623 | | | | | |
| .450 | -.132 | -.199 | -.238 | -.369 | -.583 | | | | | |
| .550 | -.128 | -.171 | -.194 | -.244 | -.541 | | | | | |
| .650 | -.088 | -.117 | -.121 | -.143 | -.503 | -.073 | -.059 | -.106 | -.378 | -.404 |
| .750 | -.040 | -.034 | -.047 | -.063 | -.454 | -.040 | -.019 | -.064 | -.334 | -.380 |
| .850 | -.031 | -.028 | -.022 | -.001 | -.404 | -.007 | -.024 | -.045 | -.282 | -.354 |
| .900 | .046 | .056 | .050 | .025 | -.378 | .015 | .045 | -.032 | -.244 | -.243 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.117 | -.066 | .391 | .603 | .718 | -1.076 | -.150 | .228 | .392 | .505 |
| .075 | -.503 | -.143 | .164 | .363 | .520 | -.480 | -.205 | -.012 | .119 | .256 |
| .150 | -.353 | -.140 | .063 | .222 | .368 | -.267 | -.161 | -.074 | -.025 | .081 |
| .250 | -.302 | -.170 | -.027 | .100 | .227 | | | | | |
| .350 | -.268 | -.188 | -.089 | .008 | .119 | | | | | |
| .450 | -.227 | -.188 | -.121 | -.044 | .038 | | | | | |
| .550 | -.177 | -.158 | -.114 | -.068 | -.012 | | | | | |
| .650 | -.105 | -.105 | -.080 | -.050 | -.032 | -.041 | -.056 | -.065 | -.077 | -.098 |
| .750 | -.035 | -.022 | -.032 | -.019 | -.048 | -.061 | -.025 | -.054 | -.073 | -.138 |
| .850 | .052 | .063 | .052 | .044 | -.048 | .000 | .049 | .015 | -.025 | -.123 |
| .900 | .087 | .084 | .076 | .062 | -.085 | .009 | .063 | .023 | -.031 | -.155 |

TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(c) $\alpha = 0^\circ$; $M = 0.85$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .744 | .682 | .601 | .317 | -.026 | .527 | .785 | .592 | .173 | -.292 |
| .025 | .280 | -.061 | -.533 | -1.086 | -1.135 | .330 | -.075 | -1.115 | -1.551 | -.784 |
| .075 | .148 | -.088 | -.379 | -.867 | -.943 | .152 | -.136 | -.413 | -1.400 | -.803 |
| .150 | .045 | -.136 | -.344 | -.692 | -.798 | .054 | -.152 | -.347 | -1.226 | -.749 |
| .250 | .018 | -.108 | -.227 | -.350 | -.623 | -.019 | -.163 | -.300 | -.334 | -.689 |
| .350 | -.027 | -.122 | -.189 | -.256 | -.438 | -.087 | -.190 | -.284 | -.291 | -.620 |
| .450 | -.073 | -.139 | -.181 | -.210 | -.319 | -.145 | -.221 | -.259 | -.277 | -.528 |
| .550 | -.087 | -.130 | -.148 | -.169 | -.241 | -.130 | -.179 | -.195 | -.217 | -.444 |
| .650 | -.047 | -.082 | -.095 | -.139 | -.161 | -.101 | -.127 | -.127 | -.149 | -.364 |
| .750 | -.033 | -.047 | -.047 | -.090 | -.132 | -.044 | -.054 | -.054 | -.065 | -.275 |
| .850 | .014 | .013 | .018 | -.023 | -.052 | .028 | .030 | .031 | .026 | -.188 |
| .900 | .042 | .055 | .057 | .021 | .000 | .068 | .073 | .079 | .072 | -.134 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.390 | .010 | .344 | .615 | .865 | -.999 | -.048 | .375 | .598 | .790 |
| .075 | -.406 | -.099 | .148 | .361 | .618 | -.454 | -.125 | .162 | .367 | .595 |
| .150 | -.322 | -.122 | .062 | .229 | .466 | -.345 | -.139 | .064 | .232 | .452 |
| .250 | -.229 | -.108 | .024 | .157 | .362 | -.286 | -.156 | -.009 | .126 | .336 |
| .350 | -.198 | -.126 | -.030 | .076 | .266 | -.262 | -.176 | -.068 | .046 | .246 |
| .450 | -.175 | -.137 | -.071 | .015 | .189 | -.238 | -.188 | -.114 | -.025 | .157 |
| .550 | -.127 | -.113 | -.067 | .002 | .163 | -.187 | -.162 | -.118 | -.045 | .114 |
| .650 | -.079 | -.062 | -.034 | .024 | .157 | -.114 | -.113 | -.075 | -.032 | .097 |
| .750 | -.035 | -.034 | -.013 | .031 | .144 | -.032 | -.031 | -.021 | .006 | .093 |
| .850 | .034 | .033 | .040 | .066 | .142 | .051 | .055 | .054 | .063 | .094 |
| .900 | .062 | .061 | .051 | .066 | .131 | .084 | .073 | .071 | .069 | .066 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .490 | .760 | .538 | .120 | -.201 | .505 | .707 | .430 | .029 | -.176 |
| .025 | .338 | -.119 | -.1.212 | -1.645 | -.600 | .177 | -.215 | -.706 | -.758 | -.593 |
| .075 | .153 | -.160 | -.622 | -1.465 | -.608 | -.022 | -.235 | -.605 | -.851 | -.390 |
| .150 | .037 | -.186 | -.415 | -1.247 | -.618 | -.103 | -.179 | -.307 | -.840 | -.427 |
| .250 | -.056 | -.201 | -.315 | -.620 | -.583 | -.052 | -.103 | -.220 | -.713 | -.421 |
| .350 | -.117 | -.218 | -.280 | -.475 | -.526 | | | | | |
| .450 | -.157 | -.224 | -.254 | -.318 | -.477 | | | | | |
| .550 | -.153 | -.193 | -.203 | -.209 | -.426 | | | | | |
| .650 | -.111 | -.133 | -.128 | -.126 | -.385 | -.084 | -.074 | -.112 | -.415 | -.313 |
| .750 | -.053 | -.040 | -.043 | -.052 | -.331 | -.046 | -.024 | -.070 | -.364 | -.294 |
| .850 | .022 | .024 | .030 | .015 | -.275 | -.013 | .023 | -.051 | -.304 | |
| .900 | .045 | .058 | .061 | .042 | -.250 | .010 | .047 | -.036 | -.266 | -.253 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.178 | -.064 | .383 | .592 | .754 | -1.167 | -.170 | .213 | .393 | .558 |
| .075 | -.421 | -.147 | .159 | .357 | .570 | -.601 | -.235 | -.043 | .106 | .323 |
| .150 | -.373 | -.149 | .057 | .217 | .430 | -.237 | -.181 | -.107 | -.059 | .152 |
| .250 | -.316 | -.190 | -.040 | .095 | .298 | | | | | |
| .350 | -.285 | -.210 | -.108 | -.004 | .193 | | | | | |
| .450 | -.244 | -.210 | -.145 | -.066 | .111 | | | | | |
| .550 | -.192 | -.177 | -.139 | -.083 | .061 | | | | | |
| .650 | -.116 | -.119 | -.098 | -.060 | .040 | -.091 | -.068 | -.071 | -.085 | -.024 |
| .750 | -.037 | -.028 | -.038 | -.026 | .029 | -.074 | -.030 | -.057 | -.078 | -.056 |
| .850 | .058 | .055 | .051 | .046 | .036 | -.005 | .048 | .016 | -.021 | -.038 |
| .900 | .086 | .084 | .077 | .066 | .000 | .001 | .063 | .025 | -.029 | -.065 |

TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(d) $\alpha = 0^\circ$; $M = 0.90$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .777 | .688 | .649 | .416 | .042 | .590 | .794 | .652 | .293 | .220 |
| .025 | .297 | -.051 | -.486 | -.993 | -1.168 | .340 | -.074 | -.996 | -1.329 | -.811 |
| .075 | .169 | -.088 | -.392 | -.785 | -.980 | .162 | -.141 | -.673 | -1.207 | -.816 |
| .150 | .063 | -.146 | -.371 | -.684 | -.838 | .068 | -.162 | -.375 | -1.089 | -.795 |
| .250 | .032 | -.121 | -.242 | -.481 | -.717 | -.009 | -.183 | -.313 | -.579 | -.759 |
| .350 | -.018 | -.138 | -.209 | -.312 | -.598 | -.085 | -.216 | -.335 | -.398 | -.723 |
| .450 | -.073 | -.161 | -.200 | -.242 | -.514 | -.155 | -.261 | -.274 | -.235 | -.658 |
| .550 | -.092 | -.150 | -.154 | -.163 | -.434 | -.140 | -.206 | -.200 | -.159 | -.582 |
| .650 | -.049 | -.098 | -.099 | -.120 | -.353 | -.108 | -.147 | -.130 | -.108 | -.510 |
| .750 | -.033 | -.064 | -.047 | -.074 | -.313 | -.041 | -.056 | -.051 | -.046 | -.432 |
| .850 | .020 | .005 | .024 | -.005 | -.215 | .039 | .032 | .041 | .042 | -.358 |
| .900 | .052 | .054 | .062 | .035 | -.152 | .083 | .080 | .087 | .080 | -.301 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.339 | .020 | .349 | .620 | .852 | -.913 | -.048 | .369 | .596 | .763 |
| .075 | -.397 | -.095 | .151 | .366 | .582 | -.569 | -.126 | .162 | .363 | .554 |
| .150 | -.333 | -.123 | .062 | .234 | .422 | -.361 | -.147 | .060 | .232 | .402 |
| .250 | -.227 | -.111 | .023 | .160 | .305 | -.289 | -.167 | -.017 | .123 | .271 |
| .350 | -.200 | -.137 | -.036 | .073 | .200 | -.281 | -.200 | -.082 | .035 | .176 |
| .450 | -.175 | -.153 | -.080 | .010 | .114 | -.236 | -.218 | -.134 | -.035 | .076 |
| .550 | -.124 | -.125 | -.083 | -.008 | .073 | -.178 | -.189 | -.142 | -.059 | .020 |
| .650 | -.063 | -.071 | -.046 | .021 | .073 | -.103 | -.125 | -.096 | -.042 | -.003 |
| .750 | -.020 | -.043 | -.029 | .021 | .045 | -.014 | -.029 | -.031 | .000 | -.012 |
| .850 | .050 | .031 | .028 | .060 | .037 | .071 | .056 | .052 | .063 | -.016 |
| .900 | .083 | .058 | .044 | .067 | .010 | .105 | .078 | .071 | .069 | -.055 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .540 | .771 | .600 | .241 | -.169 | .542 | .708 | .487 | .122 | .204 |
| .025 | .347 | -.117 | -.114 | -.414 | -.741 | -.521 | -.506 | -.507 | -.530 | -.497 |
| .075 | .166 | -.167 | -.918 | -.288 | -.754 | -.037 | -.327 | -.020 | -.278 | -.504 |
| .150 | .044 | -.206 | -.398 | -.173 | -.767 | -.152 | -.209 | -.411 | -.032 | -.541 |
| .250 | -.053 | -.232 | -.406 | -.071 | -.725 | -.059 | -.117 | -.142 | -.671 | -.546 |
| .350 | -.131 | -.256 | -.237 | -.548 | -.663 | | | | | |
| .450 | -.179 | -.260 | -.250 | -.172 | -.607 | | | | | |
| .550 | -.170 | -.220 | -.212 | -.120 | -.574 | | | | | |
| .650 | -.115 | -.154 | -.129 | -.081 | -.533 | -.076 | -.075 | -.115 | -.343 | -.454 |
| .750 | -.048 | -.031 | -.040 | -.028 | -.486 | -.033 | -.017 | -.067 | -.323 | -.429 |
| .850 | .043 | .035 | .039 | .031 | -.429 | .012 | .031 | -.048 | -.281 | -.406 |
| .900 | .066 | .066 | .071 | .054 | -.400 | .034 | .056 | -.035 | -.237 | -.389 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.061 | -.063 | .376 | .582 | .723 | -1.077 | -.183 | .198 | .382 | .518 |
| .075 | -.835 | -.154 | .154 | .345 | .522 | -.887 | -.315 | -.074 | .094 | .261 |
| .150 | -.362 | -.162 | .051 | .213 | .375 | -.331 | -.208 | -.189 | -.101 | .064 |
| .250 | -.363 | -.216 | -.056 | .084 | .233 | | | | | |
| .350 | -.251 | -.249 | -.142 | -.023 | .113 | | | | | |
| .450 | -.228 | -.241 | -.182 | -.098 | .016 | | | | | |
| .550 | -.182 | -.204 | -.169 | -.112 | -.048 | | | | | |
| .650 | -.100 | -.130 | -.115 | -.077 | -.068 | -.073 | -.068 | -.076 | -.096 | -.136 |
| .750 | -.018 | -.031 | -.043 | -.032 | -.091 | -.059 | -.028 | -.054 | -.077 | -.180 |
| .850 | .076 | .060 | .055 | .052 | -.072 | .010 | .056 | .025 | -.012 | -.148 |
| .900 | .113 | .092 | .079 | .069 | -.105 | .020 | .070 | .032 | -.017 | -.175 |

TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(e) $\alpha = 0^\circ$; $M = 0.92$.

| X C_v | C_p for - | | | | | C_p for - | | | | | | | | |
|-------------------|----------------------|-------|-------------------|--------|---------------------|---------------------|----------------------|----------------------|-------|-------------------|--------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | | | | | $Z/b_v = 0.11$ | | | | | | | $Z/b_v = 0.38$ | | |
| <i>Left side</i> | | | | | | | | | | | | | | |
| .000 | .783 | .687 | .665 | .465 | .087 | | | .605 | .799 | .674 | .352 | -.172 | | |
| .025 | .283 | -.046 | -.457 | -.962 | -1.138 | | | .330 | -.072 | -.959 | -1.282 | -.756 | | |
| .075 | .157 | -.084 | -.376 | -.752 | -.949 | | | .150 | -.145 | -.723 | -1.171 | -.783 | | |
| .150 | .046 | -.148 | -.363 | -.673 | -.806 | | | .052 | -.166 | -.408 | -1.075 | -.756 | | |
| .250 | .018 | -.119 | -.252 | -.558 | -.687 | | | .041 | -.181 | -.311 | -.649 | -.704 | | |
| .350 | -.035 | -.136 | -.211 | -.382 | -.584 | | | .112 | -.225 | -.338 | -.534 | -.705 | | |
| .450 | -.098 | -.171 | -.208 | -.321 | -.522 | | | .191 | -.283 | -.326 | -.437 | -.647 | | |
| .550 | -.125 | -.165 | -.159 | -.226 | -.454 | | | .179 | -.221 | -.181 | -.165 | -.576 | | |
| .650 | -.079 | -.103 | -.092 | -.134 | -.375 | | | .139 | -.153 | -.122 | -.076 | -.517 | | |
| .750 | -.057 | -.064 | -.039 | -.076 | -.337 | | | .067 | -.058 | -.042 | -.024 | -.440 | | |
| .850 | -.006 | .006 | .030 | .007 | .245 | | | .023 | .034 | .047 | .052 | -.372 | | |
| .900 | .033 | .053 | .064 | .035 | -.176 | | | .073 | .087 | .096 | .093 | -.316 | | |
| <i>Right side</i> | | | | | | | | | | | | | | |
| .025 | -.335 | .028 | .352 | .618 | .849 | | | -.860 | -.041 | .367 | .597 | .770 | | |
| .075 | -.407 | -.090 | .159 | .367 | .585 | | | -.660 | -.124 | .164 | .364 | .553 | | |
| .150 | -.363 | -.120 | .071 | .236 | .420 | | | -.409 | -.149 | .065 | .224 | .402 | | |
| .250 | -.264 | -.114 | .025 | .158 | .312 | | | -.306 | -.170 | -.016 | .120 | .274 | | |
| .350 | -.230 | -.144 | -.035 | .068 | .204 | | | -.324 | -.209 | -.084 | .031 | .177 | | |
| .450 | -.207 | -.165 | -.082 | -.003 | .112 | | | -.303 | -.238 | -.146 | -.049 | .076 | | |
| .550 | -.142 | -.140 | -.088 | -.021 | .074 | | | -.179 | -.202 | -.153 | -.080 | .019 | | |
| .650 | -.076 | -.080 | -.043 | .005 | .071 | | | -.110 | -.135 | -.106 | -.066 | -.010 | | |
| .750 | -.031 | -.049 | -.033 | .008 | .044 | | | -.025 | -.030 | -.032 | -.013 | -.019 | | |
| .850 | .039 | .027 | .032 | .051 | .024 | | | .065 | .058 | .053 | .052 | -.024 | | |
| .900 | .067 | .060 | .045 | .055 | -.006 | | | .093 | .084 | .074 | .069 | -.062 | | |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | | | |
| .000 | .558 | .777 | .626 | .303 | -.122 | | | .557 | .712 | .512 | .182 | -.176 | | |
| .025 | .330 | -.116 | -.1071 | -.1359 | -.732 | | | -.451 | -.449 | -.446 | -.444 | -.439 | | |
| .075 | .143 | -.171 | -.897 | -.226 | -.739 | | | -.059 | -.313 | -.990 | -.1264 | -.503 | | |
| .150 | .020 | -.208 | -.637 | -.156 | -.754 | | | -.223 | -.230 | -.732 | -.1070 | -.533 | | |
| .250 | -.075 | -.244 | -.385 | -.109 | -.726 | | | -.122 | -.115 | -.157 | -.981 | -.545 | | |
| .350 | -.173 | -.294 | -.382 | -.029 | -.665 | | | | | | | | | |
| .450 | -.230 | -.277 | -.193 | -.442 | -.601 | | | | | | | | | |
| .550 | -.208 | -.236 | -.197 | -.071 | -.568 | | | | | | | | | |
| .650 | -.142 | -.148 | -.119 | -.024 | -.542 | | | -.091 | -.072 | -.110 | -.468 | -.458 | | |
| .750 | -.050 | -.030 | .010 | .049 | | | | -.040 | -.021 | -.065 | .384 | .435 | | |
| .850 | .026 | .041 | .045 | .057 | -.439 | | | -.001 | .035 | -.046 | -.215 | -.410 | | |
| .900 | .053 | .071 | .077 | .073 | -.411 | | | .024 | .060 | -.030 | -.274 | -.394 | | |
| <i>Right side</i> | | | | | | | | | | | | | | |
| .025 | -.001 | -.059 | .374 | .582 | .725 | | | -.045 | -.183 | .197 | .381 | .519 | | |
| .075 | -.830 | -.153 | .155 | .350 | .530 | | | -.960 | -.358 | -.077 | .094 | .266 | | |
| .150 | -.511 | -.168 | .053 | .212 | .377 | | | -.649 | -.228 | -.214 | -.108 | .066 | | |
| .250 | -.380 | -.223 | -.062 | .080 | .234 | | | | | | | | | |
| .350 | -.404 | -.286 | -.155 | -.034 | .110 | | | | | | | | | |
| .450 | -.196 | -.258 | -.204 | -.118 | .016 | | | | | | | | | |
| .550 | -.187 | -.214 | -.181 | -.146 | -.054 | | | | | | | | | |
| .650 | -.112 | -.135 | -.120 | -.104 | -.078 | | | -.096 | -.064 | -.077 | -.102 | -.141 | | |
| .750 | -.027 | -.026 | -.042 | -.045 | -.096 | | | -.068 | -.026 | -.049 | -.084 | -.192 | | |
| .850 | .067 | .070 | .062 | .050 | -.079 | | | -.003 | .064 | .032 | -.011 | -.150 | | |
| .900 | .101 | .099 | .086 | .075 | -.113 | | | .006 | .077 | .040 | -.008 | -.179 | | |

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TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(f) $\alpha = 9.4^\circ$; $M = 0.60$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .512 | .797 | .500 | -.461 | -1.196 | .233 | .660 | .112 | -.775 | -1.558 |
| .025 | -.044 | -.145 | -.274 | -.822 | -2.592 | .287 | -.143 | -.770 | -1.218 | -1.385 |
| .075 | -.001 | -.134 | -.324 | -.534 | -.845 | .116 | -.161 | -.484 | -1.100 | -1.373 |
| .150 | -.026 | -.154 | -.313 | -.432 | -.619 | .028 | -.161 | -.356 | -.877 | -1.455 |
| .250 | -.021 | -.107 | -.226 | -.304 | -.412 | -.026 | -.165 | -.299 | -.407 | -1.194 |
| .350 | -.055 | -.116 | -.201 | -.257 | -.364 | -.080 | -.188 | -.285 | -.318 | -.717 |
| .450 | -.073 | -.139 | -.199 | -.234 | -.351 | -.116 | -.203 | -.265 | -.293 | -.412 |
| .550 | -.087 | -.141 | -.187 | -.211 | -.296 | -.109 | -.174 | -.212 | -.238 | -.330 |
| .650 | -.073 | -.114 | -.153 | -.184 | -.232 | -.089 | -.141 | -.160 | -.186 | -.269 |
| .750 | -.057 | -.090 | -.121 | -.134 | -.178 | -.060 | -.094 | -.107 | -.120 | -.198 |
| .850 | -.019 | -.047 | -.062 | -.068 | -.107 | .001 | -.018 | -.023 | -.029 | -.102 |
| .900 | -.010 | -.007 | -.018 | -.025 | -.057 | .033 | -.018 | -.016 | -.007 | -.059 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.172 | -.027 | .007 | .546 | .806 | -.600 | -.040 | .379 | .578 | .690 |
| .075 | -.294 | -.119 | .023 | .332 | .538 | -.404 | -.110 | .162 | .382 | .524 |
| .150 | -.271 | -.123 | .009 | .223 | .383 | -.312 | -.123 | .064 | .225 | .378 |
| .250 | -.208 | -.094 | -.005 | .164 | .289 | -.265 | -.141 | .002 | .130 | .251 |
| .350 | -.195 | -.110 | -.034 | .084 | .189 | -.244 | -.157 | -.046 | .062 | .169 |
| .450 | -.193 | -.127 | -.057 | .032 | .119 | -.240 | -.170 | -.085 | .005 | .098 |
| .550 | -.168 | -.119 | -.062 | .009 | .087 | -.204 | -.157 | -.091 | -.025 | .052 |
| .650 | -.134 | -.094 | -.053 | .007 | .075 | -.150 | -.123 | -.071 | -.020 | .043 |
| .750 | -.098 | -.081 | -.034 | .009 | .059 | -.078 | -.061 | -.034 | .000 | .039 |
| .850 | -.033 | -.020 | .007 | .039 | .078 | .001 | .006 | .025 | .046 | .057 |
| .900 | -.006 | .000 | .018 | .041 | .068 | .026 | .020 | .032 | .046 | .039 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .132 | .618 | -.023 | -.779 | -1.112 | .244 | .558 | -.046 | -.461 | -.824 |
| .025 | .285 | -.188 | -1.064 | -1.263 | -.932 | .148 | -.264 | -.888 | -.711 | -.617 |
| .075 | .114 | -.181 | -.553 | -1.225 | -.913 | -.026 | -.210 | -.489 | -.700 | -.613 |
| .150 | .010 | -.188 | -.413 | -1.152 | -.891 | -.111 | -.183 | -.317 | -.663 | -.617 |
| .250 | -.055 | -.183 | -.327 | -.838 | -.847 | -.069 | -.121 | -.226 | -.570 | -.594 |
| .350 | -.100 | -.197 | -.283 | -.434 | -.822 | | | | | |
| .450 | -.132 | -.201 | -.263 | -.263 | -.768 | | | | | |
| .550 | -.134 | -.188 | -.226 | -.222 | -.692 | | | | | |
| .650 | -.109 | -.141 | -.160 | -.166 | -.588 | -.100 | -.081 | -.137 | -.382 | -.476 |
| .750 | -.060 | -.083 | -.096 | -.102 | -.481 | -.075 | -.047 | -.110 | -.336 | -.449 |
| .850 | -.012 | -.020 | -.037 | -.047 | -.378 | -.042 | -.009 | -.087 | -.286 | -.424 |
| .900 | -.010 | .002 | .000 | -.020 | -.335 | -.017 | .009 | -.064 | -.259 | -.408 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.699 | -.054 | .372 | .562 | .629 | -.596 | -.132 | .201 | .323 | .383 |
| .075 | -.465 | -.130 | .160 | .353 | .481 | -.388 | -.188 | -.018 | .089 | .187 |
| .150 | -.330 | -.139 | .059 | .221 | .340 | -.267 | -.170 | -.101 | -.047 | .027 |
| .250 | -.289 | -.165 | -.023 | .107 | .217 | | | | | |
| .350 | -.269 | -.177 | -.080 | .028 | .119 | | | | | |
| .450 | -.235 | -.183 | -.110 | -.022 | .057 | | | | | |
| .550 | -.195 | -.165 | -.114 | -.047 | .007 | | | | | |
| .650 | -.138 | -.134 | -.091 | -.038 | -.009 | -.048 | -.078 | -.107 | -.107 | -.127 |
| .750 | -.078 | -.054 | -.057 | -.018 | -.016 | -.078 | -.061 | -.091 | -.113 | -.159 |
| .850 | -.008 | -.011 | -.023 | .025 | -.009 | -.021 | .006 | -.032 | -.070 | -.159 |
| .900 | -.035 | .038 | .036 | .043 | -.030 | -.008 | .020 | -.021 | -.075 | -.184 |

TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(g) $\alpha = 9.6^\circ$; $M = 0.80$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-----------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| Left side | | | | | | | | | | |
| .000 | .482 | .844 | .492 | -.106 | -.123 | .432 | .701 | .413 | -.156 | -.769 |
| .025 | -.075 | -.126 | -.185 | -.635 | -1.586 | .269 | -.126 | -1.003 | -1.437 | -1.104 |
| .075 | -.012 | -.130 | -.337 | -.529 | -1.079 | .107 | -.157 | -.514 | -1.313 | -1.065 |
| .150 | -.040 | -.166 | -.362 | -.501 | -.644 | .022 | -.154 | -.383 | -1.012 | -1.046 |
| .250 | -.034 | -.117 | -.258 | -.355 | -.435 | .039 | -.168 | -.322 | -.383 | -.982 |
| .350 | -.062 | -.123 | -.224 | -.290 | -.370 | .095 | -.209 | -.311 | -.331 | -.811 |
| .450 | -.091 | -.148 | -.223 | -.260 | -.351 | .147 | -.225 | -.293 | -.325 | -.589 |
| .550 | -.106 | -.160 | -.209 | -.234 | -.304 | .142 | -.198 | -.243 | -.272 | -.437 |
| .650 | -.089 | -.138 | -.172 | -.203 | -.277 | .121 | -.160 | -.189 | -.211 | -.367 |
| .750 | -.078 | -.117 | -.145 | -.159 | -.243 | .077 | -.100 | -.119 | -.136 | -.304 |
| .850 | -.036 | -.053 | -.072 | -.082 | -.162 | .006 | -.011 | -.025 | -.042 | -.207 |
| .900 | -.002 | -.005 | -.025 | -.035 | -.104 | .037 | -.035 | -.024 | -.011 | -.138 |
| Right side | | | | | | | | | | |
| .025 | -.080 | .001 | -.031 | .500 | .781 | .823 | -.035 | .363 | .573 | .708 |
| .075 | -.304 | -.110 | -.321 | .527 | .417 | -.109 | .157 | .354 | .527 | |
| .150 | -.303 | -.126 | -.002 | .219 | .382 | -.338 | -.127 | .064 | .227 | .383 |
| .250 | -.230 | -.098 | -.025 | .163 | .290 | -.286 | -.148 | -.005 | .128 | .269 |
| .350 | -.219 | -.118 | -.049 | .084 | .190 | -.276 | -.172 | -.061 | .058 | .178 |
| .450 | -.215 | -.141 | -.080 | .022 | .109 | -.263 | -.191 | -.105 | -.016 | .081 |
| .550 | -.186 | -.136 | -.080 | -.009 | .065 | -.226 | -.178 | -.121 | -.050 | .032 |
| .650 | -.151 | -.112 | -.067 | -.007 | .051 | -.165 | -.144 | -.095 | -.045 | .012 |
| .750 | -.124 | -.098 | -.055 | -.015 | .029 | -.087 | -.068 | -.049 | -.019 | .006 |
| .850 | -.048 | -.029 | -.009 | -.017 | .035 | .004 | .012 | .018 | .032 | .016 |
| .900 | -.007 | .001 | .009 | .028 | .030 | .029 | .029 | .030 | .037 | -.006 |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| Left side | | | | | | | | | | |
| .000 | .324 | .652 | .273 | -.214 | -.686 | .336 | .577 | .157 | -.217 | -.618 |
| .025 | .275 | -.181 | -.166 | -.969 | -.781 | .114 | -.284 | -.869 | -.618 | -.544 |
| .075 | .108 | -.188 | -.708 | -.934 | -.755 | -.056 | -.251 | -.691 | -.620 | -.546 |
| .150 | .002 | -.200 | -.456 | -.907 | -.724 | -.139 | -.198 | -.415 | -.629 | -.549 |
| .250 | -.068 | -.203 | -.349 | -.872 | -.695 | -.080 | -.121 | -.270 | -.579 | -.549 |
| .350 | -.125 | -.221 | -.307 | -.744 | -.677 | | | | | |
| .450 | -.163 | -.227 | -.279 | -.561 | -.653 | | | | | |
| .550 | -.165 | -.209 | -.233 | -.398 | -.613 | | | | | |
| .650 | -.127 | -.145 | -.165 | -.266 | -.573 | -.103 | -.068 | -.139 | -.363 | -.473 |
| .750 | -.065 | -.068 | -.084 | -.156 | -.523 | -.068 | -.026 | -.101 | -.326 | -.447 |
| .850 | -.009 | -.002 | -.017 | -.068 | -.462 | -.025 | -.013 | -.067 | -.287 | -.419 |
| .900 | -.020 | .029 | .020 | -.032 | -.428 | -.001 | -.036 | -.040 | -.269 | -.399 |
| Right side | | | | | | | | | | |
| .025 | -.952 | -.049 | .367 | .560 | .657 | -.999 | -.154 | .187 | .335 | .429 |
| .075 | -.502 | -.132 | .157 | .350 | .500 | -.470 | -.225 | -.051 | .088 | .223 |
| .150 | -.364 | -.142 | .058 | .219 | .362 | -.286 | -.195 | -.145 | -.065 | .036 |
| .250 | -.320 | -.180 | -.040 | .101 | .231 | | | | | |
| .350 | -.294 | -.203 | -.105 | .008 | .125 | | | | | |
| .450 | -.260 | -.210 | -.142 | -.051 | .044 | | | | | |
| .550 | -.212 | -.188 | -.145 | -.079 | -.015 | | | | | |
| .650 | -.144 | -.147 | -.108 | -.068 | -.038 | -.060 | -.062 | -.099 | -.123 | -.147 |
| .750 | -.068 | -.050 | -.060 | -.044 | -.055 | -.069 | -.036 | -.081 | -.126 | -.194 |
| .850 | -.020 | .032 | .021 | .015 | -.052 | -.007 | -.036 | -.014 | -.082 | -.184 |
| .900 | -.057 | .056 | .042 | .035 | -.083 | .011 | .050 | .000 | -.095 | -.206 |

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TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(h) $\alpha = 9.7^\circ$; $M = 0.85$.

| x c_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .418 | .864 | .465 | -.111 | .039 | .452 | .709 | .488 | .004 | -.609 |
| .025 | -.137 | -.131 | -.120 | -.557 | -.437 | .244 | -.138 | -.180 | -.576 | -.153 |
| .075 | -.054 | -.145 | -.325 | -.513 | -.039 | .075 | -.179 | -.476 | -.240 | -.103 |
| .150 | -.080 | -.192 | -.393 | -.554 | -.723 | -.010 | -.179 | -.391 | -.776 | -.036 |
| .250 | -.080 | -.139 | -.268 | -.414 | -.501 | -.083 | -.196 | -.341 | -.543 | -.923 |
| .350 | -.109 | -.144 | -.239 | -.327 | -.398 | -.140 | -.237 | -.331 | -.407 | -.783 |
| .450 | -.135 | -.176 | -.242 | -.280 | -.373 | -.202 | -.267 | -.312 | -.373 | -.636 |
| .550 | -.144 | -.189 | -.225 | -.248 | -.328 | -.196 | -.238 | -.256 | -.301 | -.524 |
| .650 | -.127 | -.162 | -.185 | -.216 | -.301 | -.176 | -.196 | -.200 | -.224 | -.447 |
| .750 | -.127 | -.145 | -.159 | -.163 | -.291 | -.127 | -.122 | -.125 | -.141 | -.371 |
| .850 | -.077 | -.074 | -.080 | -.086 | -.209 | -.042 | -.030 | -.026 | -.043 | -.269 |
| .900 | -.041 | -.020 | -.030 | -.037 | -.144 | -.003 | .025 | .026 | .013 | -.198 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.061 | -.008 | -.056 | .463 | .767 | -.949 | -.056 | .349 | .564 | .704 |
| .075 | -.348 | -.135 | -.004 | .310 | .517 | -.502 | -.134 | .144 | .344 | .523 |
| .150 | -.377 | -.149 | -.012 | .210 | .372 | -.391 | -.151 | .053 | .216 | .379 |
| .250 | -.292 | -.122 | -.030 | .152 | .282 | -.348 | -.183 | -.017 | .116 | .257 |
| .350 | -.278 | -.146 | -.064 | .070 | .178 | -.336 | -.204 | -.074 | .043 | .169 |
| .450 | -.263 | -.168 | -.090 | .006 | .093 | -.319 | -.228 | -.123 | -.038 | .070 |
| .550 | -.231 | -.165 | -.090 | -.023 | .050 | -.275 | -.219 | -.137 | -.068 | .015 |
| .650 | -.192 | -.135 | -.076 | -.024 | .037 | -.212 | -.180 | -.115 | -.066 | -.012 |
| .750 | -.170 | -.125 | -.064 | -.033 | .005 | -.128 | -.095 | -.062 | -.034 | -.019 |
| .850 | -.086 | -.050 | -.013 | .010 | .012 | -.031 | -.004 | .013 | .022 | -.015 |
| .900 | -.047 | -.018 | -.009 | .022 | -.001 | -.000 | .018 | .024 | .027 | -.039 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .344 | .658 | .352 | -.120 | -.599 | .331 | .574 | .197 | -.258 | -.597 |
| .025 | -.251 | -.190 | -.263 | -.598 | -.791 | .077 | -.339 | -.112 | -.821 | -.553 |
| .075 | .084 | -.209 | -.705 | -.387 | -.757 | -.115 | -.333 | -.741 | -.821 | -.556 |
| .150 | -.037 | -.230 | -.481 | -.100 | -.722 | -.224 | -.241 | -.434 | -.814 | -.566 |
| .250 | -.119 | -.241 | -.366 | -.836 | -.701 | -.135 | -.156 | -.270 | -.701 | -.570 |
| .350 | -.185 | -.267 | -.319 | -.571 | -.677 | | | | | |
| .450 | -.233 | -.277 | -.295 | -.370 | -.655 | | | | | |
| .550 | -.234 | -.252 | -.250 | -.268 | -.621 | | | | | |
| .650 | -.185 | -.176 | -.176 | -.176 | -.592 | | | | | |
| .750 | -.118 | -.088 | -.092 | -.094 | -.548 | | | | | |
| .850 | -.048 | -.013 | -.020 | -.026 | -.491 | | | | | |
| .900 | -.016 | .021 | .020 | .014 | -.471 | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.204 | -.071 | .355 | .547 | .656 | -1.224 | -.194 | .176 | .339 | .430 |
| .075 | -.537 | -.159 | .142 | .337 | .495 | -.647 | -.293 | -.080 | .082 | .223 |
| .150 | -.445 | -.172 | .047 | .207 | .359 | -.327 | -.235 | -.182 | -.106 | .019 |
| .250 | -.397 | -.219 | -.056 | .087 | .223 | | | | | |
| .350 | -.358 | -.250 | -.123 | -.013 | .110 | | | | | |
| .450 | -.324 | -.260 | -.167 | -.080 | .023 | | | | | |
| .550 | -.274 | -.231 | -.167 | -.108 | -.045 | | | | | |
| .650 | -.195 | -.182 | -.125 | -.093 | -.069 | | | | | |
| .750 | -.111 | -.071 | -.067 | -.058 | -.090 | | | | | |
| .850 | -.009 | .019 | .019 | .012 | -.080 | | | | | |
| .900 | .020 | .045 | .040 | .033 | -.114 | | | | | |

TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(i) $\alpha = 9.7^\circ$; $M = 0.90$.

| X C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .340 | .876 | .417 | -.021 | | .521 | .696 | -.564 | -.145 | |
| .025 | -.149 | -.128 | .002 | -.448 | | .254 | -.156 | -.1015 | -.1357 | |
| .075 | -.035 | -.162 | -.231 | -.435 | | .086 | -.212 | -.492 | -.1211 | |
| .150 | -.055 | -.228 | -.392 | -.536 | | .004 | -.214 | -.486 | -.750 | |
| .250 | -.064 | -.177 | -.301 | -.482 | | -.061 | -.225 | -.358 | -.667 | |
| .350 | -.094 | -.185 | -.264 | -.406 | | -.129 | -.270 | -.378 | -.529 | |
| .450 | -.123 | -.227 | -.277 | -.347 | | -.203 | -.324 | -.393 | -.365 | |
| .550 | -.137 | -.258 | -.271 | -.276 | | -.208 | -.333 | -.290 | -.336 | |
| .650 | -.125 | -.232 | -.213 | -.242 | | -.186 | -.322 | -.221 | -.277 | |
| .750 | -.121 | -.241 | -.195 | -.207 | | -.123 | -.161 | -.139 | -.172 | |
| .850 | -.060 | -.114 | -.099 | -.112 | | -.025 | -.032 | -.030 | -.056 | |
| .900 | -.018 | -.040 | -.040 | -.052 | | -.021 | -.024 | -.026 | -.000 | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .062 | -.019 | -.095 | .436 | | -.844 | -.072 | .327 | .555 | |
| .075 | -.266 | -.164 | -.008 | .298 | | -.535 | -.161 | .126 | .338 | |
| .150 | .375 | -.189 | -.011 | .203 | | -.415 | -.182 | .034 | .211 | |
| .250 | -.289 | -.162 | -.036 | .144 | | -.337 | -.204 | -.032 | .109 | |
| .350 | -.271 | -.187 | -.072 | .059 | | -.358 | -.242 | -.097 | .030 | |
| .450 | -.274 | -.211 | -.101 | -.011 | | -.361 | -.292 | -.157 | -.059 | |
| .550 | -.240 | -.223 | -.109 | -.038 | | -.271 | -.308 | -.184 | -.095 | |
| .650 | -.189 | -.202 | -.099 | -.039 | | -.207 | -.290 | -.159 | -.097 | |
| .750 | -.172 | -.208 | -.095 | -.056 | | -.111 | -.140 | -.089 | -.063 | |
| .850 | -.071 | -.092 | -.032 | -.013 | | -.009 | -.015 | -.003 | .000 | |
| .900 | -.028 | -.046 | -.010 | -.001 | | -.027 | -.016 | -.012 | .008 | |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .406 | .646 | .435 | .020 | | .378 | .569 | .273 | -.145 | |
| .025 | -.263 | -.200 | -1.169 | -.1427 | | .089 | -.388 | -.1203 | -.960 | |
| .075 | .094 | -.229 | -.978 | -.1299 | | -.096 | -.333 | -.1101 | -.879 | |
| .150 | -.016 | -.256 | -.489 | -.105 | | -.319 | -.405 | -.662 | -.857 | |
| .250 | -.104 | -.279 | -.444 | .852 | | -.139 | -.219 | -.219 | -.751 | |
| .350 | -.190 | -.341 | -.472 | -.676 | | | | | | |
| .450 | -.254 | -.416 | -.285 | -.529 | | | | | | |
| .550 | -.247 | -.364 | -.256 | -.404 | | | | | | |
| .650 | -.177 | -.210 | -.184 | .261 | | | | | | |
| .750 | -.094 | -.084 | -.093 | .140 | | | | | | |
| .850 | -.021 | -.009 | -.015 | -.051 | | | | | | |
| .900 | -.014 | .031 | .024 | -.008 | | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.079 | -.090 | .327 | .532 | | -.150 | -.221 | .153 | .330 | |
| .075 | -.779 | -.179 | .121 | .324 | | -.1000 | -.357 | -.099 | .071 | |
| .150 | -.412 | -.199 | .028 | .198 | | -.396 | -.389 | -.312 | -.161 | |
| .250 | -.436 | -.261 | -.075 | .070 | | | | | | |
| .350 | -.447 | -.324 | -.168 | -.034 | | | | | | |
| .450 | -.274 | -.383 | -.240 | -.118 | | | | | | |
| .550 | -.255 | -.340 | -.231 | -.163 | | | | | | |
| .650 | -.170 | -.225 | -.152 | -.140 | | | | | | |
| .750 | -.086 | -.076 | -.088 | -.090 | | | | | | |
| .850 | -.019 | .020 | .010 | -.008 | | | | | | |
| .900 | -.054 | .053 | .038 | .012 | | | | | | |

CONT'D.

TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(j) $\alpha = 9.7^\circ$; $M = 0.92$.

| $\frac{x}{C_v}$ | C_p for - | | | | C_p for - | | | | |
|-------------------|----------------------|-------|-------------------|--|---------------------|-------|---------------------|--|----------------------|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | | $\beta = 7.9^\circ$ | | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | |
| .000 | .322 | .889 | .430 | | .536 | .714 | .577 | | |
| .025 | -.147 | -.115 | .006 | | .261 | -.141 | -.1018 | | |
| .075 | -.026 | -.145 | -.228 | | .094 | -.194 | -.479 | | |
| .150 | -.043 | -.210 | -.386 | | .010 | -.198 | -.465 | | |
| .250 | -.055 | -.156 | -.287 | | -.055 | -.208 | -.347 | | |
| .350 | -.087 | -.163 | -.255 | | -.124 | -.252 | -.366 | | |
| .450 | -.121 | -.204 | -.271 | | -.198 | -.307 | -.382 | | |
| .550 | -.135 | -.236 | -.252 | | -.221 | -.307 | -.265 | | |
| .650 | -.134 | -.207 | -.199 | | -.215 | -.271 | -.211 | | |
| .750 | -.131 | -.199 | -.185 | | -.129 | -.136 | -.129 | | |
| .850 | -.071 | -.088 | -.092 | | -.028 | -.022 | -.020 | | |
| .900 | -.023 | -.026 | -.030 | | .024 | .037 | .038 | | |
| <i>Right side</i> | | | | | | | | | |
| .025 | .093 | -.003 | -.086 | | -.818 | -.057 | .335 | | |
| .075 | -.232 | -.146 | -.007 | | -.534 | -.142 | .136 | | |
| .150 | -.360 | -.170 | -.003 | | -.455 | -.165 | .042 | | |
| .250 | -.301 | -.145 | -.033 | | -.339 | -.188 | -.026 | | |
| .350 | -.278 | -.170 | -.065 | | -.363 | -.229 | -.085 | | |
| .450 | -.279 | -.194 | -.092 | | -.375 | -.271 | -.145 | | |
| .550 | -.256 | -.202 | -.100 | | -.324 | -.282 | -.171 | | |
| .650 | -.201 | -.175 | -.088 | | -.201 | -.239 | -.140 | | |
| .750 | -.182 | -.170 | -.081 | | -.109 | -.105 | -.078 | | |
| .850 | -.079 | -.070 | -.022 | | -.006 | .000 | .009 | | |
| .900 | -.028 | -.028 | -.001 | | .032 | .028 | .025 | | |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | |
| <i>Left side</i> | | | | | | | | | |
| .000 | .418 | .660 | .444 | | .385 | .581 | .284 | | |
| .025 | .265 | -.190 | -.177 | | .098 | -.385 | -.249 | | |
| .075 | .098 | -.215 | -.975 | | -.084 | -.325 | -.097 | | |
| .150 | -.010 | -.240 | -.450 | | -.328 | -.381 | -.568 | | |
| .250 | -.098 | -.262 | -.438 | | -.225 | -.177 | -.185 | | |
| .350 | -.192 | -.329 | -.451 | | | | | | |
| .450 | -.282 | -.393 | -.255 | | | | | | |
| .550 | -.287 | -.324 | -.255 | | | | | | |
| .650 | -.188 | -.182 | -.176 | | | | | | |
| .750 | -.092 | -.079 | -.086 | | | | | | |
| .850 | -.015 | -.001 | -.005 | | | | | | |
| .900 | .019 | .039 | .035 | | | | | | |
| <i>Right side</i> | | | | | | | | | |
| .025 | -.054 | -.073 | .340 | | -.125 | -.207 | .161 | | |
| .075 | -.816 | -.165 | .134 | | -.011 | -.351 | -.092 | | |
| .150 | -.422 | -.183 | .038 | | -.512 | -.364 | -.306 | | |
| .250 | -.426 | -.246 | -.066 | | | | | | |
| .350 | -.468 | -.310 | -.156 | | | | | | |
| .450 | -.373 | -.352 | -.225 | | | | | | |
| .550 | -.227 | -.299 | -.211 | | | | | | |
| .650 | -.162 | -.186 | -.149 | | | | | | |
| .750 | -.079 | -.071 | -.078 | | | | | | |
| .850 | .026 | .029 | .019 | | | | | | |
| .900 | .063 | .062 | .051 | | | | | | |

TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(k) $\alpha = 15.6^\circ$; $M = 0.60$.

| x C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .790 | .804 | .825 | .164 | .446 | .238 | .673 | .281 | .667 | .469 |
| .025 | -.300 | -.169 | -.186 | -.409 | -.144 | .302 | -.133 | -.697 | -.522 | -.949 |
| .075 | -.146 | -.169 | -.277 | -.391 | -.728 | .114 | -.172 | -.487 | -.013 | -.2078 |
| .150 | -.117 | -.194 | -.313 | -.402 | -.563 | .021 | -.181 | -.372 | -.520 | -.1408 |
| .250 | -.083 | -.147 | -.238 | -.300 | -.394 | -.054 | -.192 | -.320 | -.425 | -.527 |
| .350 | -.097 | -.147 | -.218 | -.268 | -.338 | -.106 | -.210 | -.308 | -.391 | -.516 |
| .450 | -.126 | -.176 | -.227 | -.259 | -.320 | -.146 | -.235 | -.297 | -.345 | -.471 |
| .550 | -.144 | -.183 | -.218 | -.241 | -.304 | -.149 | -.212 | -.250 | -.291 | -.399 |
| .650 | -.137 | -.156 | -.186 | -.194 | -.265 | -.133 | -.181 | -.207 | -.239 | -.326 |
| .750 | -.126 | -.145 | -.159 | -.162 | -.225 | -.101 | -.129 | -.141 | -.167 | -.243 |
| .850 | -.083 | -.089 | -.096 | -.097 | -.155 | -.045 | -.062 | -.067 | -.101 | -.157 |
| .900 | -.054 | -.048 | -.055 | -.060 | -.098 | -.178 | -.190 | -.184 | -.183 | -.162 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.081 | -.084 | -.202 | .241 | .563 | -.678 | -.113 | .337 | .535 | .694 |
| .075 | -.282 | -.176 | -.166 | .105 | .299 | -.468 | -.165 | .125 | .299 | .473 |
| .150 | -.291 | -.174 | -.114 | .051 | .159 | -.368 | -.178 | .021 | .159 | .297 |
| .250 | -.235 | -.149 | -.087 | .023 | .084 | -.409 | -.185 | -.042 | .066 | .166 |
| .350 | -.226 | -.151 | -.105 | -.017 | .021 | -.287 | -.201 | -.094 | -.017 | .066 |
| .450 | -.226 | -.176 | -.130 | -.060 | -.031 | -.275 | -.219 | -.132 | -.085 | -.015 |
| .550 | -.203 | -.169 | -.137 | -.083 | -.055 | -.246 | -.210 | -.146 | -.115 | -.062 |
| .650 | -.169 | -.147 | -.123 | -.087 | -.062 | -.189 | -.169 | -.123 | -.106 | -.076 |
| .750 | -.142 | -.127 | -.114 | -.087 | -.071 | -.121 | -.111 | -.083 | -.083 | -.067 |
| .850 | -.078 | -.066 | -.071 | -.047 | -.046 | -.045 | -.037 | -.017 | -.026 | -.040 |
| .900 | -.045 | -.044 | -.049 | -.029 | -.028 | -.022 | -.019 | -.015 | -.029 | -.044 |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | -.013 | .608 | -.010 | -.814 | -.1304 | .103 | .536 | -.130 | -.601 | -.886 |
| .025 | -.317 | -.160 | -.1069 | -.1354 | -.1134 | .168 | -.237 | -.979 | -.780 | -.748 |
| .075 | -.134 | -.187 | -.577 | -.1334 | -.1141 | -.029 | -.226 | -.493 | -.764 | -.751 |
| .150 | -.014 | -.205 | -.432 | -.1253 | -.1116 | -.124 | -.203 | -.326 | -.712 | -.742 |
| .250 | -.431 | | -.042 | -.490 | -.981 | -.101 | -.129 | -.238 | -.628 | -.703 |
| .350 | -.121 | -.226 | -.317 | -.373 | -.1017 | | | | | |
| .450 | -.158 | -.237 | -.286 | -.282 | -.873 | | | | | |
| .550 | -.173 | -.219 | -.250 | -.253 | -.701 | | | | | |
| .650 | -.142 | -.174 | -.186 | -.196 | -.523 | -.133 | -.111 | -.159 | -.420 | -.588 |
| .750 | -.097 | -.104 | -.123 | -.128 | -.365 | -.103 | -.077 | -.132 | -.364 | -.561 |
| .850 | -.060 | -.062 | -.065 | -.069 | -.250 | -.074 | -.044 | -.101 | -.309 | -.523 |
| .900 | -.042 | -.030 | -.042 | -.042 | -.202 | -.047 | -.019 | -.076 | -.275 | -.498 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.990 | -.124 | .355 | .548 | .665 | -.827 | -.201 | .188 | .313 | .387 |
| .075 | -.565 | -.181 | .127 | .336 | .509 | -.495 | -.241 | -.051 | .062 | .200 |
| .150 | -.397 | -.183 | .026 | .184 | .362 | -.327 | -.210 | -.139 | -.078 | .021 |
| .250 | -.352 | -.205 | -.062 | .069 | .220 | | | | | |
| .350 | -.314 | -.221 | -.121 | -.022 | .112 | | | | | |
| .450 | -.280 | -.226 | -.150 | -.078 | .033 | | | | | |
| .550 | -.235 | -.203 | -.155 | -.101 | -.010 | | | | | |
| .650 | -.178 | -.165 | -.130 | -.097 | -.033 | -.135 | -.115 | -.119 | -.126 | -.119 |
| .750 | -.117 | -.100 | -.092 | -.074 | -.040 | -.126 | -.089 | -.114 | -.137 | -.159 |
| .850 | -.035 | -.023 | -.022 | -.017 | -.017 | -.074 | -.019 | -.055 | -.090 | -.150 |
| .900 | -.008 | .004 | -.001 | -.002 | -.019 | -.051 | -.010 | -.042 | -.087 | -.180 |

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TABLE IV. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(I) $\alpha = 15.8^\circ$; $M = 0.80$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .358 | .839 | .695 | .547 | .146 | .442 | .729 | .511 | .125 | -.197 |
| .025 | -.1020 | -.199 | .246 | -.075 | -.097 | .294 | -.158 | -.145 | -.1677 | -.1658 |
| .075 | -.287 | -.208 | -.128 | -.260 | -.646 | .098 | -.213 | -.540 | -.955 | -.1445 |
| .150 | -.138 | -.252 | -.355 | -.453 | -.595 | .004 | -.217 | -.428 | -.676 | -.1191 |
| .250 | -.101 | -.199 | -.283 | -.348 | -.430 | -.070 | -.231 | -.373 | -.473 | -.724 |
| .350 | -.107 | -.184 | -.257 | -.305 | -.367 | -.144 | -.261 | -.361 | -.447 | -.545 |
| .450 | -.145 | -.208 | -.261 | -.305 | -.348 | -.200 | -.293 | -.346 | -.402 | -.522 |
| .550 | -.181 | -.228 | -.255 | -.293 | -.334 | -.201 | -.268 | -.299 | -.348 | -.486 |
| .650 | -.188 | -.204 | -.222 | -.263 | -.331 | -.192 | -.235 | -.246 | -.292 | -.445 |
| .750 | -.200 | -.199 | -.210 | -.230 | -.310 | -.148 | -.167 | -.170 | -.206 | -.360 |
| .850 | -.151 | -.128 | -.137 | -.147 | -.214 | -.077 | -.077 | -.081 | -.116 | -.251 |
| .900 | -.106 | -.072 | -.086 | -.095 | -.155 | -.171 | -.185 | -.170 | -.152 | -.138 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .343 | -.095 | -.957 | -.111 | .339 | -.1118 | -.134 | .333 | .500 | .624 |
| .075 | -.124 | -.222 | -.267 | -.092 | .107 | -.520 | -.201 | .104 | .253 | .371 |
| .150 | -.325 | -.232 | -.125 | -.051 | .018 | -.420 | -.213 | .004 | .122 | .214 |
| .250 | -.278 | -.196 | -.089 | -.045 | -.004 | -.360 | -.220 | -.061 | .030 | .112 |
| .350 | -.269 | -.188 | -.105 | -.060 | -.019 | -.342 | -.244 | -.119 | -.046 | .030 |
| .450 | -.262 | -.214 | -.149 | -.087 | -.040 | -.323 | -.268 | -.176 | -.122 | -.046 |
| .550 | -.233 | -.207 | -.169 | -.104 | -.057 | -.287 | -.258 | -.195 | -.156 | -.084 |
| .650 | -.203 | -.182 | -.175 | -.110 | -.064 | -.225 | -.211 | -.176 | -.147 | -.096 |
| .750 | -.192 | -.182 | -.183 | -.123 | -.086 | -.145 | -.143 | -.125 | -.119 | -.092 |
| .850 | -.112 | -.099 | -.125 | -.081 | -.064 | -.053 | -.054 | -.052 | -.063 | -.069 |
| .900 | -.073 | -.062 | -.093 | -.061 | -.058 | -.021 | -.027 | -.034 | -.060 | -.090 |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .251 | .649 | .286 | -.233 | -.744 | .223 | .557 | .081 | -.439 | -.933 |
| .025 | .319 | -.178 | -.1343 | -.1486 | -.962 | .155 | -.306 | -.170 | -.802 | -.697 |
| .075 | .131 | -.214 | -.742 | -.1396 | -.955 | -.056 | -.294 | -.767 | -.798 | -.694 |
| .150 | .007 | -.243 | -.514 | -.146 | -.912 | -.177 | -.249 | -.411 | -.769 | -.700 |
| .250 | -.218 | -.219 | -.275 | -.590 | -.843 | -.117 | -.146 | -.289 | -.695 | -.697 |
| .350 | -.156 | -.277 | -.360 | -.628 | -.852 | | | | | |
| .450 | -.209 | -.290 | -.336 | -.411 | -.792 | | | | | |
| .550 | -.224 | -.274 | -.292 | -.314 | -.720 | | | | | |
| .650 | -.188 | -.213 | -.220 | -.227 | -.631 | -.145 | -.121 | -.183 | -.486 | -.589 |
| .750 | -.127 | -.131 | -.140 | -.143 | -.530 | -.109 | -.066 | -.143 | -.430 | -.552 |
| .850 | -.067 | -.059 | -.066 | -.070 | -.421 | -.071 | -.024 | -.101 | -.364 | -.515 |
| .900 | -.035 | -.026 | -.031 | -.039 | -.370 | -.042 | -.000 | -.073 | -.326 | -.497 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.1429 | -.143 | .351 | .552 | .686 | -.1000 | -.241 | .174 | .341 | .436 |
| .075 | -.641 | -.216 | .125 | .332 | .506 | -.727 | -.303 | -.087 | .083 | .6235 |
| .150 | -.467 | -.210 | .019 | .189 | .357 | -.426 | -.246 | -.193 | -.098 | .039 |
| .250 | -.399 | -.243 | -.084 | .064 | .217 | | | | | |
| .350 | -.361 | -.279 | -.157 | -.039 | .103 | | | | | |
| .450 | -.320 | -.282 | -.204 | -.110 | .017 | | | | | |
| .550 | -.271 | -.255 | -.210 | -.141 | -.037 | | | | | |
| .650 | -.206 | -.195 | -.173 | -.135 | -.060 | -.118 | -.112 | -.131 | -.152 | -.150 |
| .750 | -.127 | -.124 | -.123 | -.102 | -.069 | -.138 | -.078 | -.120 | -.161 | -.192 |
| .850 | -.030 | -.029 | -.033 | -.034 | -.054 | -.070 | -.003 | -.051 | -.101 | -.174 |
| .900 | -.007 | -.009 | -.007 | -.015 | -.076 | -.044 | -.014 | -.034 | -.105 | -.201 |

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TABLE IV.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE MIDWING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Concluded

(m) $\alpha = 15.9^\circ$; $M = 0.85$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .375 | .858 | .699 | .464 | | .471 | .736 | .548 | .248 | |
| .025 | -1.031 | -.225 | .304 | -.164 | | .265 | -.190 | -1.215 | -1.482 | |
| .075 | -.496 | -.239 | -.066 | -.289 | | .071 | -.250 | -.607 | -.908 | |
| .150 | -.153 | -.296 | -.380 | -.469 | | -.018 | -.252 | -.486 | -.793 | |
| .250 | -.120 | -.237 | -.316 | -.428 | | -.095 | -.260 | -.396 | -.601 | |
| .350 | -.126 | -.210 | -.288 | -.356 | | -.177 | -.296 | -.398 | -.406 | |
| .450 | -.154 | -.243 | -.296 | -.322 | | -.234 | -.332 | -.371 | -.462 | |
| .550 | -.183 | -.263 | -.279 | -.305 | | -.245 | -.313 | -.322 | -.397 | |
| .650 | -.194 | -.239 | -.242 | -.301 | | -.238 | -.280 | -.275 | -.332 | |
| .750 | -.206 | -.242 | -.249 | -.284 | | -.186 | -.202 | -.194 | -.232 | |
| .850 | -.156 | -.159 | -.166 | -.181 | | -.103 | -.101 | -.099 | -.130 | |
| .900 | -.109 | -.100 | -.106 | -.118 | | -.179 | -.198 | -.160 | -.157 | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .390 | -.108 | -.967 | -.058 | | -1.127 | -.146 | .321 | .461 | |
| .075 | -.072 | -.253 | -.445 | -.088 | | -.628 | -.230 | .091 | .226 | |
| .150 | -.370 | -.271 | -.127 | -.071 | | -.501 | -.239 | -.010 | .097 | |
| .250 | -.332 | -.230 | -.102 | -.072 | | -.401 | -.246 | -.078 | .007 | |
| .350 | -.313 | -.216 | -.116 | -.089 | | -.386 | -.277 | -.142 | -.074 | |
| .450 | -.296 | -.239 | -.145 | -.116 | | -.357 | -.308 | -.208 | -.153 | |
| .550 | -.259 | -.239 | -.163 | -.129 | | -.319 | -.301 | -.231 | -.186 | |
| .650 | -.230 | -.213 | -.171 | -.133 | | -.259 | -.256 | -.211 | -.180 | |
| .750 | -.234 | -.223 | -.180 | -.154 | | -.174 | -.175 | -.154 | -.145 | |
| .850 | -.146 | -.132 | -.123 | -.108 | | -.078 | -.074 | -.072 | -.084 | |
| .900 | -.108 | -.091 | -.092 | -.091 | | -.040 | -.048 | -.049 | -.074 | |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .304 | .649 | .349 | -.074 | | .247 | .551 | .131 | .376 | |
| .025 | .294 | -.205 | -1.379 | -1.613 | | .124 | -.361 | -1.329 | -.952 | |
| .075 | .108 | -.244 | -1.145 | -1.377 | | -.091 | -.378 | -1.020 | -.929 | |
| .150 | -.021 | -.273 | -.529 | -1.130 | | -.274 | -.288 | -.557 | -.865 | |
| .250 | -.569 | -.519 | -.489 | -.664 | | -.160 | -.173 | -.262 | -.801 | |
| .350 | -.197 | -.325 | -.363 | -.702 | | | | | | |
| .450 | -.261 | -.350 | -.362 | -.478 | | | | | | |
| .550 | -.279 | -.327 | -.323 | -.354 | | | | | | |
| .650 | -.231 | -.243 | -.240 | -.254 | | | | | | |
| .750 | -.156 | -.156 | -.153 | -.162 | | | | | | |
| .850 | -.084 | -.075 | -.074 | -.079 | | | | | | |
| .900 | -.054 | -.043 | -.035 | -.042 | | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.374 | -.158 | .332 | .525 | | -1.413 | -.266 | .153 | .328 | |
| .075 | -1.118 | -.236 | .114 | .302 | | -1.021 | -.375 | -.122 | .061 | |
| .150 | -.482 | -.234 | .003 | .163 | | -.529 | -.291 | -.285 | -.147 | |
| .250 | -.468 | -.281 | -.101 | .036 | | | | | | |
| .350 | -.379 | -.324 | -.191 | -.072 | | | | | | |
| .450 | -.354 | -.332 | -.245 | .152 | | | | | | |
| .550 | -.310 | -.301 | -.252 | -.186 | | | | | | |
| .650 | -.232 | -.230 | -.208 | -.170 | | | | | | |
| .750 | -.146 | -.146 | -.146 | -.132 | | | | | | |
| .850 | -.044 | -.040 | -.048 | -.052 | | | | | | |
| .900 | -.006 | -.006 | -.021 | -.031 | | | | | | |

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TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL

(a) $\alpha = 0^\circ$; $M = 0.60$.

| $\frac{X}{C_V}$ | C_p for - | | | | | | C_p for - | | | | | |
|-----------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|--|--|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | | |
| | $Z/b_V = 0.11$ | | | | | $Z/b_V = 0.38$ | | | | | | |
| Left side | | | | | | | | | | | | |
| .000 | .750 | .643 | .601 | -.006 | -.868 | .403 | .734 | .497 | -.247 | -1.071 | | |
| .025 | .209 | -.072 | -.437 | -.809 | -1.847 | .285 | -.072 | -.503 | -1.156 | -1.326 | | |
| .075 | .089 | -.087 | -.281 | -.505 | -.788 | .116 | -.115 | -.362 | -.829 | -1.282 | | |
| .150 | .012 | -.119 | -.240 | -.376 | -.553 | .039 | -.126 | -.272 | -.476 | -1.285 | | |
| .250 | .003 | -.085 | -.158 | -.240 | -.362 | -.019 | -.137 | -.240 | -.351 | -1.030 | | |
| .350 | -.022 | -.097 | -.140 | -.206 | -.298 | -.065 | -.153 | -.235 | -.303 | -.558 | | |
| .450 | -.053 | -.106 | -.140 | -.183 | -.260 | -.105 | -.169 | -.219 | -.263 | -.317 | | |
| .550 | -.058 | -.097 | -.117 | -.151 | -.219 | -.085 | -.133 | -.167 | -.199 | -.239 | | |
| .650 | -.022 | -.058 | -.081 | -.115 | -.194 | -.065 | -.097 | -.117 | -.138 | -.198 | | |
| .750 | -.004 | -.031 | -.045 | -.077 | -.146 | -.024 | -.042 | -.056 | -.072 | -.141 | | |
| .850 | .030 | .012 | .010 | -.022 | -.073 | .030 | .017 | .014 | .007 | -.052 | | |
| .900 | .053 | .048 | .044 | .019 | -.027 | .060 | .055 | .053 | .048 | -.002 | | |
| Right side | | | | | | | | | | | | |
| .025 | -.347 | -.026 | .252 | .474 | .706 | -.627 | -.063 | .313 | .565 | .740 | | |
| .075 | -.297 | -.101 | .080 | .261 | .467 | -.349 | -.119 | .121 | .323 | .504 | | |
| .150 | -.229 | -.103 | .019 | .162 | .330 | -.279 | -.124 | .035 | .189 | .351 | | |
| .250 | -.159 | -.083 | .001 | .114 | .248 | -.227 | -.133 | -.018 | .100 | .232 | | |
| .350 | -.148 | -.097 | -.029 | .057 | .164 | -.213 | -.146 | -.058 | .044 | .150 | | |
| .450 | -.139 | -.106 | -.061 | .016 | .109 | -.193 | -.149 | -.083 | -.006 | .087 | | |
| .550 | -.105 | -.087 | -.049 | .014 | .091 | -.162 | -.133 | -.077 | -.020 | .055 | | |
| .650 | -.067 | -.045 | -.018 | .039 | .105 | -.107 | -.085 | -.058 | -.004 | .050 | | |
| .750 | -.031 | -.017 | .012 | .053 | .105 | -.040 | -.031 | -.018 | .030 | .062 | | |
| .850 | .026 | .032 | .057 | .089 | .121 | .039 | .041 | .071 | .073 | .087 | | |
| .900 | .053 | .055 | .064 | .089 | .109 | .062 | .060 | .062 | .073 | .080 | | |
| $Z/b_V = 0.66$ | | | | | | $Z/b_V = 0.93$ | | | | | | |
| Left side | | | | | | | | | | | | |
| .000 | .297 | .718 | .386 | -.235 | -.658 | .414 | .677 | .316 | -.163 | -.437 | | |
| .025 | .310 | -.106 | -.666 | -.993 | -.840 | .188 | -.192 | -.605 | -.793 | -.567 | | |
| .075 | .134 | -.135 | -.430 | -.886 | -.815 | .019 | -.160 | -.369 | -.770 | -.556 | | |
| .150 | .033 | -.155 | -.335 | -.702 | -.786 | -.053 | -.142 | -.258 | -.655 | -.594 | | |
| .250 | -.033 | -.158 | -.267 | -.448 | -.731 | -.033 | -.090 | -.181 | -.458 | -.563 | | |
| .350 | -.083 | -.169 | -.240 | -.328 | -.679 | | | | | | | |
| .450 | -.110 | -.178 | -.222 | -.267 | -.631 | | | | | | | |
| .550 | -.112 | -.151 | -.185 | -.208 | -.563 | | | | | | | |
| .650 | -.085 | -.110 | -.117 | -.149 | -.481 | -.076 | -.076 | -.102 | -.267 | -.401 | | |
| .750 | -.042 | -.045 | -.058 | -.083 | -.394 | -.055 | -.031 | -.067 | -.253 | -.369 | | |
| .850 | .021 | .008 | -.002 | -.020 | -.303 | -.028 | -.004 | -.049 | -.240 | -.335 | | |
| .900 | .035 | .030 | .030 | .007 | -.260 | -.010 | .019 | -.031 | -.206 | -.328 | | |
| Right side | | | | | | | | | | | | |
| .025 | -.631 | -.083 | .338 | .565 | .688 | -.532 | -.142 | .209 | .377 | .463 | | |
| .075 | -.435 | -.137 | .123 | .327 | .485 | -.365 | -.176 | -.002 | .125 | .219 | | |
| .150 | -.306 | -.137 | .032 | .196 | .328 | -.252 | -.146 | -.065 | -.006 | .071 | | |
| .250 | -.263 | -.160 | -.033 | .084 | .203 | | | | | | | |
| .350 | -.241 | -.164 | -.081 | .014 | .105 | | | | | | | |
| .450 | -.209 | -.167 | -.106 | -.027 | .041 | | | | | | | |
| .550 | -.164 | -.144 | -.099 | -.047 | .005 | | | | | | | |
| .650 | -.112 | -.103 | -.074 | -.029 | .002 | -.080 | -.069 | -.067 | -.072 | -.075 | | |
| .750 | -.046 | -.035 | -.033 | -.002 | .005 | -.060 | -.038 | -.070 | -.070 | -.102 | | |
| .850 | .028 | .032 | .053 | .055 | .018 | -.015 | .014 | -.011 | -.020 | -.086 | | |
| .900 | .057 | .055 | .053 | .066 | -.004 | -.006 | .030 | .003 | -.020 | -.118 | | |

TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(b) $\alpha = 0^\circ$; $M = 0.80$.

| $\frac{X}{C_V}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_V = 0.11$ | | | | | $z/b_V = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .831 | .655 | .709 | .411 | -.077 | .539 | .772 | .633 | .225 | -.345 |
| .025 | .222 | -.045 | -.419 | -.741 | -1.500 | .304 | -.052 | -.577 | -1.166 | -1.228 |
| .075 | .107 | -.076 | -.285 | -.540 | -1.061 | .130 | -.114 | -.377 | -.883 | -1.181 |
| .150 | .025 | -.116 | -.253 | -.423 | -.633 | .046 | -.131 | -.291 | -.587 | -1.039 |
| .250 | .007 | -.087 | -.167 | -.263 | -.402 | -.018 | -.146 | -.256 | -.384 | -.878 |
| .350 | -.024 | -.101 | -.148 | -.213 | -.323 | -.075 | -.167 | -.248 | -.318 | -.708 |
| .450 | -.065 | -.117 | -.152 | -.195 | -.281 | -.124 | -.198 | -.234 | -.271 | -.519 |
| .550 | -.069 | -.108 | -.131 | -.161 | -.240 | -.109 | -.152 | -.180 | -.202 | -.377 |
| .650 | -.030 | -.067 | -.088 | -.123 | -.205 | -.075 | -.111 | -.120 | -.135 | -.275 |
| .750 | -.009 | -.036 | -.046 | -.082 | -.161 | -.028 | -.045 | -.049 | -.061 | -.179 |
| .850 | .037 | .020 | .018 | -.017 | -.083 | .042 | .034 | .030 | .023 | -.076 |
| .900 | .058 | .055 | .050 | .026 | -.035 | .076 | .075 | .078 | .073 | -.023 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.320 | -.004 | .271 | .478 | .683 | -.717 | -.061 | .323 | .557 | .731 |
| .075 | -.306 | -.090 | .090 | .269 | .464 | -.377 | -.123 | .129 | .323 | .509 |
| .150 | -.245 | -.110 | .024 | .167 | .339 | -.295 | -.133 | .038 | .195 | .360 |
| .250 | -.171 | -.092 | .002 | .116 | .256 | -.250 | -.143 | -.018 | .105 | .242 |
| .350 | -.159 | -.107 | -.038 | .058 | .170 | -.227 | -.157 | -.067 | .038 | .154 |
| .450 | -.148 | -.114 | -.067 | .015 | .108 | -.215 | -.166 | -.097 | -.021 | .084 |
| .550 | -.113 | -.090 | -.058 | .011 | .091 | -.168 | -.142 | -.093 | -.029 | .046 |
| .650 | -.066 | -.051 | -.020 | .037 | .107 | -.104 | -.093 | -.062 | -.008 | .043 |
| .750 | -.034 | -.023 | .008 | .053 | .105 | -.027 | -.020 | -.006 | .026 | .050 |
| .850 | .037 | .039 | .056 | .090 | .120 | .057 | .058 | .067 | .079 | .078 |
| .900 | .060 | .066 | .069 | .097 | .107 | .081 | .072 | .078 | .085 | .063 |
| $z/b_V = 0.66$ | | | | | $z/b_V = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .474 | .749 | .553 | .122 | -.320 | .498 | .707 | .451 | .029 | -.282 |
| .025 | .324 | -.087 | -.935 | -1.125 | -.817 | .180 | -.210 | -1.027 | -.851 | -.547 |
| .075 | .143 | -.134 | -.449 | -.985 | -.810 | .004 | -.186 | -.399 | -.819 | -.568 |
| .150 | .035 | -.167 | -.362 | -.785 | -.788 | -.072 | -.154 | -.269 | -.728 | -.611 |
| .250 | -.042 | -.176 | -.285 | -.519 | -.732 | -.036 | -.087 | -.190 | -.531 | -.550 |
| .350 | -.095 | -.190 | -.253 | -.361 | -.659 | | | | | |
| .450 | -.135 | -.196 | -.233 | -.268 | -.588 | | | | | |
| .550 | -.128 | -.167 | -.183 | -.201 | -.516 | | | | | |
| .650 | -.092 | -.122 | -.119 | -.132 | -.448 | -.071 | -.061 | -.090 | -.294 | -.407 |
| .750 | -.045 | -.022 | -.043 | -.058 | -.374 | -.036 | -.013 | -.049 | -.268 | -.371 |
| .850 | .042 | .028 | .026 | .006 | -.299 | -.007 | .027 | -.021 | -.230 | -.337 |
| .900 | .057 | .049 | .061 | .037 | -.264 | .016 | .051 | -.003 | -.196 | -.322 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.949 | -.073 | .347 | .572 | .708 | -.028 | -.166 | .204 | .382 | .496 |
| .075 | -.459 | -.143 | .135 | .333 | .499 | -.421 | -.208 | -.020 | .110 | .242 |
| .150 | -.332 | -.134 | .043 | .199 | .348 | -.260 | -.167 | -.075 | -.030 | .076 |
| .250 | -.286 | -.164 | -.043 | .084 | .219 | | | | | |
| .350 | -.260 | -.195 | -.096 | .002 | .111 | | | | | |
| .450 | -.226 | -.183 | -.125 | -.049 | .035 | | | | | |
| .550 | -.172 | -.152 | -.119 | -.061 | -.004 | | | | | |
| .650 | -.104 | -.098 | -.081 | -.043 | -.010 | -.059 | -.058 | -.062 | -.067 | -.079 |
| .750 | -.027 | -.031 | -.037 | -.003 | -.013 | -.054 | -.020 | -.046 | -.052 | -.111 |
| .850 | .054 | .058 | .069 | .059 | .005 | .013 | .046 | .023 | .000 | -.089 |
| .900 | .087 | .086 | .084 | .076 | -.018 | .019 | .061 | .034 | .002 | -.115 |

