

## REPORT No. 505

### TESTS OF NACELLE-PROPELLER COMBINATIONS IN VARIOUS POSITIONS WITH REFERENCE TO WINGS

#### IV—THICK WING—VARIOUS RADIAL-ENGINE COWLINGS—TANDEM PROPELLERS

By JAMES G. McHUGH

##### SUMMARY

This report is the fourth of a series giving the results obtained from tests in the N.A.C.A. 20-foot wind tunnel to determine the interference lift and drag and the propulsive efficiency of wing-nacelle-propeller combinations. Previous reports give the results of tests with tractor propellers with various forms of nacelles and engine cowlings. This report gives the results of tests of tandem arrangements of engines and propellers in 11 positions with reference to a thick wing.

The wing had an aspect ratio of 3, and a maximum thickness of 20 percent of the chord. The engines were 4/9-scale models of a Wright J-5 radial air-cooled engine and were installed in nacelles of the same scale. The propellers were 4 feet in diameter. Tests were made with two different nacelle shapes and with several different combinations of engine cowlings. The effects of variations in propeller spacing and in the angle of cowling-ring chord to thrust line were also investigated.

The lift, drag, and propulsive efficiency were determined at several angles of attack for the 2 nacelle shapes with various combinations of engine cowlings in each of 3 nacelle locations. From these tests the nacelle and cowling combination that gave the highest net efficiency was determined and used in all other nacelle locations tested.

The results indicate that with a tandem arrangement of engines and propellers the best over-all efficiency is obtained by using a nacelle of the lowest drag it is possible to obtain without impairing the cooling of the cylinders. Of the several engine-cowling combinations tested, best results were obtained with an N.A.C.A. hood over the front cylinders and a ring over the rear cylinders. When a large nacelle is used with this cowling combination there is little difference between the net efficiencies for positions with the nacelle faired into the wing and positions with the thrust line about half a propeller diameter below the lower surface of the wing, both positions being greatly superior to any position tested above the wing. These positions and cowlings, however, are considerably inferior to the best tractor-propeller arrangements previously reported.

##### INTRODUCTION

This report is the fourth of a series giving the results of an investigation to determine the mutual interference effects of wings, nacelles, and propellers on the aerodynamic characteristics of various combinations of these bodies. The program, originally presented at the Fourth Annual Aircraft Engineering Research Conference in May 1929, has subsequently been extended and now includes nacelles with tractor, pusher, and tandem propellers and biplane as well as monoplane wings. Tests have been made with several propeller pitch settings and with numerous types of cowlings of air-cooled engines.

The first three reports of the series (references 1, 2, and 3) have given the results obtained with a tractor propeller operating in proximity to monoplane wings. This fourth report presents the results obtained from tests of tandem arrangements of propellers and radial air-cooled engines in 11 positions with reference to a thick wing. Tests were made with two different nacelle shapes and with several different engine cowlings on each nacelle. A few additional tests were made to determine the effect of propeller spacing on propulsive efficiency. In order to prevent the number of tests from becoming excessive, the test positions were limited to those which merited practical consideration.

The locations of the nacelles with reference to the wing, the shape of the nacelles, and the various types of cowlings to be used were determined from a study of domestic and foreign airplanes incorporating tandem-engine installations in their design.

In order to show the relative merits of the various arrangements of wings, nacelles, and propellers with respect to performance a system of comparison has been developed, and in this report the relative merits of the various combinations are compared for two flight conditions.

Previous to these tests very little information was available on the effect of operating propellers in tandem. A few isolated tests had been made of tandem propellers alone, but the tests discussed here are the

first that have attempted to show the mutual interference effects of wings, nacelles, and propellers.

These tests were conducted in the N.A.C.A. 20-foot propeller-research tunnel at Langley Field, Va.

#### APPARATUS AND METHOD

The propeller-research tunnel in which these tests were made is described in reference 4. With the exceptions cited below, the standard apparatus and test methods were used. The wing used in the tests had a 5-foot chord, a 15-foot span, and a maximum thick-

The propellers used, 1 right-hand tractor and 1 left-hand pusher, were both 4 feet in diameter and were geometrically similar to the Navy no. 4412, 9-foot-diameter aluminum alloy propeller. A number of full-scale tests of this propeller have been made and are discussed in references 5 and 6. The blades may be turned in the hub to give different pitch settings.

Each propeller was driven by a 10-inch-diameter, 220-volt alternating-current induction motor capable of developing 25 horsepower at 3,600 r.p.m.; the two motors were operated in parallel. Wires were led from

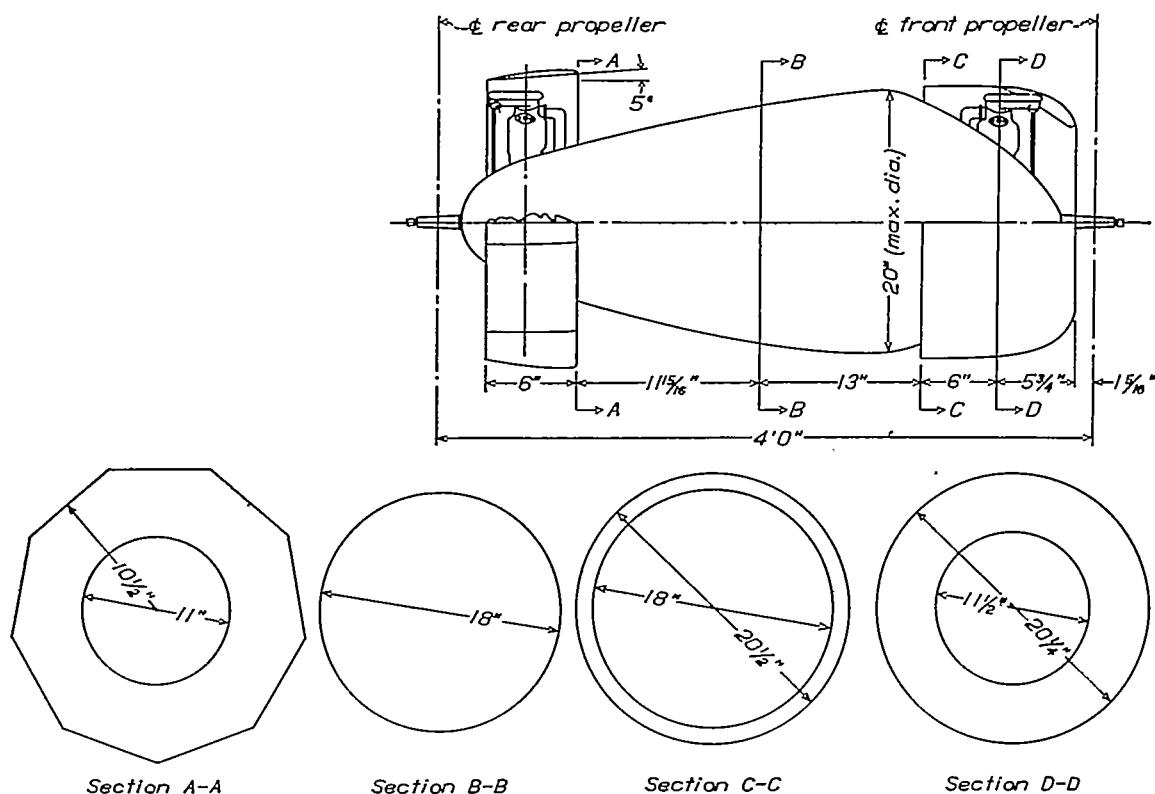


FIGURE 1.—Large nacelle and engine assembly, propeller spacing 1 diameter.

ness of 20 percent of the chord. It is described in detail in reference 1.

The engine nacelles, constructed of sheet aluminum, were similar to nacelles required for Wright J-5 radial engines and were four-ninths full scale. Detailed wooden models of the engines were installed in the nacelles. One nacelle, constructed with the dimensions given in figure 1 and called "large nacelle", represents what is believed to be the optimum practical nacelle shape for a propeller spacing of one diameter. Figure 2 shows the large nacelle modified for a propeller spacing of one and one-half diameters. The dimensions of a second nacelle, called a "small nacelle", are given in figure 3.

The engine cowlings used consisted of the N.A.C.A. hood, shown in figures 1 and 2, and the two variable-angle rings shown in figure 3. These rings are identical to the one shown in figure 3, reference 2.

the motors down the struts into the wing and along the supporting members to control equipment below. These wires were carefully taped to the struts and subsequent tests indicated that they had a negligible effect on the tare drag. A dynamometer was used for calibrating the motors and curves of active current against torque for various values of frequency were obtained for each motor.

The motors were driven from a variable-speed alternator, speed control being obtained by controlling the frequency of the current output from the alternator. Revolution speed was indicated by a condenser-type electric tachometer connected by wires to an indicating instrument on the control board.

In order to make the results obtained from the two sets of pitch settings herein discussed directly comparable with the results obtained from the tests reported in references 1, 2, and 3, the pitch of the two propellers

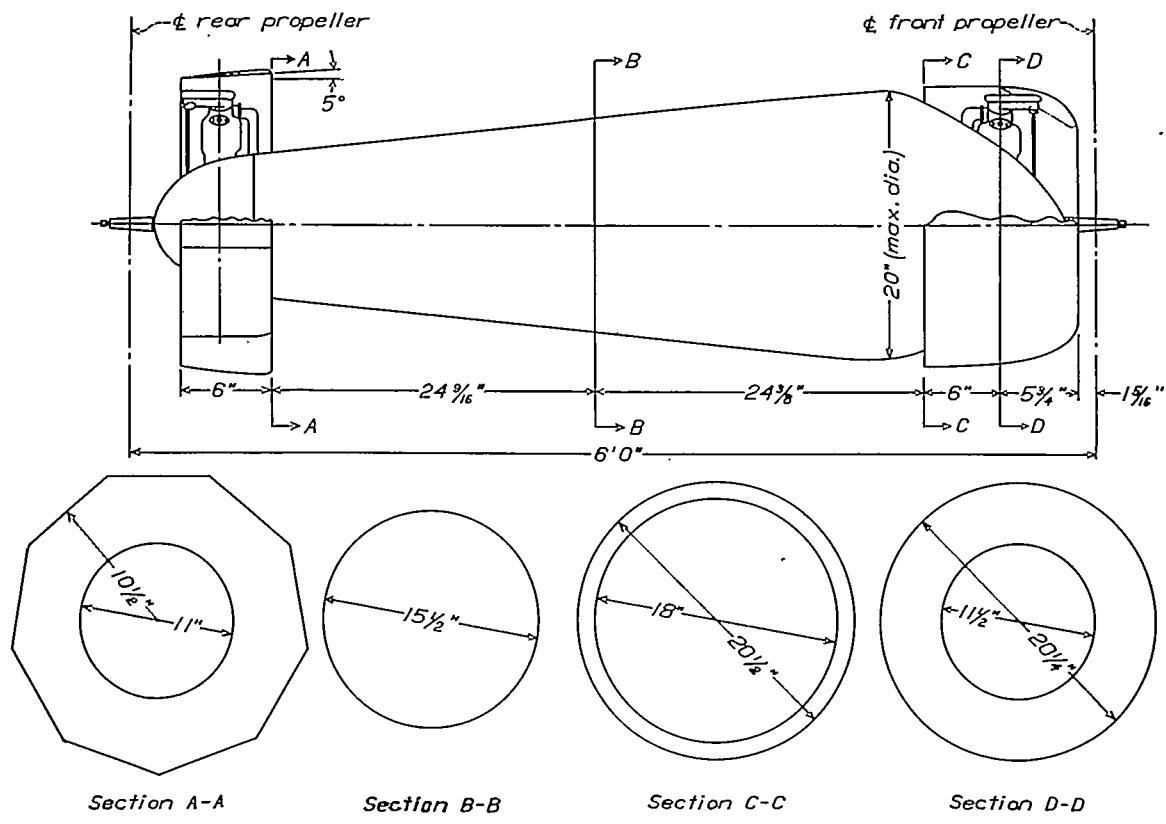
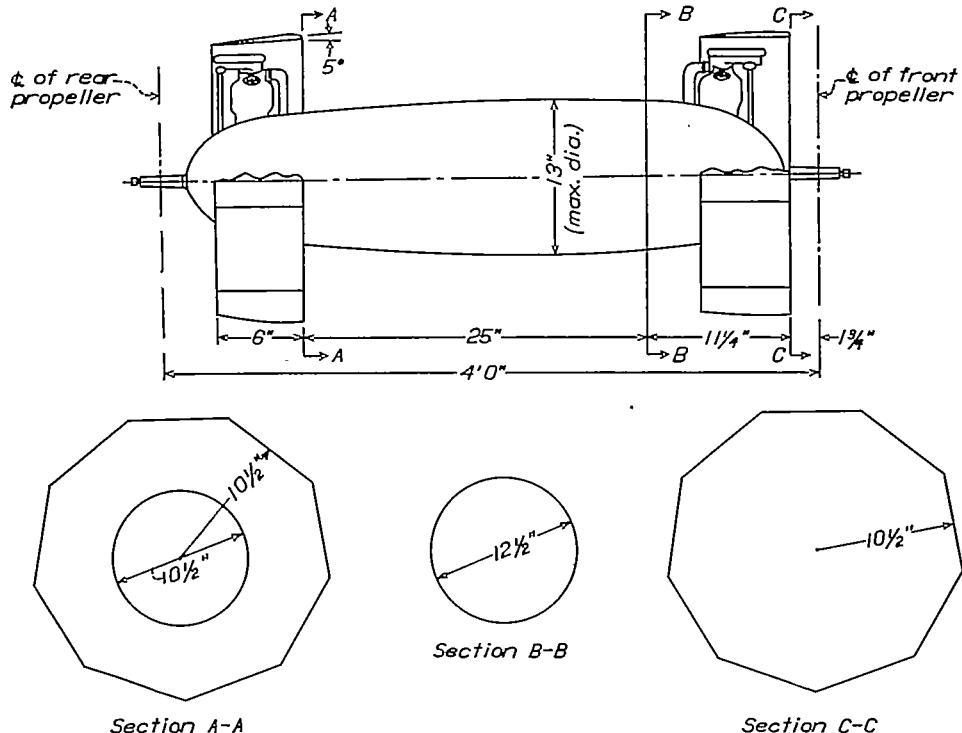
FIGURE 2.—Large nacelle and engine assembly, propeller spacing  $1\frac{1}{2}$  diameters.

FIGURE 3.—Small nacelle and engine assembly, propeller spacing 1 diameter.

was adjusted to give equal power coefficients at peak propulsive efficiency and also to bring the points of

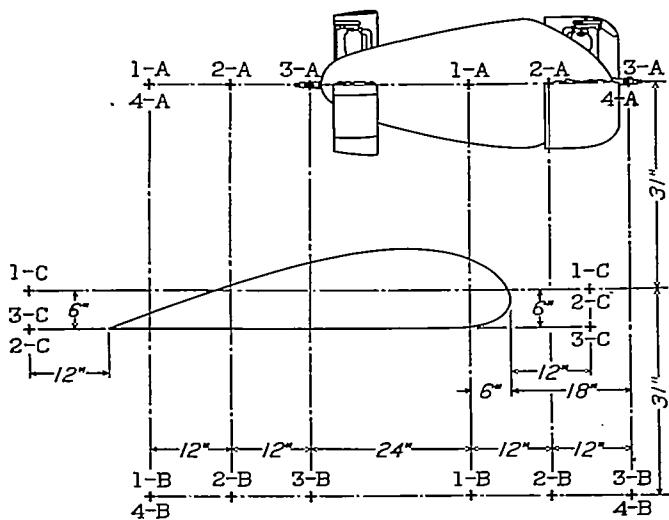


FIGURE 4.—Wing-nacelle test locations.

peak propulsive efficiency at values of  $V/nD=0.65$  for one set of pitch settings and at  $V/nD=0.83$  for the other set of pitch settings, these values of  $V/nD$  being

In order to determine the effect of nacelle shape, engine cowling, and angular setting of the variable-angle ring on the net efficiency of the wing-nacelle-propeller combination, drag and propeller tests were made using two different nacelle shapes and the following combinations of engine cowling:

With the large nacelle (fig. 1)—

Exposed cylinders front, exposed cylinders rear.  
N.A.C.A. hood front, exposed cylinders rear.  
N.A.C.A. hood front, variable-angle ring rear.  
Variable-angle ring front, variable-angle ring rear.

With the small nacelle (fig. 3)—

Exposed cylinders front, exposed cylinders rear.  
Exposed cylinders front, variable-angle ring rear.  
Variable-angle ring front, exposed cylinders rear.  
Variable-angle ring front, variable-angle ring rear.

In order to determine the optimum ring setting of the variable-angle ring, tests were made, in each of the above-mentioned combinations where the ring type of cowling was used, with the chord line of the ring sections set at several different angles with respect to the thrust line of the propellers.

All the above-mentioned nacelle and cowling arrangements were located in position 2-B as shown in figure



FIGURE 5.—Wing-nacelle combination mounted for test in position 4-A.

the points at which peak propulsive efficiency occurred in the tractor-propeller tests of references 1, 2, and 3 for the  $17^{\circ}$  and  $22^{\circ}$  pitch settings, respectively.

4, and it was found by testing some of them in positions 2-A and 1-C that their order of merit was apparently independent of nacelle location.

Using the best nacelle-cowling arrangement determined from the above-mentioned tests, tests were made with the wing and nacelle in the relative positions marked in figure 4. The nacelle positions are designated by the system of letters shown. In the figure the crosses indicate the positions of the center lines of the propeller hubs.

The wing-nacelle combinations were mounted on the balance by means of standard supports described in reference 7. With these supports the airfoil pivots about a line near the lower surface 25 percent of the chord back from the leading edge, the angle of attack being adjusted by a crank operating a post connected with a sting on the airfoil. The airfoil and nacelle mounted in one test position are shown in figure 5. Figures 6, 7, and 8 are photographs of other wing-nacelle combinations. In all cases the thrust line of the propeller was parallel to the wing chord. The lift and drag forces were measured simultaneously by balances on the floor below. The Reynolds Number varied from about 2,150,000 at the lowest air speed (50 miles per hour) to about 4,300,000 at the highest speed (100 miles per hour).

A series of tests at various air speeds was made with the wing alone at angles of attack of  $-5^\circ$ ,  $0^\circ$ ,  $5^\circ$ ,  $10^\circ$ , and  $12^\circ$ . Tests were also made without the wing, at an angle of attack of  $0^\circ$ , for a few of the more important nacelle and cowling arrangements.

With each wing-nacelle combination a run was made at several air speeds with the propellers removed. The lift, drag, moment, and air speed were measured at angles of attack of  $-5^\circ$ ,  $0^\circ$ ,  $5^\circ$ ,  $10^\circ$ , and  $12^\circ$ . A second test was then made with the propellers operating and with the tunnel operating at several air speeds. In this test the lift, drag (or thrust), torque, propeller revolution speed, and air speed were measured at angles of attack of  $-5^\circ$ ,  $0^\circ$ , and  $5^\circ$ .

Tare-drag measurements were made with the wing supported free of the balance supports. Other tests indicated that the propeller had a negligible effect on the tare drag.

## RESULTS

The measured lift and drag were reduced to the usual coefficients:

$$C_L = \frac{\text{lift}}{qS}$$

$$C_D = \frac{\text{drag}}{qS}$$

$$C_m = \frac{\text{moment}}{qSc}$$

where  $q$ , the dynamic pressure ( $\frac{1}{2}\rho V^2$ ).

$\rho$ , mass density of the air.

$V$ , velocity.

$S$ , area of the wing.

$c$ , chord of the wing.

(All moments were taken about the quarter-chord point of the wing.)

These coefficients were first plotted against the dynamic pressure  $q$  and then cross-plotted as  $C_L$ ,  $C_D$ , and  $C_m$  against  $\alpha$  (angle of attack) at values of the dynamic pressure corresponding to 50, 75, and 100 miles per hour in standard air.

The lift and drag coefficients have been plotted as polar diagrams so arranged as to facilitate comparison of the results with various cowlings in the different nacelle locations. Figure 9 shows the results for various cowlings and nacelles in position 2-A; figure 10 shows the results for position 2-B; and figure 11 the results for position 1-C. Figures 12, 13, and 14 compare the effect of various locations of the completely cowled large nacelle in positions above, below, and in the wing, respectively, and figure 15 shows the relative merits of representative nacelle locations above, below, and in the wing. In all these diagrams the polar of the wing alone is also given. All the polars are plotted from the data obtained at an air speed of 100 miles per hour. The results are also given in tables I and II together with those for two other air speeds, 50 and 75 miles per hour. The values of the moment coefficients, which were found to be the same for all air speeds, are given in table III.