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TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(c) $\alpha = 0^\circ$; $M = 0.85$.

| x C_V | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_V = 0.11$ | | | | | $z/b_V = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .852 | .657 | .744 | .509 | .051 | .582 | .785 | .674 | .338 | -.163 |
| .025 | .224 | -.038 | -.406 | -.659 | -.1334 | .300 | -.051 | -.729 | -.1439 | -.1448 |
| .075 | .109 | -.074 | -.285 | -.606 | -.984 | .126 | -.119 | -.380 | -.251 | -.136 |
| .150 | .016 | .126 | -.259 | -.476 | -.683 | .044 | -.137 | -.303 | -.421 | -.999 |
| .250 | -.002 | -.098 | -.180 | -.286 | -.450 | -.029 | -.159 | -.266 | -.370 | -.840 |
| .350 | -.036 | -.109 | -.163 | -.234 | -.362 | -.090 | -.186 | -.266 | -.310 | -.690 |
| .450 | -.078 | -.132 | -.163 | -.203 | -.315 | -.148 | -.217 | -.249 | -.274 | -.574 |
| .550 | -.085 | -.126 | -.141 | -.169 | -.260 | -.125 | -.177 | -.191 | -.206 | -.452 |
| .650 | -.044 | -.081 | -.100 | -.129 | -.219 | -.091 | -.127 | -.133 | -.143 | -.341 |
| .750 | -.020 | -.047 | -.052 | -.093 | -.173 | -.040 | -.057 | -.054 | -.063 | -.223 |
| .850 | .030 | .014 | .015 | -.022 | -.094 | .040 | .036 | .034 | .025 | -.104 |
| .900 | .052 | .051 | .054 | .024 | -.040 | .078 | .080 | .079 | .075 | -.041 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.308 | .000 | .273 | .478 | .682 | -.766 | -.069 | .315 | .549 | .734 |
| .075 | -.321 | -.096 | .086 | .266 | .467 | -.418 | -.132 | .123 | .317 | .510 |
| .150 | -.260 | -.119 | .020 | .169 | .339 | -.314 | -.143 | .032 | .196 | .362 |
| .250 | -.188 | -.106 | -.002 | .116 | .260 | -.263 | -.156 | -.026 | .100 | .247 |
| .350 | -.176 | -.122 | -.046 | .052 | .173 | -.250 | -.180 | -.081 | .029 | .165 |
| .450 | -.161 | -.133 | -.079 | .002 | .108 | -.232 | -.188 | -.118 | -.029 | .078 |
| .550 | -.122 | -.106 | -.072 | -.004 | .087 | -.183 | -.167 | -.114 | -.042 | .043 |
| .650 | -.078 | -.065 | -.025 | .032 | .102 | -.112 | -.109 | -.079 | -.019 | .037 |
| .750 | -.041 | -.030 | -.006 | .053 | .102 | -.033 | -.025 | -.022 | .024 | .048 |
| .850 | .028 | .034 | .048 | .088 | .112 | .055 | .057 | .068 | .081 | .072 |
| .900 | .062 | .064 | .058 | .095 | .102 | .085 | .077 | .076 | .089 | .055 |
| $z/b_V = 0.66$ | | | | | $z/b_V = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .513 | .759 | .598 | .234 | -.198 | .520 | .705 | .486 | .092 | -.250 |
| .025 | .321 | -.089 | -.020 | -.569 | -.803 | .162 | -.234 | -.124 | -.966 | -.590 |
| .075 | .141 | -.143 | -.443 | -.388 | -.811 | -.027 | -.225 | -.419 | -.937 | -.635 |
| .150 | .027 | -.177 | -.389 | -.196 | -.815 | -.097 | -.179 | -.268 | -.817 | -.656 |
| .250 | -.058 | -.197 | -.299 | -.286 | -.753 | -.054 | -.098 | -.198 | -.580 | -.571 |
| .350 | -.118 | -.214 | -.269 | -.297 | -.669 | | | | | |
| .450 | -.158 | -.220 | -.249 | -.260 | -.580 | | | | | |
| .550 | -.149 | -.183 | -.198 | -.194 | -.500 | | | | | |
| .650 | -.104 | -.137 | -.121 | -.126 | -.429 | -.080 | -.074 | -.091 | -.317 | -.425 |
| .750 | -.054 | -.020 | -.039 | -.051 | -.352 | -.043 | -.024 | -.046 | -.283 | -.389 |
| .850 | .035 | .029 | .029 | .018 | -.279 | -.006 | .024 | -.017 | -.243 | -.350 |
| .900 | .054 | .062 | .053 | -.243 | | .020 | .046 | .000 | -.204 | -.331 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.1061 | -.079 | .341 | .566 | .714 | -.1118 | -.191 | .190 | .380 | .504 |
| .075 | -.435 | -.159 | .125 | .330 | .504 | -.511 | -.242 | -.044 | .095 | .246 |
| .150 | -.358 | -.153 | .039 | .197 | .354 | -.242 | -.181 | -.101 | -.062 | .069 |
| .250 | -.306 | -.193 | -.057 | .078 | .220 | | | | | |
| .350 | -.273 | -.217 | -.118 | -.012 | .111 | | | | | |
| .450 | -.237 | -.208 | -.148 | -.063 | .035 | | | | | |
| .550 | -.186 | -.177 | -.141 | -.079 | -.013 | | | | | |
| .650 | -.108 | -.109 | -.096 | -.051 | -.020 | -.075 | -.064 | -.067 | -.066 | -.088 |
| .750 | -.033 | -.035 | -.047 | -.009 | -.024 | -.063 | -.028 | -.049 | -.055 | -.117 |
| .850 | .058 | .055 | .074 | .066 | -.003 | .003 | .051 | .027 | .006 | -.091 |
| .900 | .094 | .088 | .086 | .079 | -.027 | .018 | .067 | .039 | -.001 | -.119 |

TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(d) $\alpha = 0^\circ$; $M = 0.90$.

| x C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .879 | .659 | .776 | .581 | .180 | .625 | .794 | .714 | .420 | .027 |
| .025 | .232 | -.031 | -.387 | -.624 | -1.153 | .295 | -.052 | -.811 | -1.281 | -1.106 |
| .075 | .113 | -.076 | -.279 | -.626 | -.879 | .122 | -.124 | -.371 | -1.133 | -1.036 |
| .150 | .013 | -.129 | -.266 | -.519 | -.705 | .034 | -.148 | -.322 | -.794 | -.878 |
| .250 | -.010 | -.105 | -.192 | -.338 | -.483 | -.038 | -.171 | -.290 | -.431 | -.784 |
| .350 | -.049 | -.124 | -.182 | -.272 | -.358 | -.104 | -.207 | -.306 | -.379 | -.729 |
| .450 | -.097 | -.156 | -.186 | -.240 | -.404 | -.174 | -.256 | -.272 | -.305 | -.625 |
| .550 | -.109 | -.147 | -.153 | -.185 | -.331 | -.156 | -.207 | -.203 | -.204 | -.521 |
| .650 | -.054 | -.100 | -.105 | -.141 | -.262 | -.113 | -.144 | -.136 | -.144 | -.424 |
| .750 | -.033 | -.060 | -.057 | -.100 | -.222 | -.052 | -.064 | -.053 | -.073 | -.310 |
| .850 | -.019 | -.010 | -.016 | -.031 | -.140 | -.032 | -.031 | -.039 | -.019 | -.195 |
| .900 | .048 | .048 | .060 | .015 | -.078 | .076 | .079 | .092 | .059 | -.121 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.283 | .007 | .281 | .474 | .674 | -.767 | -.068 | .309 | .536 | .735 |
| .075 | -.315 | -.096 | .091 | .259 | .467 | -.452 | -.137 | .122 | .303 | .509 |
| .150 | -.280 | -.124 | .020 | .159 | .346 | -.338 | -.153 | .030 | .180 | .364 |
| .250 | -.207 | -.113 | -.005 | .100 | .265 | -.283 | -.171 | -.035 | .085 | .245 |
| .350 | -.198 | -.135 | -.057 | .037 | .176 | -.289 | -.204 | -.096 | .008 | .156 |
| .450 | -.185 | -.153 | -.093 | -.012 | .101 | -.252 | -.219 | -.141 | -.053 | .071 |
| .550 | -.138 | -.125 | -.087 | -.010 | .079 | -.194 | -.188 | -.136 | -.064 | .028 |
| .650 | -.087 | -.075 | -.040 | .019 | .096 | -.123 | -.124 | -.099 | -.039 | .020 |
| .750 | -.046 | -.041 | -.013 | .031 | .087 | -.033 | -.031 | -.031 | .002 | .025 |
| .850 | -.030 | .028 | .046 | .075 | .092 | .057 | .056 | .072 | .067 | .041 |
| .900 | .061 | .059 | .059 | .068 | .079 | .088 | .079 | .080 | .065 | .017 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .562 | .770 | .649 | .320 | -.033 | .559 | .713 | .536 | .175 | -.142 |
| .025 | .315 | -.085 | -.976 | -.402 | -.800 | .148 | -.263 | -1.077 | -1.329 | -.560 |
| .075 | .140 | -.151 | -.605 | -.1259 | -.819 | -.057 | -.311 | -.926 | -1.232 | -.592 |
| .150 | .018 | -.194 | -.418 | -.148 | -.828 | -.167 | -.204 | -.218 | -.958 | -.620 |
| .250 | -.073 | -.228 | -.389 | -.785 | -.761 | -.066 | -.112 | -.170 | -.635 | -.574 |
| .350 | -.151 | -.248 | -.251 | -.289 | -.665 | | | | | |
| .450 | -.194 | -.254 | -.263 | -.204 | -.590 | | | | | |
| .550 | -.182 | -.218 | -.208 | -.178 | -.536 | | | | | |
| .650 | -.128 | -.164 | -.125 | -.126 | -.460 | -.088 | -.077 | -.096 | -.284 | -.455 |
| .750 | -.068 | -.014 | -.037 | -.057 | -.386 | -.041 | -.020 | -.051 | -.273 | -.420 |
| .850 | -.037 | .034 | .040 | .008 | -.311 | .002 | .027 | -.018 | -.243 | -.383 |
| .900 | .057 | .059 | .075 | .035 | -.281 | .029 | .054 | .003 | -.208 | -.367 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.002 | -.084 | .330 | .551 | .714 | -1.089 | -.222 | .170 | .356 | .509 |
| .075 | -.693 | -.170 | .118 | .306 | .501 | -.924 | -.335 | -.092 | .063 | .249 |
| .150 | -.383 | -.167 | .031 | .178 | .354 | -.253 | -.208 | -.168 | -.113 | .057 |
| .250 | -.389 | -.216 | -.075 | .057 | .217 | | | | | |
| .350 | -.258 | -.255 | -.148 | -.045 | .100 | | | | | |
| .450 | -.250 | -.244 | -.183 | -.112 | .012 | | | | | |
| .550 | -.199 | -.202 | -.167 | -.124 | -.038 | | | | | |
| .650 | -.111 | -.120 | -.115 | -.084 | -.048 | -.081 | -.072 | -.076 | -.108 | -.121 |
| .750 | -.029 | -.031 | -.053 | -.031 | -.050 | -.060 | -.029 | -.048 | -.078 | -.146 |
| .850 | .066 | .059 | .075 | .052 | -.023 | .013 | .051 | .032 | -.003 | -.108 |
| .900 | .104 | .097 | .091 | .063 | -.053 | .019 | .071 | .046 | -.016 | -.132 |

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TABLE V. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(e) $\alpha = 0^\circ$; $M = 0.92$.

| x c_v | C_p for - | | | | | C_p for - | | | | | | |
|-------------------|----------------------|-------|-------------------|---------------------|---------------------|----------------------|----------------------|-------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | .889 | .653 | .785 | .640 | .204 | .639 | .799 | .736 | .492 | .061 | | |
| .025 | .237 | -.023 | -.374 | -.564 | -1.117 | .298 | -.044 | -.764 | -1.182 | -1.186 | | |
| .075 | .117 | -.070 | -.280 | -.584 | -.856 | .124 | -.123 | -.374 | -1.061 | -1.049 | | |
| .150 | .012 | -.135 | -.283 | -.505 | -.734 | .038 | -.151 | -.341 | -.933 | -.857 | | |
| .250 | -.008 | -.112 | -.200 | -.393 | -.486 | -.036 | -.174 | -.305 | -.512 | -.776 | | |
| .350 | -.049 | -.132 | -.198 | -.294 | -.340 | -.109 | -.218 | -.333 | -.440 | -.726 | | |
| .450 | -.104 | -.170 | -.212 | -.280 | -.410 | -.188 | -.281 | -.344 | -.420 | -.627 | | |
| .550 | -.119 | -.166 | -.179 | -.216 | -.368 | -.173 | -.231 | -.202 | -.190 | -.528 | | |
| .650 | -.065 | -.109 | -.115 | -.135 | -.268 | -.125 | -.156 | -.139 | -.101 | -.437 | | |
| .750 | -.037 | -.066 | -.066 | -.085 | -.244 | -.057 | -.056 | -.058 | -.039 | -.329 | | |
| .850 | .016 | .008 | .010 | -.010 | -.163 | .034 | .038 | .040 | .049 | -.218 | | |
| .900 | .047 | .052 | .050 | .037 | -.096 | .078 | .082 | .090 | .092 | -.148 | | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | -.270 | .013 | .274 | .487 | .677 | -.760 | -.065 | .301 | .543 | .739 | | |
| .075 | -.322 | -.096 | .087 | .271 | .470 | -.494 | -.143 | .108 | .314 | .516 | | |
| .150 | -.290 | -.123 | .015 | .170 | .352 | -.352 | -.157 | .023 | .191 | .367 | | |
| .250 | -.217 | -.117 | -.015 | .109 | .269 | -.299 | -.178 | -.048 | .093 | .249 | | |
| .350 | -.202 | -.141 | -.066 | .039 | .175 | -.306 | -.213 | -.113 | .015 | .161 | | |
| .450 | -.191 | -.165 | -.110 | -.014 | .097 | -.286 | -.247 | -.168 | -.060 | .060 | | |
| .550 | -.141 | -.138 | -.104 | -.021 | .077 | -.191 | -.204 | -.164 | -.080 | .026 | | |
| .650 | -.086 | -.080 | -.053 | .020 | .094 | -.119 | -.128 | -.121 | -.051 | .016 | | |
| .750 | -.044 | -.045 | -.027 | .034 | .085 | -.026 | -.028 | -.040 | .008 | .018 | | |
| .850 | .030 | .030 | .033 | .075 | .084 | .063 | .060 | .065 | .075 | .030 | | |
| .900 | .057 | .063 | .049 | .079 | .065 | .092 | .084 | .073 | .088 | .006 | | |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | .576 | .773 | .673 | .395 | -.004 | .566 | .714 | .561 | .253 | -.114 | | |
| .025 | .317 | -.085 | -.942 | -1.289 | -.813 | .137 | -.265 | -.997 | -1.314 | -.547 | | |
| .075 | .136 | -.151 | -.702 | -1.156 | -.831 | -.059 | -.297 | -.917 | -1.228 | -.570 | | |
| .150 | .014 | -.193 | -.414 | -1.090 | -.839 | -.208 | -.244 | -.457 | -1.059 | -.599 | | |
| .250 | -.079 | -.239 | -.401 | -1.014 | -.776 | -.096 | -.114 | -.147 | -.934 | -.566 | | |
| .350 | -.166 | -.292 | -.422 | -.623 | -.675 | | | | | | | |
| .450 | -.219 | -.283 | -.229 | -.175 | -.596 | | | | | | | |
| .550 | -.198 | -.239 | -.215 | -.088 | -.553 | | | | | | | |
| .650 | -.141 | -.177 | -.132 | -.063 | -.493 | -.090 | -.067 | -.100 | -.199 | -.463 | | |
| .750 | -.059 | -.015 | -.040 | -.013 | -.417 | -.038 | -.015 | -.053 | -.209 | -.430 | | |
| .850 | .038 | .037 | .039 | .045 | -.337 | .003 | .037 | -.023 | -.201 | -.391 | | |
| .900 | .057 | .068 | .075 | .072 | -.306 | .025 | .058 | -.001 | -.171 | -.375 | | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | -.971 | -.078 | .323 | .547 | .717 | -.044 | -.222 | .156 | .360 | .511 | | |
| .075 | -.726 | -.171 | .105 | .312 | .506 | -.943 | -.374 | -.110 | .072 | .251 | | |
| .150 | -.377 | -.169 | .018 | .189 | .358 | -.410 | -.247 | -.234 | -.119 | .059 | | |
| .250 | -.398 | -.232 | -.089 | .059 | .221 | | | | | | | |
| .350 | -.354 | -.308 | -.179 | -.046 | .101 | | | | | | | |
| .450 | -.235 | -.265 | -.225 | -.129 | .010 | | | | | | | |
| .550 | -.194 | -.216 | -.191 | -.144 | -.045 | | | | | | | |
| .650 | -.112 | -.122 | -.136 | -.090 | -.055 | -.090 | -.065 | -.079 | -.078 | -.121 | | |
| .750 | -.030 | -.033 | -.050 | -.025 | -.060 | -.065 | -.026 | -.048 | -.057 | -.157 | | |
| .850 | .070 | .068 | .073 | .066 | -.032 | .009 | .056 | .035 | .017 | -.113 | | |
| .900 | .104 | .097 | .088 | .084 | -.057 | .017 | .076 | .043 | .016 | -.143 | | |

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TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(f) $\alpha = 9.4^\circ$; $M = 0.60$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-----------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| Left side | | | | | | | | | | |
| .000 | .567 | .805 | .557 | .174 | -.502 | .395 | .667 | .387 | -.398 | -.1.188 |
| .025 | .028 | -.123 | -.218 | -.396 | -.909 | .227 | -.110 | -.513 | -.1.180 | -.1.641 |
| .075 | .014 | -.112 | -.216 | -.323 | -.591 | .082 | -.137 | -.366 | -.686 | -.1.618 |
| .150 | -.015 | -.132 | -.218 | -.295 | -.477 | .010 | -.137 | -.279 | -.421 | -.1.195 |
| .250 | -.011 | -.089 | -.157 | -.219 | -.338 | -.047 | -.148 | -.247 | -.346 | -.307 |
| .350 | -.038 | -.103 | -.143 | -.198 | -.293 | -.090 | -.180 | -.245 | -.318 | -.363 |
| .450 | -.072 | -.119 | -.157 | -.203 | -.272 | .126 | -.193 | -.236 | -.281 | -.357 |
| .550 | -.081 | -.123 | -.161 | -.194 | -.252 | .115 | -.162 | -.193 | -.231 | -.300 |
| .650 | -.063 | -.107 | -.134 | -.169 | -.213 | -.099 | -.130 | -.152 | -.178 | -.247 |
| .750 | -.054 | -.089 | -.104 | -.136 | -.182 | -.067 | -.089 | -.093 | -.116 | -.179 |
| .850 | -.022 | -.040 | -.052 | -.074 | -.116 | -.002 | -.017 | -.018 | -.035 | -.088 |
| .900 | -.003 | -.004 | -.009 | -.033 | -.070 | .032 | -.021 | -.023 | -.008 | -.041 |
| Right side | | | | | | | | | | |
| .025 | -.131 | -.022 | .068 | .248 | .571 | -.523 | -.051 | .300 | .510 | .696 |
| .075 | -.208 | -.105 | .023 | .176 | .359 | -.326 | -.107 | .109 | .287 | .478 |
| .150 | -.192 | -.103 | .012 | .133 | .250 | -.265 | -.121 | .030 | .162 | .328 |
| .250 | -.149 | -.078 | .005 | .098 | .182 | -.231 | -.132 | -.025 | .082 | .207 |
| .350 | -.149 | -.096 | -.027 | .043 | .100 | -.222 | -.150 | -.068 | .022 | .123 |
| .450 | -.158 | -.114 | -.052 | .004 | .041 | -.219 | -.164 | -.095 | -.031 | .053 |
| .550 | -.145 | -.110 | -.057 | -.005 | .023 | -.192 | -.153 | -.102 | -.051 | .014 |
| .650 | -.122 | -.092 | -.041 | -.008 | .023 | -.138 | -.119 | -.082 | -.042 | .005 |
| .750 | -.097 | -.076 | -.034 | -.003 | .021 | -.077 | -.062 | -.043 | -.010 | .014 |
| .850 | -.036 | -.017 | .009 | .031 | .043 | -.002 | -.001 | .028 | .034 | .053 |
| .900 | -.004 | .008 | .028 | .043 | .048 | .028 | .019 | .030 | .036 | .039 |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| Left side | | | | | | | | | | |
| .000 | .248 | .626 | .218 | -.424 | -1.109 | .295 | .572 | .091 | -.451 | -.813 |
| .025 | .254 | -.144 | -.716 | -1.026 | -1.195 | .125 | -.241 | -.707 | -.849 | -.670 |
| .075 | .096 | -.162 | -.450 | -.904 | -1.172 | -.027 | -.193 | -.397 | -.785 | -.670 |
| .150 | -.002 | -.171 | -.347 | -.762 | -1.120 | -.104 | -.175 | -.275 | -.651 | -.650 |
| .250 | -.061 | -.175 | -.284 | -.511 | -1.013 | -.077 | -.119 | -.188 | -.562 | -.607 |
| .350 | -.111 | -.189 | -.259 | -.346 | -.872 | | | | | |
| .450 | -.136 | -.191 | -.234 | -.267 | -.693 | | | | | |
| .550 | -.140 | -.175 | -.200 | -.221 | -.525 | | | | | |
| .650 | -.111 | -.134 | -.141 | -.164 | -.379 | -.102 | -.083 | -.107 | -.290 | -.484 |
| .750 | -.065 | -.074 | -.077 | -.100 | -.252 | -.074 | -.046 | -.070 | -.240 | -.463 |
| .850 | -.013 | -.024 | -.029 | -.047 | -.152 | -.038 | -.008 | -.057 | -.196 | -.434 |
| .900 | -.010 | .005 | .005 | -.012 | -.111 | -.013 | -.012 | -.036 | -.162 | -.411 |
| Right side | | | | | | | | | | |
| .025 | -.585 | -.074 | .323 | .523 | .684 | -.560 | -.155 | .178 | .328 | .439 |
| .075 | -.417 | -.134 | .114 | .305 | .500 | -.367 | -.193 | -.029 | .077 | .221 |
| .150 | -.303 | -.144 | .028 | .174 | .350 | -.258 | -.171 | -.104 | -.044 | .055 |
| .250 | -.272 | -.166 | -.052 | .071 | .218 | | | | | |
| .350 | -.260 | -.175 | -.093 | .002 | .123 | | | | | |
| .450 | -.231 | -.182 | -.116 | -.049 | .050 | | | | | |
| .550 | -.188 | -.162 | -.120 | -.067 | .018 | | | | | |
| .650 | -.133 | -.130 | -.097 | -.049 | .005 | -.090 | -.074 | -.088 | -.102 | -.086 |
| .750 | -.074 | -.058 | -.066 | -.026 | .009 | -.070 | -.053 | -.079 | -.095 | -.118 |
| .850 | -.005 | .014 | .023 | .025 | .032 | -.015 | -.010 | -.018 | -.035 | -.102 |
| .900 | -.032 | .037 | .032 | .041 | .034 | -.006 | -.026 | -.000 | -.026 | -.129 |

TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(g) $\alpha = 9.6^\circ$; $M = 0.80$.

| X C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .558 | .846 | .598 | .542 | .016 | .519 | .704 | .560 | .189 | .230 |
| .025 | -.059 | -.117 | -.130 | -.319 | -.517 | .222 | -.102 | -.491 | -.1271 | -.1477 |
| .075 | -.117 | -.219 | -.294 | -.467 | | .073 | -.143 | -.380 | -.707 | -.1376 |
| .150 | -.024 | -.143 | -.251 | -.326 | -.487 | .002 | -.140 | -.303 | -.499 | -.1080 |
| .250 | -.027 | -.099 | -.179 | -.236 | -.382 | -.054 | -.158 | -.271 | -.375 | -.407 |
| .350 | -.054 | -.114 | -.171 | -.216 | -.321 | -.106 | -.201 | -.276 | -.337 | -.410 |
| .450 | -.085 | -.137 | -.182 | -.219 | -.301 | -.156 | -.223 | -.271 | -.308 | -.392 |
| .550 | -.102 | -.155 | -.189 | -.212 | -.280 | -.147 | -.198 | -.230 | -.252 | -.348 |
| .650 | -.088 | -.134 | -.166 | -.189 | -.250 | -.126 | -.163 | -.182 | -.198 | -.305 |
| .750 | -.079 | -.117 | -.139 | -.161 | -.230 | -.080 | -.101 | -.112 | -.125 | -.227 |
| .850 | -.030 | -.057 | -.068 | -.089 | -.155 | -.006 | -.016 | -.019 | -.028 | -.126 |
| .900 | .003 | -.010 | -.018 | -.037 | -.096 | .035 | .030 | .032 | .021 | -.062 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.036 | -.007 | .002 | .233 | .301 | -.550 | -.054 | .280 | .501 | .685 |
| .075 | -.211 | -.111 | .016 | .129 | .255 | -.355 | -.116 | .098 | .279 | .465 |
| .150 | -.217 | -.113 | -.001 | .093 | .221 | -.281 | -.130 | .023 | .163 | .322 |
| .250 | -.173 | -.092 | -.012 | .073 | .176 | -.249 | -.149 | -.033 | .083 | .213 |
| .350 | -.174 | -.113 | -.046 | .028 | .110 | -.244 | -.172 | -.081 | .015 | .128 |
| .450 | -.184 | -.133 | -.075 | -.011 | .055 | -.247 | -.196 | -.122 | -.045 | .040 |
| .550 | -.168 | -.128 | -.080 | -.024 | .031 | -.217 | -.184 | -.133 | -.068 | .000 |
| .650 | -.146 | -.114 | -.068 | -.019 | .024 | -.162 | -.145 | -.104 | -.054 | -.012 |
| .750 | -.126 | -.099 | -.060 | -.019 | .018 | -.085 | -.081 | -.051 | -.019 | -.003 |
| .850 | -.047 | -.031 | -.009 | .015 | .034 | .006 | .011 | .020 | .036 | .025 |
| .900 | -.010 | .001 | .016 | .030 | .042 | .034 | .028 | .034 | .039 | .018 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .394 | .657 | .422 | -.016 | -.487 | .374 | .587 | .255 | -.129 | -.576 |
| .025 | .246 | -.155 | -.936 | -.201 | -.939 | .113 | -.249 | -.878 | -.758 | -.592 |
| .075 | .091 | -.175 | -.494 | -.138 | -.912 | -.061 | -.243 | -.512 | -.712 | -.598 |
| .150 | -.012 | -.192 | -.388 | -.955 | -.868 | -.135 | -.198 | -.300 | -.658 | -.604 |
| .250 | -.077 | -.201 | -.315 | -.592 | -.822 | -.086 | -.123 | -.216 | -.565 | -.587 |
| .350 | -.133 | -.222 | -.286 | -.330 | -.764 | | | | | |
| .450 | -.171 | -.228 | -.265 | -.278 | -.680 | | | | | |
| .550 | -.168 | -.213 | -.224 | -.235 | -.585 | | | | | |
| .650 | -.135 | -.151 | -.153 | -.158 | -.489 | -.102 | -.073 | -.109 | -.339 | -.467 |
| .750 | -.061 | -.072 | -.074 | -.080 | -.384 | -.065 | -.030 | -.072 | -.287 | -.443 |
| .850 | -.007 | -.010 | -.004 | -.010 | -.280 | -.023 | .013 | -.042 | -.227 | -.403 |
| .900 | -.017 | .025 | .029 | .021 | -.230 | .003 | .037 | -.019 | -.184 | -.384 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.769 | -.075 | .312 | .537 | .698 | -.919 | -.180 | .166 | .336 | .473 |
| .075 | -.448 | -.149 | .110 | .311 | .511 | -.427 | -.242 | -.068 | .076 | .243 |
| .150 | -.331 | -.155 | .025 | .183 | .359 | -.281 | -.198 | -.136 | -.073 | .059 |
| .250 | -.298 | -.189 | -.059 | .070 | .224 | | | | | |
| .350 | -.287 | -.208 | -.121 | -.011 | .119 | | | | | |
| .450 | -.254 | -.217 | -.153 | -.068 | .037 | | | | | |
| .550 | -.209 | -.196 | -.150 | -.088 | -.004 | | | | | |
| .650 | -.141 | -.152 | -.112 | -.068 | -.018 | -.089 | -.076 | -.083 | -.094 | -.101 |
| .750 | -.067 | -.052 | -.051 | -.033 | -.024 | -.059 | -.039 | -.068 | -.089 | -.135 |
| .850 | .022 | .027 | .026 | .039 | .005 | .005 | .034 | .002 | -.028 | -.114 |
| .900 | .060 | .051 | .052 | .054 | -.003 | .019 | .051 | .016 | -.027 | -.138 |

TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(h) $\alpha = 9.7^\circ$; $M \doteq 0.85$.

| x C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .545 | .865 | .606 | .464 | .158 | .562 | .711 | .606 | .307 | .136 |
| .025 | -.077 | -.132 | -.102 | -.238 | -.481 | .225 | -.127 | -.549 | -1.401 | -1.491 |
| .075 | -.003 | -.138 | -.220 | -.283 | -.433 | .079 | -.173 | -.395 | -.686 | -1.308 |
| .150 | -.025 | -.173 | -.274 | -.368 | -.485 | .003 | -.173 | -.325 | -.543 | -.958 |
| .250 | -.031 | -.127 | -.200 | -.294 | -.399 | -.052 | -.190 | -.291 | -.443 | -.471 |
| .350 | -.059 | -.141 | -.189 | -.266 | -.334 | -.111 | -.235 | -.298 | -.378 | -.450 |
| .450 | -.091 | -.169 | -.203 | -.258 | -.315 | -.167 | -.265 | -.296 | -.340 | -.409 |
| .550 | -.108 | -.185 | -.203 | -.240 | -.289 | -.159 | -.235 | -.251 | -.284 | -.372 |
| .650 | -.097 | -.165 | -.182 | -.214 | -.260 | -.139 | -.197 | -.200 | -.221 | -.335 |
| .750 | -.089 | -.148 | -.159 | -.187 | -.247 | -.090 | -.127 | -.126 | -.143 | -.267 |
| .850 | -.036 | -.081 | -.078 | -.113 | -.178 | -.008 | -.032 | -.028 | -.043 | -.158 |
| .900 | .006 | -.029 | -.025 | -.056 | -.119 | .044 | .023 | .024 | .016 | -.085 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .009 | -.018 | -.022 | .216 | .304 | -.538 | -.063 | .271 | .509 | .666 |
| .075 | -.198 | -.134 | -.001 | .092 | .230 | -.369 | -.136 | .092 | .282 | .449 |
| .150 | -.228 | -.141 | -.011 | .057 | .199 | -.289 | -.151 | .015 | .160 | .315 |
| .250 | -.175 | -.117 | -.029 | .044 | .165 | -.259 | -.172 | -.045 | .073 | .210 |
| .350 | -.184 | -.136 | -.063 | .004 | .104 | -.262 | -.202 | -.099 | .010 | .124 |
| .450 | -.193 | -.158 | -.092 | -.034 | .053 | -.263 | -.228 | -.143 | -.063 | .037 |
| .550 | -.176 | -.153 | -.099 | -.050 | .027 | -.231 | -.220 | -.155 | -.088 | -.008 |
| .650 | -.153 | -.136 | -.083 | -.041 | .023 | -.170 | -.177 | -.125 | -.077 | -.019 |
| .750 | -.132 | -.132 | -.076 | -.044 | .013 | -.086 | -.100 | -.069 | -.040 | -.011 |
| .850 | -.048 | -.053 | -.018 | -.007 | .026 | .006 | -.006 | .011 | .016 | .016 |
| .900 | -.003 | -.018 | -.006 | .009 | .030 | .045 | .015 | .025 | .023 | .006 |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .438 | .663 | .474 | .067 | -.382 | .403 | .588 | .293 | -.167 | -.531 |
| .025 | .255 | -.177 | -1.038 | -1.607 | -.916 | .099 | -.323 | -1.115 | -.970 | -.582 |
| .075 | .093 | -.202 | -.511 | -1.438 | -.892 | -.073 | -.332 | -.580 | -.941 | -.592 |
| .150 | -.007 | -.226 | -.429 | -.967 | -.832 | -.155 | -.241 | -.323 | -.854 | -.599 |
| .250 | -.084 | -.241 | -.343 | -.450 | -.783 | -.089 | -.159 | -.236 | -.677 | -.587 |
| .350 | -.146 | -.268 | -.306 | -.417 | -.739 | | | | | |
| .450 | -.187 | -.278 | -.287 | -.331 | -.672 | | | | | |
| .550 | -.186 | -.254 | -.246 | -.251 | -.596 | | | | | |
| .650 | -.142 | -.182 | -.170 | -.170 | -.524 | -.101 | -.095 | -.120 | -.343 | -.481 |
| .750 | -.058 | -.094 | -.088 | -.091 | -.427 | -.055 | -.047 | -.079 | -.286 | -.451 |
| .850 | -.004 | -.022 | -.012 | -.026 | -.322 | -.014 | -.001 | -.045 | -.223 | -.415 |
| .900 | .034 | -.018 | -.028 | -.014 | -.272 | .016 | .023 | -.023 | -.186 | -.396 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.852 | -.086 | .307 | .532 | .700 | -.1048 | -.207 | .152 | .342 | .478 |
| .075 | -.448 | -.166 | .103 | .310 | .510 | -.511 | -.301 | -.096 | .069 | .251 |
| .150 | -.348 | -.177 | .016 | .183 | .364 | -.269 | -.243 | -.172 | -.117 | .059 |
| .250 | -.325 | -.226 | -.076 | .064 | .226 | | | | | |
| .350 | -.293 | -.255 | -.146 | -.033 | .115 | | | | | |
| .450 | -.260 | -.260 | -.183 | -.094 | .033 | | | | | |
| .550 | -.211 | -.233 | -.176 | -.117 | -.022 | | | | | |
| .650 | -.136 | -.187 | -.136 | -.096 | -.035 | -.077 | -.088 | -.100 | -.113 | -.109 |
| .750 | -.063 | -.073 | -.069 | -.057 | -.039 | -.055 | -.057 | -.078 | -.104 | -.151 |
| .850 | .034 | .016 | .019 | .020 | -.012 | .010 | .022 | -.001 | -.038 | -.126 |
| .900 | .073 | .045 | .044 | .040 | -.022 | .033 | .036 | -.014 | -.028 | -.150 |

TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(i) $\alpha = 9.7^\circ$; $M = 0.90$.

| X C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .508 | .866 | .598 | .698 | | .600 | .711 | .654 | .423 | |
| .025 | -.137 | -.131 | -.044 | -.211 | | .209 | -.131 | -.767 | -1.192 | |
| .075 | -.032 | -.142 | -.201 | -.240 | | .057 | -.182 | -.418 | -.948 | |
| .150 | -.052 | -.183 | -.303 | -.370 | | -.015 | -.189 | -.363 | -.582 | |
| .250 | -.060 | -.138 | -.226 | -.331 | | -.074 | -.198 | -.323 | -.520 | |
| .350 | -.086 | -.151 | -.215 | -.317 | | -.140 | -.254 | -.350 | -.495 | |
| .450 | -.122 | -.182 | -.234 | -.322 | | -.209 | -.294 | -.362 | -.471 | |
| .550 | -.145 | -.202 | -.234 | -.299 | | -.214 | -.275 | -.266 | -.357 | |
| .650 | -.133 | -.186 | -.203 | -.247 | | -.196 | -.230 | -.222 | -.203 | |
| .750 | -.130 | -.173 | -.189 | -.209 | | -.126 | -.137 | -.138 | -.137 | |
| .850 | -.069 | -.083 | -.091 | -.124 | | -.030 | -.030 | -.026 | -.042 | |
| .900 | -.022 | -.031 | -.029 | -.065 | | .022 | -.026 | -.033 | -.009 | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .061 | -.018 | -.052 | .118 | | -.572 | -.067 | .271 | .485 | |
| .075 | -.184 | -.143 | -.013 | .048 | | -.436 | -.151 | .089 | .262 | |
| .150 | -.258 | -.150 | -.021 | .045 | | -.327 | -.166 | .010 | .146 | |
| .250 | -.216 | -.129 | -.040 | .036 | | -.305 | -.187 | -.049 | .055 | |
| .350 | -.225 | -.151 | -.076 | -.007 | | -.324 | -.222 | -.108 | -.010 | |
| .450 | -.236 | -.169 | -.107 | -.047 | | -.337 | -.258 | -.167 | -.090 | |
| .550 | -.217 | -.173 | -.115 | -.059 | | -.273 | -.254 | -.187 | -.121 | |
| .650 | -.188 | -.158 | -.100 | -.058 | | -.206 | -.210 | -.155 | -.116 | |
| .750 | -.173 | -.153 | -.095 | -.065 | | -.109 | -.110 | -.085 | -.070 | |
| .850 | -.074 | -.062 | -.036 | -.026 | | -.009 | -.007 | -.001 | -.002 | |
| .900 | -.023 | -.022 | -.009 | -.010 | | .031 | -.017 | .018 | .006 | |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .464 | .666 | .512 | .195 | | .421 | .589 | .340 | -.045 | |
| .025 | -.246 | -.173 | -1.048 | -.378 | | .098 | -.375 | -1.089 | -1.338 | |
| .075 | -.082 | -.207 | -.606 | -.234 | | -.094 | -.335 | -1.025 | -1.224 | |
| .150 | -.022 | -.238 | -.462 | -1.113 | | -.307 | -.294 | -.383 | -1.090 | |
| .250 | -.104 | -.259 | -.437 | -.645 | | -.140 | -.145 | -.181 | -.940 | |
| .350 | -.192 | -.315 | -.418 | -.612 | | | | | | |
| .450 | -.254 | -.321 | -.276 | -.377 | | | | | | |
| .550 | -.253 | -.298 | -.268 | -.179 | | | | | | |
| .650 | -.190 | -.191 | -.178 | -.137 | | -.118 | -.091 | -.127 | -.222 | |
| .750 | -.088 | -.091 | -.087 | -.079 | | -.073 | -.041 | -.080 | -.199 | |
| .850 | -.019 | -.011 | -.007 | -.020 | | -.022 | -.005 | -.044 | -.172 | |
| .900 | .015 | .026 | .033 | .016 | | .003 | -.034 | -.017 | -.136 | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.951 | -.089 | .308 | .517 | | -.096 | -.217 | .150 | .329 | |
| .075 | -.459 | -.181 | .107 | .295 | | -.897 | -.366 | -.109 | .052 | |
| .150 | -.405 | -.190 | .018 | .169 | | -.389 | -.287 | -.291 | -.177 | |
| .250 | -.416 | -.243 | -.084 | .040 | | | | | | |
| .350 | -.431 | -.297 | -.170 | -.067 | | | | | | |
| .450 | -.273 | -.305 | -.225 | -.152 | | | | | | |
| .550 | -.249 | -.275 | -.215 | -.183 | | | | | | |
| .650 | -.165 | -.211 | -.159 | -.141 | | -.094 | -.095 | -.105 | -.121 | |
| .750 | -.076 | -.073 | -.078 | -.063 | | -.070 | -.051 | -.078 | -.109 | |
| .850 | .026 | .023 | .018 | .004 | | .002 | -.027 | -.002 | -.031 | |
| .900 | .088 | .051 | .046 | | | .018 | -.045 | -.014 | -.018 | |

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TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(j) $\alpha = 9.7^\circ$; $M = 0.92$.

| $\frac{x}{C_V}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_V = 0.11$ | | | | | $z/b_V = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .526 | .621 | .721 | | | .602 | | .654 | .441 | |
| .025 | -.158 | -.015 | -.189 | | | .200 | | -.733 | -.1175 | |
| .075 | -.038 | -.171 | -.219 | | | .050 | | -.439 | -.914 | |
| .150 | -.055 | -.302 | -.345 | | | -.021 | | -.391 | -.564 | |
| .250 | -.061 | -.241 | -.313 | | | -.078 | | -.340 | -.498 | |
| .350 | -.088 | -.230 | -.301 | | | -.141 | | -.358 | -.479 | |
| .450 | -.124 | -.247 | -.311 | | | .220 | | -.383 | -.457 | |
| .550 | -.148 | -.260 | -.289 | | | .233 | | -.355 | -.369 | |
| .650 | -.148 | -.239 | -.236 | | | .224 | | -.240 | -.187 | |
| .750 | -.146 | -.220 | -.198 | | | .136 | | -.139 | -.121 | |
| .850 | -.082 | -.104 | -.112 | | | .034 | | -.029 | -.027 | |
| .900 | -.029 | -.042 | -.053 | | | .018 | | .031 | .022 | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .079 | -.092 | .126 | | | -.556 | | .248 | .490 | |
| .075 | -.161 | -.037 | .059 | | | .436 | | .068 | .269 | |
| .150 | -.248 | -.034 | .058 | | | .353 | | -.008 | .158 | |
| .250 | -.216 | -.050 | .047 | | | .303 | | -.068 | .070 | |
| .350 | -.225 | -.087 | .004 | | | .327 | | -.126 | .002 | |
| .450 | -.235 | -.121 | -.040 | | | .349 | | -.189 | -.079 | |
| .550 | -.223 | -.133 | -.053 | | | .316 | | .220 | -.112 | |
| .650 | -.199 | -.129 | -.049 | | | .207 | | .206 | -.105 | |
| .750 | -.183 | -.126 | -.059 | | | .107 | | -.108 | -.061 | |
| .850 | -.078 | -.060 | -.019 | | | .007 | | -.015 | .010 | |
| .900 | -.029 | -.025 | -.003 | | | .034 | | .008 | .021 | |
| $z/b_V = 0.66$ | | | | | $z/b_V = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .466 | .523 | .219 | | | .424 | | .347 | -.014 | |
| .025 | .242 | -.1024 | -.1364 | | | .095 | | -.130 | -.353 | |
| .075 | .079 | -.746 | -.1220 | | | -.092 | | -.011 | -.222 | |
| .150 | -.025 | -.471 | -.1113 | | | .324 | | -.585 | -.098 | |
| .250 | -.109 | -.439 | -.625 | | | .210 | | -.286 | -.972 | |
| .350 | -.199 | -.459 | -.597 | | | | | | | |
| .450 | -.286 | -.442 | -.426 | | | | | | | |
| .550 | -.286 | -.235 | -.158 | | | | | | | |
| .650 | -.208 | -.169 | -.118 | | | | | | | |
| .750 | -.088 | -.084 | -.064 | | | | | | | |
| .850 | -.017 | -.005 | -.006 | | | | | | | |
| .900 | .017 | .039 | .028 | | | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.926 | .292 | .521 | | | -.076 | | .145 | .341 | |
| .075 | -.540 | .094 | .301 | | | .908 | | .105 | .069 | |
| .150 | -.397 | .005 | .180 | | | -.459 | | -.320 | -.162 | |
| .250 | -.411 | -.096 | .057 | | | | | | | |
| .350 | -.447 | -.192 | -.051 | | | | | | | |
| .450 | -.358 | -.281 | -.140 | | | | | | | |
| .550 | -.231 | -.294 | -.177 | | | | | | | |
| .650 | -.161 | -.195 | -.133 | | | | | | | |
| .750 | -.075 | -.087 | -.071 | | | | | | | |
| .850 | .029 | .010 | .024 | | | | | | | |
| .900 | .067 | .040 | .045 | | | | | | | |

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TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(k) $\alpha = 15.0^\circ$; $M = 0.60$.

| x C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .782 | .807 | .543 | .216 | .562 | .645 | .244 | .202 | | |
| .025 | -.220 | -.133 | .219 | .112 | .145 | -.392 | -.817 | -.734 | | |
| .075 | -.144 | -.174 | -.082 | -.024 | .011 | -.314 | -.537 | -.564 | | |
| .150 | -.135 | -.213 | -.226 | -.154 | -.050 | -.259 | -.409 | -.469 | | |
| .250 | -.088 | -.158 | -.194 | -.154 | -.095 | -.252 | -.345 | -.426 | | |
| .350 | -.102 | -.174 | -.212 | -.188 | -.142 | -.263 | -.333 | -.408 | | |
| .450 | -.131 | -.195 | -.233 | -.217 | -.171 | -.263 | -.308 | -.385 | | |
| .550 | -.153 | -.211 | -.240 | -.228 | -.173 | -.234 | -.267 | -.337 | | |
| .650 | -.146 | -.188 | -.217 | -.213 | -.153 | -.202 | -.228 | -.294 | | |
| .750 | -.142 | -.188 | -.208 | -.194 | -.117 | -.147 | -.158 | -.222 | | |
| .850 | -.097 | -.126 | -.149 | -.136 | -.052 | -.078 | -.087 | -.163 | | |
| .900 | -.059 | -.087 | -.101 | -.092 | -.171 | -.183 | -.171 | -.149 | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.025 | -.115 | -.502 | -.179 | -.447 | .151 | .395 | .232 | | |
| .075 | -.169 | -.144 | -.164 | -.147 | -.330 | -.003 | .148 | .055 | | |
| .150 | -.196 | -.128 | -.066 | -.095 | -.272 | -.060 | .046 | -.020 | | |
| .250 | -.158 | -.099 | -.032 | -.047 | -.250 | -.106 | -.028 | -.061 | | |
| .350 | -.173 | -.108 | -.048 | -.040 | -.252 | -.138 | -.085 | -.099 | | |
| .450 | -.196 | -.135 | -.091 | -.049 | -.256 | -.167 | -.121 | -.126 | | |
| .550 | -.191 | -.144 | -.107 | -.054 | -.232 | -.170 | -.130 | -.140 | | |
| .650 | -.176 | -.135 | -.117 | -.054 | -.185 | -.144 | -.114 | -.126 | | |
| .750 | -.153 | -.119 | -.107 | -.056 | -.117 | -.101 | -.075 | -.108 | | |
| .850 | -.095 | -.071 | -.071 | -.029 | -.043 | -.019 | -.025 | -.072 | | |
| .900 | -.063 | -.044 | -.048 | -.018 | -.019 | -.028 | -.014 | -.077 | | |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .286 | .412 | -.222 | -.814 | .244 | .167 | -.422 | -.1077 | | |
| .025 | .226 | -.607 | -.1201 | -.1709 | .125 | -.682 | -.909 | -.952 | | |
| .075 | .058 | -.424 | -.954 | -.1628 | -.048 | -.410 | -.854 | -.959 | | |
| .150 | -.353 | -.623 | -.623 | -.1353 | -.126 | -.291 | -.722 | -.909 | | |
| .250 | .035 | -.291 | -.413 | -.755 | -.088 | -.204 | -.601 | -.832 | | |
| .350 | -.155 | -.282 | -.363 | -.480 | | | | | | |
| .450 | -.187 | -.268 | -.320 | -.385 | | | | | | |
| .550 | -.189 | -.236 | -.276 | -.317 | | | | | | |
| .650 | -.160 | -.183 | -.206 | -.233 | -.135 | -.133 | -.301 | -.634 | | |
| .750 | -.120 | -.122 | -.139 | -.170 | -.111 | -.103 | -.263 | -.560 | | |
| .850 | -.061 | -.069 | -.085 | -.115 | -.075 | -.076 | -.222 | -.469 | | |
| .900 | -.043 | -.035 | -.048 | -.095 | -.052 | -.064 | -.192 | -.414 | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.617 | .229 | .498 | .629 | -.642 | .135 | .333 | .484 | | |
| .075 | -.447 | .039 | .242 | .359 | -.422 | -.085 | .068 | .234 | | |
| .150 | -.335 | -.039 | .107 | .191 | -.297 | -.147 | -.066 | .064 | | |
| .250 | -.303 | -.110 | -.005 | .053 | | | | | | |
| .350 | -.288 | -.151 | -.096 | -.045 | | | | | | |
| .450 | -.263 | -.174 | -.135 | -.092 | | | | | | |
| .550 | -.223 | -.172 | -.146 | -.120 | | | | | | |
| .650 | -.169 | -.144 | -.133 | -.126 | -.088 | -.124 | -.123 | -.077 | | |
| .750 | -.111 | -.103 | -.098 | -.115 | -.106 | -.110 | -.117 | -.099 | | |
| .850 | -.028 | -.014 | -.039 | -.077 | -.052 | -.046 | -.062 | -.072 | | |
| .900 | .006 | -.003 | -.007 | -.067 | -.034 | -.028 | -.043 | -.081 | | |

TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(l) $\alpha = 15.8^\circ$; $M = 0.80$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .774 | .838 | .846 | .303 | .434 | .694 | .739 | .749 | .661 | .289 |
| .025 | -.357 | -.197 | -.053 | .525 | .423 | .089 | -.126 | -.374 | -.680 | -.280 |
| .075 | -.196 | -.193 | -.168 | .116 | .181 | -.040 | -.184 | -.341 | -.493 | -.377 |
| .150 | -.180 | -.229 | -.244 | -.178 | -.030 | -.088 | -.193 | -.291 | -.413 | -.419 |
| .250 | -.125 | -.167 | -.188 | -.194 | -.088 | -.125 | -.205 | -.285 | -.375 | -.452 |
| .350 | -.128 | -.164 | -.194 | -.224 | -.148 | -.170 | -.236 | -.307 | -.360 | -.454 |
| .450 | -.161 | -.193 | -.219 | -.245 | -.187 | -.214 | -.270 | -.315 | -.342 | -.429 |
| .550 | -.185 | -.215 | -.232 | -.252 | -.210 | -.215 | -.258 | -.283 | -.301 | -.394 |
| .650 | -.182 | -.211 | -.229 | -.240 | -.219 | -.199 | -.233 | -.250 | -.260 | -.352 |
| .750 | -.199 | -.229 | -.241 | -.254 | -.248 | -.152 | -.171 | -.179 | -.189 | -.282 |
| .850 | -.146 | -.159 | -.169 | -.181 | -.186 | -.081 | -.087 | -.095 | -.113 | -.215 |
| .900 | -.105 | -.112 | -.113 | -.132 | -.138 | -.162 | -.173 | -.168 | -.139 | -.138 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .062 | -.069 | -.232 | -.897 | -.691 | -.406 | -.126 | .101 | .222 | -.107 |
| .075 | -.162 | -.191 | -.221 | -.562 | -.292 | -.354 | -.188 | -.048 | .012 | -.114 |
| .150 | -.218 | -.200 | -.175 | -.151 | -.160 | -.305 | -.191 | -.097 | -.059 | -.113 |
| .250 | -.188 | -.159 | -.135 | -.059 | -.079 | -.276 | -.199 | -.127 | -.089 | -.108 |
| .350 | -.202 | -.170 | -.135 | -.052 | -.055 | -.289 | -.224 | -.163 | -.126 | -.123 |
| .450 | -.214 | -.194 | -.168 | -.065 | -.055 | -.297 | -.252 | -.201 | -.162 | -.138 |
| .550 | -.209 | -.202 | -.180 | -.080 | -.058 | -.273 | -.252 | -.209 | -.171 | -.142 |
| .650 | -.206 | -.197 | -.180 | -.094 | -.064 | -.226 | -.212 | -.182 | -.150 | -.131 |
| .750 | -.205 | -.200 | -.186 | -.107 | -.075 | -.149 | -.147 | -.128 | -.112 | -.114 |
| .850 | -.132 | -.128 | -.122 | -.070 | -.050 | -.058 | -.058 | -.053 | -.056 | -.085 |
| .900 | -.093 | -.090 | -.089 | -.053 | -.040 | -.028 | -.038 | -.037 | -.049 | -.087 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .469 | .665 | .582 | .316 | -.055 | .364 | .582 | .304 | -.175 | -.763 |
| .025 | .216 | -.149 | -.782 | -.1613 | -.1551 | .115 | -.256 | -.1110 | -.077 | -.945 |
| .075 | .046 | -.197 | -.473 | -.129 | -.364 | -.078 | -.283 | -.508 | -.002 | -.950 |
| .150 | -.056 | -.226 | -.411 | -.642 | -.125 | -.165 | -.239 | -.324 | -.830 | -.910 |
| .250 | -.115 | -.177 | -.306 | -.455 | -.764 | -.091 | -.147 | -.239 | -.672 | -.849 |
| .350 | -.194 | -.270 | -.326 | -.402 | -.566 | | | | | |
| .450 | -.239 | -.288 | -.317 | -.346 | -.461 | | | | | |
| .550 | -.249 | -.276 | -.282 | -.293 | -.376 | | | | | |
| .650 | -.205 | -.215 | -.212 | -.221 | -.283 | -.147 | -.131 | -.154 | -.328 | -.630 |
| .750 | -.140 | -.140 | -.135 | -.148 | -.202 | -.109 | -.085 | -.116 | -.284 | -.549 |
| .850 | -.076 | -.067 | -.063 | -.086 | -.148 | -.069 | -.040 | -.078 | -.237 | -.463 |
| .900 | -.044 | -.035 | -.028 | -.055 | -.123 | -.047 | -.022 | -.057 | -.206 | -.415 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.798 | -.161 | .225 | .477 | .522 | -.1076 | -.264 | .133 | .355 | .513 |
| .075 | -.498 | -.223 | .023 | .213 | .256 | -.548 | -.306 | -.113 | -.066 | -.248 |
| .150 | -.382 | -.209 | -.048 | .078 | .119 | -.317 | -.258 | -.180 | -.098 | .064 |
| .250 | -.353 | -.244 | -.136 | -.042 | .006 | | | | | |
| .350 | -.330 | -.279 | -.204 | -.132 | -.081 | | | | | |
| .450 | -.303 | -.280 | -.235 | -.178 | -.126 | | | | | |
| .550 | -.262 | -.255 | -.232 | -.194 | -.145 | | | | | |
| .650 | -.197 | -.197 | -.189 | -.178 | -.149 | -.108 | -.118 | -.130 | -.124 | -.088 |
| .750 | -.118 | -.125 | -.131 | -.133 | -.140 | -.112 | -.087 | -.119 | -.115 | -.107 |
| .850 | -.023 | -.026 | -.040 | -.064 | -.110 | -.041 | -.011 | -.042 | -.046 | -.075 |
| .900 | -.010 | -.004 | -.012 | -.044 | -.094 | -.026 | -.001 | -.030 | -.047 | -.093 |

TABLE V.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE HIGH WING, FUSELAGE,
VERTICAL TAIL, AND HORIZONTAL TAIL - Concluded

(m) $\alpha = 15.9^\circ$; $M = 0.85$.

| X C_V | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_V = 0.11$ | | | | | $Z/b_V = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .755 | .849 | .854 | .307 | | .704 | .741 | .748 | .647 | |
| .025 | -.547 | -.243 | -.006 | .511 | | .062 | -.158 | -.415 | -.731 | |
| .075 | -.252 | -.238 | -.160 | .127 | | -.076 | -.225 | -.380 | -.518 | |
| .150 | -.223 | -.281 | -.282 | -.184 | | -.118 | -.223 | -.323 | -.446 | |
| .250 | -.152 | -.208 | -.214 | -.223 | | -.153 | -.233 | -.310 | -.420 | |
| .350 | -.153 | -.192 | -.221 | -.252 | | -.196 | -.262 | -.332 | -.410 | |
| .450 | -.183 | -.225 | -.241 | -.274 | | -.245 | -.300 | -.343 | -.384 | |
| .550 | -.207 | -.249 | -.252 | -.268 | | -.243 | -.294 | -.306 | -.341 | |
| .650 | -.213 | -.243 | -.252 | -.261 | | -.227 | -.272 | -.279 | -.300 | |
| .750 | -.237 | -.277 | -.278 | -.287 | | -.185 | -.205 | -.204 | -.233 | |
| .850 | -.179 | -.199 | -.196 | -.213 | | -.101 | -.111 | -.110 | -.157 | |
| .900 | -.135 | -.143 | -.137 | -.163 | | -.173 | -.185 | -.167 | -.144 | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .104 | -.092 | -.346 | -1.011 | | -.441 | -.148 | .090 | .183 | |
| .075 | -.166 | -.238 | -.271 | -.614 | | -.405 | -.222 | -.065 | -.035 | |
| .150 | -.262 | -.249 | -.198 | -.189 | | -.350 | -.225 | -.115 | -.096 | |
| .250 | -.226 | -.201 | -.149 | -.096 | | -.306 | -.230 | -.142 | -.122 | |
| .350 | -.234 | -.201 | -.152 | -.078 | | -.325 | -.256 | -.177 | -.153 | |
| .450 | -.245 | -.223 | -.174 | -.093 | | -.333 | -.289 | -.218 | -.192 | |
| .550 | -.238 | -.232 | -.187 | -.102 | | -.310 | -.290 | -.227 | -.198 | |
| .650 | -.240 | -.230 | -.196 | -.115 | | -.267 | -.255 | -.207 | -.178 | |
| .750 | -.255 | -.249 | -.213 | -.131 | | -.180 | -.177 | -.146 | -.140 | |
| .850 | -.169 | -.165 | -.149 | -.099 | | -.084 | -.085 | -.065 | -.083 | |
| .900 | -.129 | -.124 | -.115 | -.081 | | -.050 | -.059 | -.055 | -.086 | |
| $Z/b_V = 0.66$ | | | | | $Z/b_V = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .499 | .669 | .599 | .368 | | .390 | .578 | .341 | -.116 | |
| .025 | .194 | -.175 | -.865 | -1.537 | | .087 | -.327 | -1.142 | -1.389 | |
| .075 | .022 | -.226 | -.495 | -1.338 | | -.124 | -.364 | -.574 | -1.173 | |
| .150 | -.084 | -.255 | -.448 | -.728 | | -.226 | -.279 | -.312 | -.973 | |
| .250 | -.274 | -.272 | -.349 | -.554 | | -.121 | -.164 | -.252 | -.751 | |
| .350 | -.226 | -.310 | -.347 | -.429 | | | | | | |
| .450 | -.278 | -.332 | -.347 | -.373 | | | | | | |
| .550 | -.293 | -.321 | -.315 | -.315 | | | | | | |
| .650 | -.243 | -.250 | -.232 | -.245 | | | | | | |
| .750 | -.163 | -.155 | -.153 | -.175 | | | | | | |
| .850 | -.095 | -.079 | -.071 | -.106 | | | | | | |
| .900 | -.063 | -.046 | -.038 | -.074 | | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.892 | -.167 | .212 | .449 | | -.1235 | -.289 | .112 | .335 | |
| .075 | -.496 | -.238 | .014 | .189 | | -.673 | -.381 | -.157 | .027 | |
| .150 | -.434 | -.232 | -.062 | .051 | | -.313 | -.291 | -.224 | -.153 | |
| .250 | -.412 | -.280 | -.153 | -.076 | | | | | | |
| .350 | -.364 | -.320 | -.230 | -.165 | | | | | | |
| .450 | -.347 | -.325 | -.268 | -.224 | | | | | | |
| .550 | -.301 | -.294 | -.264 | -.235 | | | | | | |
| .650 | -.227 | -.230 | -.217 | -.208 | | | | | | |
| .750 | -.141 | -.145 | -.150 | -.168 | | | | | | |
| .850 | -.036 | -.043 | -.054 | -.083 | | | | | | |
| .900 | -.001 | -.007 | -.023 | -.071 | | | | | | |

TABLE VI.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL
TAIL, AND HORIZONTAL TAIL

(a) $\alpha = 0^\circ$; $M = 0.60$.

| X C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .636 | .644 | .327 | -.435 | -1.287 | .281 | .728 | .301 | -.433 | -1.248 |
| .025 | .262 | -.113 | -.546 | -1.133 | -2.371 | .322 | -.094 | -.643 | -1.082 | -1.180 |
| .075 | .126 | -.119 | -.375 | -.678 | -1.461 | .142 | -.136 | -.442 | -.939 | -1.143 |
| .150 | .031 | -.140 | -.306 | -.484 | -.686 | .050 | -.143 | -.325 | -.708 | -1.094 |
| .250 | .017 | -.101 | -.202 | -.308 | -.436 | -.013 | -.152 | -.274 | -.445 | -1.048 |
| .350 | -.024 | -.113 | -.177 | -.246 | -.354 | -.068 | -.170 | -.255 | -.345 | -.883 |
| .450 | -.057 | -.126 | -.167 | -.211 | -.315 | -.105 | -.182 | -.232 | -.285 | -.672 |
| .550 | -.066 | -.108 | -.133 | -.165 | -.331 | -.096 | -.152 | -.179 | -.218 | -.505 |
| .650 | -.034 | -.073 | -.091 | -.126 | -.266 | -.073 | -.113 | -.131 | -.158 | -.377 |
| .750 | -.015 | -.036 | -.047 | -.096 | -.183 | -.034 | -.055 | -.066 | -.084 | -.264 |
| .850 | .020 | .010 | .003 | -.031 | -.097 | .024 | .017 | .015 | -.006 | -.150 |
| .900 | .040 | .038 | .038 | .006 | -.041 | .050 | .045 | .050 | .040 | -.092 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.458 | -.032 | .315 | .583 | .815 | -.634 | -.075 | .378 | .592 | .734 |
| .075 | .380 | -.115 | .128 | .338 | .530 | -.424 | -.129 | .156 | .352 | .513 |
| .150 | .294 | -.124 | .050 | .209 | .372 | -.318 | -.133 | .063 | .221 | .363 |
| .250 | -.204 | -.106 | .020 | .137 | .263 | -.260 | -.143 | -.001 | .114 | .233 |
| .350 | -.179 | -.113 | -.017 | .070 | .170 | -.234 | -.157 | -.052 | .043 | .147 |
| .450 | -.165 | -.122 | -.052 | .020 | .105 | -.216 | -.157 | -.084 | -.001 | .082 |
| .550 | -.128 | -.099 | -.052 | .010 | .080 | -.177 | -.138 | -.080 | -.020 | .038 |
| .650 | -.082 | -.059 | -.022 | .029 | .077 | -.117 | -.092 | -.057 | -.008 | .026 |
| .750 | -.034 | -.027 | .001 | .033 | .073 | -.050 | -.032 | -.020 | .015 | .033 |
| .850 | .020 | .026 | .043 | .068 | .089 | .024 | .036 | .054 | .061 | .047 |
| .900 | .045 | .043 | .052 | .068 | .080 | .052 | .052 | .057 | .061 | .031 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .234 | .718 | .253 | -.403 | -.700 | .378 | .672 | .214 | -.294 | -.482 |
| .025 | .334 | -.131 | -.856 | -1.070 | -.765 | .179 | -.177 | -.717 | -.863 | -.556 |
| .075 | .151 | -.152 | -.498 | -.969 | -.751 | .020 | -.163 | -.389 | -.810 | -.554 |
| .150 | .040 | -.163 | -.375 | -.789 | -.742 | -.050 | -.147 | -.290 | -.710 | -.591 |
| .250 | -.031 | -.168 | -.294 | -.549 | -.707 | -.040 | -.110 | -.228 | -.574 | -.589 |
| .350 | -.087 | -.182 | -.260 | -.375 | -.672 | | | | | |
| .450 | -.119 | -.189 | -.234 | -.288 | -.637 | | | | | |
| .550 | -.117 | -.170 | -.195 | -.223 | -.586 | | | | | |
| .650 | -.089 | -.119 | -.131 | -.156 | -.538 | -.080 | -.073 | -.112 | -.391 | -.419 |
| .750 | -.054 | -.055 | -.068 | -.094 | -.463 | -.059 | -.038 | -.087 | -.366 | -.394 |
| .850 | -.008 | -.006 | -.008 | -.036 | -.398 | -.038 | -.008 | -.066 | -.320 | -.371 |
| .900 | .031 | .024 | .024 | -.003 | -.354 | -.015 | .012 | -.047 | -.269 | -.354 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.715 | -.085 | .391 | .588 | .687 | -.567 | -.143 | .223 | .366 | .437 |
| .075 | -.477 | -.147 | .160 | .348 | .493 | -.368 | -.166 | .013 | .105 | .196 |
| .150 | -.336 | -.143 | .059 | .209 | .328 | -.271 | -.152 | -.045 | .006 | .068 |
| .250 | -.285 | -.166 | -.017 | .100 | .198 | | | | | |
| .350 | -.264 | -.177 | -.077 | .017 | .096 | | | | | |
| .450 | -.230 | -.177 | -.103 | -.036 | .029 | | | | | |
| .550 | -.186 | -.154 | -.103 | -.050 | -.013 | | | | | |
| .650 | -.126 | -.108 | -.075 | -.031 | -.027 | -.091 | -.069 | -.068 | -.070 | -.085 |
| .750 | -.057 | -.052 | -.036 | -.008 | -.036 | -.077 | -.045 | -.075 | -.075 | -.132 |
| .850 | .020 | .029 | .031 | .029 | -.039 | -.022 | .015 | -.015 | -.034 | -.129 |
| .900 | .050 | .054 | .052 | .054 | -.076 | -.015 | .026 | .001 | -.027 | -.155 |

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TABLE VI. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL
TAIL, AND HORIZONTAL TAIL - Continued

(b) $\alpha = 0^\circ$; $M = 0.80$.

| $\frac{X}{C_V}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|---|-------|--------|--------|----------------|---|-------|--------|--------|-------|
| | $\beta = -3.9^\circ \quad \beta = 0^\circ \quad \beta = 3.9^\circ \quad \beta = 7.9^\circ \quad \beta = 12.7^\circ$ | | | | | $\beta = -3.9^\circ \quad \beta = 0^\circ \quad \beta = 3.9^\circ \quad \beta = 7.9^\circ \quad \beta = 12.7^\circ$ | | | | |
| | $Z/b_V = 0.11$ | | | | | $Z/b_V = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .736 | .664 | .523 | .187 | -.235 | .466 | .760 | .555 | .048 | -.570 |
| .025 | .269 | -.075 | -.534 | -1.147 | -1.481 | .319 | -.080 | -.929 | -1.641 | -.974 |
| .075 | .140 | -.099 | -.365 | -.863 | -1.237 | .146 | .136 | -.446 | -1.459 | -.985 |
| .150 | .046 | -.142 | -.323 | -.535 | -.982 | .055 | .146 | -.339 | -.512 | -.935 |
| .250 | .022 | .107 | -.217 | -.303 | -.617 | .014 | .163 | -.282 | -.377 | -.846 |
| .350 | -.020 | -.122 | -.184 | -.241 | -.407 | .078 | .183 | -.270 | -.342 | -.748 |
| .450 | -.069 | -.137 | -.173 | -.215 | -.342 | .122 | .202 | -.246 | -.288 | -.633 |
| .550 | -.063 | -.113 | -.136 | -.166 | -.291 | .111 | .164 | -.185 | -.210 | -.522 |
| .650 | -.036 | -.078 | -.089 | -.130 | -.217 | .086 | .122 | -.125 | -.139 | -.431 |
| .750 | -.013 | -.048 | -.039 | -.084 | -.175 | .034 | .051 | -.054 | -.060 | -.332 |
| .850 | .020 | -.014 | -.020 | -.021 | -.104 | .036 | .031 | -.035 | -.020 | -.235 |
| .900 | .048 | .049 | .054 | .020 | -.050 | .075 | .074 | .075 | .064 | -.169 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.411 | -.008 | .314 | .583 | .812 | -.934 | -.058 | .359 | .588 | .745 |
| .075 | -.393 | -.107 | .130 | .343 | .552 | .431 | .126 | .154 | .356 | .539 |
| .150 | -.301 | -.120 | .054 | .222 | .392 | .331 | .140 | .060 | .225 | .385 |
| .250 | -.219 | -.107 | .021 | .154 | .291 | .273 | .149 | -.009 | .123 | .259 |
| .350 | -.189 | -.119 | -.026 | .081 | .192 | .248 | .166 | -.065 | .049 | .170 |
| .450 | -.166 | -.131 | -.066 | .020 | .113 | .226 | .176 | -.101 | -.010 | .085 |
| .550 | -.128 | -.107 | -.060 | .008 | .082 | .178 | .152 | -.104 | -.031 | .041 |
| .650 | -.076 | -.063 | -.027 | .026 | .085 | .110 | .102 | -.071 | -.016 | .029 |
| .750 | -.033 | -.030 | -.003 | .035 | .072 | .030 | -.023 | -.018 | .017 | .026 |
| .850 | .031 | .031 | .039 | .069 | .080 | .048 | .051 | .057 | .067 | .032 |
| .900 | .058 | .055 | .053 | .072 | .069 | .075 | .069 | .068 | .070 | .012 |
| $Z/b_V = 0.66$ | | | | | $Z/b_V = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .434 | .748 | .495 | .013 | -.395 | .463 | .695 | .383 | -.110 | -.296 |
| .025 | .334 | -.114 | -.1086 | -1.312 | -.707 | .155 | -.228 | -1.101 | -1.248 | -.492 |
| .075 | .154 | -.154 | -.535 | -1.174 | -.710 | -.004 | -.187 | -.484 | -1.043 | -.483 |
| .150 | .040 | -.178 | -.398 | -.957 | -.707 | -.075 | -.163 | -.280 | -.833 | -.523 |
| .250 | -.042 | -.186 | -.308 | -.743 | -.659 | -.046 | -.117 | -.235 | -.579 | -.502 |
| .350 | -.104 | -.201 | -.268 | -.518 | -.621 | | | | | |
| .450 | -.137 | -.205 | -.240 | -.329 | -.573 | | | | | |
| .550 | -.134 | -.181 | -.191 | -.215 | -.522 | | | | | |
| .650 | -.098 | -.125 | -.122 | -.130 | -.475 | -.067 | -.063 | -.096 | -.326 | -.391 |
| .750 | -.049 | -.175 | -.042 | -.057 | -.425 | -.049 | -.023 | -.063 | -.309 | -.366 |
| .850 | -.034 | .025 | .026 | .005 | -.371 | -.014 | .025 | -.036 | -.267 | -.336 |
| .900 | .049 | .071 | .057 | .029 | -.341 | .011 | .045 | -.015 | -.221 | -.321 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.249 | -.069 | .376 | .580 | .707 | -1.089 | -.161 | .198 | .365 | .475 |
| .075 | -.502 | -.145 | .154 | .351 | .514 | -.430 | -.186 | -.026 | .096 | .225 |
| .150 | -.348 | -.146 | .057 | .216 | .361 | -.270 | -.158 | -.069 | -.016 | .092 |
| .250 | -.301 | -.176 | -.024 | .102 | .225 | | | | | |
| .350 | -.272 | -.195 | -.098 | .008 | .116 | | | | | |
| .450 | -.231 | -.193 | -.125 | -.042 | .044 | | | | | |
| .550 | -.181 | -.166 | -.122 | -.062 | -.003 | | | | | |
| .650 | -.108 | -.108 | -.084 | -.042 | -.027 | -.072 | -.051 | -.056 | -.063 | -.072 |
| .750 | -.036 | -.031 | -.027 | -.010 | -.039 | -.054 | -.020 | -.053 | -.063 | -.127 |
| .850 | .052 | .054 | .051 | .045 | -.036 | .004 | .043 | .015 | -.013 | -.115 |
| .900 | .083 | .083 | .075 | .061 | -.068 | .014 | .058 | .027 | -.015 | -.142 |

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TABLE VI. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL
TAIL, AND HORIZONTAL TAIL - Continued

(c) $\alpha = 0^\circ$; $M = 0.85$.