The results with the propeller operating are reduced to the usual coefficients and are based on the revolution speed of the front propeller. Owing to the characteristics of the alternating-current motors used to drive the propellers the ratio

$$\frac{\text{revolution speed of the front propeller}}{\text{revolution speed of the rear propeller}}$$

was practically unity except at very low values of  $V/nD$ .

$$C_T = \frac{T - \Delta D}{\rho n_F^2 D^4}$$

$$C_{P_F} = \frac{P_F}{\rho n_F^3 D^5}$$

$$C_{P_R} = \frac{P_R}{\rho n_F^3 D^6}$$

$$C_{P_{\text{total}}} = C_{P_F} + C_{P_R}$$

$\eta$  = propulsive efficiency

$$= \frac{\text{effective thrust} \times \text{velocity of advance}}{\text{total motor power}}$$

$$= \frac{(T - \Delta D)V}{P_{\text{total}}}$$

$$= \frac{C_T}{C_{P_{\text{total}}}} \left( \frac{V}{n_F D} \right)$$

$C_s$  = propeller-operating coefficient (reference 5)

$$= \sqrt[5]{\frac{\rho V^5}{P_{\text{total}} n_F^3}}$$

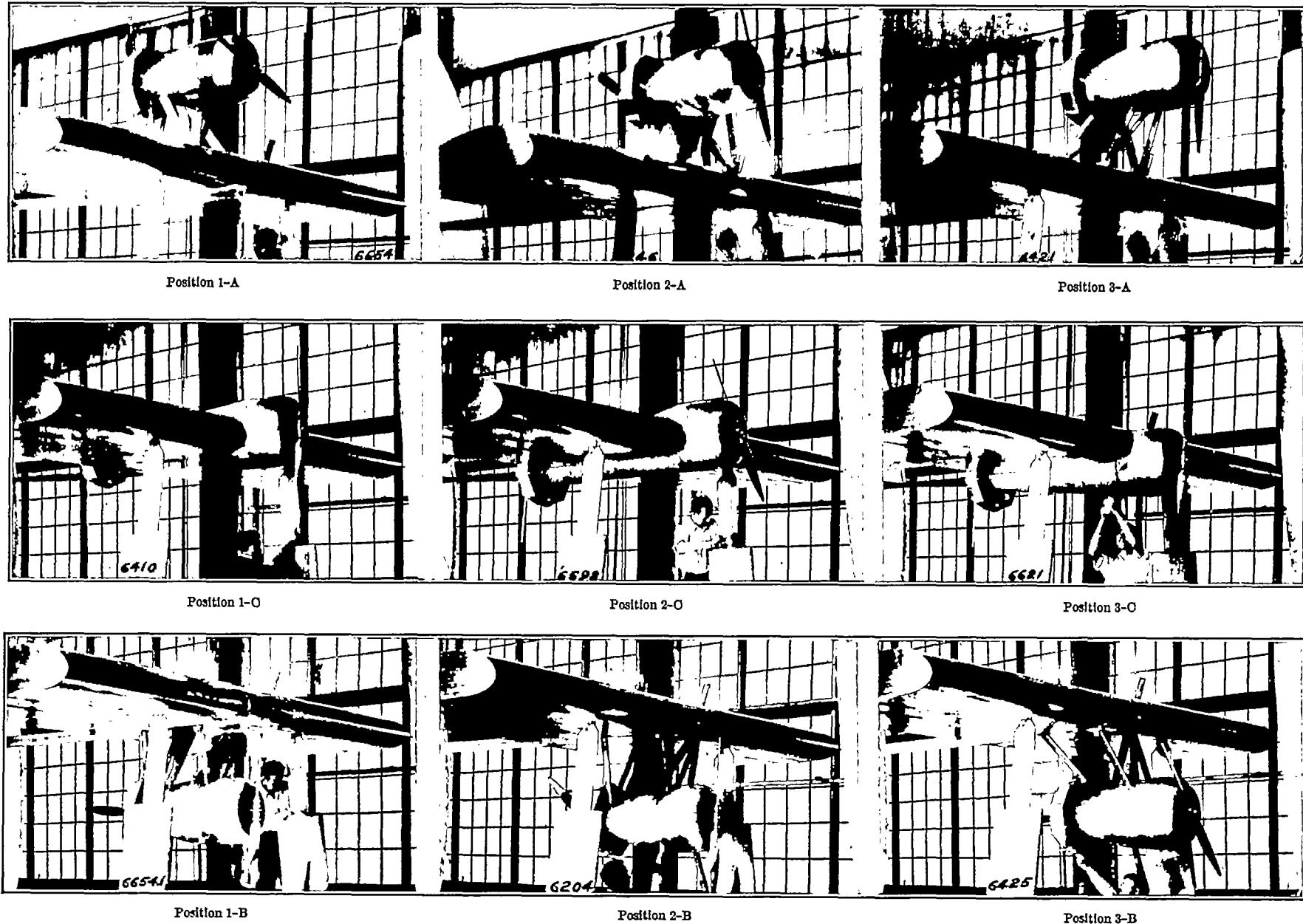
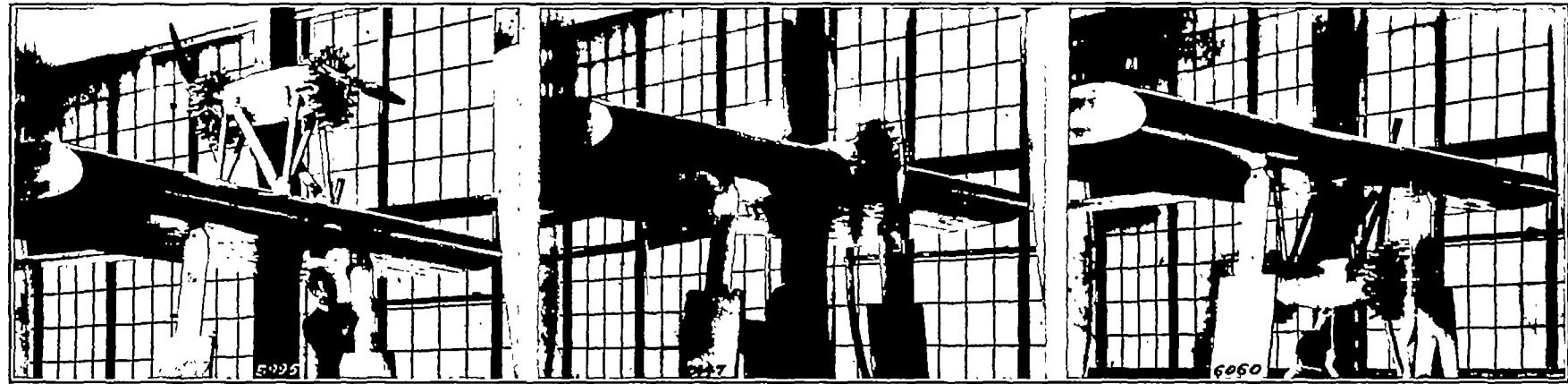


FIGURE 6.—Wing-nacelle positions with completely cowled large nacelle.



Small nacelle, exposed cylinders front and rear



Small nacelle, cowling ring front and rear

FIGURE 7.—Small nacelle with various cowlings in three different locations.



Position 2-A

Position 2-B

N.A.C.A. nacelle, exposed cylinders front and rear



Position 2-A

Position 2-B

N.A.C.A. nacelle, N.A.C.A. hood front, exposed cylinders rear

FIGURE 8.—Large nacelle with various cowlings in two different locations.

Where

 $T$ , thrust of propellers. $\Delta D$ , change in drag of body due to action of propellers. $T - \Delta D$ , effective thrust (discussed in reference 5). $n_F$ , front-propeller revolutions per unit time. $D$ , propeller diameter. $P_F$ , front-engine power. $P_R$ , rear-engine power. $P_{\text{total}}$ ,  $P_F + P_R$ . $\rho$ , mass density of the air. $C_L$  and  $C_m$  are computed as before but are now called  $C_{L_P}$  and  $C_{m_P}$ .The coefficients for all nacelle positions and cowlings at various values of  $V/nD$  and different angles of attack are given in tables IV to XI, inclusive:Table IV.—Thrust coefficient ( $C_T$ ).Table V.—Front-propeller power coefficient ( $C_{P_F}$ ).Table VI.—Rear-propeller power coefficient ( $C_{P_R}$ ).Table VII.—Propulsive efficiency ( $\eta$ ).Table VIII.—Propeller-operating coefficient ( $C_s$ ).Table IX.—Lift coefficient with propeller operating ( $C_{L_P}$ ).Table X.—Moment coefficient with propeller operating ( $C_{m_P}$ ).

Table XI.—Propeller coefficients—nacelle alone tests.

Since only individual values of the preceding coefficients are used in later comparisons, all curves are not reproduced here. Figure 16 is a typical plot of such values. (See also figs. 9-12 of reference 1.)

Aspect ratio and tunnel-wall interference corrections have not been made as the results are intended for comparative purposes only.

## ACCURACY

All readings were taken on scales and instruments that were calibrated frequently during the tests. The

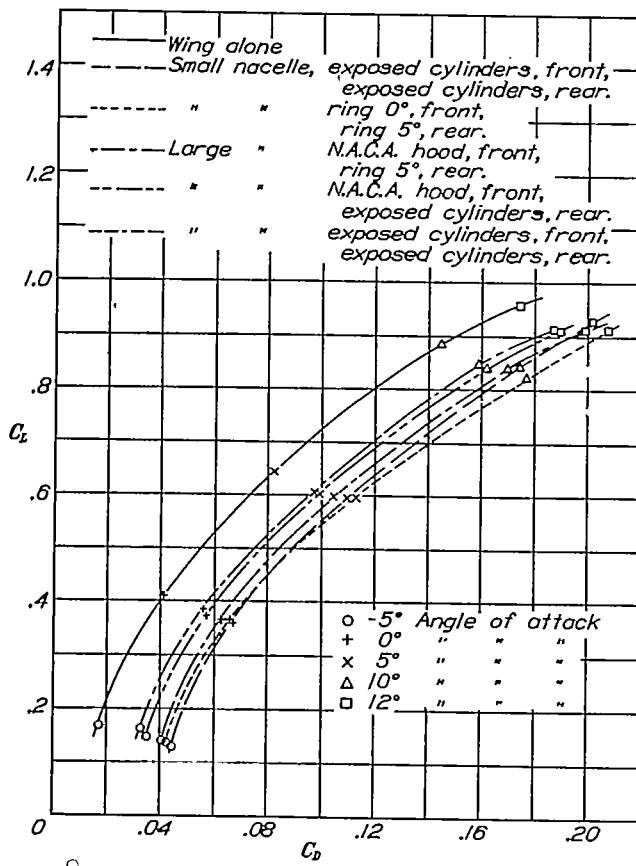


FIGURE 9.—Polar diagrams for various nacelles and cowlings in position 2-A.

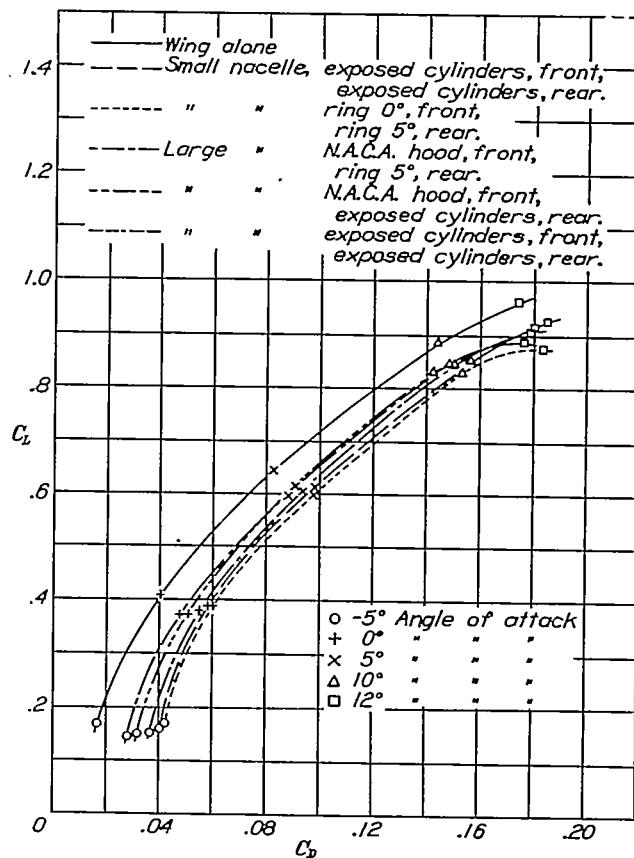


FIGURE 10.—Polar diagrams for various nacelles and cowlings in position 2-B.

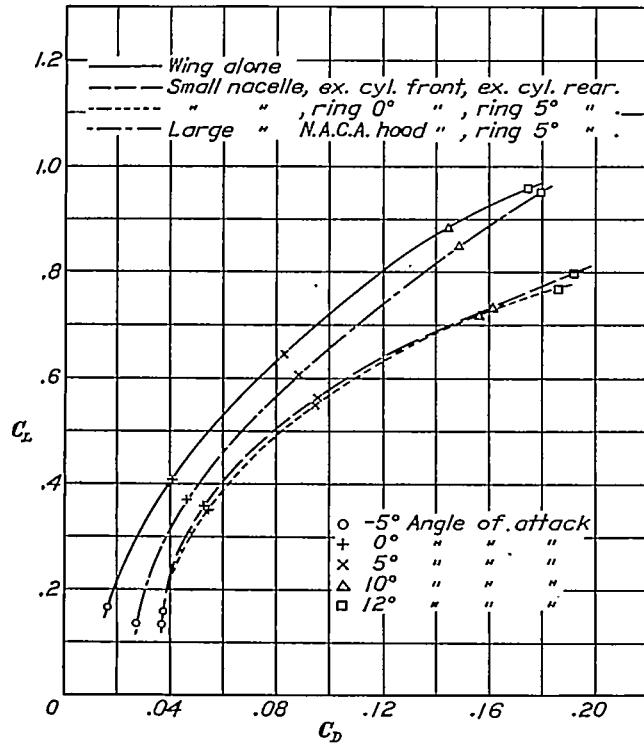


FIGURE 11.—Polar diagrams for various nacelles and cowlings in position 1-O.

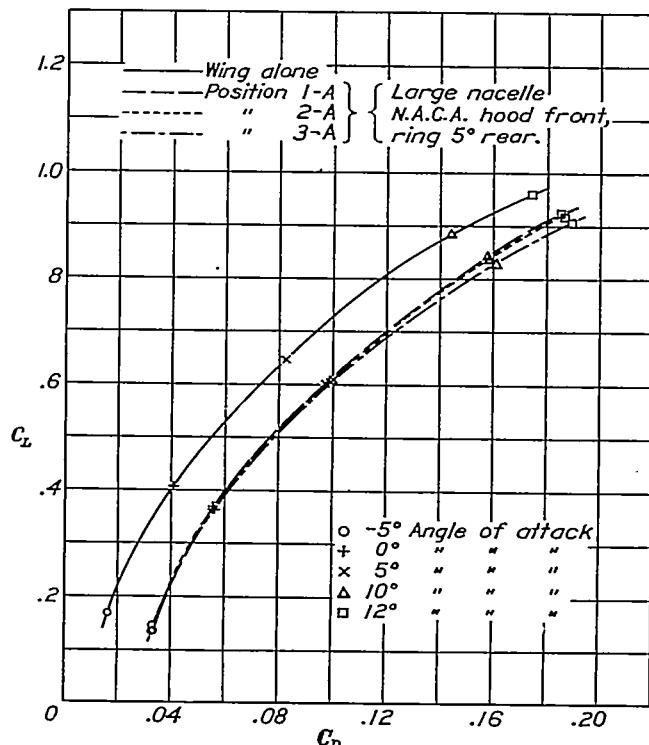


FIGURE 12.—Polar diagrams for completely cowled large nacelle in three positions above wing.

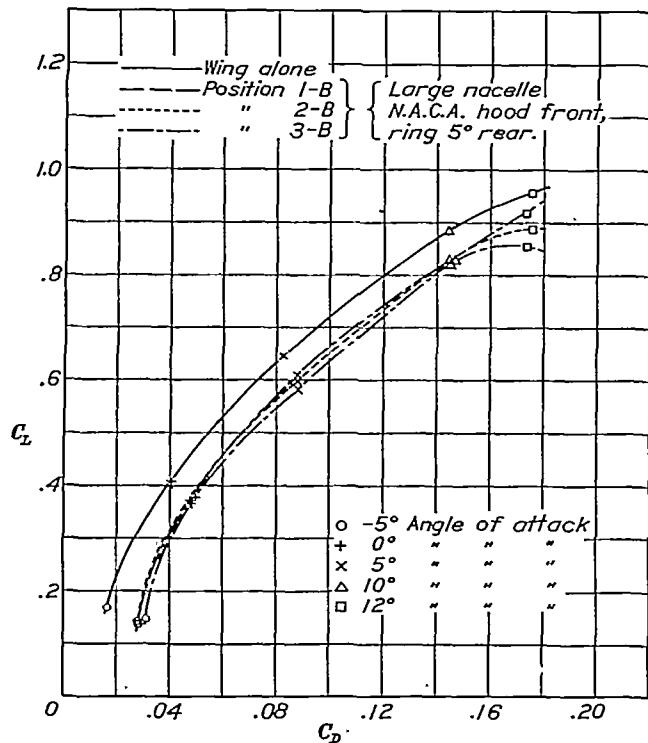


FIGURE 13.—Polar diagrams for completely cowled large nacelle in three positions below wing.

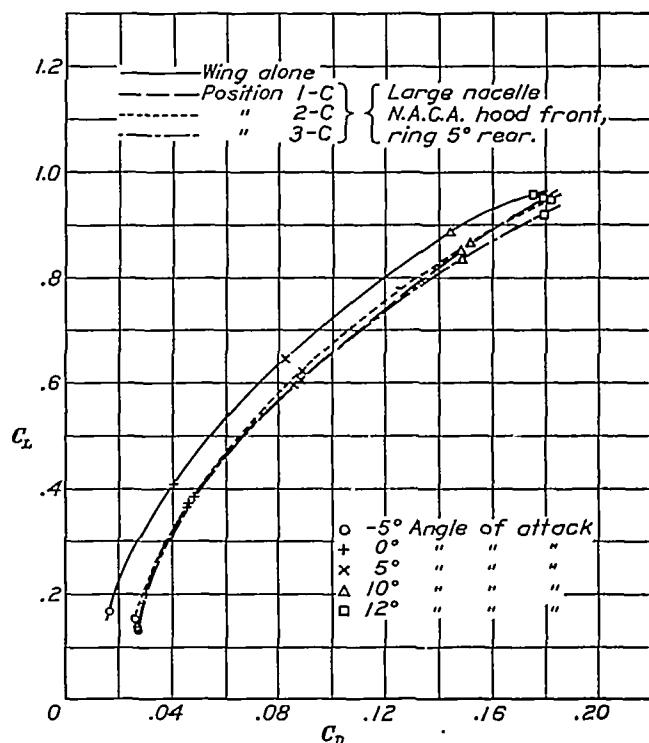


FIGURE 14.—Polar diagrams for completely cowled large nacelle in three positions in wing.

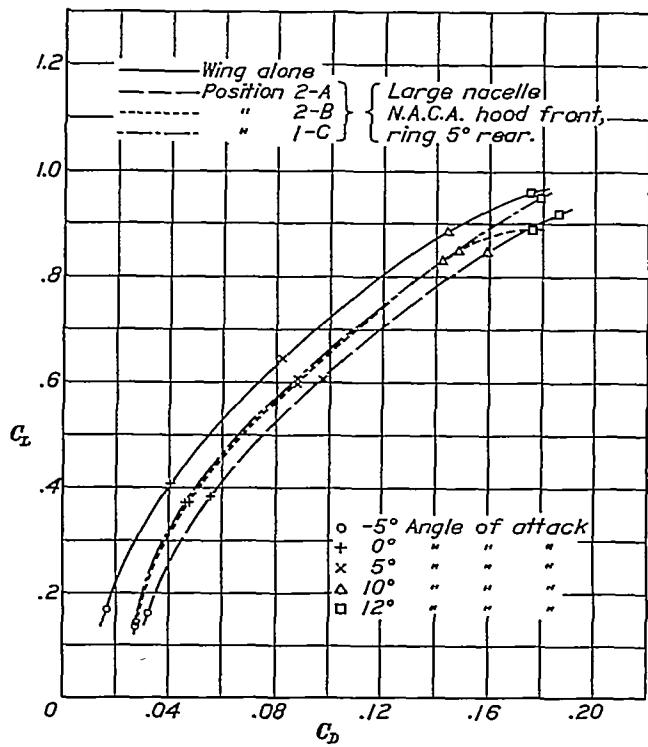


FIGURE 15.—Polar diagrams for completely cowled large nacelle above, below, and in wing.

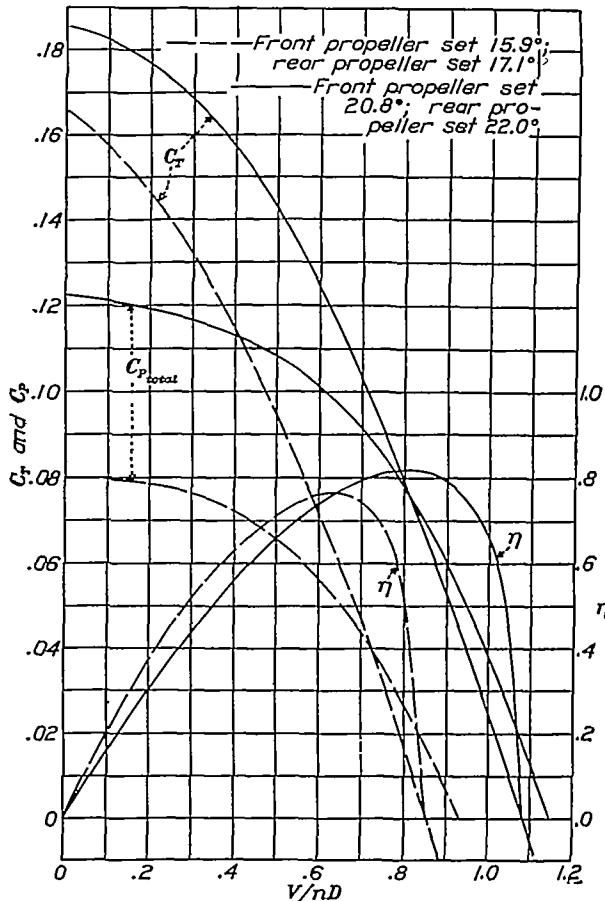


FIGURE 16.—Typical plots of  $C_{P_{total}}$ ,  $C_T$ , and  $\eta$  against  $V/nD$ . Large nacelle with N.A.C.A. hood front and variable-angle ring set 5° rear. Position 2-A. Angle of attack, 0°.

angle of attack of the airfoil was set within 5' of the desired angle with an inclinometer. The calibrations of motor torque are believed to be correct to within 0.1 foot-pound, and the motor revolution speed was measured to the nearest 10 r.p.m. The lift and drag were read to the nearest pound.

With the wing at high angles of attack, particularly near the burble point of the airfoil, the forces fluctuated rapidly and the above accuracy could not be obtained. The major portion of the faired results is believed to be correct within  $\pm 2$  percent, as indicated by the scattering of the test points.

#### DISCUSSION

The chief factors that determine the merits of a wing-nacelle-propeller combination are propulsive efficiency, lift chargeable to propeller and nacelle, and effective nacelle drag. In order to be strictly accurate, any comparison of the relative merits of a number of wing-nacelle-propeller combinations should take account of each factor. However, for a general case, no system of comparison so far devised is capable of taking into account each of the contributing factors in their exact proportion. Analysis of the problem immediately indicates that if the forces of propeller thrust and effective nacelle drag are represented as collinear vectors the force vector representing the lift chargeable to the propeller and nacelle must be represented at right angles to the force vectors of propeller thrust and effective nacelle drag, and a completely satisfactory method for evaluating lift in terms of thrust or drag is difficult to obtain.

Previous reports on this subject (references 1, 2, and 3) have taken account of the lift effect by charging to the nacelle the difference between the drag of the wing alone and the drag of the wing-nacelle combination at the angle of attack which, with propeller operating, gave the same lift coefficient as the wing alone. In this report, the various wing-nacelle-propeller combinations are compared for the high-speed and the climbing flight conditions by this method, which is fully discussed in reference 1.

It is desirable to point out here that, although the effect of the propeller and nacelle on wing lift is small at low angles of attack (at conditions corresponding to high or cruising speeds), it may be appreciable at high angles of attack (conditions corresponding to landing) and care should be used in design to consider these effects on lift for the latter condition. At high angles of attack the nacelle drag forms such a small proportion of the total drag that there is no material difference in total drag with different arrangements and the discussion of relative merit may be confined to the high-speed and climbing conditions mentioned in the preceding paragraph.

**Drag.**—Of the remaining factors affecting the merit of a wing-nacelle-propeller combination it may be said that, since the variation in propulsive efficiency for different nacelle positions is fairly small, the most important item is nacelle drag. This discussion will first consider the factors influencing the drag of the nacelle and subsequently will consider the effects of the propeller.

With reference to the polar diagrams of various nacelles and cowlings in position 2-A (fig. 9), position 2-B (fig. 10), and position 1-C (fig. 11), it will be noted that the drag of the combination with the large nacelle is appreciably less than it is with the small nacelle, regardless of the type of engine cowling used. With reference to the small nacelle it may also be seen that, except in the case of position 2-A at low angles of attack, the addition of cowling rings increased the drag over the values obtained with exposed cylinders. The effect of engine cowling on the large nacelle is shown in figures 9 and 10. It may be seen that placing the N.A.C.A. hood over the front-engine cylinders and leaving the rear engine with exposed cylinders shows a great decrease in drag as compared to that for the large nacelle with exposed cylinders both front and rear. The additional decrease in drag obtained through cowling the rear engine cylinders, although appreciable, is relatively small as compared to the reduction in drag obtained by cowling the front engine with the N.A.C.A. hood.

The effect of nacelle location on drag is of about equal importance with the effects of nacelle shape and cowling. Figures 12, 13, and 14, show the effects of variations in location of the completely cowled large nacelle in positions above the wing, below the wing, and in the wing, respectively. An inspection of these charts reveals the fact that moving the nacelle fore-and-aft has very little effect on nacelle drag, regardless of whether the nacelle be above the wing or below the wing. Figure 15 shows typical polars of the completely cowled large nacelle in positions above, below, and in the wing. It is to be noted that positions in the wing and positions below the wing are about equal with respect to drag and that both are greatly superior to positions above the wing.

The effect on nacelle drag of angular setting of the variable-angle ring is shown in figures 17 and 18. It is to be noted that the nacelle drag is not appreciably affected by rear-ring setting within the range of  $-5^\circ$  to  $10^\circ$ , but is quite sensitive to front-ring setting.

**Propulsive efficiency.**—Figures 17 and 18 show the effect, with the small nacelle, of variable-angle ring setting on propulsive efficiency. Comparisons are made at a constant value of  $V/nD$ . With reference to figure 17, it will be noted that with the rear cylinders exposed the peak of the propulsive-efficiency curve

apparently occurs at a front-ring setting of about  $5^\circ$ . Putting a ring with a setting of  $5^\circ$  over the rear cylinders increased the propulsive efficiency for all values of front-ring setting, but the maximum value apparently still occurs at a front-ring setting of about  $5^\circ$ . The

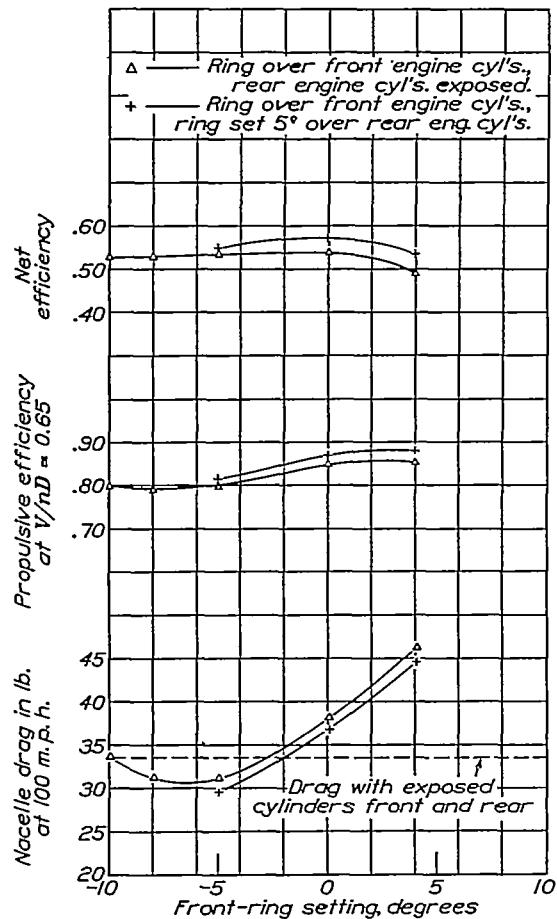


FIGURE 17.—Effect of front-ring setting on nacelle drag, propulsive efficiency, and net efficiency. Small nacelle in position 2-B.

effect of varying the angular setting of the rear ring is shown in figure 18. It may be seen that with the front cylinders exposed the propulsive efficiency continued to increase with increasing angular setting of the variable-angle ring. It is to be noted that placing the ring with an angular setting of  $0^\circ$  over the front cylinders increased the propulsive efficiency slightly and caused the point of maximum efficiency to occur at a rear-ring setting of about  $5^\circ$ .

Further consideration of the problem of ring setting shows that the point of maximum net efficiency comes neither at the ring setting which gives minimum drag nor at the setting which gives maximum propulsive efficiency, but at some intermediate point. The results shown in figures 17 and 18 show the optimum ring settings to be about  $0^\circ$  for the front ring and about  $5^\circ$  for the rear ring. For all practical cases the optimum ring settings are apparently independent of nacelle shape.

The results of these tests show that the fore-and-aft location of the nacelle with reference to the wing has very little influence on the maximum efficiency obtainable at any given value of  $C_s$  (see reference 5 for a discussion of this coefficient), the maximum variation ranging from about 2 percent for positions above the wing to about 1 percent for positions below the wing. The vertical location of the nacelle with reference to the wing does, however, have an appreciable effect. Figures 19, 20, and 21 are plots of  $\eta$  and  $V/nD$  against  $C_s$  for representative nacelle locations above, below, and in the wing, respectively. Inspection of these curves reveals that the propulsive efficiency obtained with nacelle positions below the wing is somewhat higher than that obtained with positions above the wing, and that for nacelle positions in the wing the propulsive efficiency is considerably lower than that

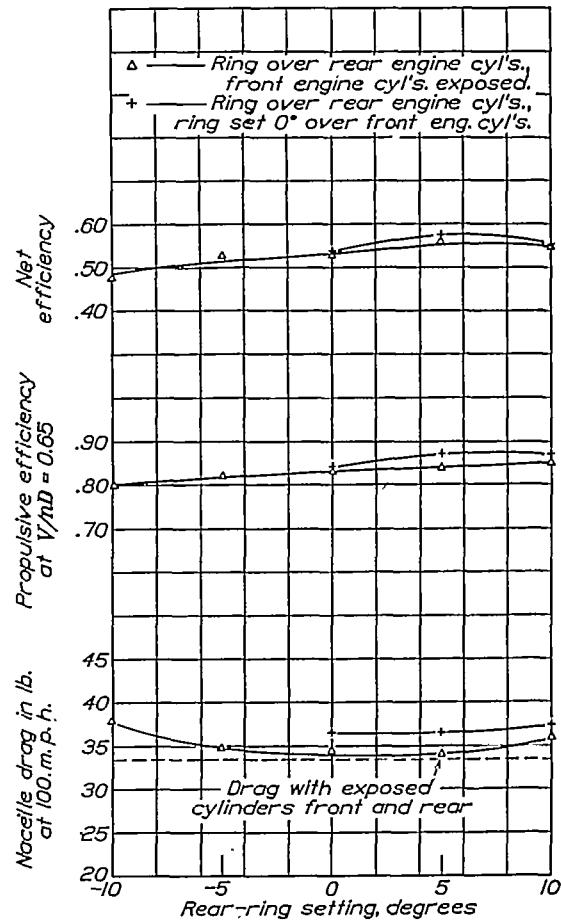


FIGURE 18.—Effect of rear-ring setting on nacelle drag, propulsive efficiency, and net efficiency. Small nacelle in position 2-B.

obtained with the nacelle located either above or below the wing.

#### COMPARISON OF RESULTS

As stated at the beginning of the discussion, the true merit of any wing-nacelle combination is determined by the interrelation of the lift, drag, and pro-

peller effects considered separately. The detailed discussion of the method given in reference 1 and used in the previous reports of this series results in the following equations:

$$\text{Propulsive efficiency} = \eta = \frac{(T - \Delta D)V}{P} = \frac{C_T}{C_P} \frac{V}{nD}$$

$$\text{Nacelle drag efficiency factor} = \frac{C_{D\sigma} - C_{Dw}}{C_P} \frac{S}{2D^2} \left( \frac{V}{nD} \right)^3$$

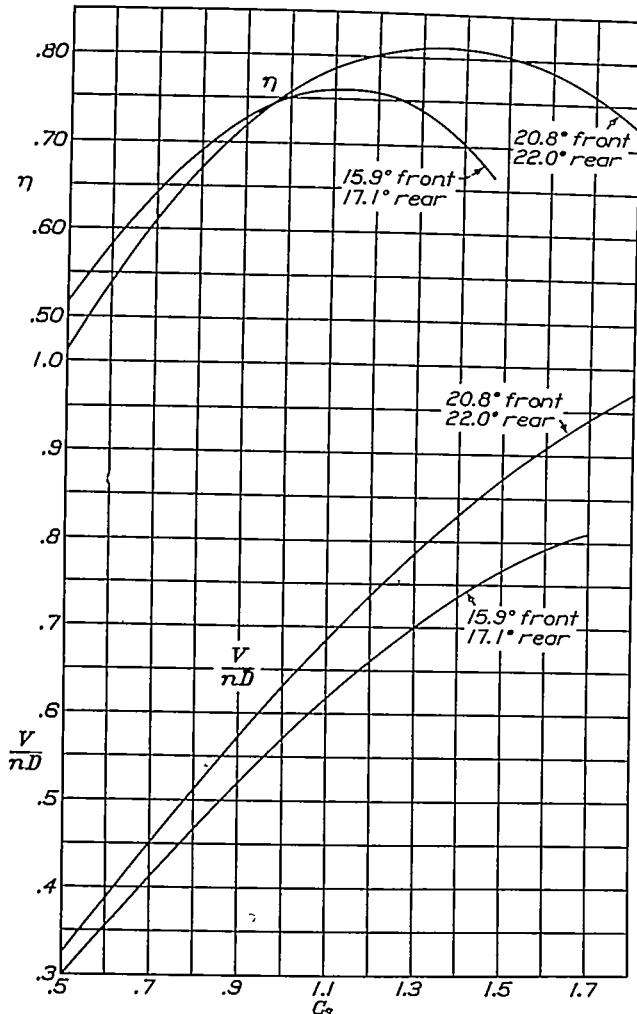


FIGURE 10.—Variation of  $\eta$  and  $V/nD$  with  $C_g$  for typical position above wing Tandem position 2-A. Angle of attack, 0°. Large nacelle with N.A.C.A. hood front, ring 5° rear. Blade angle of propeller at 0.75 R.

$$\text{Net efficiency} = \text{propulsive efficiency} - \text{nacelle drag efficiency factor} = \frac{C_T}{C_P} \frac{V}{nD} - \frac{C_{D\sigma} - C_{Dw}}{C_P} \frac{S}{2D^2} \left( \frac{V}{nD} \right)^3$$

where  $C_{Dw}$ , drag coefficient of the wing at a given angle of attack.

$C_{D\sigma}$ , drag coefficient of the wing-nacelle combination (propeller removed) at the angle of attack at which the lift coefficient with the propeller operating is the same as the lift coefficient of the wing alone at the given angle of attack.

These formulas are applied to two conditions: One for high speed and cruising with a propeller  $\frac{V}{nD} = 0.65$  and a lift coefficient corresponding to that of the wing alone at an angle of attack of 0° ( $C_L = 0.409$ ), and one for climbing with a  $\frac{V}{nD} = 0.42$  and a lift coefficient corresponding to that of the wing alone at an angle of attack of 5° ( $C_L = 0.652$ ). The  $\frac{V}{nD}$  selected for the high-speed comparison is that at which the propellers operated at maximum efficiency for pitch settings from 15.8° to 17.1°. The  $\frac{V}{nD}$  for climb is obtained by

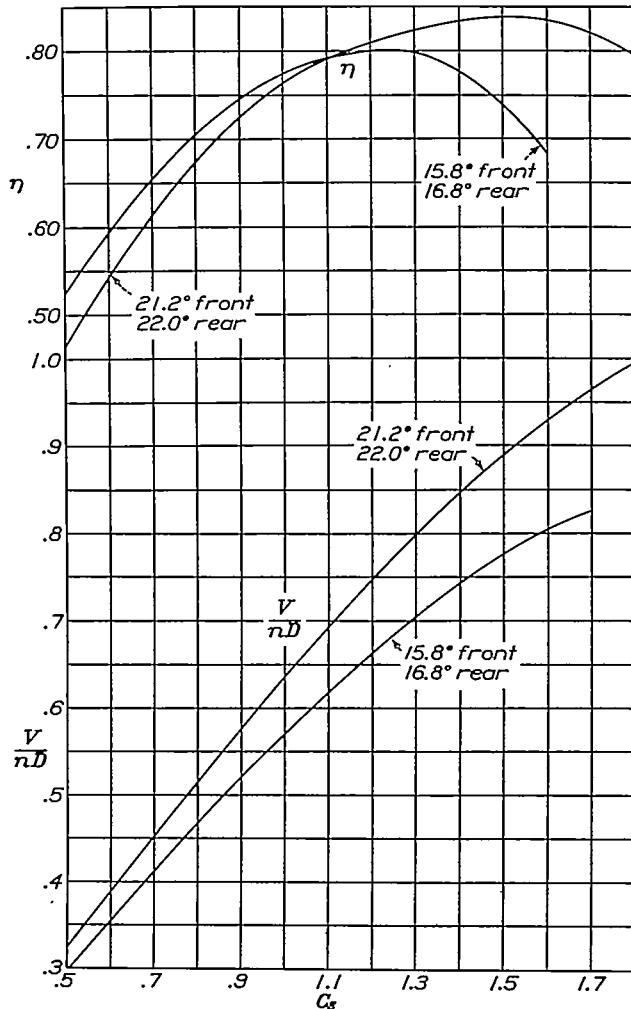


FIGURE 20.—Variation of  $\eta$  and  $V/nD$  with  $C_g$  for typical position below wing Tandem position 2-B. Angle of attack, 0°. Large nacelle with N.A.C.A. hood front, ring 5° rear. Blade angle of propeller at 0.75 R.

assuming that climbing is done at 60 percent of high speed and that the torque of the engine is constant. A diagram of the method of obtaining the drag value used in computing the nacelle drag efficiency factor is given in reference 3. The foregoing values of lift coefficient and  $\frac{V}{nD}$  are the same as have been used in

previous comparisons of results for the airfoil used in these tests and the net efficiencies may be directly compared.

It would perhaps be better to make comparisons at a constant value of  $C_s$  but there is no evidence that the relative order of merit would be changed and the

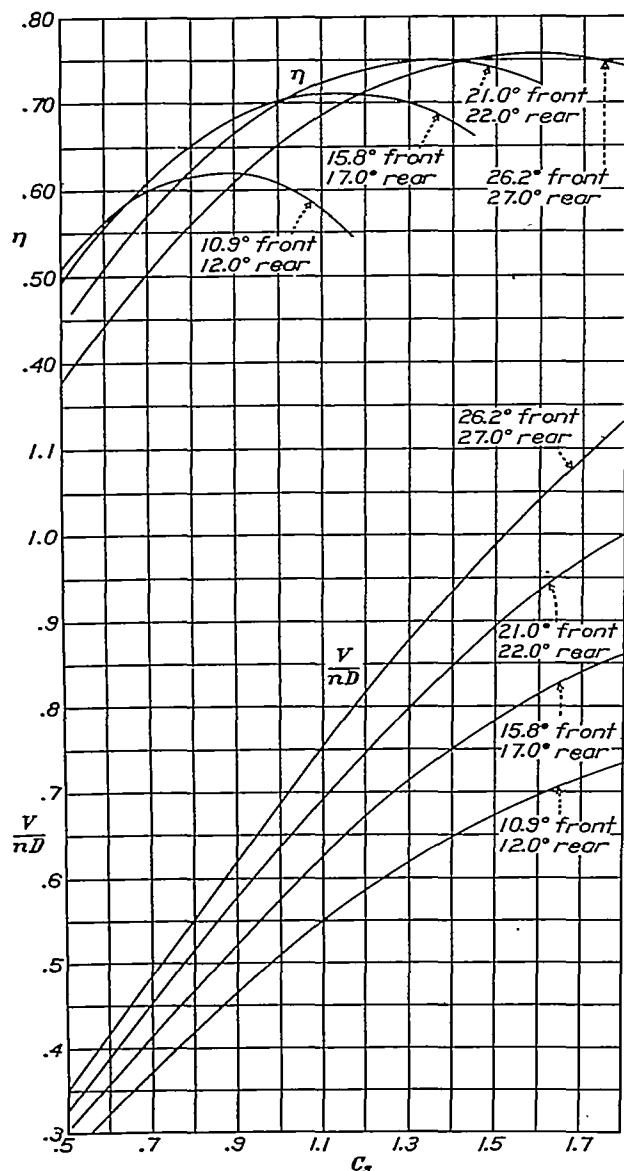


FIGURE 21.—Variation of  $\eta$  and  $V/nD$  with  $C_s$  for typical position in wing. Tandem position 1-C. Angle of attack, 0°. Large nacelle with N.A.C.A. hood front, ring 5° rear. Blade angle of propeller at 0.75 R.

resulting complication would not be justified. The order of merit of the various cowling and nacelle positions, which is the primary object of the analysis, is clearly indicated by the present computations. The results are given in table XII. For a few arrangements for which the data are incomplete, no net efficiencies are given. That these are generally poor, however, can be seen from the data given.

Examination of the table for the high-speed condition shows that the large nacelle with N.A.C.A. hood

on front engine and variable-angle ring set 5° on the rear engine located in position 2-C gives the highest net efficiency (0.614), followed closely by the same nacelle in position 2-B (net efficiency 0.611). The net efficiency is only slightly lower for other locations of the same nacelle below the wing but falls to low values for locations above the wing. Other types of cowling show lower values in all locations. With the engine cylinders exposed the net efficiency drops to very low values (0.386 for position 2-A, small nacelle).

The propulsive efficiencies are fairly high but the nacelle drag efficiency factors are also high, which accounts for the low net efficiencies. The lowest nacelle drag efficiency factor (0.106 for position 2-C) is accompanied by a low propulsive efficiency (0.720).

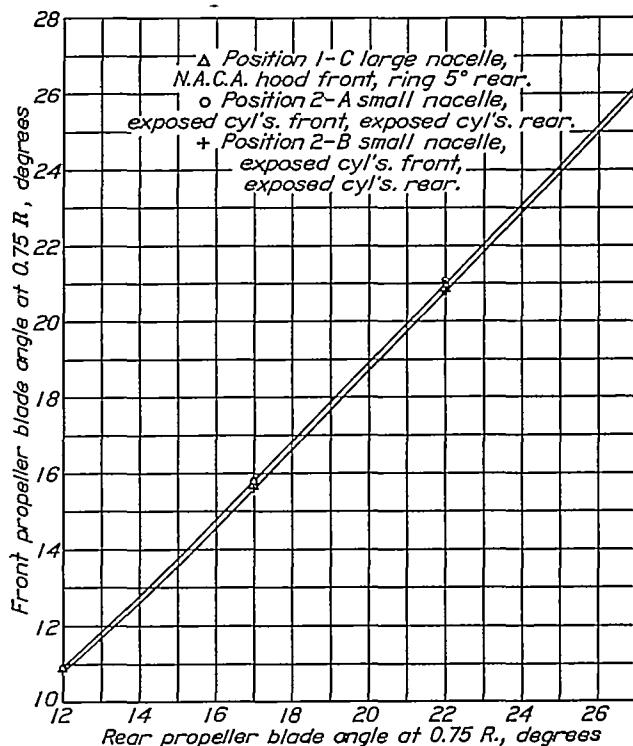


FIGURE 22.—Relation between the pitch setting of front propeller and the pitch setting of rear propeller for equal power absorbed at peak efficiency.

It appears that this arrangement would be improved by moving the front engine farther ahead of the wing, judging by the results for tractor position B of reference 1. The net efficiency for the latter is 0.752, so that the best tandem arrangement is greatly inferior to the best tractor. The cowled tractor nacelle is known to have a low drag and the general inferiority of the tandem arrangement must accordingly be charged to the high drag of the rear portion of the nacelle. In view of the satisfactory propulsive efficiencies, the study of new types of cowling or, perhaps, relocations of the rear engine should result in improved performance.

Two of the various schemes that have been advanced for improvement in the shape of tandem-propeller

nacelles are: (1) The mounting of two tractor engines in tandem, and (2) the mounting of the pusher engine forward of the tractor engine in such a manner that the two propellers face each other. Both these schemes, as well as various others that have been proposed, would undoubtedly involve serious cooling problems, and since no tests are known to have been made on them the results that might be obtained through the use of radical types of cowling are entirely problematical. It is thought, however, that there are good possibilities of discovering a nacelle cowling combination for tandem-engine nacelles that would give a lower drag than conventional arrangements.

#### PITCH-SETTING RATIO

In conventional tandem arrangement of engines and propellers it is generally desirable for the pitch settings of the two propellers to be such that both engines will turn at the same revolution speed at full throttle. In this series of tests the pitch of the two propellers was adjusted in each case to give equal power coefficients at the point of peak propulsive efficiency and, as it can be shown that for propellers of the same diameter, both driven by engines with equal torque characteristics,

$$\frac{\text{r.p.m. front propeller}}{\text{r.p.m. rear propeller}} = \sqrt{\frac{C_{P_{\text{rear}}}}{C_{P_{\text{front}}}}}$$

it is evident that when the power coefficients of both propellers are the same the propellers are both turning at the same revolution speed. The results of these tests indicate that no absolute ratio of pitch settings can be determined to fit all cases, because the required ratio is different for each nacelle location. Test results do indicate, however, that for any given nacelle location the pitch setting of one propeller is practically a straight-line function of the pitch setting of the other. Figure 22 shows the relation between the pitch setting of the rear propeller and the pitch setting of the front propeller for several typical cases.

#### DESIGN CONSIDERATIONS

There is no definite relation between engine power and engine diameter; consequently no definite ratio of nacelle drag to motor power can be established which will be generally applicable. For any given nacelle-propeller combination in which the nacelle shape and location are similar to those considered in this report the designer may, from the data presented, determine quite accurately the drag of the full-scale nacelle. The values of propulsive efficiency as obtained here should be practically the same as those that would be obtained from full-scale propeller tests and, as long as the ratio of propeller diameter to nacelle diameter is nearly the same, the values may be applied to full-scale propellers with little error.

Knowing the nacelle drag and propulsive efficiency, the designer may for his particular case determine the power available after the drag of the nacelle has been accounted for.

No data are available for determining how the slip-stream lift as obtained in these tests may be applied to full-scale airplane design. The results of these tests indicate the relative effects of the propellers on the wing lift, but judgment must be used in applying those results to airplane design.

#### CONCLUSIONS

1. With tandem propellers the effects on net efficiency of nacelle shape and cowling are of equal importance with those of nacelle location.
2. In general, tandem-propeller-nacelle positions below the wing and positions in the wing are of about equal merit, and both are greatly superior to positions above the wing.
3. Conventional tandem arrangements of radial air-cooled engines do not give as good net efficiencies as can be obtained by the use of two tractor-propeller installations of the same general arrangement.
4. The net efficiency of a tandem-nacelle-propeller combination is not greatly affected by fore-and-aft location of the nacelle with reference to the wing.

LANGLEY MEMORIAL AERONAUTICAL LABORATORY,  
NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS,  
LANGLEY FIELD, VA., January 17, 1934.