| $\frac{x}{C_V}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_V = 0.11$ | | | | | $z/b_V = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .767 | .670 | .568 | .298 | -.085 | .527 | .771 | .604 | .187 | .409 |
| .025 | .269 | -.069 | -.523 | -1.069 | -1.288 | .317 | -.082 | -1.038 | -1.475 | .922 |
| .075 | .139 | -.097 | -.379 | -.831 | -1.123 | .139 | .140 | -.422 | -1.333 | .934 |
| .150 | .039 | -.143 | -.342 | -.681 | -.958 | .052 | .154 | -.352 | -1.183 | .925 |
| .250 | .011 | -.111 | -.229 | -.364 | -.761 | -.026 | .170 | -.300 | -.334 | .850 |
| .350 | -.033 | -.123 | -.193 | -.255 | -.595 | -.089 | .196 | -.283 | -.284 | .774 |
| .450 | -.083 | -.147 | -.186 | -.206 | -.483 | .140 | .221 | -.261 | -.264 | .676 |
| .550 | -.082 | -.124 | -.142 | -.159 | -.391 | .131 | .182 | -.195 | -.203 | .581 |
| .650 | -.058 | -.083 | -.097 | -.129 | -.304 | .102 | .134 | -.129 | -.131 | .500 |
| .750 | -.033 | -.049 | -.046 | -.081 | -.259 | .045 | -.058 | -.057 | -.056 | .408 |
| .850 | .018 | .012 | .013 | -.013 | -.171 | .029 | .026 | .031 | .036 | .318 |
| .900 | .048 | .049 | .055 | .025 | -.114 | .072 | .071 | .074 | .073 | .254 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.382 | .000 | .318 | .588 | .811 | -.949 | -.075 | .356 | .592 | .739 |
| .075 | -.402 | -.106 | .133 | .352 | .549 | -.418 | -.133 | .149 | .359 | .526 |
| .150 | -.326 | -.123 | .057 | .228 | .385 | -.349 | -.147 | .055 | .227 | .369 |
| .250 | -.234 | -.111 | .018 | .159 | .274 | -.288 | -.162 | -.019 | .124 | .242 |
| .350 | -.202 | -.128 | -.033 | .079 | .171 | -.268 | -.182 | -.077 | .045 | .147 |
| .450 | -.182 | -.143 | -.077 | .015 | .086 | -.240 | -.194 | -.118 | -.020 | .055 |
| .550 | -.137 | -.117 | -.071 | .004 | .055 | -.188 | -.165 | -.121 | -.042 | .004 |
| .650 | -.082 | -.072 | -.038 | .028 | .055 | -.117 | -.114 | -.087 | -.026 | .014 |
| .750 | -.035 | -.039 | -.013 | .035 | .037 | -.033 | -.035 | -.027 | .009 | .019 |
| .850 | .034 | .029 | .037 | .067 | .039 | .049 | .050 | .055 | .067 | .014 |
| .900 | .061 | .053 | .054 | .073 | .023 | .079 | .070 | .067 | .073 | .045 |
| $z/b_V = 0.66$ | | | | | $z/b_V = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .492 | .753 | .544 | .141 | -.321 | .494 | .697 | .420 | .011 | .297 |
| .025 | .326 | -.120 | -1.158 | -1.568 | -.817 | .135 | -.235 | -1.037 | -1.254 | .553 |
| .075 | .148 | -.164 | -.625 | -1.398 | -.824 | -.038 | -.215 | -.676 | -1.090 | .550 |
| .150 | .028 | -.188 | -.405 | -1.134 | -.839 | -.105 | -.178 | -.254 | -.873 | .599 |
| .250 | -.057 | -.202 | -.314 | -.711 | -.713 | -.061 | -.127 | -.243 | -.620 | .578 |
| .350 | -.120 | -.225 | -.277 | -.408 | -.683 | | | | | |
| .450 | -.165 | -.230 | -.257 | -.279 | -.647 | | | | | |
| .550 | -.152 | -.195 | -.203 | -.182 | -.602 | | | | | |
| .650 | -.112 | -.133 | -.131 | -.107 | -.550 | -.075 | -.070 | -.104 | -.376 | .461 |
| .750 | -.058 | -.051 | -.050 | -.040 | -.486 | -.051 | -.032 | -.070 | -.337 | .434 |
| .850 | .028 | .023 | .021 | .018 | -.416 | -.009 | .020 | -.041 | -.286 | .406 |
| .900 | .051 | .051 | .054 | .047 | -.380 | .013 | .047 | -.021 | -.244 | .389 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.152 | -.082 | .366 | .583 | .702 | -.140 | -.188 | .180 | .361 | .464 |
| .075 | -.518 | -.160 | .146 | .352 | .500 | -.672 | -.225 | -.058 | .080 | .210 |
| .150 | -.370 | -.162 | .050 | .217 | .344 | -.205 | -.178 | -.100 | -.056 | .052 |
| .250 | -.315 | -.196 | -.041 | .098 | .203 | | | | | |
| .350 | -.281 | -.219 | -.118 | -.006 | .089 | | | | | |
| .450 | -.241 | -.216 | -.152 | -.063 | .000 | | | | | |
| .550 | -.192 | -.181 | -.145 | -.077 | -.052 | | | | | |
| .650 | -.114 | -.114 | -.100 | -.056 | -.079 | -.085 | -.056 | -.067 | -.070 | .130 |
| .750 | -.035 | -.039 | -.041 | -.019 | -.091 | -.061 | -.028 | -.053 | -.069 | .180 |
| .850 | .058 | .054 | .051 | .053 | -.081 | .006 | .044 | .018 | -.012 | .161 |
| .900 | .093 | .085 | .081 | .070 | -.115 | .017 | .057 | .028 | -.022 | .197 |

~~CONFIDENTIAL~~

TABLE VI.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL
TAIL, AND HORIZONTAL TAIL - Continued

(d) $\alpha = 0^\circ$; $M = 0.90$.

| $\frac{x}{C_V}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_V = 0.11$ | | | | | $z/b_V = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .799 | .681 | .613 | .394 | .068 | .585 | .785 | .657 | .318 | .223 |
| .025 | .278 | -.052 | -.484 | -.960 | -1.156 | .316 | -.068 | -.937 | -1.287 | -.825 |
| .075 | .147 | -.092 | -.388 | -.762 | -.987 | .140 | -.140 | -.706 | -1.176 | -.839 |
| .150 | .041 | -.153 | -.383 | -.678 | -.845 | .047 | -.162 | -.411 | -1.068 | -.820 |
| .250 | .013 | -.125 | -.258 | -.521 | -.687 | -.027 | -.181 | -.323 | -.648 | -.764 |
| .350 | -.034 | -.138 | -.217 | -.344 | -.581 | -.097 | -.218 | -.344 | -.470 | -.708 |
| .450 | -.091 | -.173 | -.216 | -.279 | -.504 | .160 | -.255 | -.289 | -.305 | -.633 |
| .550 | -.090 | -.146 | -.157 | -.183 | -.419 | .152 | -.210 | -.204 | -.155 | -.551 |
| .650 | -.061 | -.101 | -.098 | -.124 | -.345 | .117 | -.149 | -.132 | -.099 | -.484 |
| .750 | -.034 | -.062 | -.050 | -.075 | -.296 | .053 | -.056 | -.053 | -.036 | -.408 |
| .850 | .012 | .012 | .018 | -.012 | -.204 | .035 | .033 | .041 | .044 | -.337 |
| .900 | .041 | .051 | .055 | .030 | -.135 | .079 | .083 | .086 | .082 | -.266 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.334 | .005 | .325 | .580 | .821 | -.842 | -.072 | .352 | .580 | .754 |
| .075 | -.407 | -.108 | .139 | .347 | .565 | -.605 | -.146 | .149 | .347 | .541 |
| .150 | -.346 | -.133 | .054 | .221 | .402 | -.377 | -.157 | .050 | .213 | .388 |
| .250 | -.246 | -.126 | .013 | .145 | .294 | -.301 | -.178 | -.026 | .107 | .263 |
| .350 | -.220 | -.148 | -.042 | .060 | .191 | -.299 | -.210 | -.092 | .019 | .164 |
| .450 | -.195 | -.167 | -.090 | -.009 | .102 | -.247 | -.229 | -.142 | -.051 | .064 |
| .550 | -.136 | -.134 | -.092 | -.025 | .063 | -.185 | -.193 | -.150 | -.079 | .010 |
| .650 | -.077 | -.080 | -.050 | .005 | .063 | -.109 | -.128 | -.105 | -.059 | -.010 |
| .750 | -.026 | -.040 | -.027 | .013 | .043 | -.023 | -.027 | -.036 | -.010 | -.017 |
| .850 | .041 | .028 | .027 | .049 | .032 | .064 | .056 | .050 | .052 | -.018 |
| .900 | .071 | .059 | .043 | .053 | .013 | .091 | .080 | .067 | .063 | -.048 |
| $z/b_V = 0.66$ | | | | | $z/b_V = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .544 | .769 | .604 | .271 | -.166 | .532 | .702 | .469 | .144 | -.199 |
| .025 | .327 | -.105 | -.052 | -1.378 | -.775 | .085 | -.271 | -.985 | -1.318 | -.559 |
| .075 | .146 | -.162 | -.887 | -.1248 | -.775 | -.069 | -.277 | -.969 | -1.285 | -.513 |
| .150 | .022 | -.198 | -.485 | -.151 | -.798 | -.173 | -.214 | -.500 | -1.114 | -.556 |
| .250 | -.070 | -.229 | -.400 | -.1093 | -.655 | -.074 | -.133 | -.162 | -.964 | -.550 |
| .350 | -.149 | -.266 | -.273 | -.662 | -.629 | | | | | |
| .450 | -.192 | -.269 | -.241 | -.275 | -.601 | | | | | |
| .550 | -.176 | -.223 | -.210 | -.101 | -.562 | | | | | |
| .650 | -.124 | -.141 | -.125 | -.053 | -.527 | | | | | |
| .750 | -.063 | -.037 | -.042 | -.014 | -.477 | | | | | |
| .850 | .032 | .037 | .033 | .030 | -.422 | | | | | |
| .900 | .059 | .067 | .067 | .053 | -.380 | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.992 | -.085 | .381 | .568 | .716 | -.1037 | -.215 | .167 | .344 | .488 |
| .075 | -.801 | -.171 | .143 | .340 | .515 | -.892 | -.287 | -.097 | .049 | .228 |
| .150 | -.350 | -.167 | .045 | .206 | .364 | -.293 | -.211 | -.189 | -.108 | .068 |
| .250 | -.381 | -.222 | -.062 | .075 | .224 | | | | | |
| .350 | -.243 | -.261 | -.152 | -.041 | .102 | | | | | |
| .450 | -.246 | -.253 | -.192 | -.113 | .009 | | | | | |
| .550 | -.192 | -.205 | -.176 | -.132 | -.053 | | | | | |
| .650 | -.106 | -.120 | -.116 | -.094 | -.069 | | | | | |
| .750 | -.024 | -.031 | -.045 | -.039 | -.085 | | | | | |
| .850 | .072 | .065 | .057 | .044 | -.068 | | | | | |
| .900 | .103 | .101 | .086 | .067 | -.099 | | | | | |

TABLE VI.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(e) $\alpha = 0^\circ$; $M = 0.92$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .811 | .684 | .627 | .442 | .111 | .593 | .791 | .681 | .381 | -.179 |
| .025 | .267 | -.060 | -.466 | -.885 | -1.154 | .309 | -.075 | -.927 | -1.174 | -.816 |
| .075 | .133 | -.100 | -.389 | -.714 | -.973 | .126 | -.151 | -.719 | -1.070 | -.825 |
| .150 | .019 | -.166 | -.396 | -.650 | -.832 | .030 | -.174 | -.434 | -.972 | -.792 |
| .250 | -.011 | -.139 | -.295 | -.570 | -.671 | -.050 | -.195 | -.341 | -.713 | -.763 |
| .350 | -.060 | -.155 | -.238 | -.406 | -.578 | -.126 | -.244 | -.360 | -.576 | -.710 |
| .450 | -.124 | -.196 | -.238 | -.365 | -.531 | -.203 | -.295 | -.365 | -.494 | -.643 |
| .550 | -.129 | -.178 | -.179 | -.273 | -.446 | -.199 | -.242 | -.190 | -.288 | -.571 |
| .650 | -.094 | -.120 | -.104 | -.170 | -.379 | -.149 | -.167 | -.125 | -.084 | -.506 |
| .750 | -.069 | -.075 | -.052 | -.088 | -.343 | -.078 | -.068 | -.048 | -.016 | -.434 |
| .850 | -.017 | -.007 | .019 | -.020 | -.251 | .010 | .031 | .044 | .052 | -.376 |
| .900 | -.017 | .043 | .059 | .027 | -.186 | .055 | .077 | .090 | .094 | -.312 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.354 | -.002 | .324 | .577 | .824 | -.903 | -.094 | .353 | .564 | .750 |
| .075 | -.438 | -.125 | .139 | .342 | .567 | -.677 | -.166 | .147 | .339 | .538 |
| .150 | -.403 | -.151 | .050 | .213 | .399 | -.450 | -.174 | .048 | .208 | .387 |
| .250 | -.306 | -.143 | .009 | .138 | .292 | -.342 | -.198 | -.031 | .100 | .261 |
| .350 | -.259 | -.163 | -.055 | .048 | .189 | -.350 | -.232 | -.101 | .008 | .161 |
| .450 | -.236 | -.186 | -.106 | -.026 | .092 | -.327 | -.264 | -.163 | -.072 | .055 |
| .550 | -.168 | -.161 | -.108 | -.046 | .056 | -.200 | -.220 | -.171 | -.105 | -.002 |
| .650 | -.100 | -.096 | -.063 | -.017 | .051 | -.126 | -.142 | -.125 | -.091 | -.025 |
| .750 | -.049 | -.052 | -.038 | -.009 | .024 | -.041 | -.039 | -.042 | -.037 | -.035 |
| .850 | .022 | .018 | .023 | .032 | .011 | .051 | .050 | .048 | .040 | -.039 |
| .900 | .050 | .051 | .039 | .043 | -.020 | .077 | .072 | .065 | .060 | -.077 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .550 | .769 | .631 | .334 | -.127 | .538 | .706 | .497 | .205 | -.179 |
| .025 | .315 | -.114 | -.1030 | -.1260 | -.758 | .124 | -.258 | -.1051 | -.1218 | -.527 |
| .075 | .132 | -.174 | -.886 | -.1146 | -.762 | -.092 | -.299 | -.968 | -.173 | -.512 |
| .150 | .007 | -.212 | -.711 | -.1054 | -.787 | -.248 | -.258 | -.785 | -.1038 | -.551 |
| .250 | -.092 | -.249 | -.402 | -.1008 | -.667 | -.133 | -.150 | -.262 | -.874 | -.554 |
| .350 | -.184 | -.318 | -.439 | -.968 | -.637 | | | | | |
| .450 | -.251 | -.299 | -.198 | -.545 | -.606 | | | | | |
| .550 | -.225 | -.252 | -.186 | -.133 | -.575 | | | | | |
| .650 | -.161 | -.139 | -.118 | -.021 | -.550 | | | | | |
| .750 | -.061 | -.046 | -.035 | .022 | -.509 | | | | | |
| .850 | .015 | .032 | .042 | .060 | -.456 | | | | | |
| .900 | .041 | .064 | .077 | .078 | -.424 | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -1.021 | -.102 | .359 | .559 | .712 | -1.054 | -.234 | .168 | .342 | .490 |
| .075 | -.858 | -.198 | .143 | .330 | .511 | -.939 | -.352 | -.102 | .049 | .225 |
| .150 | -.573 | -.190 | .046 | .204 | .362 | -.657 | -.260 | -.224 | -.119 | .062 |
| .250 | -.410 | -.246 | -.068 | .068 | .221 | | | | | |
| .350 | -.425 | -.319 | -.172 | -.061 | .092 | | | | | |
| .450 | -.219 | -.277 | -.225 | -.144 | -.010 | | | | | |
| .550 | -.196 | -.227 | -.199 | -.174 | -.075 | | | | | |
| .650 | -.126 | -.126 | -.124 | -.128 | -.098 | | | | | |
| .750 | -.041 | -.038 | -.044 | -.059 | -.111 | | | | | |
| .850 | .059 | .061 | .059 | .041 | -.091 | | | | | |
| .900 | .090 | .093 | .088 | .073 | -.125 | | | | | |

TABLE VI.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(f) $\alpha = 9.4^\circ$; $M = 0.60$.

| $\frac{x}{C_V}$ | C_p for - | | | | | C_p for - | | | | | | | | | |
|-------------------|----------------------|--------|-------------------|--------|---------------------|---------------------|----------------------|----------------------|--------|-------------------|--------|---------------------|---------------------|----------------------|--------|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | |
| | | | $Z/b_V = 0.11$ | | | | | | | $Z/b_V = 0.38$ | | | | | |
| <i>Left side</i> | | | | | | | | | | | | | | | |
| .000 | .451 | .820 | .562 | .091 | -1.139 | .032 | .629 | .041 | -1.040 | -1.040 | .629 | .041 | -1.040 | -1.040 | -1.779 |
| .025 | -1.127 | -1.127 | -1.041 | -1.463 | -1.002 | .323 | -1.080 | -1.747 | -1.359 | -1.359 | -1.747 | -1.359 | -1.647 | -1.647 | |
| .075 | .006 | -1.130 | -1.169 | -1.417 | -1.702 | .155 | -1.107 | -1.416 | -1.452 | -2.034 | -1.416 | -1.452 | -1.452 | -2.034 | |
| .150 | .013 | -1.148 | -1.215 | -1.375 | -1.524 | .071 | -1.112 | -1.295 | -1.428 | -1.665 | -1.295 | -1.428 | -1.428 | -1.665 | |
| .250 | .011 | -1.127 | -1.158 | -1.271 | -1.364 | .004 | -1.127 | -1.251 | -1.320 | -1.433 | -1.251 | -1.320 | -1.320 | -1.433 | |
| .350 | -1.023 | -1.123 | -1.164 | -1.234 | -1.301 | -.058 | -1.155 | -1.249 | -1.320 | -1.389 | -1.155 | -1.249 | -1.249 | -1.389 | |
| .450 | -1.065 | -1.155 | -1.176 | -1.228 | -1.287 | -.097 | -1.173 | -1.235 | -1.290 | -1.371 | -1.173 | -1.235 | -1.235 | -1.371 | |
| .550 | -1.095 | -1.173 | -1.180 | -1.216 | -1.273 | -.099 | -1.155 | -1.199 | -1.241 | -1.324 | -1.155 | -1.199 | -1.199 | -1.324 | |
| .650 | -1.099 | -1.159 | -1.160 | -1.188 | -1.241 | -.097 | -1.132 | -1.160 | -1.200 | -1.280 | -1.132 | -1.160 | -1.160 | -1.280 | |
| .750 | -1.104 | -1.150 | -1.144 | -1.156 | -1.206 | -.067 | -1.089 | -1.110 | -1.142 | -1.224 | -1.089 | -1.110 | -1.110 | -1.224 | |
| .850 | -1.065 | -1.100 | -1.089 | -1.091 | -1.120 | -.012 | -1.016 | -1.034 | -1.059 | -1.143 | -1.016 | -1.034 | -1.034 | -1.143 | |
| .900 | -1.028 | -1.064 | -1.048 | -1.040 | -1.062 | .022 | .021 | .002 | -1.015 | -1.085 | .021 | .002 | -1.015 | -1.085 | |
| <i>Right side</i> | | | | | | | | | | | | | | | |
| .025 | .029 | -.089 | -.055 | .195 | .662 | -.604 | -.018 | .386 | .532 | .609 | -.018 | .386 | .532 | .532 | .609 |
| .075 | -1.168 | -1.143 | .014 | .174 | .506 | -.372 | -.073 | .183 | .350 | .479 | -.073 | .183 | .350 | .350 | .479 |
| .150 | -1.202 | -1.132 | .036 | .160 | .390 | -.283 | -.089 | .091 | .223 | .356 | -.089 | .091 | .223 | .223 | .356 |
| .250 | -1.161 | -1.114 | .030 | .156 | .305 | -.234 | -.107 | .023 | .128 | .242 | -.107 | .023 | .128 | .128 | .242 |
| .350 | -1.168 | -1.123 | -.009 | .112 | .216 | -.225 | -.127 | .023 | .059 | .168 | -.127 | .023 | .059 | .059 | .168 |
| .450 | -1.182 | -1.150 | -.055 | .061 | .138 | -.218 | -.141 | .075 | .001 | .091 | -.141 | .075 | .001 | .001 | .091 |
| .550 | -1.175 | -1.159 | -.073 | .020 | .100 | -.191 | -.139 | .089 | -.031 | .049 | -.191 | -.139 | -.031 | -.031 | .049 |
| .650 | -1.159 | -1.150 | -.080 | -.001 | .068 | -.145 | -.118 | .073 | -.031 | .033 | -.145 | -.118 | -.031 | -.031 | .033 |
| .750 | -1.136 | -1.137 | -.082 | -.020 | .042 | -.090 | -.073 | .043 | -.010 | .029 | -.090 | -.073 | -.010 | -.010 | .029 |
| .850 | -1.069 | -1.080 | -.037 | .015 | .063 | -.017 | .009 | .014 | .031 | .045 | -.017 | .009 | .014 | .031 | .045 |
| .900 | -1.042 | -1.055 | -.014 | .024 | .059 | .011 | .018 | .025 | .031 | .038 | .011 | .018 | .025 | .031 | .038 |
| $Z/b_V = 0.66$ | | | | | | | | $Z/b_V = 0.93$ | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | | | | |
| .000 | -.005 | .563 | -.098 | -.786 | -1.255 | .151 | .506 | -.096 | -.431 | -.802 | .151 | .506 | -.096 | -.431 | -.802 |
| .025 | .293 | -1.137 | -.945 | -1.107 | -1.009 | .135 | -1.221 | -.804 | -.646 | -.619 | .135 | -1.221 | -.804 | -.646 | -.619 |
| .075 | .132 | -1.150 | -1.482 | -1.077 | -1.002 | -.028 | -1.196 | -.427 | -.613 | -.614 | -.028 | -1.196 | -.427 | -.613 | -.614 |
| .150 | .034 | -1.157 | -1.356 | -1.040 | -1.004 | .113 | -1.166 | -.267 | -.576 | -.605 | .113 | -1.166 | -.267 | -.576 | -.605 |
| .250 | -1.037 | -1.159 | -.281 | -.807 | -1.018 | -.072 | -1.114 | -.187 | -.488 | -.570 | -.072 | -1.114 | -.187 | -.488 | -.570 |
| .350 | -1.085 | -1.168 | -.258 | -.419 | -.927 | | | | | | | | | | |
| .450 | -1.122 | -1.182 | -.231 | -.232 | -.765 | | | | | | | | | | |
| .550 | -1.127 | -1.166 | -.201 | -.202 | -.607 | | | | | | | | | | |
| .650 | -1.097 | -1.125 | -.146 | -.156 | -.440 | -.097 | -.066 | -.107 | -.331 | -.477 | -.097 | -.066 | -.107 | -.331 | -.477 |
| .750 | -1.058 | -1.071 | -.085 | -.098 | -.287 | -.062 | -.025 | -.073 | -.292 | -.461 | -.062 | -.025 | -.073 | -.292 | -.461 |
| .850 | -1.014 | -1.016 | -.025 | -.040 | -.176 | -.028 | -.007 | -.043 | -.248 | -.433 | -.028 | -.007 | -.043 | -.248 | -.433 |
| .900 | .004 | .007 | .002 | -.010 | -.129 | -.003 | .027 | -.028 | -.211 | -.408 | -.003 | .027 | -.028 | -.211 | -.408 |
| <i>Right side</i> | | | | | | | | | | | | | | | |
| .025 | -.730 | -.043 | .367 | .505 | .558 | -.590 | -.134 | .185 | .276 | .332 | -.590 | -.134 | .185 | .276 | .332 |
| .075 | -.434 | .112 | .157 | .327 | .442 | -.370 | -.173 | -.023 | .068 | .156 | -.370 | -.173 | -.023 | .068 | .156 |
| .150 | -.306 | -.118 | .062 | .195 | .316 | -.244 | -.159 | -.107 | -.068 | -.006 | -.244 | -.159 | -.107 | -.068 | -.006 |
| .250 | -.271 | -.146 | -.016 | .091 | .193 | | | | | | | | | | |
| .350 | -.248 | -.162 | -.069 | .015 | .103 | | | | | | | | | | |
| .450 | -.223 | -.168 | -.101 | -.031 | .040 | | | | | | | | | | |
| .550 | -.186 | -.153 | -.110 | -.057 | .001 | | | | | | | | | | |
| .650 | -.134 | -.123 | -.078 | -.047 | -.013 | -.053 | -.059 | -.085 | -.105 | -.120 | -.053 | -.059 | -.085 | -.105 | -.120 |
| .750 | -.076 | -.073 | -.048 | -.027 | -.009 | -.069 | -.034 | -.073 | -.105 | -.157 | -.069 | -.034 | -.073 | -.105 | -.157 |
| .850 | .004 | .025 | .023 | .024 | .012 | -.014 | .023 | -.009 | -.061 | -.141 | -.014 | .023 | -.009 | -.061 | -.141 |
| .900 | .029 | .039 | .036 | .038 | .015 | .006 | .039 | -.002 | -.061 | -.157 | .006 | .039 | -.002 | -.061 | -.157 |

TABLE VI.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(g) $\alpha = 9.6^\circ$; $M = 0.80$.

| $\frac{\kappa}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| Left side | | | | | | | | | | |
| .000 | .451 | .871 | .577 | .270 | -.398 | .262 | .667 | .236 | -.384 | -.962 |
| .025 | -.129 | .018 | -.372 | -.575 | .324 | -.068 | -.857 | -.1336 | -1.222 | |
| .075 | .008 | -.120 | -.152 | -.406 | -.524 | .164 | -.098 | -.441 | -1.307 | -1.222 |
| .150 | .023 | -.144 | -.236 | -.416 | -.451 | .081 | -.103 | -.294 | -.717 | -1.088 |
| .250 | .022 | -.120 | -.170 | -.296 | -.236 | .014 | -.121 | -.259 | -.316 | -.684 |
| .350 | -.013 | -.118 | -.174 | -.244 | -.188 | -.056 | -.164 | -.262 | -.320 | -.379 |
| .450 | -.060 | -.153 | -.190 | -.232 | -.174 | -.107 | -.194 | -.256 | -.301 | -.293 |
| .550 | -.100 | -.184 | -.201 | -.224 | -.155 | -.121 | -.181 | -.222 | -.264 | -.249 |
| .650 | -.119 | -.179 | -.183 | -.205 | -.141 | -.122 | -.159 | -.184 | -.226 | -.207 |
| .750 | -.127 | -.185 | -.178 | -.185 | -.120 | -.086 | -.107 | -.122 | -.157 | -.149 |
| .850 | -.084 | -.121 | -.106 | -.105 | -.045 | -.019 | -.023 | -.033 | -.066 | -.047 |
| .900 | -.053 | -.075 | -.060 | -.047 | .018 | -.017 | -.021 | -.016 | -.011 | .013 |
| Right side | | | | | | | | | | |
| .025 | .102 | -.065 | -.076 | .195 | .626 | -.717 | -.011 | .386 | .539 | .691 |
| .075 | -.148 | -.141 | .018 | .187 | .555 | -.380 | -.068 | .193 | .353 | .566 |
| .150 | -.209 | -.130 | .042 | .152 | .487 | -.279 | -.080 | .100 | .236 | .450 |
| .250 | -.163 | -.109 | .034 | .148 | .411 | -.239 | -.103 | .033 | .148 | .350 |
| .350 | -.172 | -.120 | -.005 | .110 | .321 | -.233 | -.132 | -.024 | .071 | .274 |
| .450 | -.183 | -.147 | -.056 | .062 | .247 | -.232 | -.164 | -.082 | -.003 | .195 |
| .550 | -.180 | -.165 | -.082 | .021 | .198 | -.206 | -.164 | -.105 | -.041 | .148 |
| .650 | -.166 | -.164 | -.094 | -.011 | .165 | -.157 | -.141 | -.097 | -.052 | .122 |
| .750 | -.162 | -.168 | -.105 | -.037 | .129 | -.091 | -.084 | -.060 | -.028 | .118 |
| .850 | -.098 | -.056 | -.006 | .141 | -.009 | -.007 | -.010 | -.021 | .136 | |
| .900 | -.066 | -.028 | -.007 | .143 | -.020 | -.019 | -.024 | -.026 | .123 | |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| Left side | | | | | | | | | | |
| .000 | .193 | .592 | .154 | -.392 | -.751 | .242 | .520 | .096 | -.285 | -.614 |
| .025 | -.293 | -.126 | -.987 | -.1031 | -.701 | .130 | -.237 | -.729 | -.595 | -.438 |
| .075 | .143 | -.146 | -.622 | -.1012 | -.726 | -.043 | -.237 | -.583 | -.580 | -.437 |
| .150 | .034 | -.161 | -.369 | -.1015 | -.698 | -.142 | -.184 | -.381 | -.541 | -.430 |
| .250 | -.037 | -.173 | -.302 | -.909 | -.669 | -.071 | -.117 | -.221 | -.471 | -.405 |
| .350 | -.094 | -.194 | -.271 | -.645 | -.633 | | | | | |
| .450 | -.145 | -.205 | -.245 | -.265 | -.564 | | | | | |
| .550 | -.157 | -.194 | -.212 | -.185 | -.477 | | | | | |
| .650 | -.121 | -.142 | -.148 | -.157 | -.370 | -.086 | -.055 | -.099 | -.339 | -.301 |
| .750 | -.068 | -.069 | -.076 | -.095 | -.264 | -.043 | -.008 | -.060 | .316 | -.282 |
| .850 | -.009 | -.002 | -.008 | -.035 | -.168 | -.010 | -.027 | -.019 | -.272 | -.254 |
| .900 | .016 | .024 | .025 | -.002 | -.121 | .014 | .050 | -.007 | -.246 | -.246 |
| Right side | | | | | | | | | | |
| .025 | -.907 | -.042 | .356 | .510 | .642 | -.819 | -.147 | .172 | .305 | .453 |
| .075 | -.476 | -.110 | .163 | .328 | .526 | -.456 | -.213 | -.050 | .079 | .281 |
| .150 | -.312 | -.120 | .068 | .206 | .414 | -.242 | -.182 | -.146 | -.083 | .111 |
| .250 | -.273 | -.159 | -.021 | .096 | .303 | | | | | |
| .350 | -.260 | -.182 | -.088 | .009 | .209 | | | | | |
| .450 | -.235 | -.193 | -.125 | -.055 | .139 | | | | | |
| .550 | -.195 | -.175 | -.132 | -.083 | .094 | | | | | |
| .650 | -.135 | -.132 | -.099 | -.067 | .076 | -.034 | -.051 | -.074 | -.107 | -.020 |
| .750 | -.063 | -.078 | -.059 | -.040 | .071 | -.045 | -.017 | -.059 | -.115 | -.052 |
| .850 | .028 | .041 | .024 | .023 | .086 | .022 | .048 | .007 | -.067 | -.040 |
| .900 | .054 | .059 | .050 | .045 | .074 | -.037 | -.062 | -.025 | -.066 | -.062 |

TABLE VI. - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL
TAIL, AND HORIZONTAL TAIL - Continued

(h) $\alpha = 9.7^\circ$; $M = 0.85$.

| X C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .461 | .895 | .586 | .304 | -.482 | .318 | .679 | .316 | -.231 | -.910 |
| .025 | -.123 | .047 | -.331 | -.634 | -.325 | -.072 | -.847 | -.300 | -.426 | -.1426 |
| .075 | .006 | -.123 | -.141 | -.391 | -.633 | .167 | -.102 | -.462 | -.154 | -.293 |
| .150 | .026 | -.143 | -.250 | -.447 | -.644 | .080 | -.106 | -.298 | -.756 | -.145 |
| .250 | .024 | -.119 | -.181 | -.320 | -.422 | .013 | -.123 | -.267 | -.397 | -.892 |
| .350 | -.016 | -.117 | -.178 | -.261 | -.319 | -.060 | -.167 | -.274 | -.338 | -.598 |
| .450 | -.060 | -.153 | -.195 | -.243 | -.325 | .116 | -.207 | -.274 | -.317 | -.490 |
| .550 | -.103 | -.186 | -.210 | -.231 | -.308 | .137 | -.199 | -.241 | -.291 | -.432 |
| .650 | -.126 | -.189 | -.192 | -.217 | -.291 | .143 | -.180 | -.201 | -.253 | -.398 |
| .750 | -.145 | -.204 | -.201 | -.206 | -.292 | .104 | -.123 | -.135 | -.177 | -.339 |
| .850 | -.094 | -.137 | -.124 | -.123 | -.217 | -.026 | -.029 | -.042 | -.077 | -.223 |
| .900 | -.053 | -.086 | -.069 | -.060 | -.135 | .017 | .022 | .015 | -.017 | -.135 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .123 | -.059 | -.095 | .184 | .504 | -.790 | -.001 | .381 | .540 | .649 |
| .075 | -.142 | -.140 | .010 | .183 | .470 | -.386 | -.063 | .190 | .354 | .504 |
| .150 | -.212 | -.125 | .041 | .147 | .414 | -.282 | -.080 | .101 | .239 | .381 |
| .250 | -.166 | -.105 | .034 | .140 | .337 | -.243 | -.106 | .030 | .152 | .271 |
| .350 | -.175 | -.116 | -.006 | .104 | .240 | -.240 | -.136 | -.030 | .069 | .182 |
| .450 | -.189 | -.146 | -.053 | .059 | .152 | -.246 | -.174 | -.095 | -.016 | .084 |
| .550 | -.186 | -.170 | -.088 | .016 | .088 | -.222 | -.182 | -.126 | -.060 | .023 |
| .650 | -.172 | -.167 | -.109 | -.023 | .045 | -.175 | -.159 | -.116 | -.074 | -.013 |
| .750 | -.172 | -.183 | -.129 | -.071 | -.012 | -.099 | -.099 | -.076 | -.048 | -.022 |
| .850 | -.092 | -.110 | -.072 | -.030 | -.001 | -.010 | -.002 | -.000 | -.004 | -.004 |
| .900 | -.052 | -.070 | -.043 | -.013 | .006 | .024 | .021 | .017 | .014 | -.006 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .236 | .598 | .219 | -.307 | -.797 | .262 | .524 | .121 | -.286 | -.721 |
| .025 | -.292 | -.130 | -1.019 | -1.166 | -.848 | .102 | -.273 | -.778 | -.660 | -.585 |
| .075 | .139 | -.152 | -.661 | -1.137 | -.849 | -.064 | -.278 | -.641 | -.640 | -.589 |
| .150 | .030 | -.167 | -.384 | -1.086 | .821 | -.166 | -.197 | -.412 | -.608 | -.588 |
| .250 | -.049 | -.183 | -.321 | -.888 | -.783 | -.109 | -.130 | -.237 | -.534 | -.565 |
| .350 | -.115 | -.211 | -.290 | -.530 | -.756 | | | | | |
| .450 | -.162 | -.229 | -.267 | -.248 | -.699 | | | | | |
| .550 | -.179 | -.216 | -.230 | -.233 | -.624 | | | | | |
| .650 | -.139 | -.156 | -.159 | -.183 | -.541 | -.087 | -.062 | -.102 | -.366 | -.465 |
| .750 | -.083 | -.075 | -.085 | -.106 | -.446 | -.043 | -.012 | -.059 | -.321 | -.441 |
| .850 | -.010 | -.001 | -.013 | -.036 | -.364 | -.004 | -.034 | -.020 | -.273 | -.405 |
| .900 | -.017 | -.032 | -.023 | -.002 | -.306 | -.024 | -.058 | -.008 | -.237 | -.383 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.913 | -.035 | .345 | .503 | .592 | -.881 | -.159 | .164 | .304 | .388 |
| .075 | -.499 | -.106 | .156 | .323 | .460 | -.524 | -.243 | -.066 | .074 | .194 |
| .150 | -.316 | -.119 | .064 | .207 | .336 | -.255 | -.202 | -.177 | -.111 | -.005 |
| .250 | -.295 | -.166 | -.029 | .090 | .213 | | | | | |
| .350 | -.273 | -.194 | -.102 | -.006 | .105 | | | | | |
| .450 | -.243 | -.210 | -.151 | -.078 | .021 | | | | | |
| .550 | -.203 | -.193 | -.161 | -.111 | -.037 | | | | | |
| .650 | -.137 | -.146 | -.125 | -.100 | -.059 | -.069 | -.053 | -.086 | -.121 | -.151 |
| .750 | -.066 | -.090 | -.072 | -.064 | -.074 | -.043 | -.018 | -.066 | -.127 | -.203 |
| .850 | -.027 | -.045 | -.017 | .010 | -.054 | .026 | -.053 | -.004 | -.073 | -.186 |
| .900 | -.059 | -.066 | -.044 | .032 | -.064 | .044 | -.069 | -.025 | -.067 | -.197 |

TABLE VI - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL
TAIL, AND HORIZONTAL TAIL - Continued