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TABLE I  
LIFT COEFFICIENT WITHOUT PROPELLER

$$C_L = \frac{\text{lift}}{qS}$$

Nacelle position	Type of nacelle	Engine cowling		50 m.p.h. R.N.=2,160,000				75 m.p.h. R.N.=3,220,000				100 m.p.h. R.N.=4,300,000				
		Front	Rear	-5°	0°	5°	10°	-5°	0°	5°	10°	-5°	0°	5°	10°	
<b>Angle of attack</b>																
		<b>Wing alone</b>		0.179	0.417	0.652	0.889	0.175	0.414	0.650	0.887	0.169	0.409	0.646	0.885	
1-A	Large	N.A.C.A. hood	Ring 5°	.167	.400	.633	.868	.153	.387	.620	.866	.134	.370	.601	.840	
2-A	do	do	do	.170	.383	.605	.850	.167	.383	.606	.848	.162	.385	.607	.846	
	do	Exposed cylinders	do	.175	.390	.619	.854	.165	.377	.613	.848	.149	.375	.608	.840	
	Small	do	do	.145	.384	.617	.846	.144	.378	.608	.842	.142	.370	.598	.840	
	do	N.A.C.A. hood	Ring 5°	.172	.385	.618	.850	.165	.380	.609	.845	.130	.363	.597	.842	
	do	Ring 0°	do	.163	.380	.618	.842	.140	.370	.608	.833	.123	.358	.588	.820	
	3-A	Large	N.A.C.A. hood	do	.154	.366	.610	.833	.150	.387	.610	.830	.146	.367	.610	.830
	4-A	do	do	do	.166	.402	.628	.852	.148	.385	.615	.848	.124	.360	.598	.840
	do	Ring 5°	do	.155	.368	.615	.850	.154	.374	.610	.848	.163	.385	.607	.843	
	1-B	do	do	Ring 5°	.167	.390	.633	.863	.157	.380	.624	.848	.143	.368	.610	.830
	2-B	do	do	Ring 0°	.160	.380	.607	.830	.154	.374	.604	.830	.148	.370	.600	.828
	do	do	Ring 5°	.173	.393	.613	.840	.162	.388	.606	.836	.145	.373	.598	.830	
	do	do	Ring 10°	.160	.382	.618	.833	.158	.380	.610	.838	.157	.373	.598	.833	
	do	do	Exposed cylinders	.178	.400	.628	.848	.165	.390	.624	.846	.150	.375	.605	.845	
	do	Exposed cylinders	do	.170	.390	.620	.853	.163	.388	.615	.848	.162	.380	.607	.842	
	do	Ring 5°	do	.174	.388	.625	.842	.168	.388	.620	.840	.160	.382	.608	.838	
	do	Ring 10°	do	.173	.408	.613	.846	.164	.396	.605	.843	.163	.380	.599	.840	
	do	Ring 15°	do	.180	.406	.615	.840	.170	.394	.610	.838	.158	.376	.605	.835	
	Small	do	do	do	.183	.398	.620	.850	.170	.395	.618	.850	.160	.392	.614	.860
	do	do	Ring 10°	.175	.403	.632	.845	.170	.395	.620	.840	.160	.390	.606	.840	
	do	do	Ring 5°	.180	.403	.620	.838	.175	.396	.614	.838	.163	.388	.607	.833	
	do	do	Ring 0°	.174	.400	.623	.846	.166	.395	.614	.842	.157	.390	.605	.838	
	do	do	Ring -5°	.172	.400	.620	.840	.170	.397	.618	.840	.167	.390	.612	.840	
	do	do	Ring -10°	.185	.400	.617	.850	.177	.400	.617	.860	.170	.400	.617	.860	
	do	do	Ring 4°	.190	.400	.632	.840	.170	.390	.624	.840	.163	.380	.616	.840	
	do	do	Ring 0°	.187	.406	.632	.840	.170	.390	.624	.840	.167	.390	.617	.840	
	do	do	Ring -5°	.177	.400	.620	.845	.170	.395	.625	.840	.178	.384	.617	.840	
	do	do	Ring -8°	.190	.397	.630	.848	.175	.395	.635	.850	.164	.395	.615	.844	
	do	do	Ring -10°	.194	.410	.630	.844	.184	.396	.628	.848	.163	.384	.624	.843	
	do	do	Ring 4°	.167	.395	.625	.845	.167	.393	.615	.835	.165	.380	.605	.820	
	do	do	Ring 5°	.187	.404	.630	.857	.178	.384	.617	.834	.170	.383	.600	.834	
	do	do	Ring 0°	.168	.385	.615	.843	.170	.388	.610	.840	.170	.390	.600	.830	
	do	do	Ring 10°	.174	.400	.625	.840	.168	.392	.620	.835	.168	.382	.613	.830	
	do	do	Ring 0°	.190	.400	.630	.844	.184	.395	.625	.840	.175	.390	.615	.838	
3-B	Large	N.A.C.A. hood	Ring 5°	.148	.378	.605	.820	.148	.378	.605	.825	.160	.378	.585	.820	
4-B	do	do	do	.153	.386	.606	.830	.148	.380	.600	.830	.140	.375	.594	.828	
1-C	do	do	do	.164	.380	.616	.860	.147	.376	.610	.855	.138	.370	.605	.850	
	Small	do	do	.158	.386	.577	.743	.158	.363	.570	.740	.168	.360	.563	.735	
	do	do	Ring 0°	.165	.357	.560	.713	.145	.355	.558	.728	.135	.353	.560	.720	
2-C	Large	N.A.C.A. hood	do	.178	.404	.635	.864	.168	.395	.630	.863	.152	.385	.622	.803	
3-C	do	do	do	.155	.404	.618	.848	.145	.385	.610	.840	.135	.365	.598	.834	

TABLE II  
DRAG COEFFICIENT WITHOUT PROPELLER

$$C_D = \frac{\text{drag}}{qS}$$

Nacelle position	Type of nacelle	Engine cowling		50 m.p.h. R.N.=2,150,000				75 m.p.h. R.N.=3,220,000				100 m.p.h. R.N.=4,300,000				
		Front	Rear	-5°	0°	5°	10°	-5°	0°	5°	10°	-5°	0°	5°	10°	
Angle of attack.....				0.0180	0.0425	0.0830	0.1440	0.0175	0.0415	0.0825	0.1440	0.0165	0.0405	0.0825	0.1440	
		Wing alone														
1-A	Large.....	N.A.C.A. hood.....	Ring 5°.....	.0362	.0577	.0998	.1598	.0350	.0570	.0988	.1588	.0335	.0560	.0975	.1575	
2-A	do.....	do.....	do.....	.0342	.0582	.0980	.1625	.0338	.0560	.0978	.1608	.0324	.0555	.0970	.1588	
	do.....	Exposed cylinders.....	do.....	.0374	.0590	.0995	.1640	.0360	.0580	.0990	.1630	.0350	.0568	.0980	.1617	
	Small.....	do.....	do.....	.0410	.0640	.1063	.1700	.0409	.0633	.1060	.1698	.0405	.0622	.1043	.1697	
	do.....	N.A.C.A. hood.....	Ring 5°.....	.0455	.0690	.1130	.1785	.0448	.0680	.1115	.1750	.0440	.0645	.1095	.1738	
	do.....	Ring 0°.....	do.....	.0415	.0655	.1140	.1770	.0412	.0655	.1133	.1762	.0408	.0650	.1125	.1747	
				.0455	.0690	.1153	.1780	.0440	.0678	.1140	.1770	.0420	.0658	.1128	.1760	
3-A	Large.....	N.A.C.A. hood.....	do.....	.0340	.0578	.1020	.1635	.0338	.0670	.1010	.1620	.0330	.0560	.1000	.1603	
4-A	do.....	do.....	do.....	.0380	.0610	.1027	.1640	.0363	.0590	.1015	.1628	.0340	.0570	.0995	.1608	
	do.....	Ring 0°.....	do.....	.0370	.0585	.1025	.1638	.0360	.0580	.1005	.1620	.0340	.0570	.0985	.1595	
1-B	do.....	do.....	Ring 5°.....	.0290	.0490	.0900	.1480	.0285	.0485	.0890	.1473	.0280	.0478	.0878	.1460	
2-B	do.....	do.....	Ring 0°.....	.0305	.0510	.0905	.1482	.0300	.0498	.0900	.1470	.0300	.0480	.0895	.1455	
	do.....	do.....	Ring 5°.....	.0295	.0495	.0902	.1478	.0290	.0485	.0890	.1430	.0280	.0475	.0878	.1440	
	do.....	do.....	Ring 10°.....	.0310	.0495	.0900	.1485	.0300	.0485	.0880	.1430	.0285	.0475	.0875	.1450	
	do.....	do.....	Exposed cylinders.....	.0320	.0415	.0920	.1505	.0315	.0510	.0915	.1495	.0315	.0505	.0910	.1480	
	do.....	Exposed cylinders.....	do.....	.0380	.0600	.0960	.1530	.0375	.0558	.0950	.1520	.0365	.0548	.0935	.1500	
	do.....	Ring -5°.....	do.....	.0385	.0555	.0950	.1640	.0380	.0845	.0940	.1630	.0368	.0835	.0830	.1515	
	do.....	Ring -10°.....	do.....	.0370	.0540	.0940	.1530	.0365	.0835	.0935	.1510	.0340	.0830	.0930	.1485	
	do.....	Ring -15°.....	do.....	.0365	.0555	.0960	.1530	.0360	.0850	.0950	.1520	.0350	.0840	.0930	.1505	
	Small.....	Exposed cylinders.....	do.....	.0410	.0598	.0995	.1575	.0405	.0892	.0990	.1590	.0400	.0880	.0980	.1560	
	do.....	do.....	Ring 10°.....	.0420	.0595	.0980	.1530	.0415	.0890	.0980	.1525	.0408	.0893	.0980	.1520	
	do.....	do.....	Ring 5°.....	.0410	.0595	.0975	.1525	.0405	.0855	.0965	.1520	.0400	.0852	.0980	.1515	
	do.....	do.....	Ring 0°.....	.0410	.0580	.0975	.1525	.0405	.0830	.0970	.1540	.0400	.0835	.0983	.1520	
	do.....	do.....	Ring -5°.....	.0402	.0585	.0980	.1560	.0400	.0880	.0980	.1580	.0400	.0885	.0980	.1540	
	do.....	do.....	Ring -10°.....	.0414	.0600	.1020	.1680	.0405	.0898	.1000	.1670	.0400	.0863	.0980	.1560	
	do.....	do.....	Ring 4°.....	.0465	.0645	.1030	.1615	.0463	.0640	.1030	.1695	.0460	.0645	.1030	.1665	
	do.....	Ring 0°.....	do.....	.0424	.0620	.1000	.1660	.0422	.0608	.0999	.1558	.0420	.0603	.0993	.1555	
	do.....	Ring -5°.....	do.....	.0415	.0578	.0980	.1580	.0407	.0570	.0980	.1560	.0400	.0588	.0970	.1560	
	do.....	Ring -8°.....	do.....	.0390	.0575	.0980	.1530	.0380	.0570	.0975	.1525	.0385	.0568	.0960	.1520	
	do.....	Ring -10°.....	do.....	.0395	.0588	.0990	.1580	.0390	.0680	.0980	.1565	.0389	.0680	.0965	.1545	
	do.....	Ring 4°.....	Ring 6°.....	.0480	.0650	.1015	.1670	.0470	.0640	.1010	.1570	.0460	.0637	.1005	.1660	
	do.....	Ring -5°.....	do.....	.0390	.0570	.0950	.1530	.0380	.0560	.0950	.1520	.0370	.0559	.0940	.1605	
	do.....	Ring 0°.....	do.....	.0440	.0615	.0995	.1600	.0430	.0605	.0985	.1645	.0420	.0595	.0975	.1525	
	do.....	do.....	Ring 10°.....	.0465	.0615	.0995	.1600	.0445	.0610	.0985	.1645	.0430	.0600	.0975	.1535	
	do.....	do.....	Ring 0°.....	.0430	.0605	.1000	.1680	.0425	.0600	.0995	.1545	.0420	.0595	.0985	.1525	
3-B	Large.....	N.A.C.A. hood.....	Ring 5°.....	.0325	.0495	.0875	.1460	.0320	.0495	.0875	.1450	.0310	.0490	.0880	.1440	
4-B	do.....	do.....	do.....	.0325	.0500	.0885	.1460	.0315	.0490	.0880	.1450	.0295	.0480	.0870	.1450	
1-O	do.....	do.....	do.....	.0295	.0488	.0895	.1600	.0285	.0480	.0890	.1490	.0270	.0460	.0880	.1480	
	Small.....	Exposed cylinders.....	Exposed cylinders.....	.0400	.0555	.0985	.1620	.0390	.0540	.0970	.1615	.0375	.0525	.0950	.1605	
	do.....	Ring 0°.....	Ring 5°.....	.0385	.0575	.0940	.1580	.0375	.0560	.0940	.1570	.0365	.0540	.0940	.1560	
2-O	Large.....	N.A.C.A. hood.....	do.....	.0285	.0510	.0930	.1615	.0275	.0495	.0910	.1515	.0260	.0480	.0890	.1515	
3-O	do.....	do.....	do.....	.0300	.0495	.0895	.1610	.0285	.0475	.0880	.1490	.0270	.0455	.0855	.1460	

TABLE III  
MOMENT COEFFICIENT WITHOUT PROPELLER

$$C_m = \frac{\text{moment}}{qSc}$$

Nacelle position	Type of nacelle	Engine cowling		Angle of attack				
		Front	Rear	-5°	0°	5°	10°	12°
		Wing alone		-0.073	-0.067	-0.063	-0.066	-0.069
1-A	Large	N.A.C.A. hood	Ring 5°	-0.067	-0.063	-0.063	-0.072	-0.072
2-A	do	do	do	-0.064	-0.060	-0.055	-0.063	-0.070
	do	do	Exposed cylinders	-0.061	-0.059	-0.058	-0.063	-0.064
	do	Exposed cylinders	do	-0.061	-0.058	-0.056	-0.062	-0.058
	Small	do	do	-0.061	-0.058	-0.059	-0.062	-0.066
	do	N.A.C.A. hood	Ring 5°	-0.064	-0.053	-0.055	-0.055	-0.059
	do	Ring 0°	do	-0.056	-0.053	-0.050	-0.053	-0.059
3-A	Large	N.A.C.A. hood	do	-0.060	-0.054	-0.051	-0.056	-0.053
4-A	do	do	do	-0.061	-0.055	-0.057	-0.058	-0.057
	do	do	Ring 0°	-0.059	-0.054	-0.053	-0.057	-0.059
1-B	do	do	Ring 5°	-0.067	-0.063	-0.064	-0.071	-0.070
2-B	do	do	Ring 0°	-0.074	-0.070	-0.068	-0.070	-0.080
	do	do	Ring 5°	-0.073	-0.070	-0.067	-0.072	-0.078
	do	do	Ring 10°	-0.078	-0.069	-0.068	-0.072	-0.076
	do	do	Exposed cylinders	-0.076	-0.072	-0.071	-0.073	-0.077
	do	Exposed cylinders	do	-0.076	-0.071	-0.069	-0.074	-0.080
	do	Ring -5°	do	-0.077	-0.070	-0.071	-0.076	-0.083
	do	Ring -10°	do	-0.077	-0.072	-0.070	-0.071	-0.081
	do	Ring -15°	do	-0.076	-0.071	-0.071	-0.073	-0.070
	Small	do	do	-0.078	-0.071	-0.074	-0.076	-0.072
	do	do	Ring 10°	-0.078	-0.070	-0.069	-0.074	-0.077
	do	do	Ring 5°	-0.074	-0.070	-0.071	-0.074	-0.070
	do	do	Ring 0°	-0.076	-0.070	-0.068	-0.074	-0.082
	do	do	Ring -5°	-0.070	-0.070	-0.070	-0.075	-0.081
	do	do	Ring -10°	-0.077	-0.070	-0.069	-0.076	-0.080
	do	do	Ring -15°	-0.076	-0.071	-0.071	-0.073	-0.070
	do	do	Ring 4°	-0.080	-0.074	-0.076	-0.082	-0.084
	do	do	Ring 0°	-0.078	-0.076	-0.074	-0.076	-0.082
	do	do	Ring -5°	-0.081	-0.073	-0.074	-0.074	-0.079
	do	do	Ring -8°	-0.077	-0.078	-0.073	-0.073	-0.080
	do	do	Ring -10°	-0.076	-0.074	-0.072	-0.076	-0.078
	do	do	Ring 4°	-0.081	-0.072	-0.071	-0.077	-0.086
	do	do	Ring -5°	-0.075	-0.070	-0.069	-0.072	-0.080
	do	do	Ring 0°	-0.080	-0.073	-0.071	-0.072	-0.082
	do	do	Ring 10°	-0.081	-0.073	-0.074	-0.074	-0.083
	do	do	Ring 0°	-0.078	-0.072	-0.071	-0.075	-0.082
3-B	Large	N.A.C.A. hood	Ring 5°	-0.082	-0.076	-0.073	-0.075	-0.076
4-B	do	do	do	-0.078	-0.071	-0.066	-0.070	-0.071
1-C	do	do	do	-0.077	-0.066	-0.055	-0.060	-0.059
	Small	do	do	-0.068	-0.066	-0.063	-0.073	-0.073
	do	do	do	-0.076	-0.062	-0.053	-0.061	-0.060
2-C	Large	N.A.C.A. hood	do	-0.077	-0.063	-0.061	-0.057	-0.057
3-C	do	do	do	-0.085	-0.073	-0.070	-0.064	-0.069

TABLE IV

THRUST COEFFICIENT,  $C_T = \frac{T - \Delta D}{\rho_{air} V^2 D}$

ANGLE OF ATTACK =  $-5^\circ$

**Front propeller:** Right hand no. 4412—4-foot diameter. **Rear propeller:** Left hand no. 4412—4-foot diameter.

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 $R$		$\frac{V}{nD}$									Propeller pitch at 0.75 $R$		$\frac{V}{nD}$											
		Front	Rear	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	1588	1481	1343	1106	0.973	0.748	0.605	0.226	-0.0103	22.0	22.0	1803	1757	1682	1581	1448	1276	1065	0.838	0.690	0.304	-0.0041	
2-A	do	do	do	15.9	17.1	1580	1468	1335	1156	0.957	0.742	0.498	0.223	-0.0098	20.8	22.0	1830	1770	1687	1578	1432	1284	1048	0.820	0.573	0.292	-0.025	
	do	do	Exposed cylinders	15.9	17.1	1585	1460	1320	1144	0.944	0.720	0.477	0.210	-0.0087	20.8	22.0	1819	1772	1697	1593	1453	1260	1043	0.808	0.561	0.280	-0.027	
	do	do	Exposed cylinders	15.9	17.1	1539	1443	1320	1160	0.969	0.754	0.517	0.258	-0.0043	20.8	22.0	1820	1755	1670	1557	1412	1238	1045	0.833	0.604	0.352	0.004	
Small	do	do	do	15.7	17.0	1516	1598	1254	1087	0.904	0.695	0.467	0.300	-0.0090	20.8	22.0	1748	1707	1635	1540	1406	1230	1020	0.800	0.567	0.310	0.046	
	do	N.A.C.A. hood	Ring 5°	15.8	16.8	1549	1440	1300	1128	0.928	0.714	0.483	0.210	-0.0090	21.2	22.0	1860	1806	1728	1625	1488	1315	1110	0.890	0.665	0.419	0.016	
	do	Ring 0°	do	15.8	16.8	1559	1449	1310	1140	0.951	0.760	0.621	0.268	-0.0043	21.2	22.0	1860	1806	1728	1625	1488	1315	1110	0.890	0.665	0.419	0.016	
3-A	Large	N.A.C.A. hood	do	15.9	17.8	1603	1491	1348	1170	0.985	0.747	0.500	0.200	-0.0100	20.9	22.7	1813	1765	1688	1585	1440	1251	1030	0.797	0.542	0.270	-0.0033	
4-A	do	do	do	15.9	17.0	1539	1425	1282	1116	0.929	0.720	0.490	0.220	-0.0088	21.2	22.0	1811	1754	1678	1569	1430	1250	1040	0.814	0.681	0.318	.0014	
1-B	do	do	Ring 0°	15.9	17.0	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	
2-B	do	do	Ring 5°	16.5	17.0	1578	1460	1312	1140	0.987	0.745	0.510	0.248	-0.0086	21.8	22.0	1835	1785	1706	1600	1488	1280	1060	0.847	0.612	0.320	0.006	
	do	do	Ring 0°	15.8	16.8	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	
	do	do	Ring 5°	15.8	16.8	1542	1342	1290	1128	0.935	0.724	0.490	0.228	-0.0050	21.2	22.0	1828	1781	1708	1601	1469	1284	1035	0.867	0.624	0.350	0.055	
	do	do	Ring 10°	15.8	16.8	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	
	do	do	Exposed cylinders	15.8	16.8	1564	1447	1305	1138	0.942	0.727	0.495	0.230	-0.0070	21.2	22.0	1805	1780	1672	1585	1430	1262	1068	0.843	0.600	0.338	0.052	
	do	do	Exposed cylinders	15.8	16.8	1564	1444	1303	1140	0.960	0.758	0.532	0.290	-0.0112	21.2	22.0	1800	1760	1698	1474	1311	1116	0.898	0.660	0.420	0.0176		
	do	do	Ring -5°	15.8	16.8	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do		
	do	do	Ring -10°	15.8	16.8	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do		
	do	do	Ring -15°	15.8	16.8	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do		
Small	do	do	Ring 10°	15.8	17.0	1501	1380	1260	1102	0.929	0.724	0.493	0.249	-0.0006	21.1	22.0	1766	1712	1633	1540	1408	1240	1050	0.846	0.620	0.370	0.0116	
	do	do	Ring 5°	15.8	17.0	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do		
	do	do	Ring 0°	15.8	17.0	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do		
	do	do	Ring -5°	15.8	17.0	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do		
	do	do	Ring -10°	15.8	17.0	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do		
	do	do	Ring 4°	15.8	17.0	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do		
	do	do	Ring 0°	15.8	17.0	1532	1438	1316	1166	0.971	0.762	0.537	0.288	-0.0110	21.1	22.0	1811	1755	1678	1572	1442	1280	1090	0.868	0.655	0.400	0.0141	
	do	do	Ring -5°	15.8	17.0	1546	1435	1295	1132	0.967	0.758	0.534	0.281	-0.0038	21.1	22.0	1811	1755	1678	1572	1442	1280	1090	0.868	0.655	0.400	0.0141	
	do	do	Ring -8°	15.8	17.0	1529	1422	1286	1124	0.959	0.740	0.511	0.246	-0.0040	21.1	22.0	1777	1718	1638	1535	1405	1243	1060	0.844	0.610	0.360	0.0100	
	do	do	Ring -10°	15.8	17.0	1532	1422	1285	1120	0.941	0.743	0.510	0.251	-0.0020	21.1	22.0	1779	1730	1659	1560	1429	1250	1060	0.855	0.645	0.390	0.0128	
	do	do	Ring 4°	15.8	17.0	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do			
	do	do	Ring -5°	15.8	17.0	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do			
	do	do	Ring 0°	15.8	17.0	1549	1450	1327	1170	0.995	0.793	0.574	0.320	-0.0040	21.1	22.0	1802	1755	1690	1598	1479	1324	1132	0.920	0.700	0.462	0.0119	
	do	do	Ring 10°	15.8	17.0	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do			
	do	do	Ring 0°	15.8	17.0	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do			
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2	1548	1440	1299	1127	0.991	0.719	0.494	0.223	-0.0070	20.8	22.0	1814	1744	1662	1551	1408	1202	1027	0.808	0.566	0.290	0.0033	
4-B	do	do	do	16.1	17.0	1563	1461	1327	1160	0.970	0.770	0.549	0.292	-0.0000	21.3	22.0	1830	1788	1702	1600	1462	1288	1090	0.880	0.689	0.408	0.0130	
1-C	do	do	do	do	15.8	17.0	1498	1388	1282	1093	0.919	0.726	0.519	0.289	-0.0024	21.0	22.0	1763	1705	1626	1522	1390	1220	1031	0.830	0.608	0.368	0.0123
Small	do	do	do	do	14.7	15.6	1428	1299	1151	0.994	0.822	0.645	0.451	0.226	-0.0035	21.2	22.0	1742	1698	1627	1534	1416	1262	1094	0.914	0.724	0.286	0.0123
	do	do	do	do	14.7	15.6	1418	1298	1157	1003	0.940	0.603	0.471	0.237	-0.0003	do	do	do	do	do	do	do	do	do	do	do		
2-C	Large	N.A.C.A. hood	do	15.8	17.0	1510	1400	1285	1107	0.929	0.740	0.535	0.310	-0.0060	21.0	22.0	1705	1703	1620	1510	1380	1220	1045	0.856	0.648	0.430	0.0185	
3-C	do	do	do	do	15.8	17.0	1506	1388	1260	1090	0.920	0.733	0.538	0.310	-0.0031	21.0	22.0	1740	1690	1617	1520	1398	1240	1058	0.881	0.658	0.430	0.0180