(i) $\alpha = 9.7^\circ$; $M = 0.90$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | | | |
|-----------------|----------------------|-------|-------------------|---------------------|---------------------|----------------------|----------------------|--------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | | | |
| Left side | | | | | | | | | | | | |
| .000 | .478 | .915 | .599 | .343 | -.367 | .386 | .684 | .391 | -.116 | -.729 | | |
| .025 | | -.131 | .072 | -.276 | -.515 | .339 | -.081 | -.1029 | -.1414 | -.1321 | | |
| .075 | .017 | -.136 | -.121 | -.350 | -.558 | .180 | -.118 | -.453 | -.957 | -.1211 | | |
| .150 | .039 | -.166 | -.267 | -.449 | -.617 | .101 | -.123 | -.321 | -.680 | -.1080 | | |
| .250 | .036 | -.139 | -.190 | -.335 | -.504 | .034 | -.139 | -.276 | -.503 | -.900 | | |
| .350 | .003 | -.133 | -.187 | -.268 | -.328 | -.041 | -.187 | -.291 | -.361 | -.591 | | |
| .450 | -.047 | -.173 | -.204 | -.238 | -.305 | -.105 | -.238 | -.295 | -.327 | -.488 | | |
| .550 | -.090 | -.211 | -.219 | -.225 | -.295 | -.144 | -.250 | -.255 | -.305 | -.434 | | |
| .650 | -.128 | -.228 | -.206 | -.217 | -.278 | -.170 | -.292 | -.222 | -.256 | -.414 | | |
| .750 | -.172 | -.309 | -.230 | -.214 | -.307 | -.127 | -.214 | -.144 | -.170 | -.382 | | |
| .850 | -.111 | -.186 | -.135 | -.113 | -.266 | -.027 | -.050 | -.040 | -.063 | -.272 | | |
| .900 | -.062 | -.109 | -.075 | -.047 | -.186 | .022 | -.019 | -.015 | -.002 | -.189 | | |
| Right side | | | | | | | | | | | | |
| .025 | .169 | -.068 | -.096 | .191 | .413 | -.856 | -.007 | .387 | .554 | .657 | | |
| .075 | -.111 | -.158 | .008 | .191 | .441 | .377 | -.077 | .197 | .366 | .508 | | |
| .150 | -.218 | -.144 | .046 | .158 | .413 | .288 | -.097 | .110 | .251 | .385 | | |
| .250 | .164 | -.123 | .039 | .152 | .347 | .236 | -.118 | .038 | .157 | .275 | | |
| .350 | -.176 | -.135 | -.005 | .116 | .248 | .243 | -.157 | -.024 | .082 | .189 | | |
| .450 | -.181 | -.167 | -.049 | .066 | .164 | .257 | -.207 | -.099 | -.006 | .087 | | |
| .550 | -.184 | -.199 | -.088 | .024 | .096 | .230 | -.243 | -.141 | -.056 | .015 | | |
| .650 | -.173 | -.214 | -.119 | -.022 | .040 | .178 | -.263 | -.149 | -.083 | -.030 | | |
| .750 | -.185 | -.275 | -.156 | -.082 | -.042 | .093 | -.183 | -.100 | -.062 | -.050 | | |
| .850 | -.090 | -.166 | -.091 | -.037 | -.041 | .001 | -.021 | -.010 | -.003 | -.036 | | |
| .900 | -.055 | -.106 | -.056 | -.017 | -.040 | .038 | -.010 | -.008 | -.018 | -.048 | | |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | | | |
| Left side | | | | | | | | | | | | |
| .000 | .295 | .601 | .286 | -.204 | -.695 | .300 | .524 | .155 | -.323 | -.660 | | |
| .025 | .306 | -.136 | -.104 | -.482 | -.821 | .131 | -.314 | -.099 | -.877 | -.571 | | |
| .075 | .155 | -.162 | -.644 | -.370 | -.813 | .043 | -.290 | -.886 | -.793 | -.563 | | |
| .150 | .053 | -.184 | -.403 | -.888 | -.772 | .250 | -.327 | -.383 | -.718 | -.566 | | |
| .250 | -.033 | -.209 | -.366 | -.694 | -.743 | .122 | -.167 | -.147 | -.631 | -.556 | | |
| .350 | -.111 | -.264 | -.326 | -.401 | -.711 | | | | | | | |
| .450 | -.188 | -.323 | -.271 | -.320 | -.668 | | | | | | | |
| .550 | -.221 | -.309 | -.244 | -.257 | -.609 | | | | | | | |
| .650 | -.161 | -.241 | -.167 | -.177 | -.550 | | | | | | | |
| .750 | -.078 | -.081 | -.080 | -.086 | -.487 | | | | | | | |
| .850 | .001 | .003 | -.005 | -.017 | -.415 | | | | | | | |
| .900 | .035 | .039 | .034 | .020 | -.381 | | | | | | | |
| Right side | | | | | | | | | | | | |
| .025 | -1.040 | -.042 | .352 | .512 | .601 | -1.085 | -.178 | .174 | .324 | .401 | | |
| .075 | -.454 | -.118 | .162 | .332 | .464 | -.645 | -.303 | -.064 | .089 | .210 | | |
| .150 | -.319 | -.133 | .071 | .217 | .342 | -.277 | -.320 | -.275 | -.122 | -.009 | | |
| .250 | -.326 | -.192 | -.028 | .101 | .218 | | | | | | | |
| .350 | -.313 | -.248 | -.117 | .001 | .103 | | | | | | | |
| .450 | -.260 | -.302 | -.180 | -.086 | .007 | | | | | | | |
| .550 | -.210 | -.286 | -.196 | -.124 | -.062 | | | | | | | |
| .650 | -.134 | -.228 | -.139 | -.108 | -.096 | | | | | | | |
| .750 | -.049 | -.084 | -.077 | -.059 | -.109 | | | | | | | |
| .850 | .048 | .043 | .018 | .016 | -.081 | | | | | | | |
| .900 | .080 | .068 | .048 | .039 | -.100 | | | | | | | |

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TABLE VI - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL TAIL, AND HORIZONTAL TAIL - Continued

(j) $\alpha = 9.7^\circ$; $M = 0.92$.

| x c_v | C_p for - | | | | | C_p for - | | | | | | |
|-------------------|----------------------|-------|-------------------|---------------------|---------------------|----------------------|----------------------|--------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | .479 | .924 | .610 | .358 | -.327 | .399 | .690 | .420 | -.034 | -.669 | | |
| .025 | -.115 | .089 | -.243 | -.478 | .327 | -.071 | -.1024 | -.1348 | -.1269 | | | |
| .075 | .000 | -.122 | -.112 | -.324 | -.535 | .174 | -.106 | -.471 | -.934 | -.169 | | |
| .150 | .023 | -.153 | -.271 | -.442 | -.601 | .087 | -.112 | -.329 | -.695 | -.050 | | |
| .250 | .021 | -.126 | -.197 | -.377 | -.544 | .019 | -.126 | -.277 | -.542 | -.901 | | |
| .350 | -.014 | -.116 | -.194 | -.310 | -.369 | -.058 | -.171 | -.295 | -.419 | -.650 | | |
| .450 | -.062 | -.160 | -.214 | -.270 | -.323 | .126 | -.226 | -.312 | -.336 | -.511 | | |
| .550 | -.106 | -.195 | -.236 | -.237 | -.303 | .167 | -.242 | -.290 | -.333 | -.463 | | |
| .650 | -.147 | -.209 | -.216 | -.235 | -.290 | .209 | -.267 | -.237 | -.328 | -.441 | | |
| .750 | -.198 | -.280 | -.262 | -.264 | -.319 | .153 | -.170 | -.156 | -.203 | -.418 | | |
| .850 | -.136 | -.157 | -.148 | -.144 | -.315 | .047 | -.042 | -.045 | -.081 | -.316 | | |
| .900 | -.082 | -.098 | -.081 | -.066 | -.240 | .009 | -.024 | -.019 | -.011 | -.217 | | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | .159 | -.052 | -.103 | .174 | .379 | -.822 | .005 | .386 | .549 | .663 | | |
| .075 | -.123 | -.144 | .006 | .181 | .433 | -.396 | -.065 | .199 | .362 | .512 | | |
| .150 | -.235 | -.128 | .047 | .152 | .414 | -.306 | -.081 | .107 | .248 | .391 | | |
| .250 | -.182 | -.110 | .041 | .142 | .349 | -.251 | -.107 | .037 | .154 | .278 | | |
| .350 | -.194 | -.118 | .002 | .106 | .248 | -.262 | -.140 | -.023 | .077 | .190 | | |
| .450 | -.204 | -.149 | -.051 | .056 | .162 | -.281 | -.191 | -.101 | -.014 | .087 | | |
| .550 | -.205 | -.178 | -.090 | .014 | .092 | -.259 | -.224 | -.155 | -.080 | .014 | | |
| .650 | -.192 | -.194 | -.131 | -.035 | .033 | -.205 | -.234 | -.187 | -.124 | -.044 | | |
| .750 | -.213 | -.249 | -.177 | -.119 | -.058 | -.109 | -.145 | -.120 | -.106 | -.076 | | |
| .850 | -.109 | -.143 | -.107 | -.082 | -.075 | -.014 | -.002 | -.020 | -.026 | -.066 | | |
| .900 | -.066 | -.094 | -.068 | -.051 | -.079 | .026 | -.020 | -.006 | -.001 | -.076 | | |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | | | |
| <i>Left side</i> | | | | | | | | | | | | |
| .000 | .302 | .610 | .311 | -.128 | -.658 | .300 | .525 | .182 | -.256 | -.656 | | |
| .025 | .298 | -.126 | -.131 | -.390 | -.834 | .080 | -.306 | -.153 | -.926 | -.593 | | |
| .075 | .143 | -.149 | -.716 | -.220 | .821 | -.058 | -.280 | -.045 | -.825 | -.577 | | |
| .150 | .034 | -.175 | -.409 | -.069 | -.779 | -.301 | -.314 | -.457 | -.755 | -.577 | | |
| .250 | -.051 | -.196 | -.370 | -.747 | -.742 | -.153 | -.126 | -.153 | -.685 | -.572 | | |
| .350 | -.135 | -.254 | -.388 | -.524 | -.712 | | | | | | | |
| .450 | -.222 | -.313 | -.295 | -.420 | -.668 | | | | | | | |
| .550 | -.260 | -.300 | -.245 | -.327 | -.617 | | | | | | | |
| .650 | -.188 | -.196 | -.169 | -.202 | -.563 | -.093 | -.059 | -.103 | -.357 | -.493 | | |
| .750 | -.094 | -.073 | -.080 | -.102 | -.507 | -.045 | -.006 | -.057 | -.279 | -.474 | | |
| .850 | -.012 | .005 | .001 | -.022 | -.443 | .006 | .046 | -.006 | -.206 | -.439 | | |
| .900 | .023 | .043 | .041 | .020 | -.406 | .034 | .068 | .023 | -.169 | -.420 | | |
| <i>Right side</i> | | | | | | | | | | | | |
| .025 | -.1008 | -.029 | .349 | .505 | .605 | -.1065 | -.165 | .173 | .322 | .408 | | |
| .075 | -.448 | -.107 | .162 | .326 | .466 | -.727 | -.298 | -.064 | .085 | .213 | | |
| .150 | -.332 | -.120 | .073 | .213 | .346 | -.362 | -.304 | -.290 | -.145 | -.015 | | |
| .250 | -.345 | -.178 | -.027 | .103 | .221 | | | | | | | |
| .350 | -.368 | -.238 | -.122 | -.013 | .104 | | | | | | | |
| .450 | -.266 | -.288 | -.211 | -.107 | .003 | | | | | | | |
| .550 | -.235 | -.264 | -.245 | -.181 | -.080 | | | | | | | |
| .650 | -.147 | -.204 | -.157 | -.156 | -.117 | -.089 | -.056 | -.088 | -.127 | -.210 | | |
| .750 | -.066 | -.069 | -.085 | -.098 | -.138 | -.040 | -.013 | -.061 | -.127 | -.244 | | |
| .850 | .035 | .052 | .018 | -.003 | -.108 | .031 | .060 | .018 | -.061 | -.236 | | |
| .900 | .071 | .072 | .052 | .026 | -.124 | .052 | .081 | .036 | -.049 | -.241 | | |

TABLE VI.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL
TAIL, AND HORIZONTAL TAIL - Continued

(k) $\alpha = 15.6^\circ$; $M = 0.60$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .387 | .843 | .702 | .613 | .321 | -.292 | .756 | -.157 | -1.566 | -2.173 |
| .025 | -.512 | -.248 | .148 | -.040 | -.449 | .362 | -.014 | -.642 | -2.111 | -2.173 |
| .075 | -.198 | -.221 | -.068 | -.175 | -.458 | .213 | -.066 | -.408 | -.601 | -2.442 |
| .150 | -.083 | -.216 | -.230 | -.270 | -.465 | .132 | -.075 | -.307 | -.504 | -.628 |
| .250 | -.021 | -.180 | -.225 | -.215 | -.343 | .055 | -.100 | -.269 | -.442 | -.557 |
| .350 | -.035 | -.162 | -.235 | -.219 | -.284 | -.007 | -.137 | -.269 | -.426 | -.552 |
| .450 | -.085 | -.196 | -.269 | -.242 | -.270 | -.062 | -.175 | -.273 | -.410 | -.529 |
| .550 | -.129 | -.223 | -.278 | -.251 | -.251 | -.079 | -.164 | -.246 | -.394 | -.490 |
| .650 | -.168 | -.239 | -.278 | -.258 | -.233 | -.088 | -.155 | -.221 | -.373 | -.444 |
| .750 | -.205 | -.246 | -.273 | -.261 | -.212 | -.069 | -.116 | -.162 | -.311 | -.373 |
| .850 | -.198 | -.207 | -.219 | -.201 | -.139 | -.033 | -.066 | -.098 | -.221 | -.297 |
| .900 | -.173 | -.175 | -.180 | -.155 | -.097 | -.003 | -.023 | -.055 | -.164 | -.238 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .256 | -.155 | -.403 | -.024 | .156 | -.806 | -.043 | .353 | .454 | .493 |
| .075 | -.076 | -.239 | -.228 | .006 | .183 | -.441 | -.084 | .194 | .323 | .441 |
| .150 | -.223 | -.209 | -.098 | .048 | .202 | -.329 | -.093 | .107 | .225 | .344 |
| .250 | -.228 | -.175 | -.030 | .071 | .144 | -.278 | -.109 | .052 | .146 | .250 |
| .350 | -.237 | -.164 | -.052 | .034 | .133 | -.269 | -.139 | -.009 | .084 | .172 |
| .450 | -.271 | -.207 | -.098 | -.017 | .123 | -.271 | -.168 | -.057 | .027 | .098 |
| .550 | -.273 | -.223 | -.125 | -.065 | .075 | -.255 | -.173 | -.084 | -.008 | .054 |
| .650 | -.269 | -.225 | -.150 | -.097 | .029 | -.221 | -.157 | -.080 | -.024 | .031 |
| .750 | -.255 | -.223 | -.164 | -.120 | -.001 | -.159 | -.114 | -.055 | -.015 | .029 |
| .850 | -.198 | -.182 | -.150 | -.097 | .015 | -.092 | -.045 | -.014 | .013 | .041 |
| .900 | -.166 | -.155 | -.137 | -.081 | .011 | -.053 | -.034 | -.004 | .020 | .031 |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | -.324 | .485 | -.276 | -1.120 | -1.180 | -.079 | .415 | -.296 | .640 | .729 |
| .025 | -.330 | -.064 | -.902 | -1.157 | -1.127 | .137 | -.153 | -.802 | -.621 | .709 |
| .075 | .181 | -.091 | -.635 | -1.198 | -1.215 | -.033 | -.175 | -.510 | -.596 | .723 |
| .150 | .077 | -.107 | -.373 | -1.240 | -1.477 | -.115 | -.162 | -.255 | -.564 | .700 |
| .250 | .002 | -.123 | -.260 | -.628 | -1.288 | -.122 | -.112 | -.173 | -.525 | .661 |
| .350 | -.049 | -.141 | -.237 | -.203 | -.798 | | | | | |
| .450 | -.095 | -.157 | -.228 | -.226 | -.403 | | | | | |
| .550 | -.118 | -.148 | -.203 | -.224 | -.293 | | | | | |
| .650 | -.088 | -.112 | -.148 | -.171 | -.224 | | | | | |
| .750 | -.060 | -.071 | -.096 | -.123 | -.169 | | | | | |
| .850 | -.019 | -.016 | -.036 | -.054 | -.093 | | | | | |
| .900 | -.003 | -.005 | -.007 | -.033 | -.067 | | | | | |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.870 | -.071 | .344 | .431 | .459 | -.627 | -.164 | .160 | .241 | .261 |
| .075 | -.670 | -.107 | .169 | .300 | .404 | -.462 | -.191 | -.059 | .038 | .107 |
| .150 | -.109 | .075 | .192 | .305 | | -.333 | -.168 | -.143 | -.084 | -.026 |
| .250 | -.260 | -.127 | -.004 | .093 | .192 | | | | | |
| .350 | -.251 | -.146 | -.059 | .006 | .105 | | | | | |
| .450 | -.221 | -.155 | -.091 | -.033 | .045 | | | | | |
| .550 | -.193 | -.141 | -.098 | -.054 | .006 | | | | | |
| .650 | -.147 | -.109 | -.082 | -.061 | -.017 | | | | | |
| .750 | -.095 | -.061 | -.059 | -.040 | -.021 | | | | | |
| .850 | -.012 | .018 | .009 | .006 | .002 | | | | | |
| .900 | .018 | .037 | .030 | .025 | .006 | | | | | |

TABLE VI.- PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL
TAIL, AND HORIZONTAL TAIL - Continued

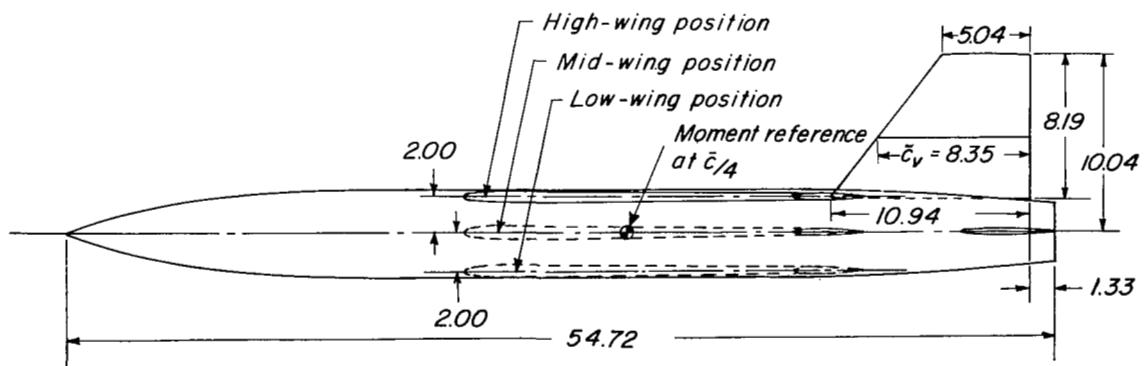
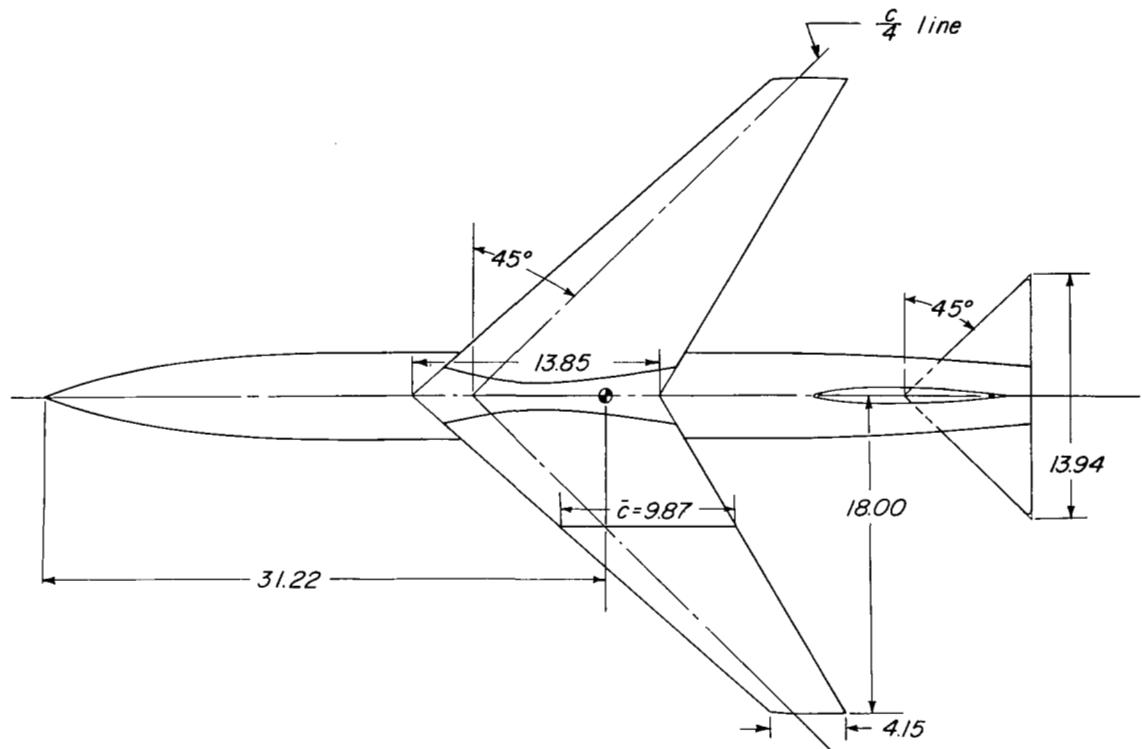
(1) $\alpha = 15.8^\circ$; $M = 0.80$.

| $\frac{x}{C_v}$ | C_p for - | | | | | C_p for - | | | | |
|-----------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $Z/b_v = 0.11$ | | | | | $Z/b_v = 0.38$ | | | | |
| Left side | | | | | | | | | | |
| •000 | .565 | .910 | .801 | .730 | .405 | .114 | .814 | .229 | .726 | -1.497 |
| •025 | -.663 | -.228 | .207 | .083 | -.259 | .362 | .015 | -.566 | -1.511 | -1.752 |
| •075 | -.200 | -.213 | -.015 | -.096 | -.349 | .224 | -.050 | -.397 | -.683 | -1.868 |
| •150 | -.070 | -.205 | -.222 | -.278 | -.489 | .151 | -.062 | -.302 | -.541 | -.777 |
| •250 | -.004 | -.155 | -.218 | -.236 | -.384 | .079 | -.082 | -.262 | -.459 | -.615 |
| •350 | -.019 | -.128 | -.222 | -.215 | -.301 | .004 | -.128 | -.265 | -.429 | -.518 |
| •450 | -.067 | -.173 | -.253 | -.236 | -.276 | -.053 | -.181 | -.274 | -.423 | -.554 |
| •550 | -.114 | -.198 | -.262 | -.235 | -.252 | -.082 | -.186 | -.265 | -.411 | -.557 |
| •650 | -.157 | -.224 | -.270 | -.258 | -.258 | -.106 | -.189 | -.248 | -.403 | -.507 |
| •750 | -.207 | -.271 | -.299 | -.294 | -.266 | -.097 | -.155 | -.191 | -.320 | -.423 |
| •850 | -.215 | -.244 | -.259 | -.245 | -.202 | -.056 | -.096 | -.121 | -.219 | -.332 |
| •900 | -.200 | -.210 | -.221 | -.200 | -.152 | -.021 | -.050 | -.069 | -.151 | -.264 |
| Right side | | | | | | | | | | |
| •025 | .317 | -.116 | -.452 | -.063 | .127 | -.698 | -.044 | .348 | .463 | .534 |
| •075 | -.027 | -.237 | -.225 | -.005 | .157 | -.438 | -.088 | .204 | .334 | .452 |
| •150 | -.222 | -.202 | -.075 | .050 | .186 | -.330 | -.087 | .134 | .248 | .358 |
| •250 | -.230 | -.155 | -.006 | .083 | .164 | -.276 | -.096 | .072 | .170 | .268 |
| •350 | -.230 | -.137 | -.027 | .054 | .098 | -.268 | -.137 | .013 | .103 | .187 |
| •450 | -.261 | -.183 | -.066 | .004 | .080 | -.279 | -.180 | -.049 | .030 | .104 |
| •550 | -.271 | -.208 | -.107 | -.047 | .044 | -.273 | -.195 | -.083 | -.013 | .044 |
| •650 | -.268 | -.224 | -.149 | -.099 | -.013 | -.239 | -.189 | -.095 | -.039 | .013 |
| •750 | -.291 | -.253 | -.181 | -.146 | -.061 | -.184 | -.149 | -.073 | -.028 | .006 |
| •850 | -.238 | -.216 | -.164 | -.128 | -.050 | -.106 | -.079 | -.026 | -.002 | .021 |
| •900 | -.212 | -.189 | -.152 | -.118 | -.051 | -.073 | -.065 | -.015 | -.008 | .010 |
| $Z/b_v = 0.66$ | | | | | $Z/b_v = 0.93$ | | | | | |
| Left side | | | | | | | | | | |
| •000 | -.109 | .521 | -.043 | -.788 | -.102 | .002 | .431 | .165 | .559 | -.793 |
| •025 | .339 | -.038 | -.845 | -.192 | -.021 | .151 | -.173 | -.862 | -.629 | -.757 |
| •075 | .193 | -.073 | -.695 | -.204 | -.033 | -.037 | -.207 | -.774 | -.596 | -.763 |
| •150 | .086 | -.099 | -.406 | -.189 | -.222 | -.149 | -.181 | -.288 | -.563 | -.763 |
| •250 | .008 | -.123 | -.271 | -.814 | -.164 | -.132 | -.114 | -.145 | -.527 | -.729 |
| •350 | -.059 | -.154 | -.250 | -.155 | -.888 | | | | | |
| •450 | -.117 | -.175 | -.239 | -.213 | -.621 | | | | | |
| •550 | -.143 | -.169 | -.221 | -.230 | -.472 | | | | | |
| •650 | -.112 | -.131 | -.158 | -.181 | -.341 | | | | | |
| •750 | -.074 | -.084 | -.101 | -.128 | -.247 | | | | | |
| •850 | -.024 | -.001 | -.029 | -.057 | -.141 | | | | | |
| •900 | -.002 | .014 | -.001 | -.027 | -.099 | | | | | |
| Right side | | | | | | | | | | |
| •025 | -.898 | -.053 | .358 | .447 | .486 | -.813 | -.175 | .175 | .265 | .281 |
| •075 | -.724 | -.097 | .187 | .313 | .412 | -.530 | -.228 | -.058 | .057 | .130 |
| •150 | -.391 | -.097 | .098 | .213 | .311 | -.365 | -.178 | -.149 | -.082 | -.028 |
| •250 | -.273 | -.122 | .011 | .109 | .200 | | | | | |
| •350 | -.261 | -.161 | -.060 | .018 | .103 | | | | | |
| •450 | -.238 | -.173 | -.101 | -.042 | .023 | | | | | |
| •550 | -.207 | -.161 | -.121 | -.074 | -.025 | | | | | |
| •650 | -.157 | -.122 | -.101 | -.077 | -.044 | | | | | |
| •750 | -.096 | -.064 | -.061 | -.053 | -.050 | | | | | |
| •850 | -.010 | .023 | .009 | .001 | -.019 | | | | | |
| •900 | .031 | .050 | .037 | .018 | -.019 | | | | | |

TABLE VI - PRESSURE COEFFICIENTS FOR THE COMBINATION OF THE FUSELAGE, VERTICAL TAIL, AND HORIZONTAL TAIL - Concluded

(m) $\alpha = 15.9^\circ$; $M = 0.85$.

| x C_v | C_p for - | | | | | C_p for - | | | | |
|-------------------|----------------------|-------------------|---------------------|---------------------|----------------------|----------------------|-------------------|---------------------|---------------------|----------------------|
| | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ | $\beta = -3.9^\circ$ | $\beta = 0^\circ$ | $\beta = 3.9^\circ$ | $\beta = 7.9^\circ$ | $\beta = 12.7^\circ$ |
| | $z/b_v = 0.11$ | | | | | $z/b_v = 0.38$ | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | .621 | .926 | .836 | .759 | .412 | .213 | .836 | .314 | -.569 | -.1246 |
| .025 | -.701 | -.215 | .226 | .114 | -.195 | .352 | .012 | -.543 | -.1373 | -.1606 |
| .075 | -.210 | -.218 | .001 | -.076 | -.292 | .216 | -.056 | -.411 | -.720 | -.1641 |
| .150 | -.074 | -.207 | -.226 | -.285 | -.473 | .150 | -.066 | -.319 | -.585 | -.820 |
| .250 | -.002 | -.157 | -.226 | -.265 | -.437 | .080 | -.081 | -.272 | -.499 | -.686 |
| .350 | -.024 | -.123 | -.226 | -.246 | -.322 | .005 | -.127 | -.273 | -.463 | -.444 |
| .450 | -.065 | -.174 | -.262 | -.258 | -.276 | -.062 | -.188 | -.288 | -.447 | -.594 |
| .550 | -.108 | -.192 | -.260 | -.241 | -.252 | -.098 | -.197 | -.279 | -.437 | -.616 |
| .650 | -.161 | -.228 | -.272 | -.264 | -.276 | -.127 | -.211 | -.269 | -.432 | -.549 |
| .750 | -.223 | -.286 | -.321 | -.331 | -.309 | -.120 | -.184 | -.216 | -.362 | -.473 |
| .850 | -.226 | -.262 | -.279 | -.287 | -.249 | -.072 | -.114 | -.140 | -.244 | -.365 |
| .900 | -.212 | -.227 | -.240 | -.238 | -.185 | -.036 | -.066 | -.085 | -.167 | -.280 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | .338 | -.103 | -.506 | -.095 | .112 | -.675 | -.044 | .337 | .455 | .548 |
| .075 | -.011 | -.248 | -.239 | -.030 | .141 | -.450 | -.091 | .205 | .330 | .458 |
| .150 | -.229 | -.204 | -.080 | .039 | .182 | -.335 | -.089 | .136 | .243 | .366 |
| .250 | -.234 | -.151 | -.009 | .073 | .169 | -.282 | -.100 | .075 | .167 | .277 |
| .350 | -.232 | -.131 | -.029 | .045 | .098 | -.275 | -.140 | .015 | .095 | .196 |
| .450 | -.262 | -.178 | -.068 | -.007 | .065 | -.289 | -.194 | -.054 | .020 | .107 |
| .550 | -.272 | -.204 | -.108 | -.061 | .028 | -.289 | -.215 | -.098 | -.036 | .042 |
| .650 | -.272 | -.227 | -.153 | -.118 | -.033 | -.260 | -.211 | -.111 | -.068 | .000 |
| .750 | -.311 | -.271 | -.200 | -.173 | -.093 | -.203 | -.168 | -.097 | -.062 | -.016 |
| .850 | -.259 | -.237 | -.186 | -.160 | -.086 | -.121 | -.097 | -.048 | -.026 | -.004 |
| .900 | -.230 | -.205 | -.173 | -.154 | -.089 | -.087 | -.081 | -.035 | -.017 | -.010 |
| $z/b_v = 0.66$ | | | | | $z/b_v = 0.93$ | | | | | |
| <i>Left side</i> | | | | | | | | | | |
| .000 | -.051 | .534 | .015 | -.683 | -.187 | .002 | .424 | -.138 | -.566 | -.770 |
| .025 | .341 | -.040 | -.886 | -.1232 | -.1067 | .144 | -.184 | -.949 | -.659 | -.745 |
| .075 | .194 | -.074 | -.724 | -.1232 | -.1049 | -.051 | -.239 | -.838 | -.633 | -.758 |
| .150 | .088 | -.103 | -.428 | -.1223 | -.147 | -.181 | -.205 | -.341 | -.601 | -.754 |
| .250 | .005 | -.130 | -.289 | -.856 | -.085 | -.156 | -.130 | -.150 | -.566 | -.728 |
| .350 | -.072 | -.168 | -.269 | -.189 | -.870 | | | | | |
| .450 | .133 | -.197 | -.260 | -.246 | -.680 | | | | | |
| .550 | -.167 | -.194 | -.236 | -.275 | -.549 | | | | | |
| .650 | -.137 | -.154 | -.180 | -.219 | -.410 | -.108 | -.063 | -.114 | -.369 | -.578 |
| .750 | -.092 | -.100 | -.114 | -.153 | -.309 | -.064 | -.020 | -.067 | -.278 | -.529 |
| .850 | -.035 | -.005 | -.042 | -.075 | -.191 | -.015 | -.029 | -.014 | -.200 | -.454 |
| .900 | -.008 | .014 | -.008 | -.040 | -.145 | .014 | .052 | .018 | -.150 | -.406 |
| <i>Right side</i> | | | | | | | | | | |
| .025 | -.952 | -.050 | .359 | .445 | .494 | -.1054 | -.182 | .170 | .262 | .292 |
| .075 | -.781 | -.099 | .186 | .305 | .418 | -.577 | -.254 | -.071 | .046 | .138 |
| .150 | -.404 | -.099 | .098 | .206 | .323 | -.318 | -.202 | -.174 | -.108 | -.030 |
| .250 | -.283 | -.140 | .008 | .102 | .205 | | | | | |
| .350 | -.276 | -.177 | -.071 | .004 | .101 | | | | | |
| .450 | -.260 | -.198 | -.125 | -.072 | .019 | | | | | |
| .550 | -.236 | -.191 | -.146 | -.111 | -.041 | | | | | |
| .650 | -.177 | -.148 | -.127 | -.111 | -.073 | -.095 | -.053 | -.084 | -.161 | -.221 |
| .750 | -.113 | -.090 | -.078 | -.086 | -.079 | -.059 | -.017 | -.065 | -.159 | -.229 |
| .850 | -.016 | .017 | -.001 | -.027 | -.044 | -.007 | .052 | -.007 | -.091 | -.098 |
| .900 | .022 | .044 | .028 | -.004 | -.044 | .032 | .068 | .024 | -.061 | -.190 |

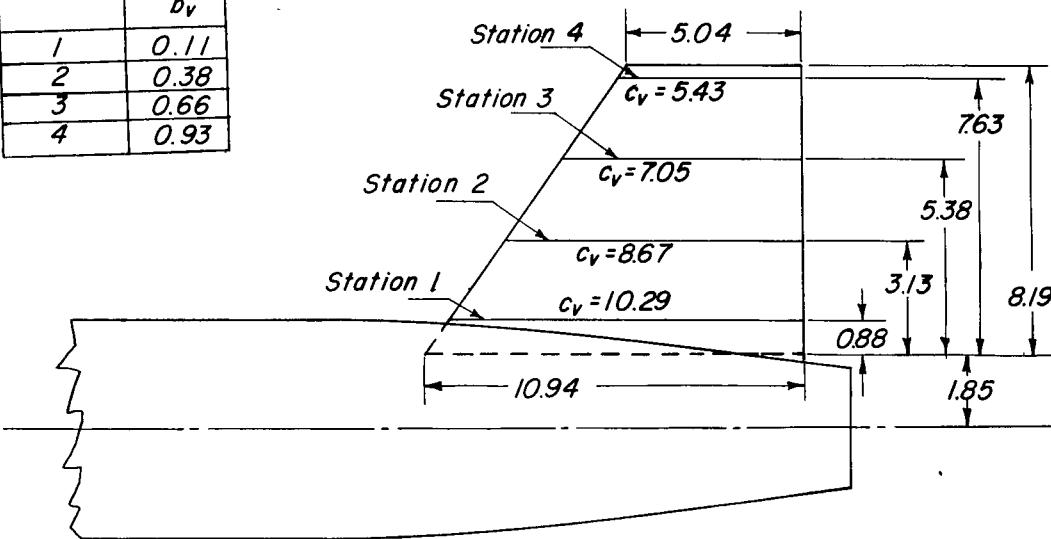


(a) Complete model.

Figure 1.- Details of test model. All linear dimensions are in inches.

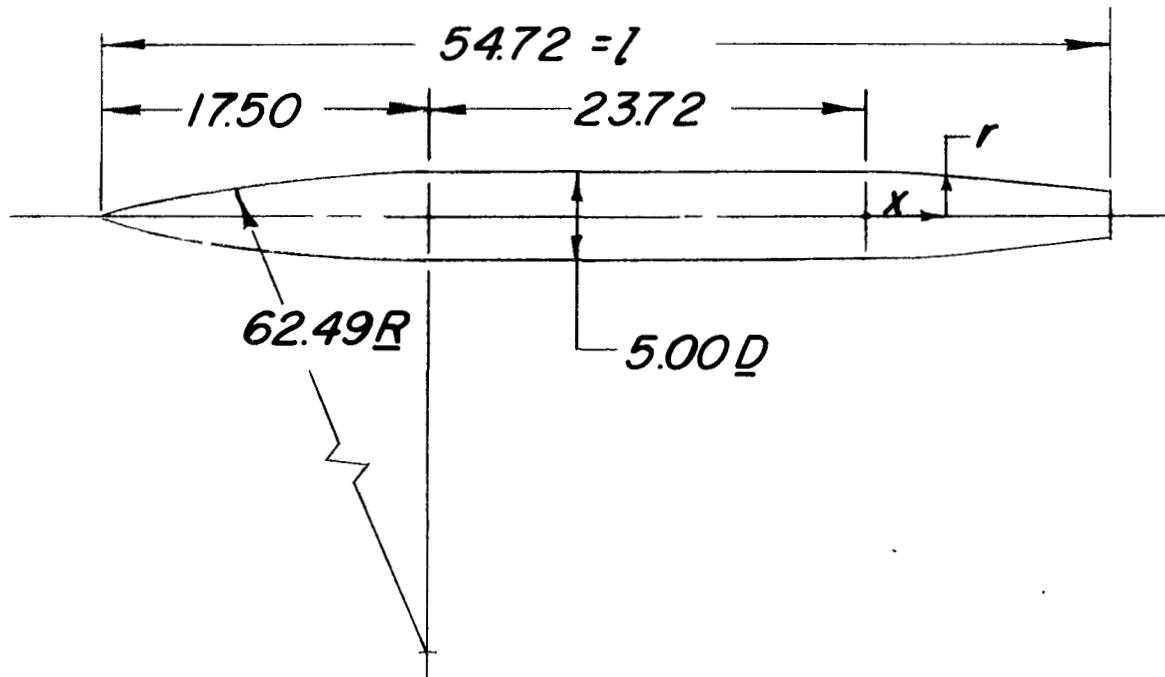
| Upper and lower surface chordwise locations of orifices for all spanwise stations, x/c_v | |
|--|--|
| .000 | |
| .025 | |
| .075 | |
| .150 | |
| .250 | |
| .350 | |
| .450 | |
| .550 | |
| .650 | |
| .750 | |
| .850 | |
| .900 | |

| Station | $\frac{z}{b_v}$ |
|---------|-----------------|
| 1 | 0.11 |
| 2 | 0.38 |
| 3 | 0.66 |
| 4 | 0.93 |



(b) Details of vertical-tail pressure-orifice locations.

Figure 1.- Continued.

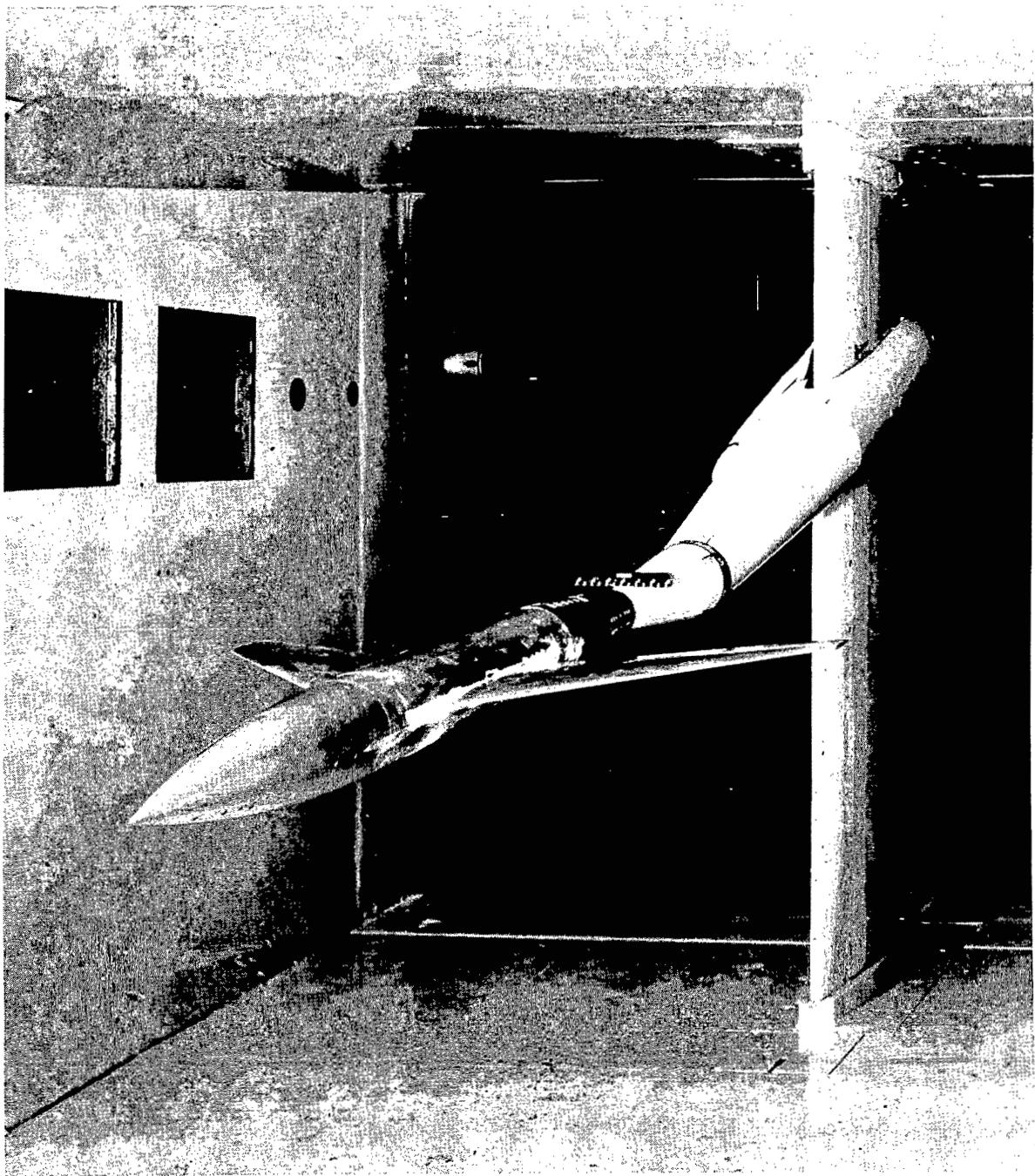


Afterbody Coordinates

| $\frac{x}{l}$ | $\frac{r}{l}$ |
|--------------------------------|---------------|
| 0 | .0456 |
| .0320 | .0445 |
| .0639 | .0427 |
| .1187 | .0390 |
| <i>Straight-line taper</i> | |
| .2460 | .0301 |

(c) Fuselage dimensions; fineness ratio, 10.94.

Figure 1.- Concluded.

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Figure 2.- Photograph of model mounted on sting-support system in Langley high-speed 7- by 10-foot tunnel.

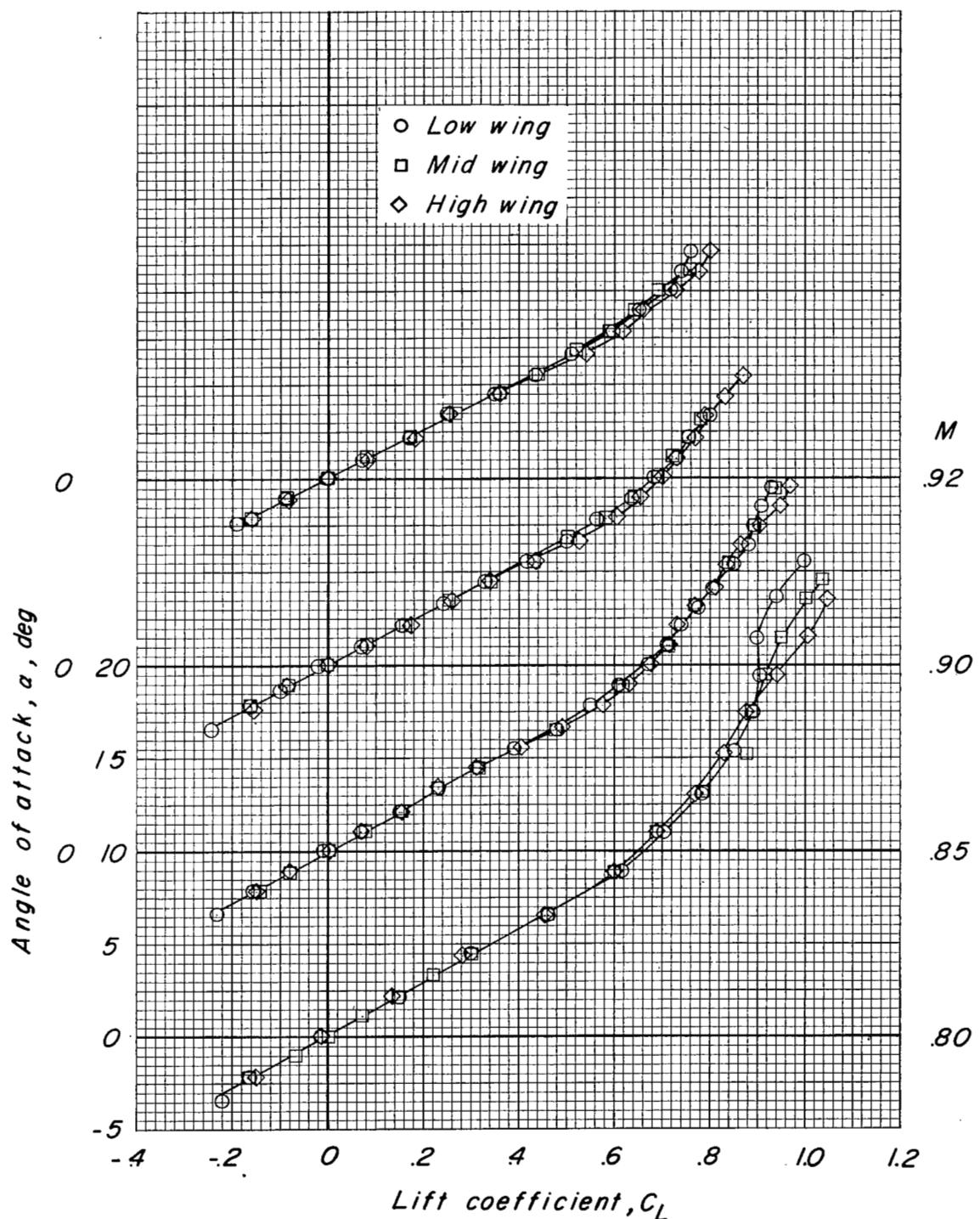


Figure 3.- Variation of model lift coefficient with angle of attack.
Horizontal tail off.

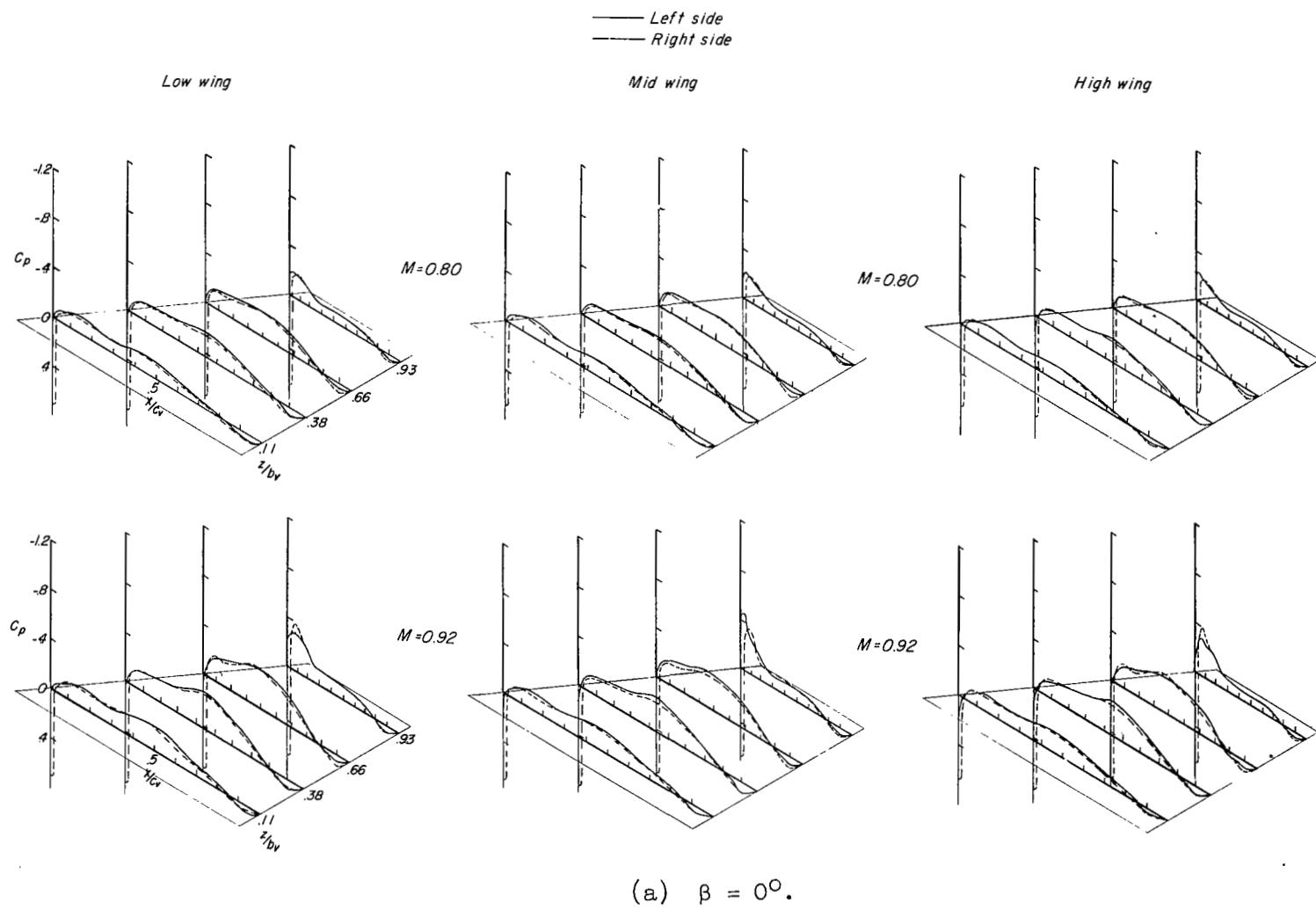


Figure 4.- Effect of wing height on vertical-tail chordwise pressure distribution. $i_t = 0^\circ$; $\alpha = 0^\circ$.

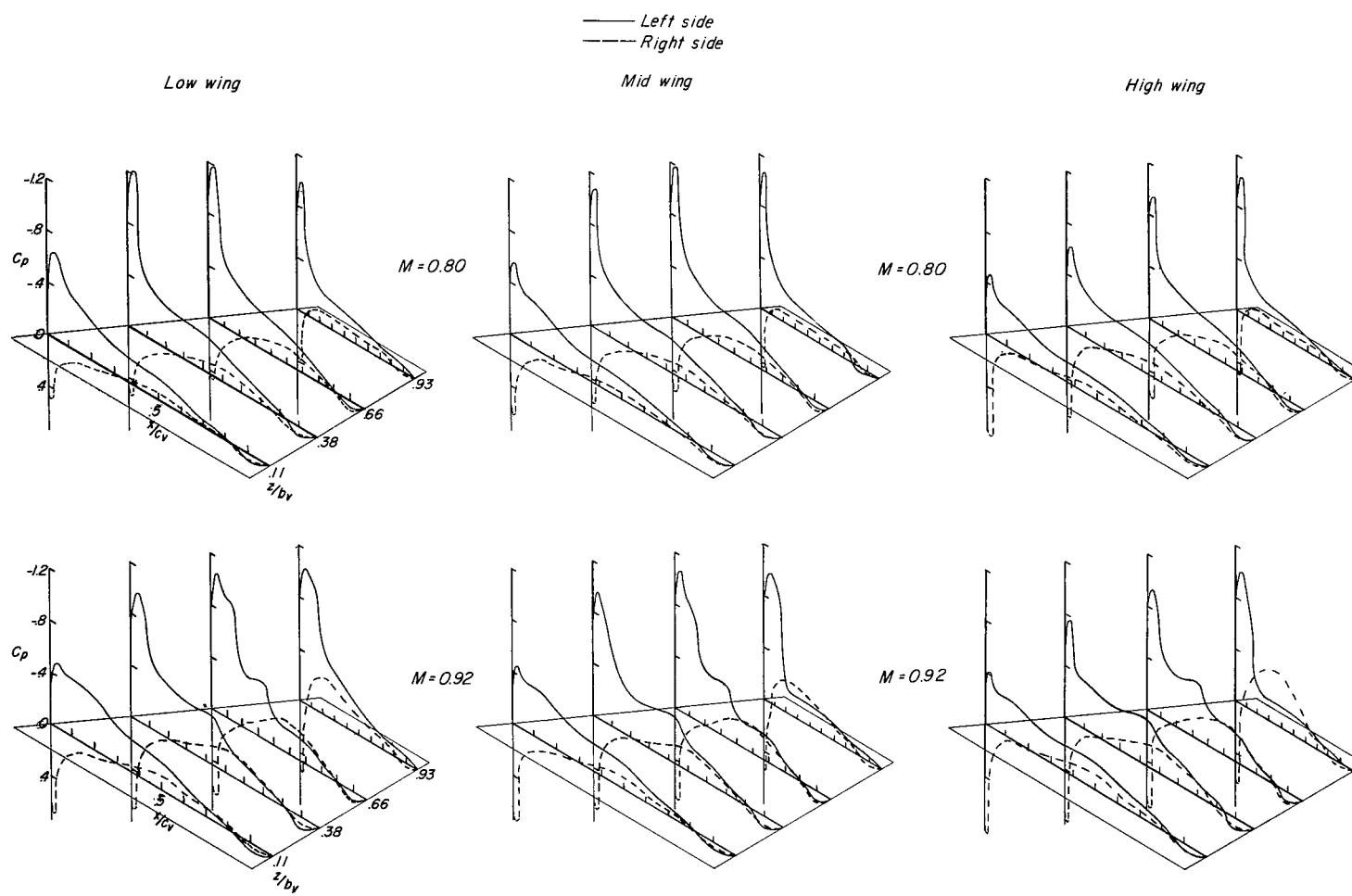
(b) $\beta = 3.9^\circ$.

Figure 4.- Continued.

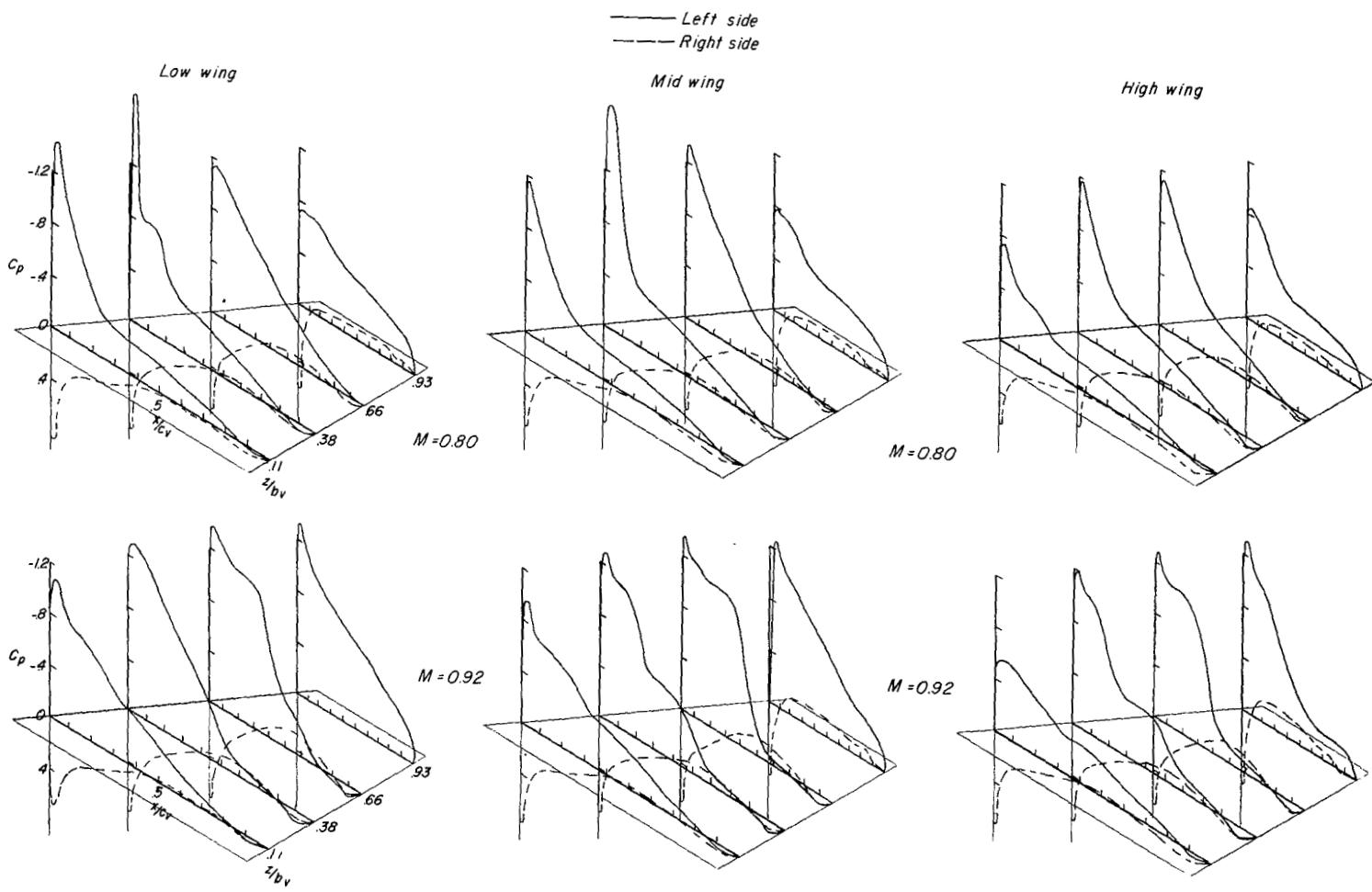
(c) $\beta = 7.8^\circ$.

Figure 4.- Continued.

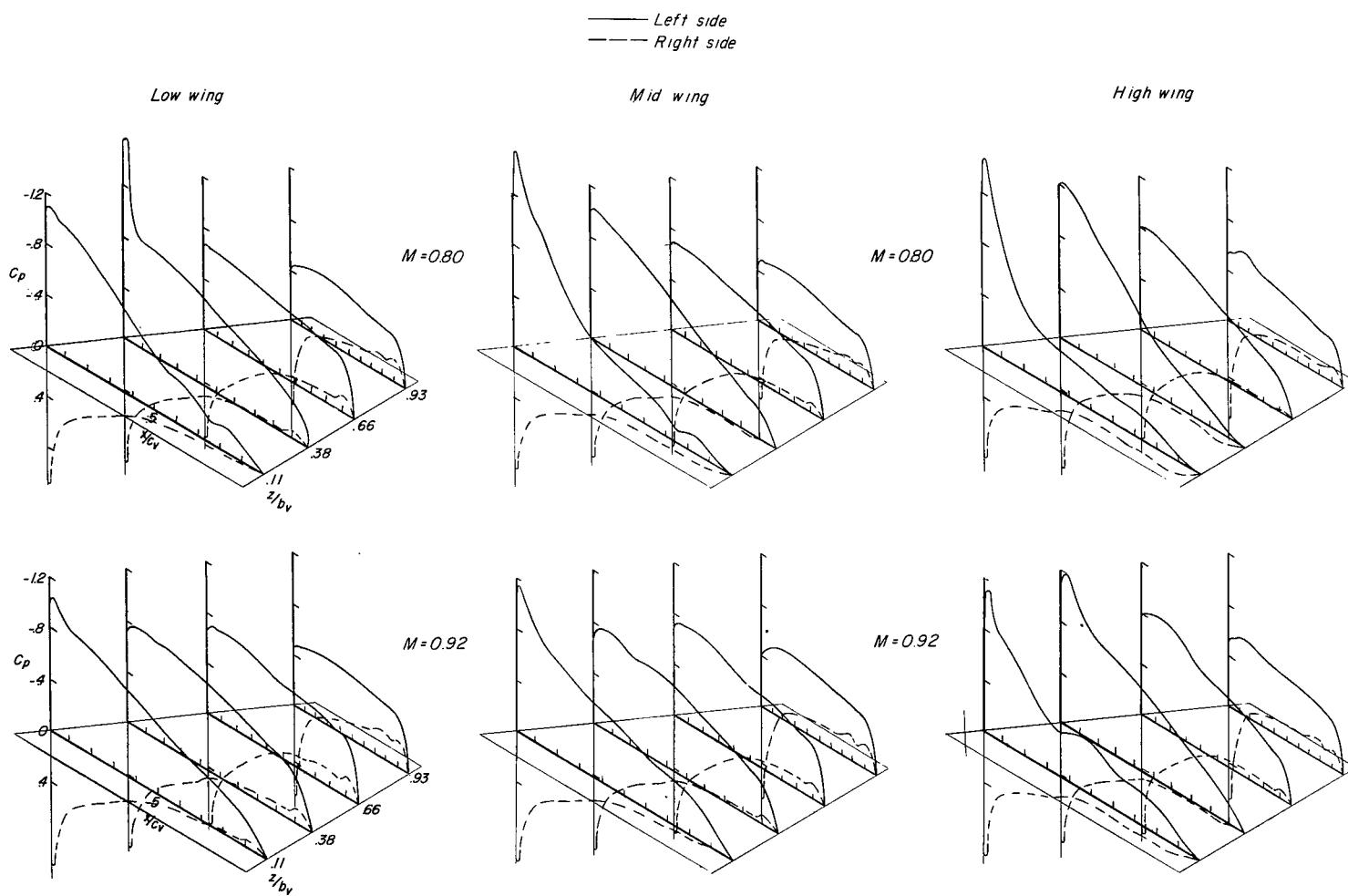
(d) $\beta = 12.7^\circ$.

Figure 4.- Concluded.

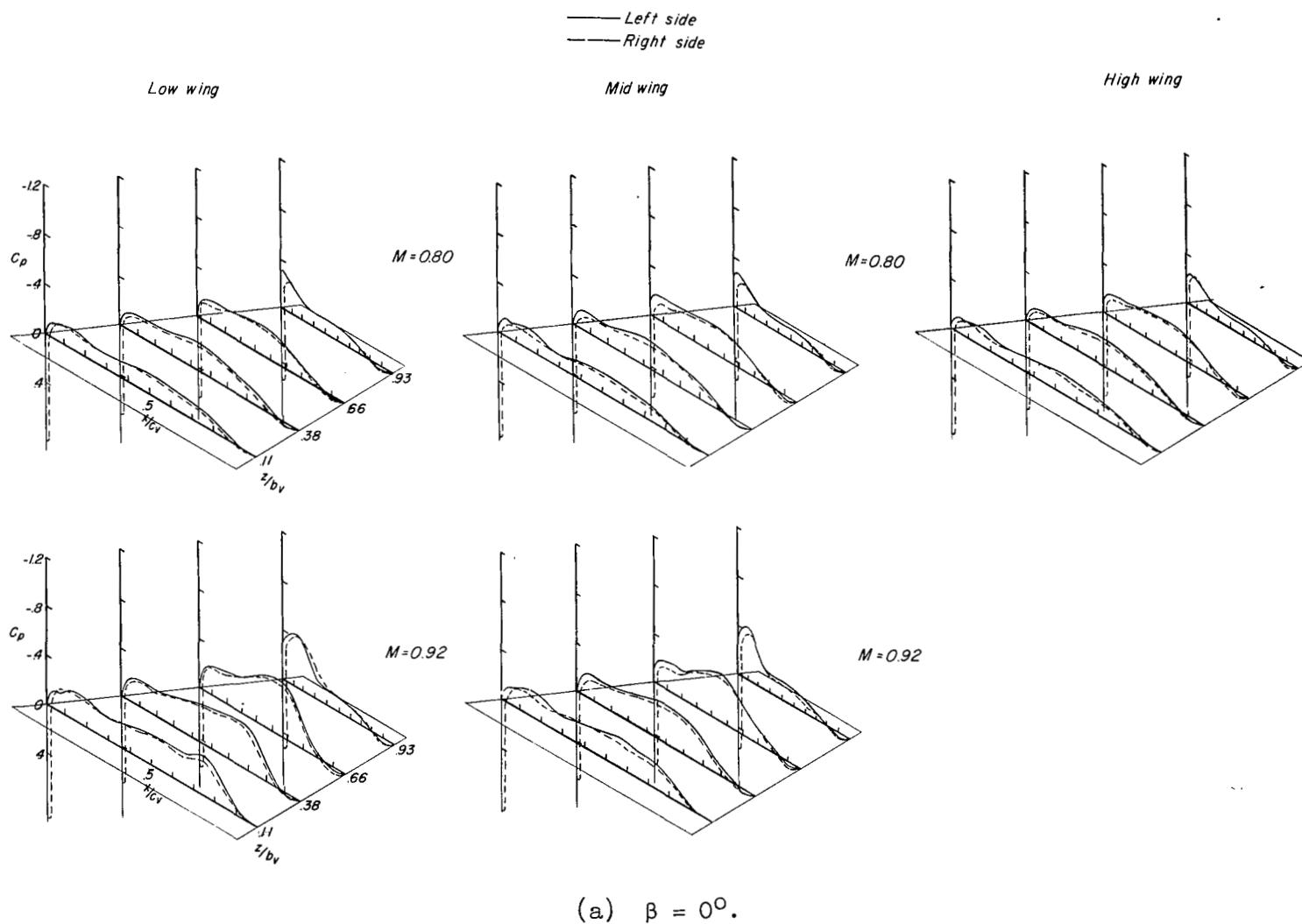
(a) $\beta = 0^\circ$.

Figure 5.- Effect of wing height on vertical-tail pressure distribution. $i_t = 0^\circ$; $\alpha = 9.6^\circ$.

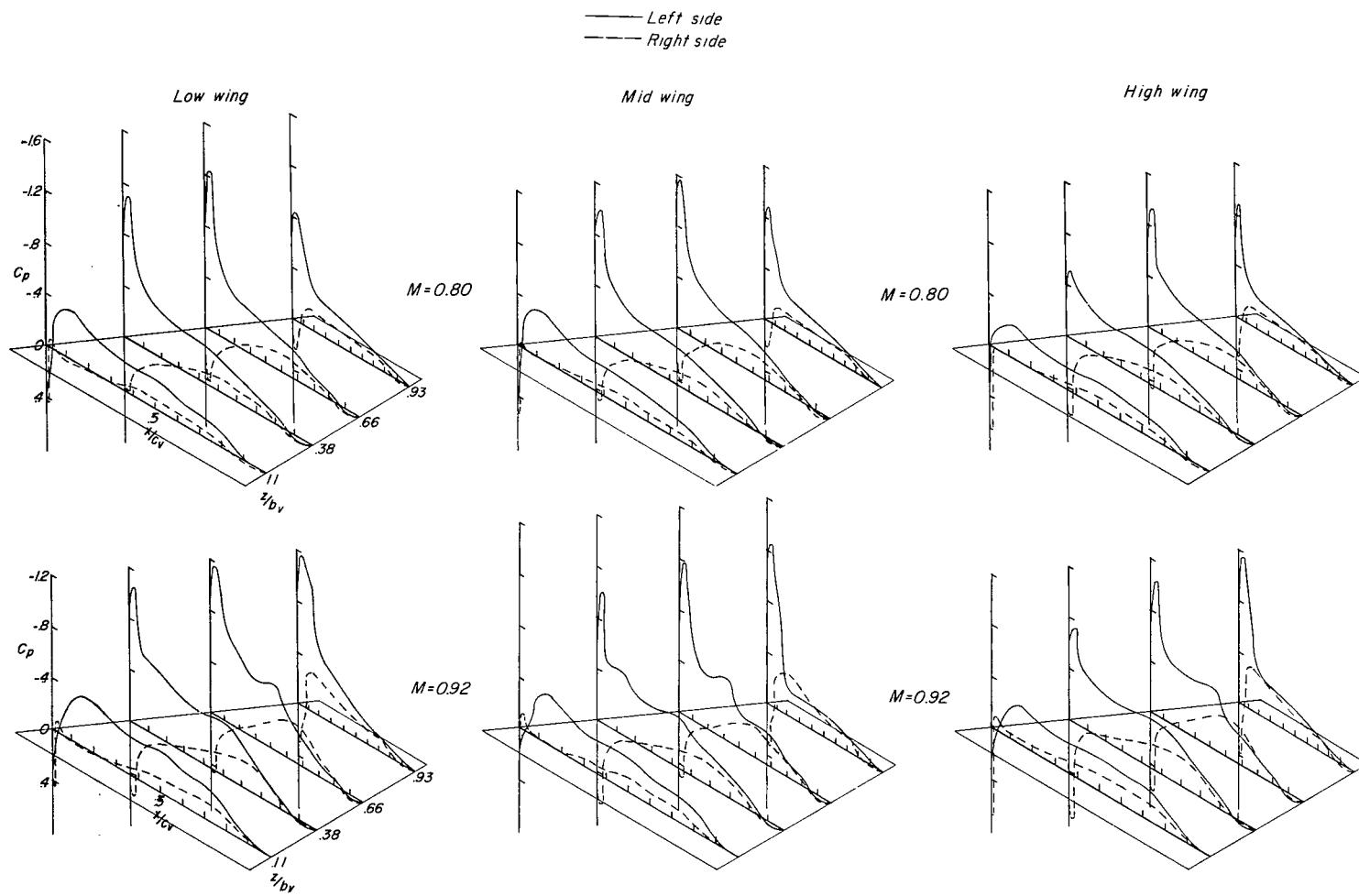
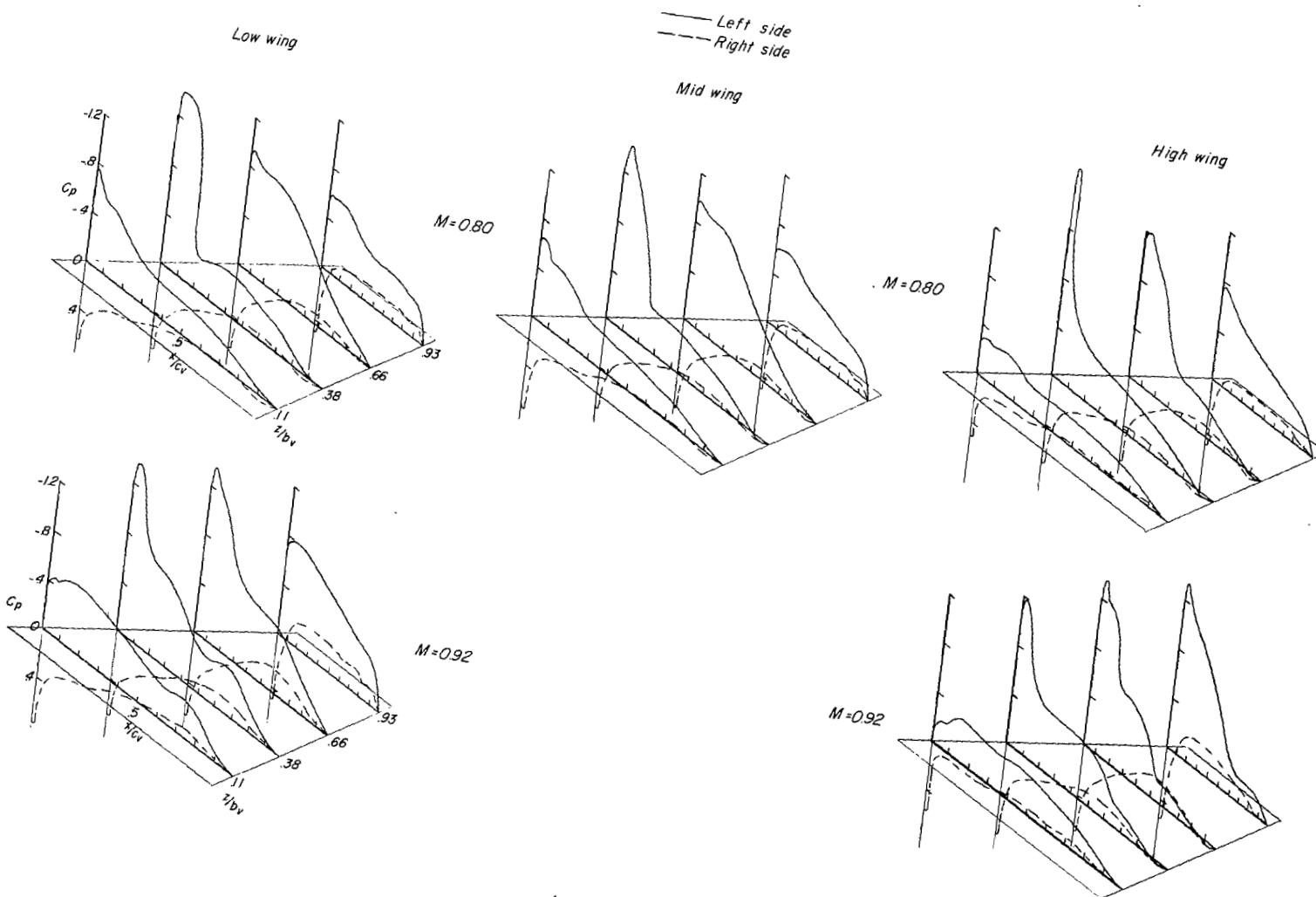
(b) $\beta = 3.9^\circ$.

Figure 5.- Continued.



(c) $\beta = 7.8^\circ$.

Figure 5.- Continued.