TABLE IV—Continued

THRUST COEFFICIENT,  $C_T = \frac{T - \Delta D}{\rho n_p^2 D^4}$ —Continued

ANGLE OF ATTACK=0°

Front propeller: Right hand no. 4412—4-foot diameter. Rear propeller: Left hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R		$\frac{V}{nD}$										Propeller pitch at 0.75 R		$\frac{V}{nD}$											
				Front	Rear	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	0.0	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
		Front	Rear																										
1-A	Large	N.A.C.A. hood	Ring 5°	°	°	17.0	17.0	0.1573	0.1475	0.1325	0.1152	0.0948	0.0720	0.0469	0.0169	-0.0163	22.0	22.0	0.1835	0.1780	0.1600	0.1585	0.1440	0.1258	0.1040	0.0817	0.0580	0.0205	-----
2-A	do	do	do	15.0	17.1	0.1576	0.1468	0.1324	0.1148	0.0941	0.0717	0.0467	0.0178	-0.0150	20.8	22.0	0.1825	0.1705	0.1631	0.1570	0.1426	0.1248	0.1033	0.0792	0.0530	0.0250	-0.0060		
2-A	do	do	Exposed cylinders	15.0	17.1	0.1561	0.1453	0.1318	0.1140	0.0931	0.0708	0.0460	0.0170	-0.0180	20.8	22.0	0.1830	0.1769	0.1630	0.1568	0.1414	0.1220	0.1010	0.0780	0.0524	0.0240	-0.0090		
2-A	do	do	Exposed cylinders	15.0	17.1	0.1575	0.1460	0.1317	0.1140	0.0939	0.0734	0.0494	0.0220	-0.0070	20.8	22.0	0.1845	0.1779	0.1688	0.1570	0.1420	0.1238	0.1041	0.0832	0.0590	0.0300	-0.0010		
2-A	Small	do	do	15.7	17.0	0.1523	0.1405	0.1258	0.1080	0.0886	0.0688	0.0449	0.0176	-0.0100	20.8	22.0	0.1744	0.1690	0.1610	0.1507	0.1370	0.1203	0.1004	0.0770	0.0521	0.0245	-----		
2-A	do	N.A.C.A. hood	Ring 5°	15.8	16.8	0.1575	0.1440	0.1280	0.1102	0.0909	0.0698	0.0470	0.0204	-0.0107	20.8	22.0	0.1744	0.1690	0.1610	0.1507	0.1370	0.1203	0.1004	0.0770	0.0521	0.0245	-----		
2-A	do	do	Ring 0°	15.8	16.8	0.1532	0.1405	0.1320	0.1160	0.0950	0.0748	0.0508	0.0231	-0.0042	21.2	22.0	0.1836	0.1797	0.1728	0.1632	0.1488	0.1310	0.1104	0.0880	0.0642	0.0382	.0098		
3-A	Large	N.A.C.A. hood	do	15.9	17.8	0.1603	0.1400	0.1345	0.1162	0.0956	0.0722	0.0478	0.0185	-0.0150	20.0	22.7	0.1888	0.1773	0.1687	0.1571	0.1420	0.1230	0.1022	0.0780	0.0507	0.0203	-0.0100		
4-A	do	do	do	15.9	17.0	0.1580	0.1435	0.1289	0.1118	0.0930	0.0714	0.0480	0.0207	-0.0098	21.2	22.0	0.1803	0.1742	0.1662	0.1552	0.1414	0.1230	0.1035	0.0810	0.0560	0.0280	-0.0020		
1-B	do	do	Ring 0°	15.0	17.0	0.1548	0.1428	0.1278	0.1102	0.0910	0.0697	0.0469	0.0190	-0.0123	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
1-B	do	do	Ring 5°	16.5	17.0	0.1599	0.1473	0.1381	0.1109	0.0986	0.0781	0.0548	0.0291	.0011	21.8	22.0	0.1838	0.1785	0.1712	0.1612	0.1481	0.1320	0.1120	0.0903	0.0668	0.0390	.0090		
2-B	do	do	Ring 0°	15.8	16.8	0.1533	0.1428	0.1294	0.1134	0.0956	0.0750	0.0532	0.0270	.0000	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring 5°	15.8	16.8	0.1560	0.1480	0.1317	0.1160	0.0959	0.0780	0.0530	0.0295	-0.0029	21.2	22.0	0.1826	0.1773	0.1700	0.1600	0.1470	0.1303	0.1107	0.0894	0.0660	0.0403	.0137		
2-B	do	do	Ring 10°	15.8	16.8	0.1588	0.1460	0.1328	0.1161	0.0970	0.0760	0.0541	0.0296	.0000	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Exposed cylinders	15.8	16.8	0.1553	0.1435	0.1302	0.1125	0.0940	0.0742	0.0528	0.0275	-0.0029	21.2	22.0	0.1820	0.1779	0.1710	0.1611	0.1473	0.1295	0.1068	0.0883	0.0647	0.0404	.0156		
2-B	do	do	do	15.8	16.8	0.1553	0.1443	0.1305	0.1144	0.0968	0.0770	0.0558	0.0316	.0038	21.2	22.0	0.1825	0.1778	0.1708	0.1613	0.1488	0.1328	0.1145	0.0947	0.0723	0.0474	.0207		
2-B	do	do	Ring -5°	15.8	16.8	0.1562	0.1454	0.1317	0.1150	0.0962	0.0760	0.0550	0.0323	.0060	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring -10°	15.8	16.8	0.1580	0.1439	0.1298	0.1134	0.0950	0.0752	0.0530	0.0393	.0017	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring -15°	15.8	16.8	0.1560	0.1449	0.1310	0.1147	0.0970	0.0772	0.0550	0.0310	.0038	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	Small	do	do	16.8	17.0	0.1529	0.1418	0.1280	0.1122	0.0949	0.0740	0.0538	0.0293	.0028	21.1	22.0	0.1702	0.1741	0.1668	0.1568	0.1438	0.1267	0.1080	0.0877	0.0655	0.0410	.0166		
2-B	do	do	Ring 10°	16.8	17.0	0.1577	0.1450	0.1318	0.1162	0.0986	0.0807	0.0589	0.0340	.0073	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring 5°	15.8	17.0	0.1558	0.1435	0.1305	0.1100	0.0906	0.0804	0.0580	0.0328	.0060	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring 0°	15.8	17.0	0.1570	0.1458	0.1318	0.1158	0.0977	0.0781	0.0570	0.0339	.0070	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring -5°	15.8	17.0	0.1545	0.1440	0.1309	0.1144	0.0945	0.0770	0.0555	0.0320	.0057	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring -10°	15.8	17.0	0.1519	0.1406	0.1270	0.1111	0.0940	0.0760	0.0542	0.0303	.0060	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring 4°	15.8	17.0	0.1530	0.1430	0.1308	0.1171	0.0900	0.0809	0.0567	0.0384	.0100	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring 0°	15.8	17.0	0.1594	0.1435	0.1304	0.1146	0.0968	0.0782	0.0578	0.0384	.0081	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring -5°	15.8	17.0	0.1572	0.1428	0.1305	0.1127	0.0946	0.0746	0.0520	0.0275	.0005	21.1	22.0	0.1765	0.1760	0.1679	0.1582	0.1440	0.1268	0.1080	0.0880	0.0652	0.0409	.0134		
2-B	do	do	Ring -8°	15.8	17.0	0.1528	0.1428	0.1288	0.1127	0.0946	0.0746	0.0520	0.0275	.0005	21.1	22.0	0.1780	0.1727	0.1652	0.1548	0.1411	0.1244	0.1048	0.0880	0.0638	0.0458	.0120		
2-B	do	do	Ring -10°	15.8	17.0	0.1535	0.1420	0.1284	0.1128	0.0944	0.0751	0.0542	0.0304	.0043	21.1	22.0	0.1743	0.1711	0.1676	0.1578	0.1449	0.1290	0.1102	0.0900	0.0681	0.0450	.0200		
2-B	do	do	Ring 4°	15.8	17.0	0.1584	0.1471	0.1344	0.1194	0.0981	0.0764	0.0632	0.0397	.0160	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring -5°	15.8	17.0	0.1545	0.1450	0.1321	0.1165	0.0980	0.0778	0.0650	0.0314	.0047	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring 0°	15.8	17.0	0.1562	0.1460	0.1335	0.1182	0.0999	0.0814	0.0693	0.0369	.0100	21.1	22.0	0.1803	0.1762	0.1696	0.1610	0.1490	0.1340	0.1165	0.0970	0.0754	0.0568	.0230		
2-B	do	do	Ring -10°	15.8	17.0	0.1562	0.1465	0.1338	0.1180	0.0999	0.0808	0.0686	0.0383	.0100	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
2-B	do	do	Ring 0°	15.8	17.0	0.1536	0.1432	0.1307	0.1163	0.0979	0.0794	0.0686	0.0347	.0080	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----		
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2	0.1540	0.1428	0.1290	0.1126	0.0945	0.0760	0.0524	0.0264	-0.0040	20.8	22.0	0.1820	0.1764	0.1683	0.1578	0.1433	0.1246	0.1047	0.0830	0.0600	0.0344	.0062		
4-B	do	do	do	16.1	17.0	0.1559	0.1443	0.1310	0.1152	0.0978	0.0770	0.0554	0.0300	.0020	21.3	22.0	0.1798	0.1748	0.1675	0.1580	0.1452	0.1281	0.1078	0.0864	0.0638	0.0394	.0120		
1-C	do	do	do	15.8	17.0	0.1497	0.1387	0.1260	0.1085	0.0907	0.0710	0.0505	0.0278	.0040	21.0	22.0	0.1739	0.1675	0.1590	0.1482	0.1353	0.1193	0.1016	0.0					

TABLE IV—Continued

$$\text{THRUST COEFFICIENT, } C_T = \frac{T - \Delta D}{\rho n p^2 D^4} \text{—Continued}$$

ANGLE OF ATTACK=5°

Front propeller: Right hand no. 4412—4 foot diameter. Rear propeller: Left hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R	$\frac{V}{nD}$										Propeller pitch at 0.75 R		$\frac{V}{nD}$										
					Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
		Front	Rear																								
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	0.1690	0.1480	0.1332	0.1144	0.0919	0.0680	0.0420	0.0120	-0.0210	22.0	22.0	0.1803	0.1731	0.1040	0.1518	0.1368	0.1190	0.0980	0.0780	0.0480	0.0160	.....
2-A	do	do	do	15.9	17.1	0.1680	0.1460	0.1301	0.1110	0.0903	0.0729	0.0418	0.0132	-0.0155	20.8	22.0	0.1848	0.1771	0.1670	0.1640	0.1380	0.1188	0.0978	0.0740	0.0470	0.0183	-0.0115
	do	Exposed cylinders	do	15.9	17.1	0.1685	0.1440	0.1284	0.1100	0.0899	0.0679	0.0429	0.0130	-0.0204	20.8	22.0	0.1846	0.1771	0.1672	0.1643	0.1380	0.1190	0.0978	0.0748	0.0487	0.0200	-0.0099
	do	Exposed cylinders	do	15.9	17.1	0.1640	0.1420	0.1284	0.1113	0.0916	0.0700	0.0463	0.0100	-0.0120	20.8	22.0	0.1824	0.1745	0.1642	0.1610	0.1354	0.1177	0.0986	0.0778	0.0533	0.0260	-0.0057
	Small	do	do	15.7	17.0	0.1498	0.1381	0.1285	0.1059	0.0863	0.0648	0.0400	0.0120	-0.0103	20.8	22.0	0.1780	0.1710	0.1615	0.1494	0.1343	0.1160	0.0987	0.0736	0.0480	0.0208	-0.0065
	do	N.A.C.A. hood	Ring 5°	15.8	16.8	0.1650	0.1427	0.1274	0.1090	0.0903	0.0607	0.0471	0.0214	-0.0090	21.2	22.0	0.1865	0.1789	0.1698	0.1682	0.1440	0.1272	0.1090	0.0882	0.0638	0.0350	0.0060
	do	Ring 0°	do	15.8	16.8	0.1682	0.1442	0.1295	0.1125	0.0939	0.0730	0.0488	0.0210	-0.0080	21.2	22.0	0.1865	0.1789	0.1698	0.1682	0.1440	0.1272	0.1090	0.0882	0.0638	0.0350	0.0060
3-A	Large	N.A.C.A. hood	do	15.9	17.8	0.1600	0.1440	0.1272	0.1090	0.0900	0.0680	0.0428	0.0130	-0.0185	20.9	22.7	0.1845	0.1778	0.1677	0.1649	0.1388	0.1201	0.0990	0.0755	0.0488	0.0100	-0.012
4-A	do	do	do	15.9	17.0	0.1532	0.1420	0.1277	0.1100	0.0900	0.0684	0.0451	0.0180	-0.0120	21.2	22.0	0.1818	0.1751	0.1604	0.1549	0.1400	0.1214	0.1008	0.0781	0.0538	0.0200	-0.003
1-B	do	do	Ring 5°	16.5	17.0	0.1588	0.1487	0.1354	0.1190	0.1004	0.0705	0.0500	0.0432	0.0063	21.8	22.0	0.1846	0.1802	0.1727	0.1629	0.1497	0.1322	0.1143	0.0940	0.0714	0.0459	0.0183
2-B	do	do	Ring 0°	15.8	16.8	0.1688	0.1460	0.1320	0.1159	0.0970	0.0704	0.0548	0.0315	0.0050	21.2	22.0	0.1840	0.1791	0.1717	0.1620	0.1493	0.1333	0.1145	0.0939	0.0719	0.0468	0.0247
	do	do	Ring 5°	15.8	16.8	0.1688	0.1460	0.1320	0.1159	0.0970	0.0704	0.0548	0.0315	0.0050	21.2	22.0	0.1840	0.1791	0.1717	0.1620	0.1493	0.1333	0.1145	0.0939	0.0719	0.0468	0.0247
	do	do	Ring 10°	15.8	16.8	0.1688	0.1460	0.1320	0.1159	0.0970	0.0704	0.0548	0.0315	0.0050	21.2	22.0	0.1810	0.1758	0.1681	0.1680	0.1457	0.1300	0.1120	0.0920	0.0700	0.0468	0.0247
	do	do	Exposed cylinders	15.8	16.8	0.1642	0.1437	0.1300	0.1142	0.0970	0.0780	0.0567	0.0320	0.0053	21.2	22.0	0.1810	0.1758	0.1681	0.1680	0.1457	0.1300	0.1120	0.0920	0.0700	0.0468	0.0247
	do	do	Ring -5°	15.8	16.8	0.1559	0.1448	0.1314	0.1155	0.0970	0.0784	0.0577	0.0351	0.0100	21.2	22.0	0.1827	0.1780	0.1710	0.1615	0.1487	0.1327	0.1146	0.0951	0.0744	0.0519	0.0280
	do	do	Ring -10°	15.8	16.8	0.1559	0.1448	0.1314	0.1155	0.0970	0.0784	0.0577	0.0351	0.0100	21.2	22.0	0.1827	0.1780	0.1710	0.1615	0.1487	0.1327	0.1146	0.0951	0.0744	0.0519	0.0280
	do	do	Ring -15°	15.8	16.8	0.1559	0.1448	0.1314	0.1155	0.0970	0.0784	0.0577	0.0351	0.0100	21.2	22.0	0.1827	0.1780	0.1710	0.1615	0.1487	0.1327	0.1146	0.0951	0.0744	0.0519	0.0280
	do	do	Ring 10°	15.8	17.0	0.1513	0.1410	0.1280	0.1121	0.0948	0.0767	0.0580	0.0328	0.0079	21.1	22.0	0.1763	0.1718	0.1649	0.1655	0.1438	0.1281	0.1100	0.0960	0.0680	0.0456	0.0216
	do	do	Ring 5°	15.8	17.0	0.1513	0.1410	0.1280	0.1121	0.0948	0.0767	0.0580	0.0328	0.0079	21.1	22.0	0.1763	0.1718	0.1649	0.1655	0.1438	0.1281	0.1100	0.0960	0.0680	0.0456	0.0216
	do	do	Ring 0°	15.8	17.0	0.1513	0.1410	0.1280	0.1121	0.0948	0.0767	0.0580	0.0328	0.0079	21.1	22.0	0.1763	0.1718	0.1649	0.1655	0.1438	0.1281	0.1100	0.0960	0.0680	0.0456	0.0216
	do	do	Ring -5°	15.8	17.0	0.1513	0.1410	0.1280	0.1121	0.0948	0.0767	0.0580	0.0328	0.0079	21.1	22.0	0.1763	0.1718	0.1649	0.1655	0.1438	0.1281	0.1100	0.0960	0.0680	0.0456	0.0216
	do	do	Ring -10°	15.8	17.0	0.1513	0.1410	0.1280	0.1121	0.0948	0.0767	0.0580	0.0328	0.0079	21.1	22.0	0.1763	0.1718	0.1649	0.1655	0.1438	0.1281	0.1100	0.0960	0.0680	0.0456	0.0216
	do	do	Ring 4°	15.8	17.0	0.1519	0.1420	0.1300	0.1160	0.0978	0.0793	0.0589	0.0371	0.0130	21.1	22.0	0.1830	0.1770	0.1680	0.1682	0.1450	0.1289	0.1105	0.0910	0.0690	0.0463	0.0230
	do	do	Ring -8°	15.8	17.0	0.1513	0.1410	0.1280	0.1121	0.0948	0.0767	0.0560	0.0346	0.0121	21.1	22.0	0.1830	0.1770	0.1680	0.1682	0.1450	0.1289	0.1105	0.0910	0.0690	0.0463	0.0230
	do	do	Ring -10°	15.8	17.0	0.1513	0.1410	0.1280	0.1121	0.0948	0.0767	0.0560	0.0346	0.0121	21.1	22.0	0.1830	0.1770	0.1680	0.1682	0.1450	0.1289	0.1105	0.0910	0.0690	0.0463	0.0230
	do	do	Ring 4°	15.8	17.0	0.1524	0.1402	0.1273	0.1118	0.0947	0.0761	0.0558	0.0318	0.0050	21.1	22.0	0.1806	0.1750	0.1670	0.1510	0.1430	0.1276	0.1099	0.0906	0.0695	0.0460	0.0219
	do	do	Ring -5°	15.8	17.0	0.1528	0.1402	0.1273	0.1118	0.0947	0.0761	0.0558	0.0318	0.0050	21.1	22.0	0.1806	0.1750	0.1670	0.1510	0.1430	0.1276	0.1099	0.0906	0.0695	0.0460	0.0219
	do	do	Ring 0°	15.8	17.0	0.1528	0.1402	0.1273	0.1118	0.0947	0.0761	0.0558	0.0318	0.0050	21.1	22.0	0.1806	0.1750	0.1670	0.1510	0.1430	0.1276	0.1099	0.0906	0.0695	0.0460	0.0219
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2	0.1532	0.1430	0.1300	0.1130	0.0950	0.0740	0.0545	0.0322	0.0096	20.8	22.0	0.1817	0.1734	0.1646	0.1642	0.1421	0.1265	0.1074	0.0873	0.0638	0.0426	0.0183
4-B	do	do	do	16.1	17.0	0.1570	0.1407	0.1331	0.1160	0.0981	0.0775	0.0550	0.0310	0.0049	21.3	22.0	0.1837	0.1778	0.1702	0.1698	0.1463	0.1299	0.1108	0.0902	0.0676	0.0420	0.0160
1-C	do	do	do	15.8	17.0	0.1490	0.1305	0.1218	0.1042	0.0855	0.0670	0.0475	0.0260	0.0066	21.0	22.0	0.1720	0.1650	0.1558	0.1440	0.1301	0.1145	0.0970	0.0794	0.0581	0.0360	0.0130
	do	do	do	14.7	16.6	0.1402	0.1267	0.1113	0.0950	0.0774	0.0686	0.0417	0.0217	0.0010	21.2	22.0	0.1702	0.1636	0.1590	0.1473	0.1343	0.1196	0.1040	0.0871	0.0687	0.0460	0.0300
2-O	Large	N.A.C.A. hood	do	15.8	17.0	0.1500	0.1382	0.1242	0.1080	0.0904	0.0712	0.0518	0.0207	0.0065	21.0	22.0	0.1700	0.1605	0.1607	0.1490	0.1350	0.1185	0.1000	0.0802	0.0684	0.0460	0.0180
3-O	do	do	do	15.8	17.0	0.1479	0.1302	0.1225	0.1065	0.0890	0.0700	0.0511	0.0300	0.0060	21.0	22.0	0.1724	0.1602	0.1582	0.1475	0.1348	0.1198	0.1019	0.0830	0.0630	0.0421	0.0200

TABLE V

$$\text{FRONT PROPELLER POWER COEFFICIENT, } C_{P_f} = \frac{P_f}{\rho n_f^3 D^3}$$

ANGLE OF ATTACK=-5°

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R	$\frac{V}{nD}$									Propeller pitch at 0.75 R	$\frac{V}{nD}$												
					0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1		
		Front	Rear		Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9		
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	0.0413	0.0416	0.0410	0.0392	0.0363	0.0314	0.0243	0.0182	0.0038	22.0	22.0	0.0628	0.0618	0.0606	0.0590	0.0570	0.0540	0.0493	0.0420	0.0334	0.0210	0.0038
2-A	do	do	do	15.9	17.1	0.0380	0.0385	0.0385	0.0370	0.0342	0.0300	0.0240	0.0160	0.0050	20.8	22.0	0.0580	0.0578	0.0570	0.0555	0.0537	0.0502	0.0458	0.0398	0.0320	0.0210	0.0085
	do	do	Exposed cylinders	15.9	17.1	0.0380	0.0380	0.0380	0.0370	0.0338	0.0293	0.0239	0.0164	0.0056	20.8	22.0	0.0578	0.0576	0.0570	0.0558	0.0540	0.0506	0.0460	0.0395	0.0315	0.0210	0.0100
	do	do	do	15.9	17.1	0.0385	0.0384	0.0380	0.0368	0.0335	0.0295	0.0235	0.0157	0.0053	20.8	22.0	0.0580	0.0574	0.0565	0.0553	0.0534	0.0500	0.0407	0.0410	0.0330	0.0238	0.0115
	Small	do	do	15.7	17.0	0.0404	0.0398	0.0371	0.0345	0.0312	0.0208	0.0144	0.0058	20.8	22.0	0.0580	0.0572	0.0560	0.0544	0.0524	0.0498	0.0460	0.0387	0.0301	0.0195	0.0060	
	do	N.A.C.A. hood	Ring 5°	15.8	16.8	0.0384	0.0363	0.0362	0.0358	0.0362	0.0286	0.0244	0.0140	0.0050	21.2	22.0	0.0580	0.0580	0.0580	0.0573	0.0558	0.0521	0.0477	0.0420	0.0340	0.0240	0.0113
	do	Ring 0°	do	15.8	16.8	0.0368	0.0360	0.0366	0.0368	0.0328	0.0286	0.0223	0.0144	0.0038	21.2	22.0	0.0580	0.0580	0.0580	0.0573	0.0558	0.0521	0.0477	0.0420	0.0340	0.0240	0.0113
3-A	Large	N.A.C.A. hood	do	15.9	17.8	0.0370	0.0370	0.0370	0.0366	0.0340	0.0298	0.0238	0.0160	0.0056	20.8	22.7	0.0550	0.0560	0.0550	0.0540	0.0510	0.0470	0.0410	0.0330	0.0230	0.0105	
4-A	do	do	do	15.9	17.0	0.0365	0.0364	0.0362	0.0360	0.0340	0.0298	0.0238	0.0155	0.0055	21.2	22.0	0.0580	0.0578	0.0574	0.0560	0.0547	0.0518	0.0480	0.0428	0.0348	0.0240	0.0110
1-B	do	do	Ring 5°	16.8	17.0	0.0390	0.0388	0.0383	0.0368	0.0388	0.0288	0.0220	0.0125	0.0010	21.8	22.0	0.0622	0.0610	0.0598	0.0580	0.0560	0.0530	0.0482	0.0410	0.0314	0.0190	0.0040
2-B	do	do	Ring 0°	15.8	16.8	0.0365	0.0368	0.0365	0.0362	0.0328	0.0282	0.0221	0.0140	0.0040	21.2	22.0	0.0584	0.0578	0.0572	0.0564	0.0551	0.0520	0.0484	0.0420	0.0335	0.0225	0.0095
	do	do	Ring 5°	15.8	16.8	0.0368	0.0368	0.0368	0.0368	0.0328	0.0288	0.0228	0.0148	0.0048	21.2	22.0	0.0573	0.0568	0.0562	0.0552	0.0538	0.0518	0.0470	0.0418	0.0330	0.0228	0.0107
	do	do	Ring 10°	15.8	16.8	0.0368	0.0368	0.0368	0.0368	0.0328	0.0288	0.0228	0.0163	0.0056	21.2	22.0	0.0580	0.0574	0.0571	0.0564	0.0558	0.0525	0.0482	0.0422	0.0344	0.0245	0.0130
	do	do	Exposed cylinders	15.8	16.8	0.0367	0.0367	0.0367	0.0365	0.0328	0.0288	0.0228	0.0163	0.0056	21.2	22.0	0.0580	0.0574	0.0571	0.0564	0.0558	0.0525	0.0482	0.0422	0.0344	0.0245	0.0130
	do	do	Ring -8°	15.8	16.8	do	21.2	22.0	0.0580	0.0574	0.0571	0.0564	0.0558	0.0525	0.0482	0.0422	0.0344	0.0245	0.0130								
	do	do	Ring -10°	15.8	16.8	do	21.2	22.0	0.0580	0.0574	0.0571	0.0564	0.0558	0.0525	0.0482	0.0422	0.0344	0.0245	0.0130								
	do	do	Ring -15°	15.8	16.8	do	21.2	22.0	0.0580	0.0574	0.0571	0.0564	0.0558	0.0525	0.0482	0.0422	0.0344	0.0245	0.0130								
	do	do	Ring 10°	15.8	17.0	0.0370	0.0370	0.0366	0.0361	0.0321	0.0278	0.0218	0.0135	0.0035	21.1	22.0	0.0608	0.0594	0.0579	0.0558	0.0537	0.0504	0.0459	0.0398	0.0318	0.0210	0.0088
	do	do	Ring 8°	15.8	17.0	0.0370	0.0370	0.0366	0.0361	0.0321	0.0278	0.0218	0.0135	0.0035	21.1	22.0	0.0608	0.0594	0.0579	0.0558	0.0537	0.0504	0.0459	0.0398	0.0318	0.0210	0.0088
	do	do	Ring 0°	15.8	17.0	0.0370	0.0370	0.0366	0.0361	0.0321	0.0278	0.0218	0.0135	0.0035	21.1	22.0	0.0608	0.0594	0.0579	0.0558	0.0537	0.0504	0.0459	0.0398	0.0318	0.0210	0.0088
	do	do	Ring -5°	15.8	17.0	0.0370	0.0370	0.0366	0.0361	0.0321	0.0278	0.0218	0.0135	0.0035	21.1	22.0	0.0608	0.0594	0.0579	0.0558	0.0537	0.0504	0.0459	0.0398	0.0318	0.0210	0.0088
	do	do	Ring -8°	15.8	17.0	0.0370	0.0370	0.0366	0.0361	0.0321	0.0278	0.0218	0.0135	0.0035	21.1	22.0	0.0608	0.0594	0.0579	0.0558	0.0537	0.0504	0.0459	0.0398	0.0318	0.0210	0.0088
	do	do	Ring -10°	15.8	17.0	0.0370	0.0370	0.0366	0.0361	0.0321	0.0278	0.0218	0.0135	0.0035	21.1	22.0	0.0608	0.0594	0.0579	0.0558	0.0537	0.0504	0.0459	0.0398	0.0318	0.0210	0.0088
	do	do	Ring 4°	15.8	17.0	0.0370	0.0370	0.0366	0.0361	0.0321	0.0278	0.0218	0.0135	0.0035	21.1	22.0	0.0608	0.0594	0.0579	0.0558	0.0537	0.0504	0.0459	0.0398	0.0318	0.0210	0.0088
	do	do	Ring 0°	15.8	17.0	0.0374	0.0374	0.0370	0.0366	0.0327	0.0280	0.0218	0.0140	0.0040	21.1	22.0	0.0600	0.0595	0.0580	0.0563	0.0540	0.0510	0.0468	0.0408	0.0330	0.0220	0.0090
	do	do	Ring -6°	15.8	17.0	0.0374	0.0374	0.0370	0.0366	0.0327	0.0280	0.0218	0.0140	0.0040	21.1	22.0	0.0600	0.0595	0.0580	0.0563	0.0540	0.0510	0.0468	0.0408	0.0330	0.0220	0.0090
	do	do	Ring -8°	15.8	17.0	0.0374	0.0374	0.0372	0.0364	0.0322	0.0278	0.0216	0.0138	0.0020	21.1	22.0	0.0600	0.0590	0.0574	0.0558	0.0538	0.0510	0.0467	0.0402	0.0316	0.0208	0.0078
	do	do	Ring -10°	15.8	17.0	0.0370	0.0370	0.0366	0.0363	0.0325	0.0280	0.0218	0.0137	0.0035	21.1	22.0	0.0600	0.0590	0.0574	0.0558	0.0538	0.0510	0.0467	0.0402	0.0316	0.0230	0.0105
	do	do	Ring 4°	15.8	17.0	0.0370	0.0370	0.0366	0.0361	0.0321	0.0278	0.0218	0.0135	0.0035	21.1	22.0	0.0600	0.0590	0.0575	0.0558	0.0538	0.0508	0.0458	0.0398	0.0318	0.0210	0.0088
	do	do	Ring 0°	15.8	17.0	0.0370	0.0370	0.0365	0.0362	0.0320	0.0279	0.0219	0.0140	0.0040	21.1	22.0	0.0598	0.0590	0.0575	0.0558	0.0538	0.0508	0.0458	0.0398	0.0318	0.0210	0.0088
	do	do	Ring 10°	15.8	17.0	0.0370	0.0370	0.0365	0.0362	0.0320	0.0279	0.0219	0.0140	0.0040	21.1	22.0	0.0598	0.0590	0.0575	0.0558	0.0538	0.0508	0.0458	0.0398	0.0318	0.0210	0.0088
	do	do	Ring 0°	15.8	17.0	0.0370	0.0370	0.0365	0.0362	0.0320	0.0279	0.0219	0.0140	0.0040	21.1	22.0	0.0598	0.0590	0.0575	0.0558	0.0538	0.0508	0.0458	0.0398	0.0318	0.0210	0.0088
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2	0.0363	0.0363	0.0360	0.0352	0.0324	0.0278	0.0220	0.0145	0.0045	20.8	22.0	0.0540	0.0540	0.0540	0.0540	0.0527	0.0503	0.0468	0.0398	0.0318	0.0206	0.0080
4-B	do	do	do	16.1	17.0	0.0382	0.0381	0.0380	0.0375	0.0346	0.0304	0.0245	0.0163	0.0070	21.3	22.0	0.0588	0.0586	0.0582	0.0572	0.0558	0.0535	0.0494	0.0			

TABLE V—Continued  
 FRONT PROPELLER POWER COEFFICIENT,  $C_{P_F} = \frac{P_F}{\rho n_F^3 D^3}$ —Continued  
 ANGLE OF ATTACK=0°

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.	V $\frac{nD}{nD}$										Propeller pitch at 0.75 R.	V $\frac{nD}{nD}$												
					Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1
		Front	Rear	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	0.0408	0.0408	0.0400	0.0383	0.0353	0.0300	0.0222	0.0120	0.0000	22.0	22.0	0.0610	0.0610	0.0602	0.0585	0.0567	0.0520	0.0476	0.0407	0.0303	0.0170	0.0000	
2-A	do	do	do	15.9	17.1	0.0376	0.0380	0.0380	0.0365	0.0333	0.0288	0.0222	0.0188	0.0035	20.8	22.0	0.0588	0.0578	0.0568	0.0554	0.0535	0.0500	0.0451	0.0380	0.0299	0.0180	0.0050	
	do	do	Exposed cylinders	15.9	17.1	0.0382	0.0390	0.0376	0.0365	0.0332	0.0285	0.0223	0.0140	0.0035	20.6	22.0	0.0582	0.0578	0.0568	0.0556	0.0535	0.0502	0.0458	0.0390	0.0305	0.0184	0.0040	
	Small	do	do	15.7	17.0	0.0368	0.0367	0.0360	0.0342	0.0308	0.0268	0.0197	0.0112	0.0010	20.8	22.0	0.0578	0.0572	0.0568	0.0560	0.0530	0.0500	0.0469	0.0396	0.0305	0.0190	0.0060	
	do	N.A.C.A. hood	Ring 5°	15.8	16.8	0.0376	0.0373	0.0370	0.0368	0.0325	0.0278	0.0215	0.0130	0.0025	21.2	22.0	0.0572	0.0569	0.0568	0.0540	0.0520	0.0488	0.0438	0.0368	0.0278	0.0168	0.0040	
	do	Ring 0°	do	15.8	16.8	0.0368	0.0368	0.0368	0.0358	0.0325	0.0278	0.0215	0.0132	0.0020	21.2	22.0	0.0592	0.0586	0.0583	0.0576	0.0556	0.0522	0.0470	0.0402	0.0310	0.0205	0.0070	
3-A	Large	N.A.C.A. hood	do	15.9	17.8	0.0372	0.0372	0.0372	0.0368	0.0338	0.0294	0.0230	0.0145	0.0035	20.9	22.7	0.0546	0.0546	0.0546	0.0544	0.0532	0.0505	0.0465	0.0400	0.0315	0.0218	0.0075	
4-A	do	do	do	15.9	17.0	0.0389	0.0368	0.0365	0.0357	0.0330	0.0289	0.0225	0.0142	0.0030	21.2	22.0	0.0598	0.0590	0.0580	0.0568	0.0546	0.0518	0.0476	0.0413	0.0330	0.0220	0.0082	
1-B	do	do	Ring 5°	10.5	17.0	0.0390	0.0390	0.0387	0.0370	0.0348	0.0302	0.0243	0.0160	0.0000	21.8	22.0	0.0619	0.0610	0.0600	0.0585	0.0565	0.0537	0.0498	0.0436	0.0350	0.0240	0.0100	
2-B	do	do	Ring 0°	15.8	16.8	0.0370	0.0370	0.0369	0.0359	0.0335	0.0298	0.0239	0.0167	0.0078	21.2	22.0	0.0584	0.0583	0.0578	0.0568	0.0552	0.0528	0.0490	0.0436	0.0357	0.0254	0.0130	
	do	do	Ring 5°	15.8	16.8	0.0363	0.0363	0.0363	0.0355	0.0330	0.0289	0.0235	0.0163	0.0068	21.2	22.0	0.0584	0.0583	0.0578	0.0568	0.0552	0.0528	0.0490	0.0436	0.0357	0.0254	0.0130	
	do	do	Ring 10°	15.8	16.8	0.0363	0.0363	0.0363	0.0358	0.0330	0.0290	0.0238	0.0165	0.0068	21.2	22.0	0.0590	0.0588	0.0588	0.0572	0.0561	0.0528	0.0488	0.0433	0.0362	0.0273	0.0165	
	do	do	Exposed cylinders	15.8	16.8	0.0368	0.0368	0.0368	0.0358	0.0330	0.0290	0.0235	0.0162	0.0072	21.2	22.0	0.0604	0.0590	0.0582	0.0570	0.0552	0.0530	0.0492	0.0438	0.0368	0.0277	0.0170	
	do	do	Ring -5°	15.8	16.8	0.0375	0.0370	0.0362	0.0353	0.0325	0.0275	0.0215	0.0145	0.0077	21.2	22.0	0.0583	0.0575	0.0568	0.0555	0.0537	0.0515	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring -10°	15.8	16.8	0.0370	0.0370	0.0367	0.0357	0.0333	0.0294	0.0240	0.0165	0.0075	21.2	22.0	0.0583	0.0575	0.0568	0.0555	0.0537	0.0515	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring -15°	15.8	16.8	0.0370	0.0370	0.0367	0.0356	0.0330	0.0295	0.0248	0.0160	0.0075	21.2	22.0	0.0583	0.0575	0.0568	0.0555	0.0537	0.0515	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring 10°	15.8	17.0	0.0370	0.0370	0.0368	0.0355	0.0330	0.0286	0.0230	0.0164	0.0068	21.1	22.0	0.0576	0.0574	0.0568	0.0553	0.0541	0.0514	0.0470	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring 5°	15.8	17.0	0.0367	0.0367	0.0365	0.0355	0.0330	0.0289	0.0235	0.0162	0.0068	21.1	22.0	0.0576	0.0574	0.0568	0.0553	0.0541	0.0514	0.0470	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring 0°	15.8	17.0	0.0367	0.0367	0.0367	0.0356	0.0330	0.0290	0.0236	0.0162	0.0068	21.1	22.0	0.0576	0.0574	0.0568	0.0553	0.0541	0.0514	0.0470	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring -5°	15.8	17.0	0.0368	0.0368	0.0368	0.0356	0.0332	0.0291	0.0232	0.0160	0.0070	21.1	22.0	0.0583	0.0581	0.0575	0.0568	0.0555	0.0533	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring -10°	15.8	17.0	0.0365	0.0360	0.0360	0.0350	0.0327	0.0280	0.0230	0.0163	0.0075	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Exposed cylinders	15.8	17.0	0.0380	0.0380	0.0375	0.0358	0.0330	0.0280	0.0230	0.0163	0.0070	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring 4°	15.8	17.0	0.0364	0.0364	0.0364	0.0358	0.0330	0.0280	0.0230	0.0164	0.0068	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring 0°	15.8	17.0	0.0364	0.0364	0.0364	0.0354	0.0320	0.0285	0.0230	0.0164	0.0068	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring -5°	15.8	17.0	0.0373	0.0373	0.0373	0.0360	0.0330	0.0283	0.0236	0.0163	0.0070	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring -8°	15.8	17.0	0.0382	0.0383	0.0373	0.0358	0.0330	0.0288	0.0230	0.0160	0.0068	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring -10°	15.8	17.0	0.0370	0.0370	0.0370	0.0350	0.0327	0.0287	0.0230	0.0165	0.0070	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring 4°	15.8	17.0	0.0372	0.0370	0.0364	0.0360	0.0330	0.0287	0.0230	0.0162	0.0078	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring 0°	15.8	17.0	0.0368	0.0368	0.0368	0.0355	0.0332	0.0285	0.0238	0.0162	0.0065	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring 10°	15.8	17.0	0.0370	0.0370	0.0370	0.0350	0.0328	0.0286	0.0230	0.0165	0.0072	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
	do	do	Ring 0°	15.8	17.0	0.0369	0.0369	0.0368	0.0356	0.0328	0.0286	0.0230	0.0160	0.0060	21.1	22.0	0.0583	0.0575	0.0568	0.0555	0.0543	0.0521	0.0476	0.0413	0.0340	0.0230	0.0125	
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2	0.0359	0.0358	0.0360	0.0351	0.0327	0.0285	0.0228	0.0160	0.0057	20.8	22.0	0.0540	0.0540	0.0540	0.0540	0.0539	0.0528	0.0503	0.0402	0.0405	0.0322	0.0230	0.0120
4-B	do	do	do	16.1	17.0	0.0380	0.0380	0.0380	0.0370	0.0350	0.0312	0.0283	0.0175	0.0060	21.3	22.0	0.0605	0.0600	0.0600	0.0600	0.0578	0.0555	0.0528	0.0488	0.0430	0.0355	0.0250	0.0130
1-C	do	do	do	15.8	17.0	0.0369	0.0368	0.0367	0.0364	0.0338	0.0302	0.0250	0.0172	0.0076	21.0	22.0	0.0565	0.0565	0.0565	0.0565	0.0568	0.0547</td						

TABLE V—Continued

TABLE V—Continued  
FRONT PROPELLER POWER COEFFICIENT,  $C_{P_f} = \frac{P_f}{\rho n_p^3 D^5}$ —Continued  
ANGLE OF ATTACK = 5°

**Front propeller:** Right-hand no. 4412—4-foot diameter. **Rear propeller:** Left-hand no. 4412—4-foot diameter.

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.		$\frac{V}{nD}$							Propeller pitch at 0.75 R.		$\frac{V}{nD}$													
		Front	Rear	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	0.0112	0.0412	0.0412	0.0406	0.0388	0.0345	0.0275	0.0202	0.0090	22.0	22.0	0.0620	0.0620	0.0007	0.0580	0.0557	0.0514	0.0460	0.0380	0.0200	0.0100		
2-A	do	do	do	15.9	17.1	0.0375	0.0375	0.0373	0.0365	0.0333	0.0275	0.0206	0.0118	0.0000	20.8	22.0	0.0660	0.0550	0.0588	0.0550	0.0532	0.0495	0.0440	0.0370	0.0277	0.0148		
	do	Exposed cylinders	do	15.9	17.1	0.0375	0.0375	0.0373	0.0369	0.0362	0.0334	0.0284	0.0217	0.0123	0.0000	20.8	22.0	0.0668	0.0560	0.0558	0.0555	0.0536	0.0495	0.0440	0.0370	0.0275	0.0155	0.0000
	Small	do	do	15.9	17.1	0.0375	0.0373	0.0369	0.0362	0.0340	0.0302	0.0250	0.0180	0.0092	20.8	22.0	0.0680	0.0575	0.0502	0.0643	0.0515	0.0478	0.0428	0.0356	0.0240	0.0120		
	do	N.A.C.A. hood	Ring 5°	15.8	16.8	0.0370	0.0370	0.0370	0.0368	0.0321	0.0271	0.0203	0.0120	0.0018	21.2	22.0	0.0680	0.0578	0.0570	0.0586	0.0550	0.0512	0.0470	0.0396	0.0300	0.0177	.0042	
	do	Ring 0°	do	15.8	16.8	0.0370	0.0370	0.0368	0.0366	0.0321	0.0270	0.0200	0.0110	0.0000	21.2	22.0	0.0680	0.0578	0.0570	0.0586	0.0550	0.0512	0.0470	0.0396	0.0300	0.0177		
3-A	Large	N.A.C.A. hood	do	15.9	17.8	0.0370	0.0370	0.0370	0.0366	0.0330	0.0280	0.0215	0.0130	0.0020	20.9	22.7	0.0673	0.0572	0.0570	0.0560	0.0545	0.0513	0.0460	0.0392	0.0300	0.0100	.0063	
4-A	do	do	do	15.9	17.0	0.0366	0.0365	0.0365	0.0362	0.0332	0.0288	0.0221	0.0135	0.0033	21.2	22.0	0.0685	0.0580	0.0572	0.0660	0.0542	0.0515	0.0471	0.0410	0.0312	0.0191	.0050	
	do	Ring 0°	do	15.9	17.0										21.2	22.0	0.0685	0.0580	0.0572	0.0660	0.0542	0.0515	0.0471	0.0410	0.0312	0.0191		
1-B	do	do	Ring 5°	16.5	17.0	0.0388	0.0388	0.0388	0.0387	0.0368	0.0318	0.0205	0.0100	0.0100	21.8	22.0	0.0615	0.0610	0.0600	0.0690	0.0670	0.0551	0.0518	0.0462	0.0305	0.0300	0.0180	
2-B	do	do	Ring 0°	15.8	16.8	0.0370	0.0370	0.0370	0.0368	0.0338	0.0288	0.0248	0.0180	0.0007	21.2	22.0	0.0600	0.0590	0.0588	0.0575	0.0560	0.0538	0.0504	0.0467	0.0387	0.0300	0.0160	
	do	Ring 10°	do	15.8	16.8	0.0370	0.0370	0.0370	0.0368	0.0338	0.0288	0.0248	0.0180	0.0007	21.2	22.0	0.0600	0.0590	0.0588	0.0575	0.0560	0.0538	0.0504	0.0467	0.0387	0.0300	0.0160	
	do	Exposed cylinders	do	15.8	16.8	0.0367	0.0367	0.0367	0.0365	0.0340	0.0308	0.0253	0.0188	0.0103	21.2	22.0	0.0577	0.0575	0.0572	0.0562	0.0560	0.0535	0.0500	0.0463	0.0382	0.0300	0.0165	
	do	Ring -5°	do	15.8	16.8	0.0370	0.0370	0.0370	0.0368	0.0330	0.0280	0.0245	0.0187	0.0105	21.2	22.0	0.0690	0.0588	0.0578	0.0568	0.0538	0.0497	0.0448	0.0380	0.0300	0.0165		
	do	Ring -10°	do	15.8	16.8										21.2	22.0	0.0690	0.0588	0.0578	0.0568	0.0538	0.0497	0.0448	0.0380	0.0300	0.0165		
	do	Ring -15°	do	15.8	16.8										21.2	22.0	0.0690	0.0588	0.0578	0.0568	0.0538	0.0497	0.0448	0.0380	0.0300	0.0165		
	do	Ring 0°	do	15.8	16.8										21.2	22.0	0.0690	0.0588	0.0578	0.0568	0.0538	0.0497	0.0448	0.0380	0.0300	0.0165		
	do	Ring 5°	do	15.8	17.0	0.0370	0.0370	0.0368	0.0366	0.0332	0.0288	0.0240	0.0173	0.0090	21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
	do	Ring 10°	do	15.8	17.0										21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
	do	Ring 15°	do	15.8	17.0										21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
	do	Ring 0°	do	15.8	17.0										21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
	do	Ring 5°	do	15.8	17.0										21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
	do	Ring 10°	do	15.8	17.0										21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
	do	Ring 15°	do	15.8	17.0										21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
	do	Ring 0°	do	15.8	17.0										21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
	do	Ring 5°	do	15.8	17.0										21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
	do	Ring 10°	do	15.8	17.0										21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
	do	Ring 15°	do	15.8	17.0										21.1	22.0	0.0605	0.0600	0.0680	0.0646	0.0620	0.0582	0.0453	0.0365	0.0272	0.0155		
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2	0.0368	0.0368	0.0368	0.0364	0.0330	0.0290	0.0237	0.0163	0.0073	20.8	22.0	0.0640	0.0540	0.0540	0.0533	0.0510	0.0471	0.0415	0.0347	0.0258	0.0136		
4-B	do	do	do	16.1	17.0	0.0380	0.0380	0.0380	0.0374	0.0354	0.0318	0.0260	0.0188	0.0096	21.3	22.0	0.0580	0.0578	0.0576	0.0570	0.0560	0.0540	0.0507	0.0454	0.0380	0.0285	0.0160	
1-C	do	do	do	15.8	17.0	0.0365	0.0345	0.0364	0.0359	0.0335	0.0295	0.0243	0.0170	0.0080	21.0	22.0	0.0588	0.0603	0.0567	0.0580	0.0552	0.0530	0.0490	0.0435	0.0365	0.0265	0.0160	
	do	Exposed cylinders	do	14.7	16.6	0.0369	0.0330	0.0324	0.0300	0.0283	0.0200	0.0124	0.0030	21.2	22.0	0.0603	0.0590	0.0578	0.0570	0.0560	0.0546	0.0513	0.0460	0.0388	0.0285	0.0175		
	do	Ring 0°	do	14.7	16.6	0.0325	0.0325	0.0322	0.0300	0.0280	0.0205	0.0133	0.0046															
2-C	Large	N.A.C.A. hood	do	15.8	17.0	0.0369	0.0369	0.0369	0.0367	0.0345	0.0310	0.0257	0.0183	0.0090	21.0	22.0	0.0582	0.0580	0.0576	0.0563	0.0555	0.0532	0.0495	0.0440	0.0370	0.0270	0.0145	
3-C	do	do	do	15.8	17.0	0.0368	0.0368	0.0368	0.0363	0.0340	0.0302	0.0232	0.0185	0.0095	21.0	22.0	0.0590	0.0590	0.0588	0.0572	0.0558	0.0534	0.0498	0.0448	0.0380	0.0290	0.0188	