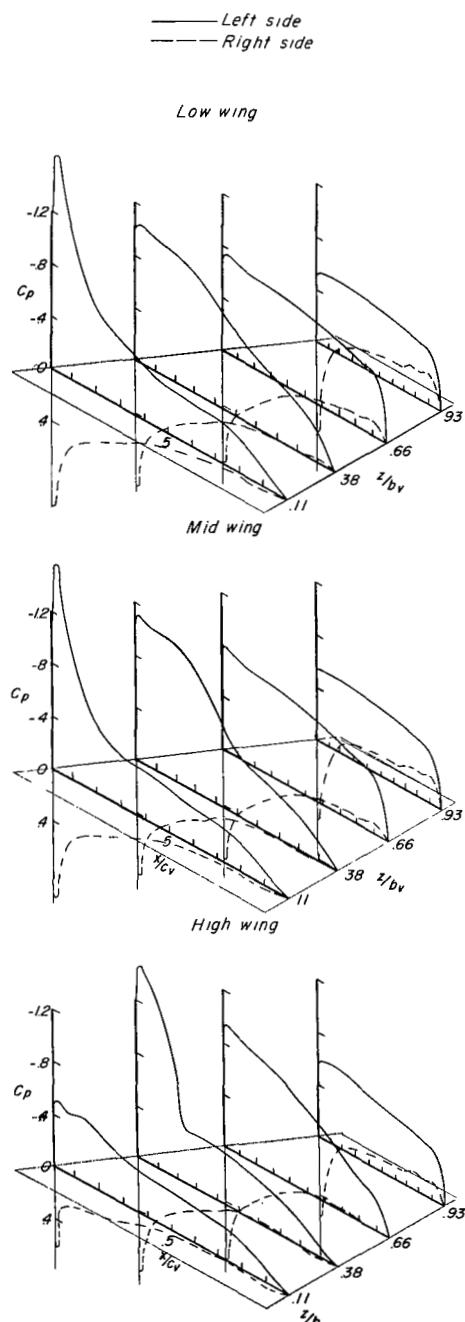
(d) $\beta = 12.7^\circ$.

Figure 5.- Concluded.

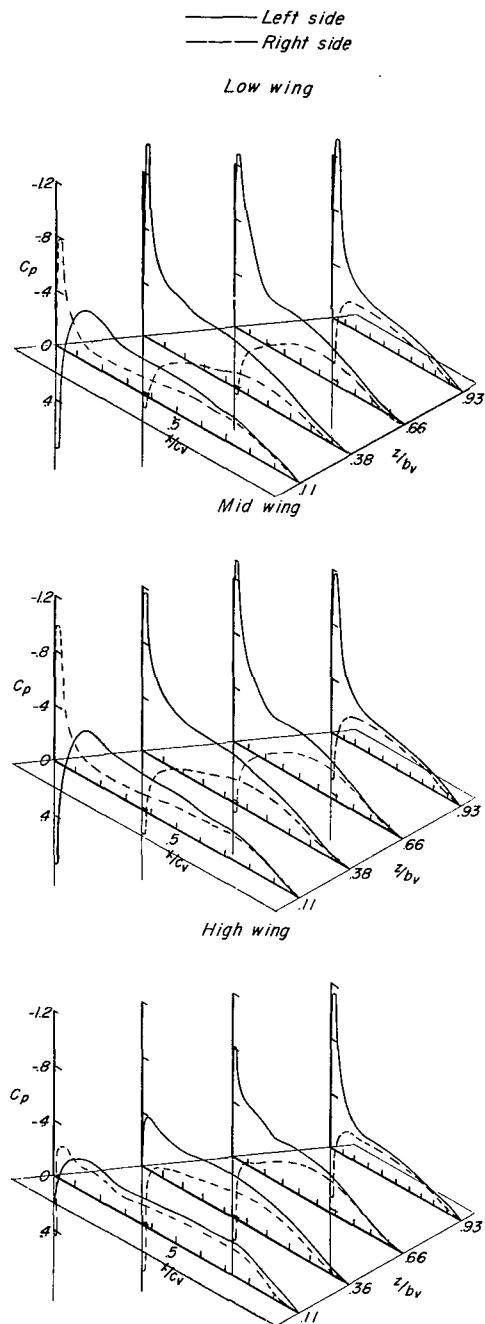


Figure 6.- Effect of wing height on the vertical-tail chordwise pressure distribution. $i_t = 0^\circ$; $\alpha = 15.8^\circ$; $\beta = 3.9^\circ$; $M = 0.80$.

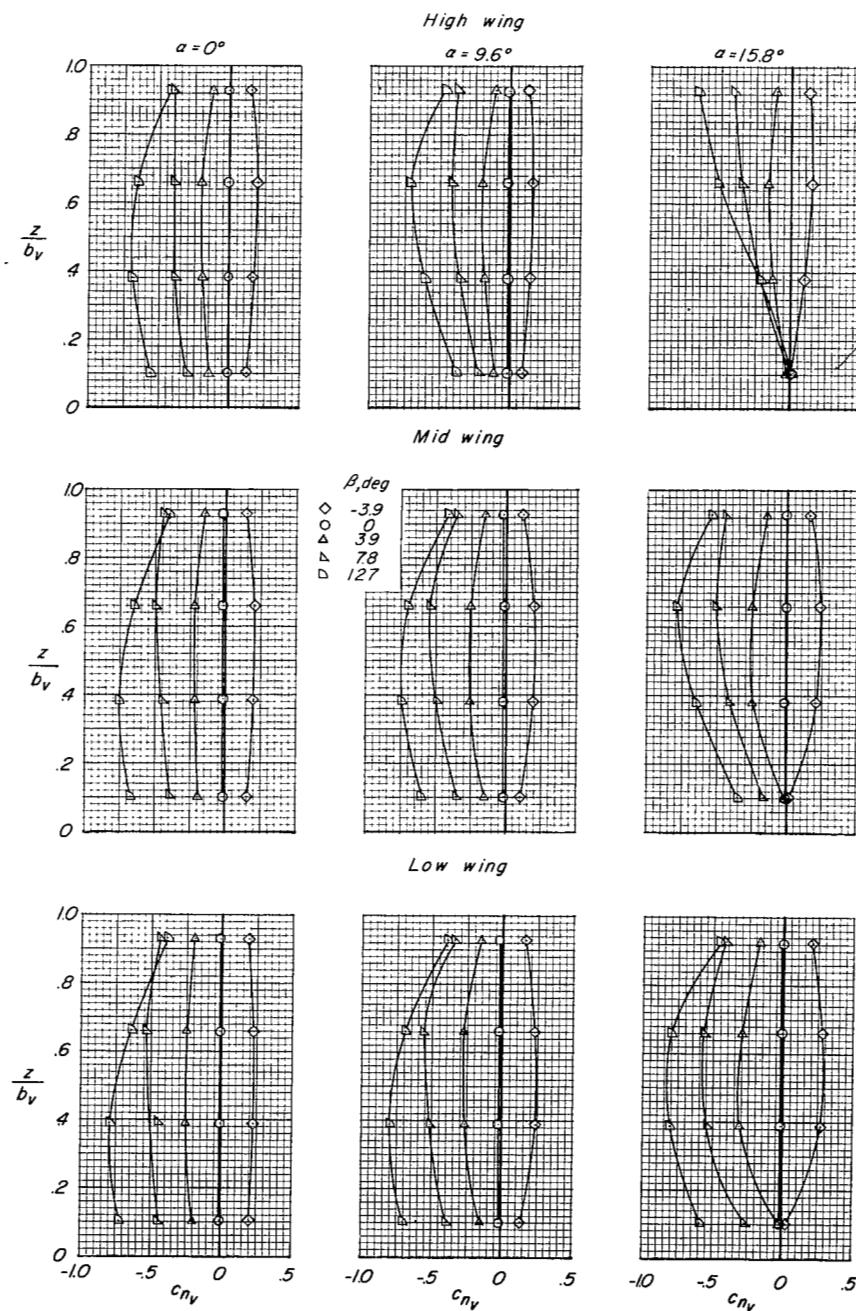
(a) $M = 0.80$.

Figure 7.- Effect of angle of sideslip on the spanwise variation of vertical-tail section normal-force coefficients. $i_t = 0^\circ$.

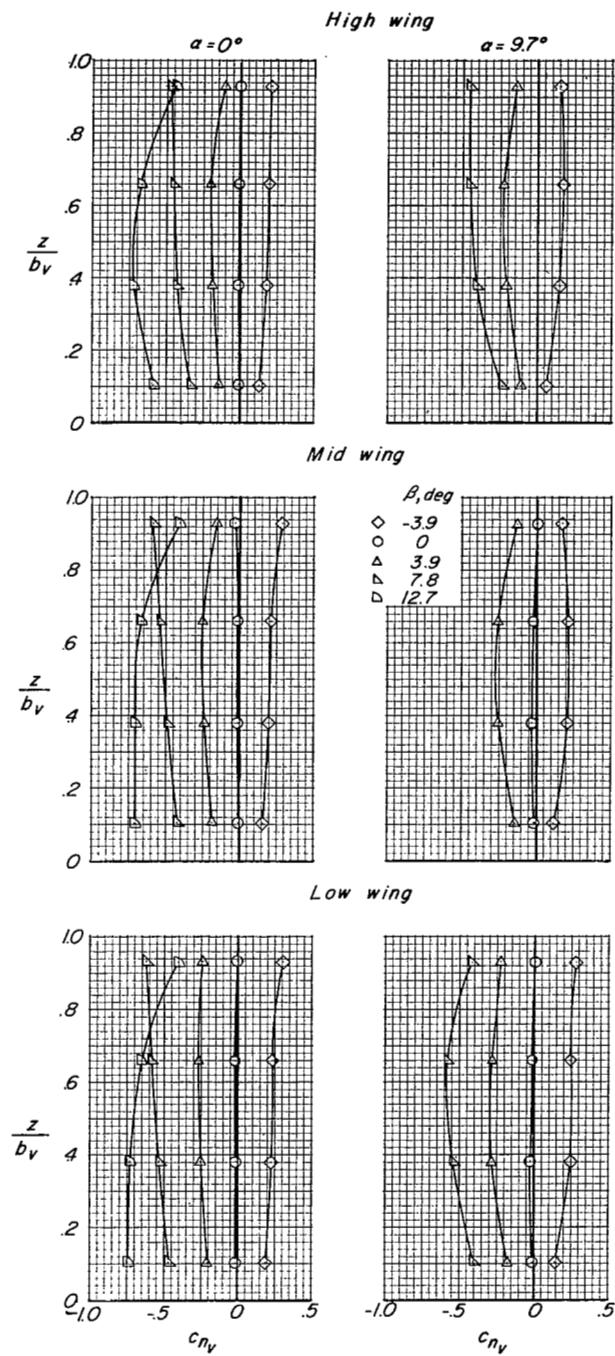
(b) $M = 0.92$.

Figure 7.- Concluded.

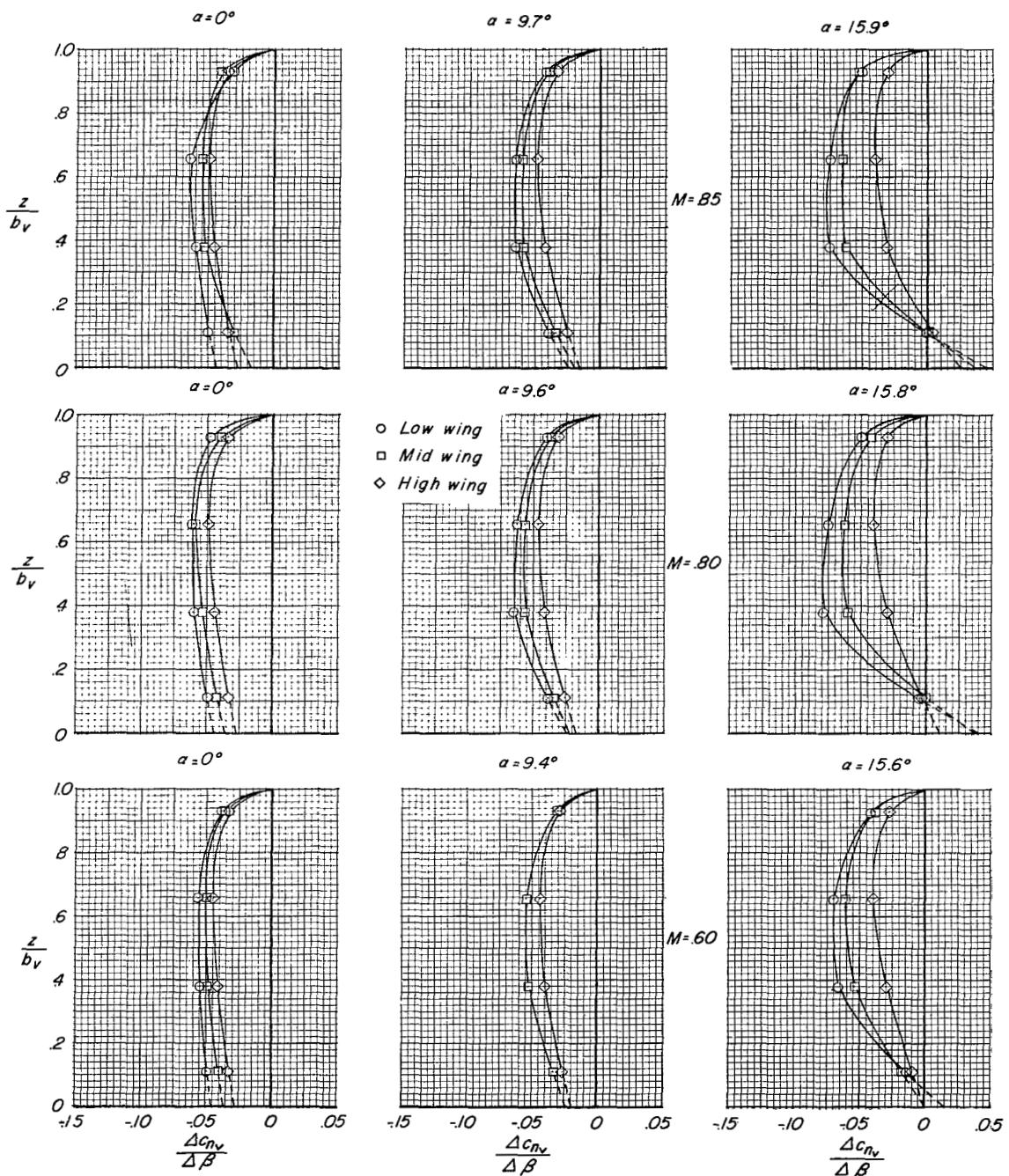


Figure 8.- Effect of wing height on the spanwise variation of vertical-tail section normal-force coefficient per degree of sideslip. $\Delta\beta \approx 8^\circ$; $i_t = 0^\circ$.

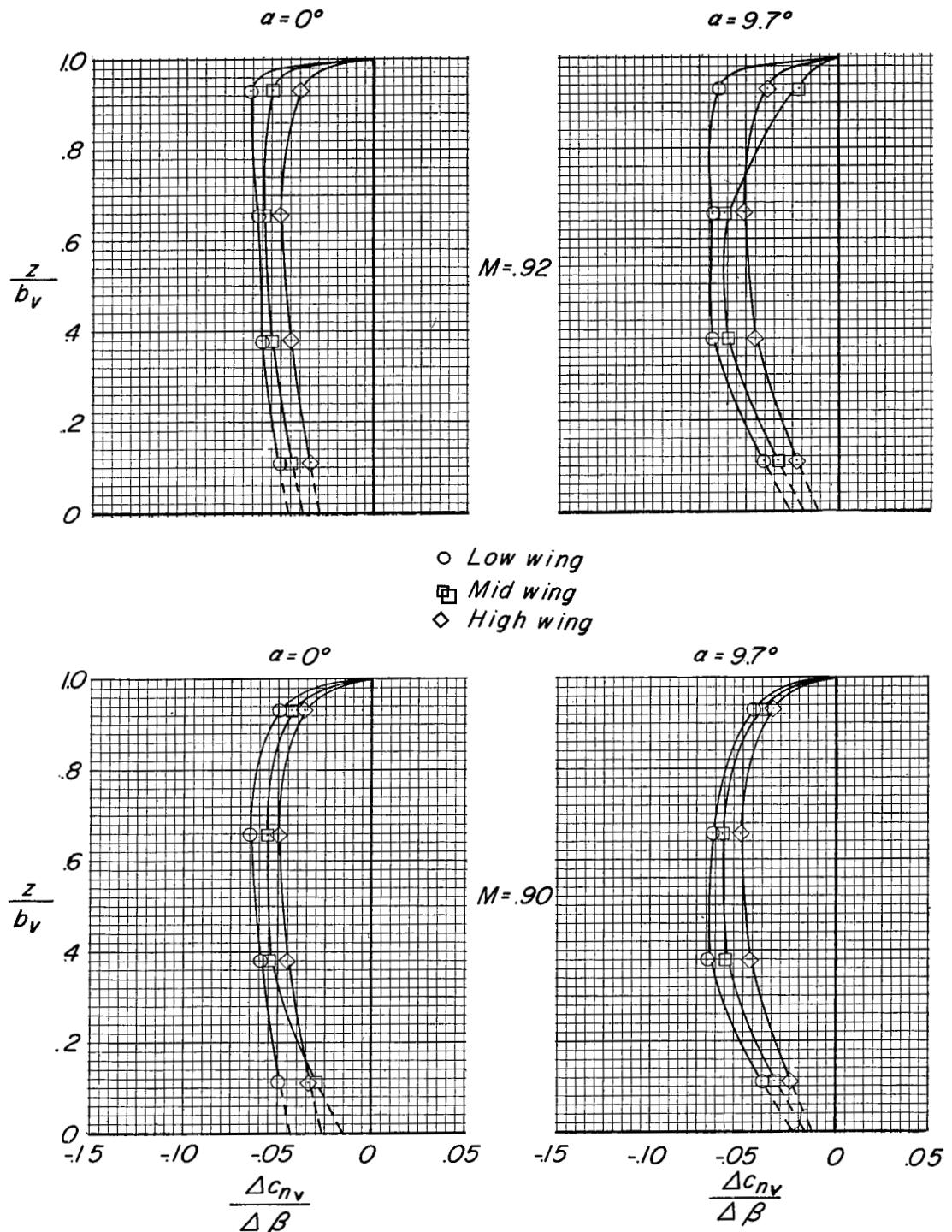


Figure 8.- Concluded.

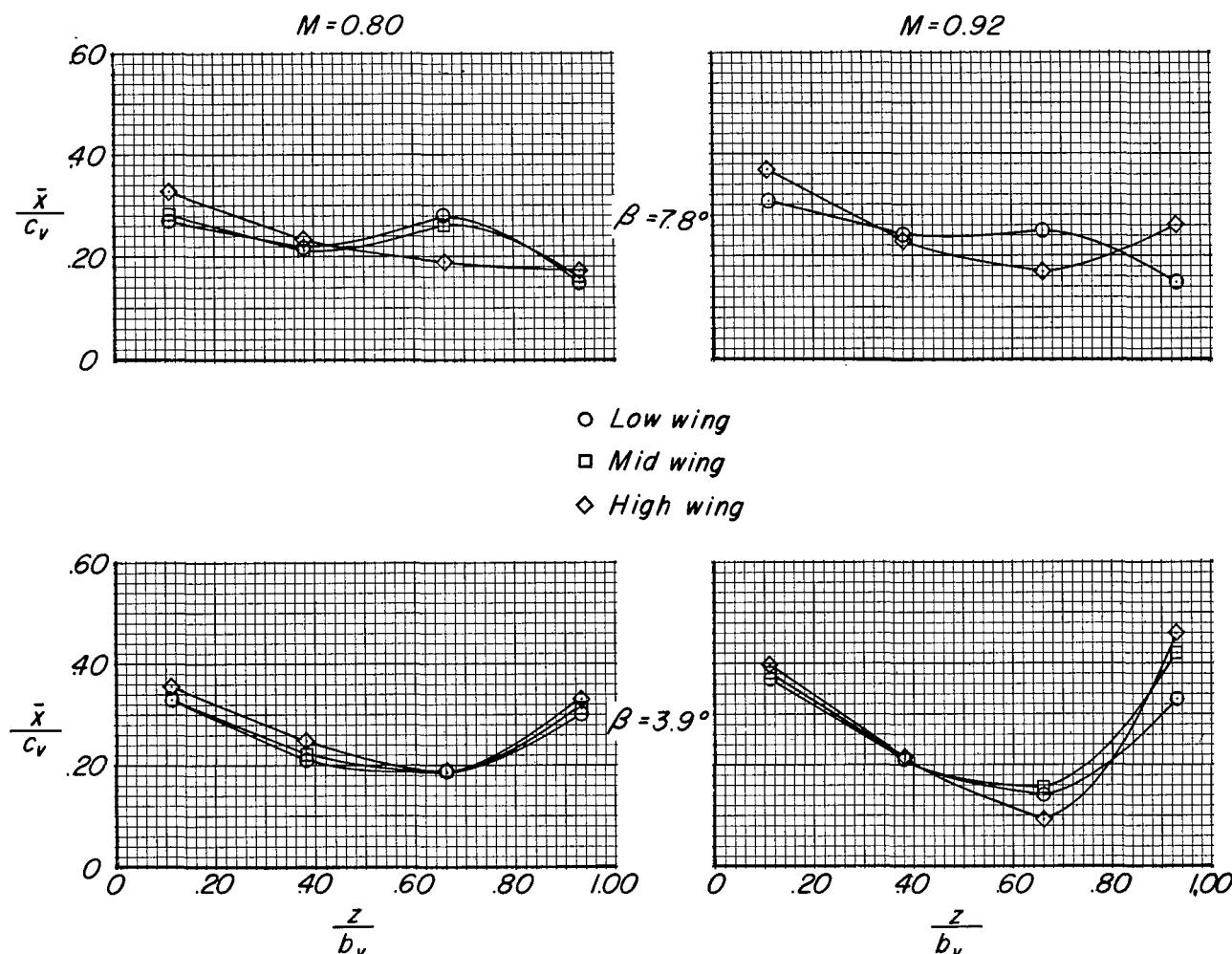
(b) $\alpha = 9.6^\circ$.

Figure 9.- Continued.

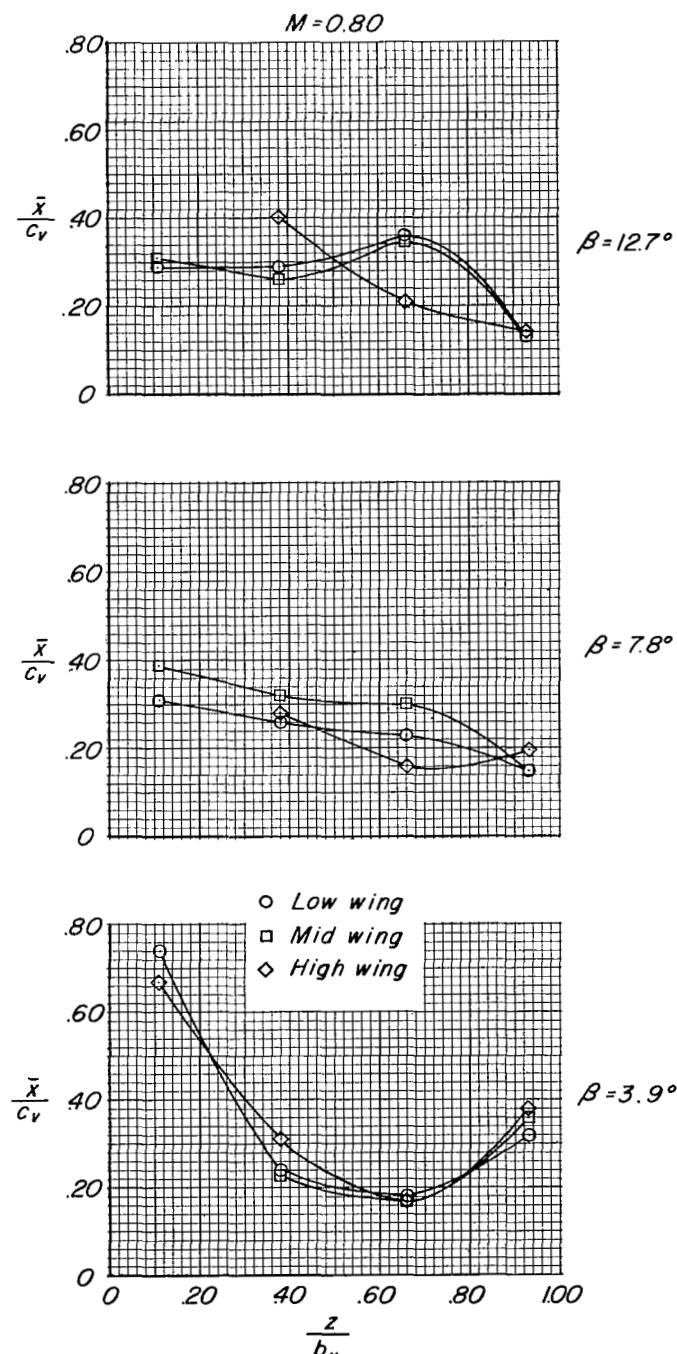
(c) $\alpha = 15.8^\circ$.

Figure 9.- Concluded.

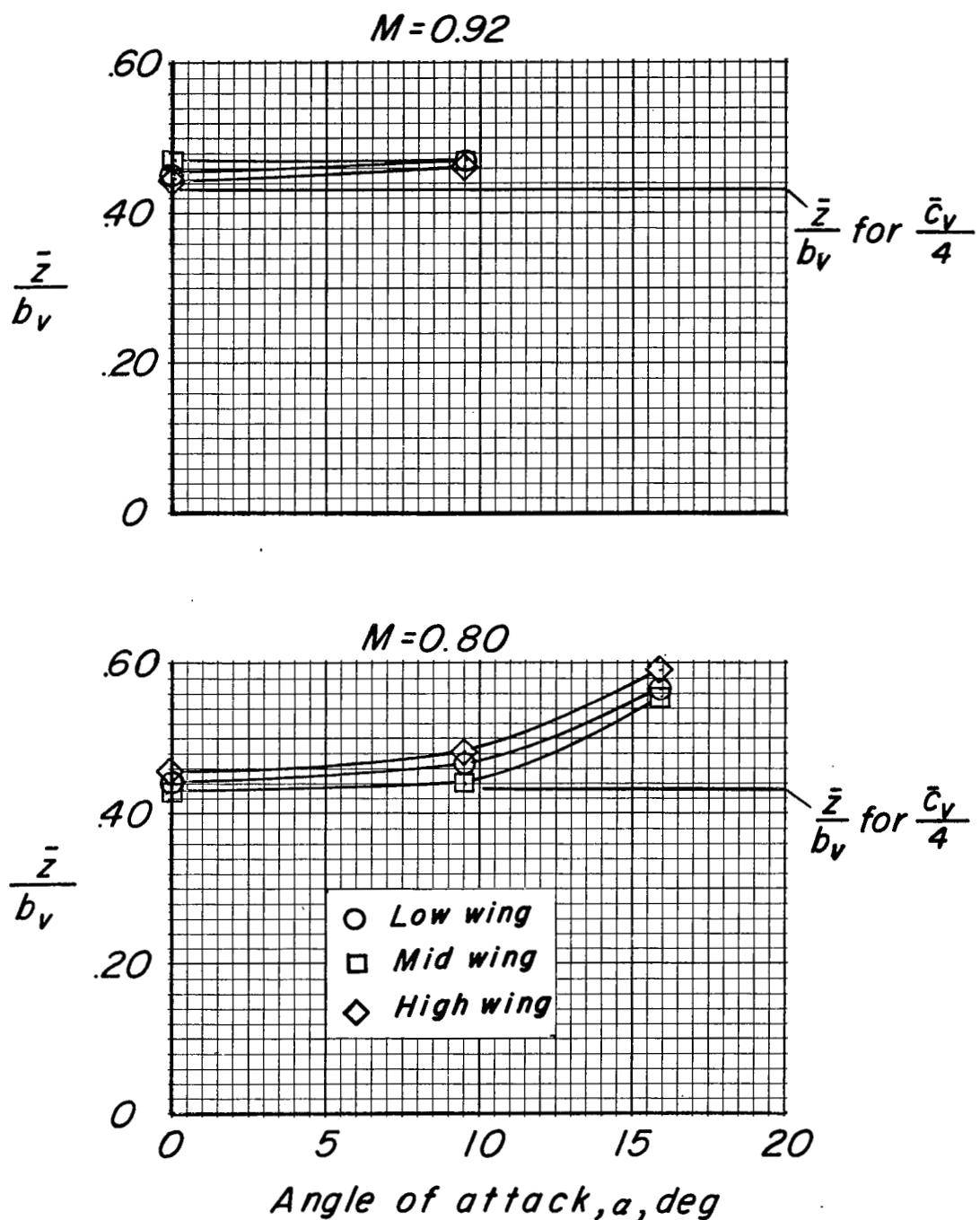


Figure 10.- Effect of wing height on the variation of the spanwise location of the vertical-tail center of pressure with angle of attack.
 $\Delta\beta \approx 8^\circ$; $i_t = 0^\circ$.

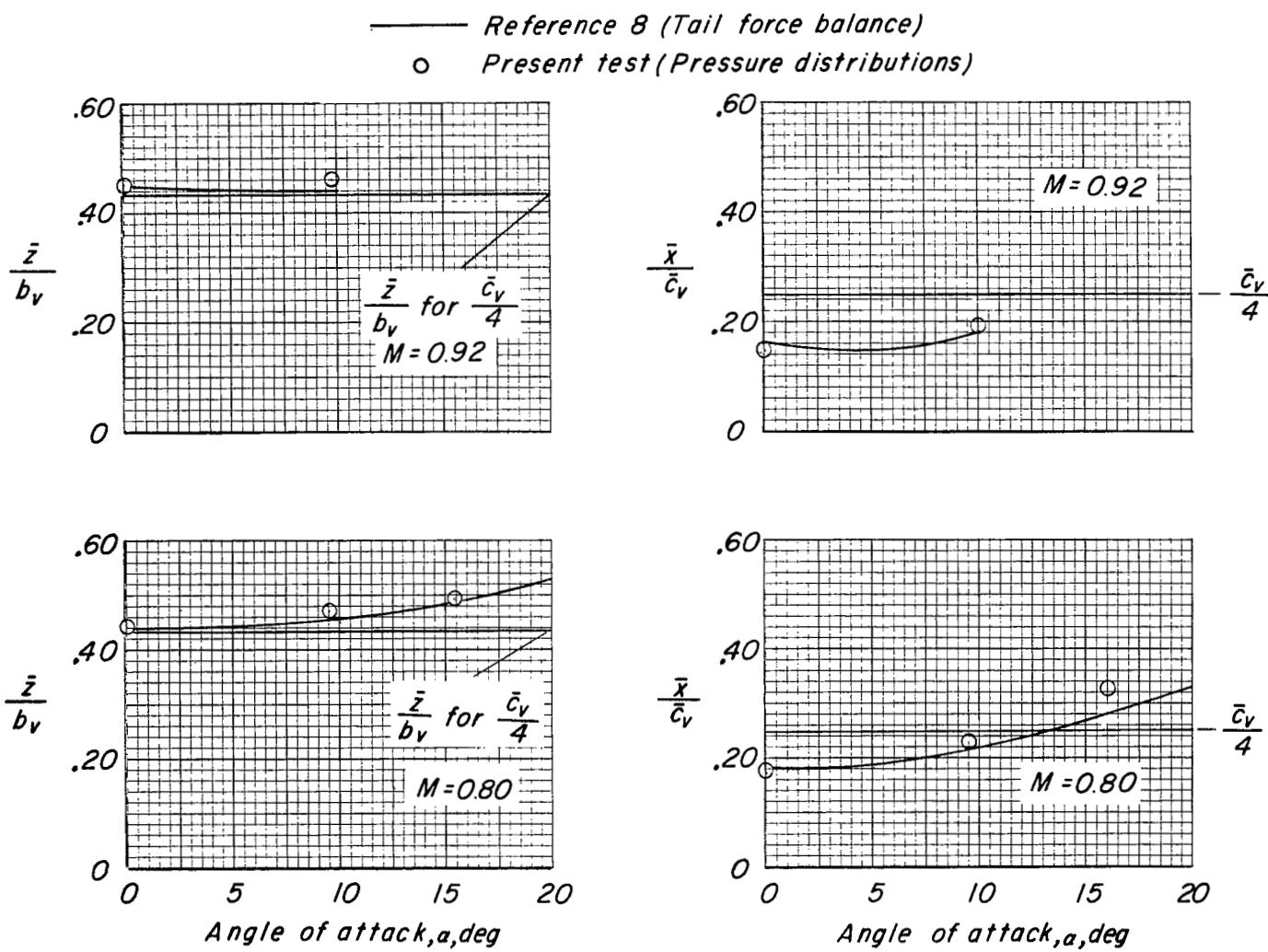


Figure 11.- Comparison of the location of the vertical-tail centers of pressure as obtained from force measurements and pressure measurements. $\Delta\beta \approx 8^\circ$; $i_t = 0^\circ$.

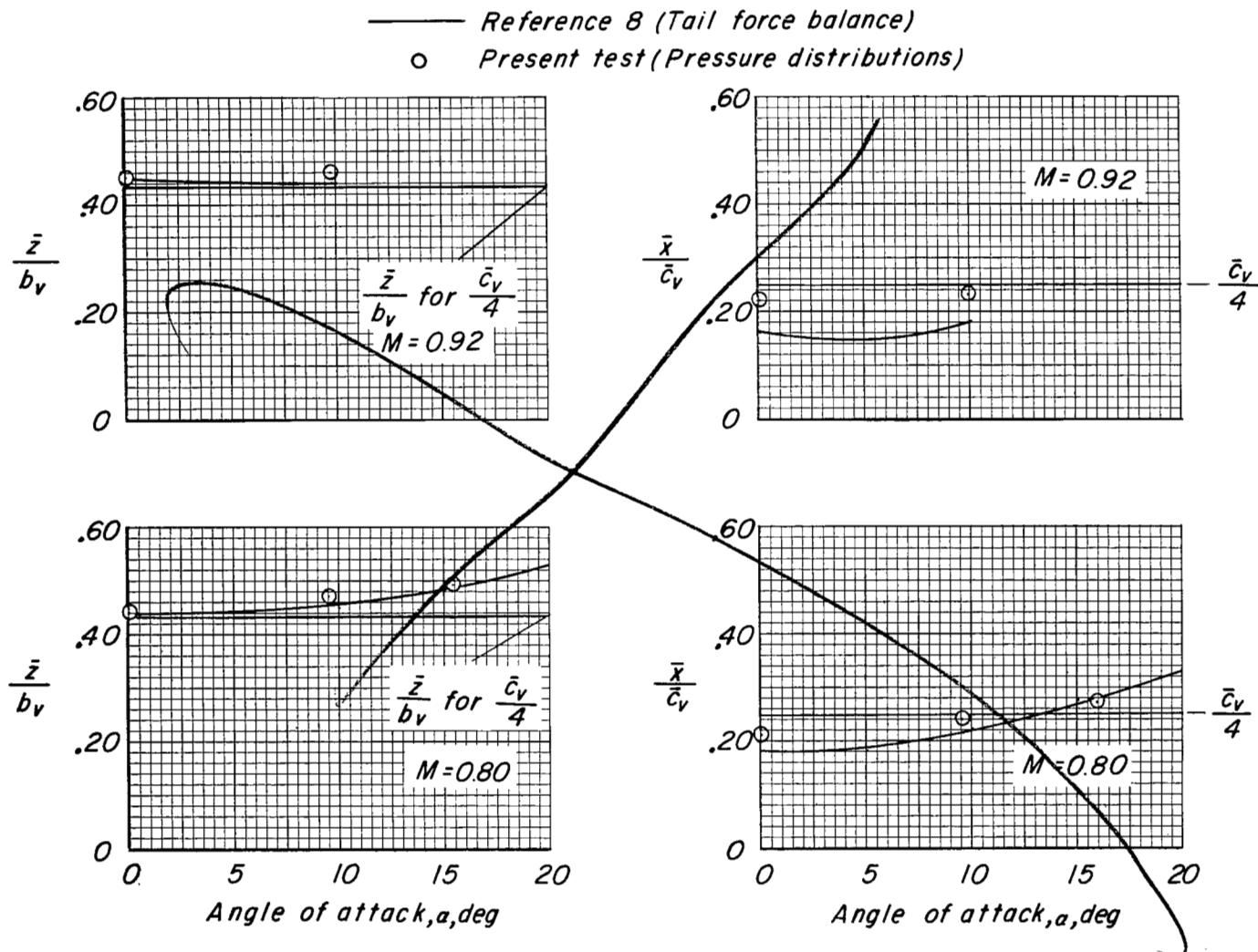


Figure 11.- Comparison of the location of the vertical-tail spanwise centers of pressure as obtained from force measurements and pressure measurements. Wing off; $\Delta\beta \approx 8^\circ$; $i_t = 0^\circ$.

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