TABLE VI  
REAR PROPELLER POWER COEFFICIENT,  $C_{P_R} = \frac{P_R}{\rho n_F^3 D^5}$   
ANGLE OF ATTACK =  $-5^\circ$

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.	$\frac{V}{nD}$										Propeller pitch at 0.75 R.		$\frac{V}{nD}$																						
					Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1											
		Front	Rear		Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1											
1-A	Large	N.A.C.A. hood	Ring $5^\circ$	17.0	17.0	0.0435	0.0414	0.0392	0.0372	0.0356	0.0290	0.0236	0.0188	0.0055	17.0	17.0	0.0435	0.0414	0.0392	0.0372	0.0356	0.0290	0.0236	0.0188	0.0055	22.0	22.0	0.0652	0.0642	0.0614	0.0590	0.0561	0.0528	0.0475	0.0412	0.0331	0.0220	0.0092	
2-A	do	do	do	15.9	17.1	0.0421	0.0408	0.0389	0.0370	0.0352	0.0281	0.0224	0.0143	0.0040	15.9	17.1	0.0421	0.0414	0.0391	0.0365	0.0330	0.0279	0.0217	0.0137	0.0044	20.8	22.0	0.0632	0.0612	0.0595	0.0574	0.0548	0.0513	0.0464	0.0397	0.0305	0.0197	0.0068	
2-A	do	do	Exposed cylinders	15.9	17.1	0.0422	0.0414	0.0391	0.0365	0.0330	0.0279	0.0217	0.0137	0.0044	15.9	17.1	0.0421	0.0408	0.0386	0.0361	0.0331	0.0284	0.0223	0.0149	0.0058	20.8	22.0	0.0641	0.0632	0.0617	0.0595	0.0565	0.0536	0.0464	0.0400	0.0391	0.0300	0.0197	0.0077
2-A	do	do	do	15.9	17.1	0.0421	0.0408	0.0386	0.0361	0.0331	0.0284	0.0223	0.0149	0.0058	15.9	17.1	0.0421	0.0408	0.0386	0.0361	0.0331	0.0284	0.0223	0.0149	0.0058	20.8	22.0	0.0632	0.0612	0.0595	0.0574	0.0548	0.0513	0.0464	0.0397	0.0305	0.0197	0.0068	
2-A	Small	N.A.C.A. hood	Ring $5^\circ$	15.8	16.8	0.0418	0.0411	0.0382	0.0353	0.0320	0.0277	0.0213	0.0140	0.0054	15.8	16.8	0.0414	0.0403	0.0380	0.0352	0.0319	0.0276	0.0218	0.0144	0.0054	21.2	22.0	0.0628	0.0620	0.0605	0.0584	0.0557	0.0519	0.0470	0.0402	0.0317	0.0207	0.0083	
2-A	do	do	Ring $0^\circ$	15.8	16.8	0.0414	0.0403	0.0380	0.0352	0.0319	0.0276	0.0218	0.0144	0.0054	15.8	16.8	0.0414	0.0403	0.0380	0.0352	0.0319	0.0276	0.0218	0.0144	0.0054	21.2	22.0	0.0628	0.0620	0.0605	0.0584	0.0557	0.0519	0.0470	0.0402	0.0317	0.0207	0.0083	
3-A	Large	N.A.C.A. hood	do	15.9	17.8	0.0455	0.0442	0.0420	0.0388	0.0349	0.0302	0.0236	0.0160	0.0045	15.9	17.8	0.0455	0.0442	0.0420	0.0388	0.0349	0.0302	0.0236	0.0160	0.0045	20.8	22.7	0.0648	0.0640	0.0625	0.0598	0.0567	0.0528	0.0471	0.0306	0.0300	0.0184	0.0000	
4-A	do	do	do	15.9	17.0	0.0408	0.0403	0.0388	0.0360	0.0330	0.0291	0.0230	0.0158	0.0060	15.9	17.0	0.0408	0.0403	0.0388	0.0360	0.0330	0.0291	0.0230	0.0158	0.0060	21.2	22.0	0.0620	0.0617	0.0600	0.0578	0.0553	0.0520	0.0479	0.0413	0.0325	0.0218	0.0080	
1-B	do	do	Ring $0^\circ$	15.8	17.0	0.0428	0.0415	0.0392	0.0368	0.0337	0.0290	0.0250	0.0186	0.0100	15.8	17.0	0.0428	0.0415	0.0392	0.0368	0.0337	0.0290	0.0250	0.0186	0.0100	21.8	22.0	0.0642	0.0630	0.0611	0.0584	0.0560	0.0526	0.0481	0.0427	0.0364	0.0253	0.0140	
2-B	do	do	Ring $0^\circ$	15.8	16.8	0.0408	0.0395	0.0370	0.0350	0.0325	0.0288	0.0236	0.0166	0.0070	15.8	16.8	0.0408	0.0395	0.0370	0.0350	0.0325	0.0288	0.0236	0.0166	0.0070	21.2	22.0	0.0641	0.0630	0.0613	0.0589	0.0561	0.0530	0.0485	0.0427	0.0348	0.0245	0.0128	
2-B	do	do	Ring $5^\circ$	15.8	16.8	0.0408	0.0395	0.0370	0.0350	0.0325	0.0288	0.0236	0.0166	0.0070	15.8	16.8	0.0408	0.0395	0.0370	0.0350	0.0325	0.0288	0.0236	0.0166	0.0070	21.2	22.0	0.0641	0.0630	0.0613	0.0589	0.0561	0.0530	0.0485	0.0427	0.0348	0.0245	0.0128	
2-B	do	do	Ring $10^\circ$	15.8	16.8	0.0407	0.0397	0.0376	0.0352	0.0325	0.0282	0.0233	0.0165	0.0074	15.8	16.8	0.0407	0.0397	0.0376	0.0352	0.0325	0.0282	0.0233	0.0165	0.0074	21.2	22.0	0.0617	0.0608	0.0593	0.0577	0.0552	0.0517	0.0470	0.0417	0.0340	0.0242	0.0133	
2-B	do	do	Exposed cylinders	15.8	16.8	0.0410	0.0400	0.0384	0.0352	0.0325	0.0288	0.0242	0.0170	0.0078	15.8	16.8	0.0410	0.0400	0.0384	0.0352	0.0325	0.0288	0.0242	0.0170	0.0078	21.2	22.0	0.0622	0.0624	0.0608	0.0580	0.0555	0.0520	0.0478	0.0423	0.0353	0.0255	0.0160	
2-B	do	do	Ring $-5^\circ$	15.8	16.8	0.0410	0.0400	0.0384	0.0352	0.0325	0.0288	0.0242	0.0170	0.0078	15.8	16.8	0.0410	0.0400	0.0384	0.0352	0.0325	0.0288	0.0242	0.0170	0.0078	21.2	22.0	0.0622	0.0624	0.0608	0.0580	0.0555	0.0520	0.0478	0.0423	0.0353	0.0255	0.0160	
2-B	do	do	Ring $-10^\circ$	15.8	16.8	0.0410	0.0400	0.0384	0.0352	0.0325	0.0288	0.0242	0.0170	0.0078	15.8	16.8	0.0410	0.0400	0.0384	0.0352	0.0325	0.0288	0.0242	0.0170	0.0078	21.2	22.0	0.0622	0.0624	0.0608	0.0580	0.0555	0.0520	0.0478	0.0423	0.0353	0.0255	0.0160	
2-B	do	do	Ring $-15^\circ$	15.8	16.8	0.0410	0.0400	0.0384	0.0352	0.0325	0.0288	0.0242	0.0170	0.0078	15.8	16.8	0.0410	0.0400	0.0384	0.0352	0.0325	0.0288	0.0242	0.0170	0.0078	21.2	22.0	0.0622	0.0624	0.0608	0.0580	0.0555	0.0520	0.0478	0.0423	0.0353	0.0255	0.0160	
2-B	do	do	do	15.8	17.0	0.0398	0.0385	0.0365	0.0345	0.0318	0.0276	0.0222	0.0163	0.0060	15.8	17.0	0.0398	0.0385	0.0365	0.0345	0.0318	0.0276	0.0222	0.0163	0.0060	21.1	22.0	0.0615	0.0606	0.0588	0.0564	0.0538	0.0504	0.0469	0.0402	0.0352	0.0260	0.0149	
2-B	do	do	Ring $5^\circ$	15.8	17.0	0.0410	0.0400	0.0384	0.0361	0.0334	0.0291	0.0238	0.0173	0.0060	15.8	17.0	0.0410	0.0400	0.0384	0.0361	0.0334	0.0291	0.0238	0.0173	0.0060	21.1	22.0	0.0642	0.0630	0.0611	0.0584	0.0560	0.0526	0.0481	0.0427	0.0364	0.0253	0.0140	
2-B	do	do	Ring $0^\circ$	15.8	17.0	0.0410	0.0400	0.0384	0.0361	0.0334	0.0291	0.0238	0.0173	0.0060	15.8	17.0	0.0410	0.0400	0.0384	0.0361	0.0334	0.0291	0.0238	0.0173	0.0060	21.1	22.0	0.0642	0.0630	0.0611	0.0584	0.0560	0.0526	0.0481	0.0427	0.0364	0.0253	0.0140	
2-B	do	do	Ring $-5^\circ$	15.8	17.0	0.0410	0.0400	0.0384	0.0361	0.0334	0.0291	0.0238	0.0173	0.0060	15.8	17.0	0.0410	0.0400	0.0384	0.0361	0.0334	0.0291	0.0238	0.0173	0.0060	21.1	22.0	0.0642	0.0630	0.0611	0.0584	0.0560	0.0526	0.0481	0.0427	0.0364	0.0253	0.0140	
2-B	do	do	Ring $-10^\circ$	15.8	17.0	0.0410	0.0400	0.0384	0.0361	0.0334	0.0291	0.0238	0.0173	0.0060	15.8	17.0	0.0410	0.0400	0.0384	0.0361	0.0334	0.0291	0.0238	0.0173	0.0060	21.1	22.0	0.0642	0.0630	0.0611	0.0584	0.0560	0.0526	0.0481	0.0427	0.0364	0.0253	0.0140	
2-B	do	do	Ring $4^\circ$	15.8	17.0	0.0408	0.0397	0.0379	0.0356	0.0326	0.0287	0.0233	0.0173	0.0060	15.8	17.0	0.0408	0.0397	0.0379	0.0356	0.0326	0.0287	0.0233	0.0173	0.0060	21.1	22.0	0.0637	0.0632	0.0603	0.0573	0.0540	0.0517	0.0470	0.0417	0.0342	0.0260	0.0130	
2-B	do	do	Ring $0^\circ$	15.8	17.0	0.0408	0.0397	0.0379	0.0356	0.0326	0.0287	0.0233	0.0173	0.0060	15.8	17.0	0.0408	0.0397	0.0379	0.0356	0.0326	0.0287	0.0233	0.0173	0.0060	21.1	22.0	0.0637	0.0632	0.0603	0.0573	0.0540	0.0517	0.0470	0.0417	0.0342	0.0260	0.0130	
2-B	do	do	Ring $-8^\circ$	15.8	17.0	0.0410	0.0414	0.0393	0.0362	0.0327	0.0289	0.0238	0.0179	0.0065	15.8	17.0	0.0410	0.0414	0.0393	0.0362	0.0327	0.0289	0.0238	0.0179	0														

TABLE VI—Continued

$$\text{REAR PROPELLER POWER COEFFICIENT, } C_{P_R} = \frac{P_R}{\rho n_r^3 D^3} \text{—Continued}$$

ANGLE OF ATTACK=0°

Front propeller: Right-hand no. 4412 - 4-foot diameter. Rear propeller: Left-hand no. 4412 - 4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.	$\frac{V}{nD}$										Propeller pitch at 0.75 R.	$\frac{V}{nD}$												
		Front	Rear		Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	0.0432	0.0410	0.0306	0.0374	0.0334	0.0280	0.0220	0.0140	0.0052	22.0	22.0	0.0643	0.0620	0.0010	0.0508	0.0563	0.0524	0.0477	0.0410	0.0321	0.0214	0.0090	
2-A	do	do	do	15.9	17.1	0.0422	0.0400	0.0383	0.0301	0.0324	0.0281	0.0220	0.0135	0.0040	20.8	22.0	0.0624	0.0614	0.0000	0.0583	0.0645	0.0510	0.0462	0.0393	0.0303	0.0105	0.0070	
do	do	Exposed cylinders	do	15.9	17.1	0.0421	0.0410	0.0388	0.0300	0.0326	0.0284	0.0218	0.0141	0.0041	20.8	22.0	0.0623	0.0618	0.0000	0.0578	0.0630	0.0510	0.0460	0.0390	0.0305	0.0183	0.0060	
do	do	do	do	15.9	17.1	0.0423	0.0409	0.0386	0.0305	0.0328	0.0284	0.0221	0.0144	0.0043	20.8	22.0	0.0642	0.0621	0.0000	0.0595	0.0670	0.0544	0.0608	0.0396	0.0305	0.0100	0.0060	
Small	do	N.A.C.A. hood	Ring 5°	15.7	17.0	0.0409	0.0399	0.0374	0.0344	0.0310	0.0260	0.0210	0.0133	0.0040	20.8	22.0	0.0608	0.0595	0.0000	0.0584	0.0658	0.0526	0.0488	0.0438	0.0372	0.0283	0.0182	0.0070
do	do	Ring 0°	do	15.8	16.8	0.0432	0.0410	0.0387	0.0352	0.0319	0.0278	0.0218	0.0132	0.0045	21.2	22.0	0.0630	0.0620	0.0000	0.0583	0.0660	0.0518	0.0468	0.0394	0.0305	0.0183	0.0070	
3-A	Large	N.A.C.A. hood	do	15.9	17.8	0.0448	0.0441	0.0421	0.0392	0.0348	0.0293	0.0220	0.0120	0.0015	20.9	22.7	0.0649	0.0643	0.0027	0.0603	0.0573	0.0528	0.0460	0.0395	0.0295	0.0148	0.0000	
4-A	do	do	do	15.9	17.0	0.0413	0.0403	0.0385	0.0358	0.0330	0.0289	0.0227	0.0148	0.0055	21.2	22.0	0.0638	0.0630	0.0012	0.0588	0.0550	0.0510	0.0460	0.0407	0.0320	0.0210	0.0083	
1-B	do	do	Ring 0°	15.9	17.0	0.0416	0.0407	0.0389	0.0350	0.0323	0.0282	0.0224	0.0141	0.0052	21.2	22.0	0.0638	0.0620	0.0000	0.0595	0.0670	0.0537	0.0490	0.0437	0.0368	0.0264	0.0185	
2-B	do	do	Ring 5°	15.8	17.0	0.0424	0.0413	0.0393	0.0368	0.0330	0.0303	0.0249	0.0181	0.0000	21.8	22.0	0.0636	0.0626	0.0012	0.0595	0.0670	0.0537	0.0490	0.0437	0.0368	0.0264	0.0185	
do	do	Ring 0°	do	15.8	16.8	0.0404	0.0397	0.0377	0.0358	0.0324	0.0288	0.0237	0.0170	0.0083	21.2	22.0	0.0631	0.0618	0.0003	0.0584	0.0658	0.0527	0.0488	0.0431	0.0351	0.0255	0.0161	
do	do	Ring 5°	do	15.8	16.8	0.0411	0.0403	0.0394	0.0360	0.0325	0.0285	0.0236	0.0165	0.0082	21.2	22.0	0.0631	0.0618	0.0003	0.0584	0.0658	0.0527	0.0488	0.0431	0.0351	0.0255	0.0161	
do	do	Ring 10°	do	15.8	16.8	0.0412	0.0402	0.0381	0.0358	0.0325	0.0280	0.0238	0.0169	0.0084	21.2	22.0	0.0630	0.0624	0.0011	0.0586	0.0661	0.0524	0.0476	0.0422	0.0351	0.0261	0.0167	
do	do	Exposed cylinders	do	15.8	16.8	0.0406	0.0393	0.0373	0.0347	0.0322	0.0281	0.0236	0.0172	0.0084	21.2	22.0	0.0643	0.0631	0.0008	0.0583	0.0661	0.0521	0.0478	0.0430	0.0364	0.0278	0.0170	
do	do	Ring -5°	do	15.8	16.8	0.0417	0.0403	0.0381	0.0352	0.0320	0.0281	0.0238	0.0169	0.0082	21.2	22.0	0.0630	0.0624	0.0011	0.0586	0.0661	0.0521	0.0478	0.0422	0.0351	0.0261	0.0167	
do	do	Ring -10°	do	15.8	16.8	0.0409	0.0393	0.0370	0.0348	0.0319	0.0288	0.0236	0.0170	0.0083	21.2	22.0	0.0630	0.0624	0.0011	0.0586	0.0661	0.0521	0.0478	0.0422	0.0351	0.0261	0.0167	
do	do	Ring -15°	do	15.8	16.8	0.0410	0.0396	0.0375	0.0350	0.0324	0.0288	0.0240	0.0168	0.0080	21.2	22.0	0.0619	0.0610	0.0006	0.0586	0.0660	0.0520	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	do	do	15.8	17.0	0.0402	0.0392	0.0371	0.0349	0.0314	0.0278	0.0227	0.0166	0.0085	21.1	22.0	0.0619	0.0610	0.0006	0.0586	0.0660	0.0520	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	Ring 10°	do	15.8	17.0	0.0407	0.0402	0.0385	0.0359	0.0320	0.0295	0.0248	0.0185	0.0083	21.2	22.0	0.0630	0.0620	0.0010	0.0586	0.0660	0.0520	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	Ring 5°	do	15.8	17.0	0.0408	0.0400	0.0383	0.0359	0.0322	0.0296	0.0246	0.0177	0.0084	21.2	22.0	0.0630	0.0624	0.0011	0.0586	0.0661	0.0521	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	Ring 0°	do	15.8	17.0	0.0412	0.0401	0.0382	0.0358	0.0326	0.0298	0.0243	0.0180	0.0084	21.2	22.0	0.0630	0.0624	0.0011	0.0586	0.0661	0.0521	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	Ring -5°	do	15.8	17.0	0.0418	0.0405	0.0386	0.0361	0.0329	0.0293	0.0248	0.0181	0.0084	21.2	22.0	0.0630	0.0624	0.0011	0.0586	0.0661	0.0521	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	Ring -10°	do	15.8	17.0	0.0420	0.0405	0.0383	0.0363	0.0326	0.0298	0.0242	0.0181	0.0086	21.2	22.0	0.0630	0.0624	0.0011	0.0586	0.0661	0.0521	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	Ring 4°	do	15.8	17.0	0.0420	0.0405	0.0383	0.0363	0.0326	0.0298	0.0242	0.0181	0.0086	21.2	22.0	0.0630	0.0624	0.0011	0.0586	0.0661	0.0521	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	Ring 0°	do	15.8	17.0	0.0408	0.0397	0.0381	0.0354	0.0327	0.0287	0.0236	0.0173	0.0083	21.2	22.0	0.0630	0.0620	0.0010	0.0586	0.0660	0.0520	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	Ring -5°	do	15.8	17.0	0.0407	0.0394	0.0374	0.0357	0.0327	0.0289	0.0241	0.0173	0.0088	21.1	22.0	0.0630	0.0620	0.0010	0.0574	0.0652	0.0520	0.0467	0.0415	0.0340	0.0240	0.0144	
do	do	Ring -8°	do	15.8	17.0	0.0413	0.0402	0.0381	0.0358	0.0326	0.0290	0.0238	0.0170	0.0089	21.1	22.0	0.0615	0.0613	0.0010	0.0580	0.0653	0.0523	0.0467	0.0402	0.0331	0.0240	0.0138	
do	do	Ring -10°	do	15.8	17.0	0.0408	0.0399	0.0377	0.0352	0.0325	0.0285	0.0241	0.0180	0.0087	21.1	22.0	0.0628	0.0620	0.0011	0.0584	0.0654	0.0524	0.0467	0.0402	0.0331	0.0240	0.0138	
do	do	Ring 4°	Ring 5°	15.8	17.0	0.0420	0.0411	0.0394	0.0384	0.0357	0.0337	0.0301	0.0264	0.0193	0.0118	21.2	22.0	0.0630	0.0627	0.0011	0.0586	0.0661	0.0521	0.0468	0.0413	0.0340	0.0253	0.0145
do	do	Ring 5°	do	15.8	17.0	0.0413	0.0404	0.0386	0.0351	0.0326	0.0292	0.0242	0.0174	0.0091	21.2	22.0	0.0630	0.0627	0.0011	0.0586	0.0661	0.0521	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	Ring 0°	do	15.8	17.0	0.0410	0.0398	0.0381	0.0359	0.0324	0.0297	0.0247	0.0180	0.0097	21.1	22.0	0.0637	0.0619	0.0000	0.0576	0.0553	0.0520	0.0480	0.0420	0.0356	0.0263	0.0153	
do	do	Ring 10°	do	15.8	17.0	0.0424	0.0418	0.0400	0.0370	0.0349	0.0321	0.0294	0.0183	0.0104	21.2	22.0	0.0630	0.0624	0.0011	0.0586	0.0661	0.0521	0.0468	0.0413	0.0340	0.0253	0.0145	
do	do	Ring 0°	do	15.8	17.0	0.0408	0.0402	0.0386	0.0358	0.0336	0.0305	0.0297	0.0240	0.0183	0.0100	21.2	22.0	0.0630	0.0624	0.0011	0.0586	0.0661	0.0521	0.0468	0.0413	0.0340	0.0253	0.0145
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2	0.0421	0.0413	0.0304	0.0369	0.0335	0.0295	0.0242	0.0172	0.0071	20.8	22.0	0.0620	0.0620	0.0010	0.0586	0.0560	0.0518	0.0473	0.0404	0.0314	0.0217	0.0113	
4-B	do	do	do	16.1	17.0	0.0410	0.0410	0.0390	0.0370	0.0341	0.0304	0.0254	0.0185	0.0090</														

TABLE VI—Continued

REAR PROPELLER POWER COEFFICIENT,  $C_{P_R} = \frac{P_R}{\rho n_F^3 D^5}$ —Continued

ANGLE OF ATTACK=5°

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.		$\frac{V}{nD}$									Propeller pitch at 0.75 R.		$\frac{V}{nD}$										
						Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
		Front	Rear	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1
1-A	Large	N.A.O.A. hood	Ring 5°	17.0	17.0	0.0433	0.0410	0.0416	0.0391	0.0366	0.0335	0.0299	0.0220	0.0149	22.0	22.0	0.0652	0.0630	0.0611	0.0588	0.0558	0.0520	0.0471	0.0409	0.0312	0.0188	
2-A	do	do	do	15.9	17.1	0.0438	0.0420	0.0396	0.0364	0.0332	0.0283	0.0220	0.0141	0.0040	20.8	22.0	0.0680	0.0611	0.0600	0.0576	0.0546	0.0509	0.0455	0.0380	0.0293	0.0162	
2-A	do	do	Exposed cylinders	15.9	17.1	0.0426	0.0414	0.0394	0.0363	0.0330	0.0282	0.0219	0.0132	0.0029	20.8	22.0	0.0637	0.0630	0.0608	0.0582	0.0550	0.0509	0.0467	0.0385	0.0288	0.0163	0.0022
2-A	Small	do	do	15.9	17.1	0.0415	0.0410	0.0392	0.0356	0.0320	0.0278	0.0222	0.0142	0.0040	20.8	22.0	0.0636	0.0617	0.0603	0.0574	0.0541	0.0500	0.0450	0.0388	0.0298	0.0180	0.0061
2-A	do	N.A.O.A. hood	Ring 5°	15.7	17.0	0.0403	0.0391	0.0349	0.0344	0.0308	0.0292	0.0204	0.0129	0.0045	20.8	22.0	0.0618	0.0608	0.0584	0.0560	0.0523	0.0481	0.0432	0.0375	0.0284	0.0183	
2-A	do	Ring 0°	do	15.8	16.9	0.0403	0.0399	0.0381	0.0352	0.0319	0.0274	0.0215	0.0140	0.0052	21.2	22.0	0.0635	0.0630	0.0617	0.0592	0.0562	0.0521	0.0484	0.0397	0.0310	0.0198	0.0066
3-A	Large	N.A.O.A. hood	do	15.9	17.8	0.0446	0.0436	0.0407	0.0370	0.0341	0.0285	0.0211	0.0113	-0.0010	20.9	22.7	0.0682	0.0646	0.0630	0.0612	0.0577	0.0525	0.0463	0.0378	0.0278	0.0168	0.0030
4-A	do	do	do	15.9	17.0	0.0418	0.0407	0.0390	0.0358	0.0327	0.0282	0.0223	0.0143	0.0053	21.2	22.0	0.0635	0.0627	0.0612	0.0588	0.0560	0.0520	0.0471	0.0402	0.0312	0.0192	0.0059
1-B	do	do	Ring 5°	16.8	17.0	0.0427	0.0420	0.0402	0.0373	0.0338	0.0301	0.0252	0.0192	0.0112	21.8	22.0	0.0640	0.0628	0.0613	0.0592	0.0570	0.0532	0.0492	0.0438	0.0350	0.0261	0.0150
2-B	do	do	Ring 0°	15.8	16.8	do	do	do	do	do	do	do	do	do	21.2	22.0	0.0533	0.0620	0.0604	0.0584	0.0568	0.0537	0.0500	0.0445	0.0388	0.0279	0.0166
2-B	do	do	Ring 5°	15.8	16.8	0.0412	0.0400	0.0380	0.0361	0.0326	0.0280	0.0242	0.0174	0.0090	21.2	22.0	0.0533	0.0620	0.0604	0.0584	0.0568	0.0537	0.0500	0.0445	0.0388	0.0279	0.0166
2-B	do	do	Ring 10°	15.8	16.8	do	do	do	do	do	do	do	do	do	21.2	22.0	0.0523	0.0613	0.0598	0.0581	0.0560	0.0525	0.0487	0.0431	0.0357	0.0260	0.0149
2-B	do	do	Exposed cylinders	15.8	16.8	0.0108	0.0399	0.0382	0.0355	0.0330	0.0295	0.0240	0.0168	0.0087	21.2	22.0	0.0523	0.0610	0.0598	0.0587	0.0567	0.0544	0.0489	0.0436	0.0361	0.0276	0.0187
2-B	do	do	Ring -5°	15.8	16.8	do	do	do	do	do	do	do	do	do	21.2	22.0	0.0524	0.0618	0.0608	0.0587	0.0567	0.0544	0.0489	0.0436	0.0361	0.0276	0.0187
2-B	do	do	Ring -10°	15.8	16.8	do	do	do	do	do	do	do	do	do	21.2	22.0	0.0524	0.0618	0.0608	0.0587	0.0567	0.0544	0.0489	0.0436	0.0361	0.0276	0.0187
2-B	do	do	Ring -15°	15.8	16.8	do	do	do	do	do	do	do	do	do	21.2	22.0	0.0524	0.0618	0.0608	0.0587	0.0567	0.0544	0.0489	0.0436	0.0361	0.0276	0.0187
2-B	do	do	Ring 10°	15.8	17.0	0.0405	0.0395	0.0379	0.0351	0.0319	0.0283	0.0232	0.0167	0.0090	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring 5°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring 0°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring -5°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring -10°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring -15°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring 4°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring 0°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring -5°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring -10°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring -15°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring 6°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring -5°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.1	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring 0°	15.8	17.0	0.0421	0.0410	0.0391	0.0368	0.0337	0.0298	0.0252	0.0191	0.0118	21.0	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring 10°	15.8	17.0	0.0421	0.0410	0.0391	0.0368	0.0337	0.0298	0.0252	0.0191	0.0118	21.0	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
2-B	do	do	Ring 0°	15.8	17.0	do	do	do	do	do	do	do	do	do	21.0	22.0	0.0617	0.0618	0.0599	0.0577	0.0548	0.0500	0.0473	0.0420	0.0352	0.0203	0.0160
3-B	Large	N.A.O.A. hood	Ring 5°	15.7	17.2	0.0412	0.0409	0.0395	0.0370	0.0338	0.0298	0.0247	0.0183	0.0093	20.8	22.0	0.0625	0.0620	0.0605	0.0588	0.0563	0.0523	0.0471	0.0418	0.0340	0.0260	0.0136
4-B	do	do	do	16.1	17.0	0.0434	0.0426	0.0408	0.0384	0.0348	0.0305	0.0255	0.0189	0.0102	21.3	22.0	0.0648	0.0635	0.0617	0.0598	0.0570	0.0540	0.0507	0.0454	0.0370	0.0267	0.0150
1-C	do	do	do	15.8	17.0	0.0413	0.0407	0.0391	0.0371	0.0339	0.0300	0.0240	0.0190	0.0110	21.0	22.0	0.0613	0.0615	0.0610	0.0599	0.0573	0.0540	0.0500	0.0446	0.0374	0.0265	0.0175
1-C	do	do	do	14.7	15.6	0.0358	0.0352	0.0336	0.0312	0.0293	0.0255	0.0213	0.0158	0.0103	21.2	22.0	0.0619	0.0607	0.0593	0.0577	0.0543	0.0500	0.0459	0.0401	0.0325	0.0228	
2-C	Large	N.A.O.A. hood	do	15.8	17.0	0.0422	0.0419	0.0401	0.0377	0.0350	0.0311																

TABLE VII

$$\text{PROPELLUSIVE EFFICIENCY, } \eta = \frac{(T - \Delta D)V}{P}$$

ANGLE OF ATTACK=-5°

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.	$\frac{V}{nD}$									Propeller pitch at 0.75 R.	$\frac{V}{nD}$												
					Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1
		Front	Rear		Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1
1-A	Large	N.A.O.A. hood	Ring 5°	17.0	17.0	0.187	0.357	0.502	0.612	0.690	0.743	0.738	0.681	.....	22.0	22.0	0.141	0.281	0.414	0.536	0.640	0.717	0.770	0.800	0.708	0.707	.....
2-A	do	do	do	15.0	17.1	.107	.370	.517	.621	.711	.766	.760	.689	.....	20.8	22.0	.151	.207	.434	.550	.602	.741	.795	.828	.825	.718	.....
	do	do	Exposed cylinders	15.0	17.1	.195	.389	.513	.622	.703	.756	.741	.677	.....	20.8	22.0	.149	.203	.420	.554	.650	.740	.793	.822	.821	.688	.....
	Small	do	do	15.0	17.1	.192	.344	.510	.636	.727	.781	.790	.676	.....	20.8	22.0	.151	.294	.429	.552	.658	.734	.790	.832	.860	.800	0.524
	do	N.A.O.A. hood	Ring 5°	15.8	16.8	.198	.372	.520	.630	.722	.775	.780	.602	.....	20.8	22.0	.148	.203	.430	.553	.603	.748	.798	.831	.847	.795	.370
	do	Ring 0°	do	15.8	16.8	.190	.377	.527	.642	.735	.803	.827	.731	.....	21.2	22.0	.164	.301	.437	.561	.608	.767	.821	.868	.910	.937	.820
3-A	Large	N.A.O.A. hood	do	15.9	17.8	.194	.308	.511	.620	.700	.747	.740	.640	.....	20.0	22.7	.161	.207	.431	.552	.660	.720	.767	.701	.774	.082	.....
4-A	do	do	do	15.9	17.0	.108	.372	.513	.620	.693	.730	.732	.568	.....	21.2	22.0	.160	.293	.428	.548	.650	.722	.759	.777	.777	.693	.081
1-B	do	do	Ring 0°	15.9	17.0	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
2-B	do	do	Ring 5°	16.5	17.0	.193	.304	.508	.620	.709	.762	.760	.631	.....	21.8	22.0	.145	.238	.423	.547	.651	.727	.777	.810	.824	.723	.049
	do	do	Ring 5°	15.8	16.8	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	do	do	Ring 10°	15.8	16.8	.200	.377	.528	.641	.720	.762	.730	.691	.....	21.2	22.0	.149	.205	.432	.555	.655	.730	.785	.819	.822	.745	.271
	do	do	Exposed cylinders	15.8	16.8	.201	.378	.528	.630	.719	.765	.757	.694	.....	21.2	22.0	.152	.203	.434	.554	.650	.720	.778	.808	.806	.720	.240
	do	do	Ring -5°	15.8	16.8	.200	.377	.526	.645	.730	.795	.804	.720	.....	21.2	22.0	.150	.294	.430	.556	.673	.751	.813	.850	.862	.624	.064
	do	do	Ring -10°	15.8	16.8	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	do	do	Ring -15°	15.8	16.8	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	Small	Exposed cylinders	do	15.8	17.0	.105	.307	.513	.631	.727	.784	.794	.638	.....	21.1	22.0	.145	.238	.421	.540	.650	.738	.800	.846	.888	.804	.541
	do	do	Ring 10°	15.8	17.0	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	do	do	Ring 5°	15.8	17.0	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	do	do	Ring 0°	15.8	17.0	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	do	do	Ring 5°	15.8	17.0	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	do	do	Ring 10°	15.8	17.0	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	do	do	Ring 0°	15.8	17.0	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	do	do	Ring 5°	15.8	17.0	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	do	do	Ring 10°	15.8	17.0	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
	do	do	Ring 0°	15.8	17.0	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	
3-B	Large	N.A.O.A. hood	Ring 5°	15.7	17.2	.195	.367	.513	.628	.710	.758	.762	.691	.....	20.8	22.0	.158	.305	.440	.560	.654	.728	.777	.803	.808	.724	.227
4-B	do	do	do	16.1	17.0	.193	.364	.509	.618	.702	.758	.765	.651	.....	21.3	22.0	.148	.289	.423	.543	.642	.714	.766	.800	.816	.772	.502
1-C	do	do	do	15.8	17.0	.193	.380	.493	.602	.684	.729	.735	.642	.....	21.0	22.0	.149	.289	.417	.530	.622	.695	.740	.768	.757	.690	.430
1-C	Small	Exposed cylinders	Exposed cylinders	14.7	15.6	.207	.330	.519	.629	.704	.751	.766	.639	.....	21.2	22.0	.140	.280	.414	.535	.637	.711	.769	.817	.855	.870	.839
2-C	Large	N.A.O.A. hood	do	15.8	17.0	.193	.361	.499	.602	.670	.716	.720	.651	.....	21.0	22.0	.147	.286	.414	.525	.616	.683	.735	.770	.783	.764	.562
3-C	do	do	do	15.8	17.0	.193	.360	.498	.601	.630	.722	.744	.663	.....	21.0	22.0	.143	.279	.407	.520	.610	.695	.743	.770	.794	.755	.536

TABLE VII—Continued

$$\text{PROPELLER EFFICIENCY, } \eta = \frac{(T - \Delta D)V}{P} \text{—Continued}$$

ANGLE OF ATTACK=0°

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.		V/nD									Propeller pitch at 0.75 R.		V/nD												
						Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1
		Front	Rear	Front	Rear																								
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	0.187	0.368	0.499	0.608	0.690	0.734	0.733	0.508	0.722	0.22.0	0.22.0	0.147	0.287	0.418	0.538	0.637	0.719	0.785	0.800	0.800	0.800	0.090		
2-A	do	do	do	16.9	17.1	.197	.374	.520	.632	.716	.760	.740	.522	20.8	22.0	.151	.296	.432	.550	.660	.710	.792	.813	.793	.867	do	do	do	
	do	do	Exposed cylinders	15.9	17.1	.198	.371	.517	.624	.704	.749	.730	.484	20.8	22.0	.151	.295	.430	.554	.651	.724	.774	.800	.786	.854	do	do	do	
	do	do	Exposed cylinders	15.9	17.1	.198	.370	.520	.633	.713	.774	.783	.624	20.8	22.0	.151	.298	.437	.561	.662	.736	.792	.840	.871	.790	do	do	do	
	Small	do	do	15.7	17.0	.199	.307	.514	.630	.716	.780	.772	.574	20.8	22.0	.148	.290	.425	.549	.655	.744	.804	.838	.838	.700	do	do	do	
	do	do	N.A.C.A. hood	15.8	16.8	.199	.368	.508	.622	.708	.761	.772	.607	21.2	22.0	.160	.297	.436	.563	.669	.755	.825	.884	.839	.062	Ring 0°	do	do	
	do	do	Ring 0°	15.8	16.8	.198	.374	.524	.648	.744	.807	.826	.700	21.2	22.0	.160	.297	.436	.563	.669	.755	.825	.884	.839	.062	0.747	do	do	do
3-A	Large	N.A.C.A. hood	do	15.9	17.8	.195	.307	.509	.611	.697	.730	.740	.546	20.9	22.7	.154	.298	.432	.543	.643	.716	.768	.785	.748	.580	do	do	do	
4-A	do	do	do	15.9	17.0	.198	.372	.516	.625	.705	.742	.743	.571	21.2	22.0	.148	.285	.418	.583	.641	.717	.766	.791	.776	.052	Ring 0°	do	do	
1-B	do	do	Ring 5°	16.5	17.0	.195	.367	.512	.628	.718	.774	.780	.684	21.8	22.0	.147	.289	.424	.540	.652	.736	.794	.828	.887	.702	.421	do	do	do
2-B	do	do	Ring 0°	15.8	16.8	.198	.372	.520	.630	.726	.781	.783	.662	21.2	22.0	.150	.295	.432	.556	.662	.741	.793	.825	.889	.791	.536	do	do	do
	do	do	Ring 5°	15.8	16.8	.201	.378	.529	.641	.731	.780	.790	.685	21.2	22.0	.150	.295	.432	.556	.662	.741	.793	.825	.889	.791	.536	do	do	do
	do	do	Ring 10°	15.8	16.8	.202	.382	.534	.654	.740	.791	.800	.710	21.2	22.0	.140	.294	.429	.552	.664	.738	.797	.820	.817	.756	.533	do	do	do
	do	do	Exposed cylinders	15.8	16.8	.200	.376	.524	.638	.719	.773	.779	.701	21.2	22.0	.147	.291	.431	.560	.674	.761	.820	.872	.889	.604	.670	do	do	do
	do	do	Exposed cylinders	15.8	16.8	.200	.380	.530	.650	.744	.800	.820	.750	21.2	22.0	.147	.291	.431	.560	.674	.761	.820	.872	.889	.604	.670	do	do	do
	do	do	Ring -5°	15.8	16.8	.197	.374	.520	.644	.735	.792	.820	.774	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring -10°	15.8	16.8	.199	.377	.526	.644	.729	.781	.781	.700	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring -15°	15.8	16.8	.200	.378	.527	.640	.734	.793	.813	.734	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring 10°	15.8	17.0	.198	.372	.518	.638	.729	.794	.819	.733	21.1	22.0	.150	.294	.431	.556	.664	.747	.808	.850	.868	.850	.677	do	do	do
	do	do	Ring 5°	15.8	17.0	.205	.381	.528	.649	.754	.830	.862	.800	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring 0°	15.8	17.0	.200	.374	.522	.650	.748	.820	.848	.794	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring -5°	15.8	17.0	.201	.379	.527	.645	.744	.810	.840	.798	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring -10°	15.8	17.0	.191	.361	.512	.638	.732	.802	.830	.762	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring 4°	15.8	17.0	.197	.373	.522	.651	.764	.835	.867	.832	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring 0°	15.8	17.0	.205	.374	.524	.645	.741	.820	.855	.817	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring -5°	15.8	17.0	.196	.368	.506	.626	.726	.787	.795	.714	21.1	22.0	.145	.297	.425	.554	.660	.741	.800	.840	.863	.850	.667	do	do	do
	do	do	Ring 8°	15.8	17.0	.191	.363	.512	.628	.717	.778	.788	.685	21.1	22.0	.145	.297	.424	.554	.664	.738	.795	.840	.863	.803	.512	do	do	do
	do	do	Ring -10°	15.8	17.0	.197	.370	.512	.630	.718	.788	.804	.720	21.1	22.0	.148	.290	.420	.554	.664	.751	.812	.860	.888	.774	do	do	do	
	do	do	Ring 4°	15.8	17.0	.200	.377	.530	.666	.769	.834	.907	.885	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring -8°	15.8	17.0	.198	.377	.529	.651	.736	.801	.819	.770	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring 10°	15.8	17.0	.196	.372	.521	.643	.766	.839	.885	.872	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
	do	do	Ring 0°	15.8	17.0	.193	.371	.521	.640	.741	.817	.882	.856	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
3-B	Large	N.A.C.A. hood	Ring 8°	15.7	17.2	.198	.370	.510	.620	.716	.776	.780	.650	20.8	22.0	.150	.302	.440	.560	.650	.733	.784	.821	.849	.770	.316	do	do	do
4-B	do	do	do	16.1	17.0	.198	.367	.510	.622	.708	.760	.765	.667	21.3	22.0	.143	.284	.418	.541	.647	.726	.777	.804	.812	.770	.472	do	do	do
1-O	do	do	do	15.8	17.0	.192	.358	.496	.596	.670	.708	.707	.618	21.0	22.0	.148	.286	.412	.520	.610	.681	.727	.747	.787	.862	.422	do	do	do
	do	do	Exposed cylinders	14.7	15.6	.208	.380	.517	.619	.688	.724	.716	.573	21.2	22.0	.141	.279	.409	.525	.617	.683	.729	.768	.806	.718	do	do	do	
	do	do	Ring 0°	14.7	15.6	.205	.379	.519	.621	.703	.757	.790	.720	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do
2-C	Large	N.A.C.A. hood	do	15.8	17.0	.190	.357	.495	.602	.670	.710	.715	.636	21.0	22.0	.149	.280	.410	.531	.624	.694	.736	.762	.784	.723	.572	do	do	do
3-C	do	do	do	15.8	17.0	.193	.360	.496	.600	.674	.721	.720	.651	21.0	22.0	.144	.284	.415	.531	.627	.693	.743	.772	.794	.803	.689	do	do	do

TABLE VII—Continued

PROPELLANT EFFICIENCY,  $\eta = \frac{(T - \Delta D)V}{P}$  —Continued  
 ANGLE OF ATTACK =  $5^\circ$

**Front propeller:** Right hand no. 4412—4-foot diameter. **Rear propeller:** Left hand no. 4412—4-foot diameter.

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.	V/nD										Propeller pitch at 0.76 R.		V/nD												
					Front	Rear	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
		Front	Rear		Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	0.188	0.357	0.501	0.605	0.675	0.711	0.837	0.402	—	—	—	22.0	22.0	0.141	0.277	0.404	0.517	0.614	0.690	0.756	0.760	0.755	0.880	—
2-A	do	do	do	15.0	17.1	0.195	0.367	0.508	0.609	0.690	0.720	0.822	0.413	—	—	—	20.8	22.0	0.158	0.301	0.433	0.548	0.640	0.710	0.765	0.700	0.742	0.590	—
...do	do	Exposed cylinders	do	15.0	17.1	0.194	0.365	0.500	0.602	0.681	0.724	0.700	0.410	—	—	—	20.8	22.0	0.164	0.298	0.420	0.541	0.636	0.712	0.769	0.787	0.776	0.830	—
...do	do	do	do	15.9	17.1	0.195	0.364	0.504	0.620	0.699	0.748	0.738	0.574	—	—	—	20.8	22.0	0.152	0.295	0.425	0.538	0.634	0.714	0.776	0.820	0.837	0.777	—
Small	do	do	do	15.7	17.0	0.195	0.367	0.503	0.619	0.708	0.760	0.730	0.434	—	—	—	20.8	22.0	0.149	0.280	0.422	0.542	0.640	0.726	0.787	0.808	0.701	0.872	—
do	N.A.C.A. hood	Ring 5°	do	15.8	16.8	0.199	0.371	0.508	0.610	0.705	0.763	0.738	0.680	—	—	—	21.2	22.0	0.163	0.297	0.429	0.546	0.648	0.739	0.817	0.800	0.838	0.642	0.611
do	Ring 0°	do	do	15.8	16.8	0.199	0.374	0.517	0.630	0.734	0.808	0.820	0.080	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
3-A	Large	N.A.C.A. hood	do	15.0	17.8	0.195	0.358	0.491	0.503	0.671	0.722	0.704	0.428	—	—	—	20.0	22.7	0.151	0.292	0.419	0.529	0.620	0.604	0.752	0.784	0.708	0.846	—
4-A	do	do	do	15.0	17.0	0.197	0.368	0.508	0.611	0.683	0.724	0.711	0.509	—	—	—	21.2	22.0	0.149	0.290	0.422	0.540	0.635	0.703	0.760	0.770	0.775	0.880	—
...do	do	Ring 0°	do	15.9	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
1-B	do	do	Ring 5°	16.5	17.0	0.195	0.308	0.514	0.620	0.721	0.771	0.770	0.717	—	—	—	21.8	22.0	0.147	0.291	0.428	0.551	0.657	0.782	0.705	0.830	0.852	0.818	0.010
2-B	do	do	Ring 0°	15.8	16.8	0.200	0.379	0.523	0.648	0.733	0.780	0.783	0.712	—	—	—	21.2	22.0	0.161	0.296	0.433	0.553	0.658	0.743	0.798	0.833	0.851	0.851	0.763
...do	do	Ring 5°	do	15.8	16.8	0.200	0.379	0.523	0.648	0.733	0.780	0.783	0.712	—	—	—	21.2	22.0	0.151	0.296	0.431	0.553	0.658	0.736	0.794	0.833	0.853	0.840	0.714
...do	do	Ring 10°	do	15.8	16.8	0.199	0.375	0.520	0.634	0.724	0.782	0.804	0.725	—	—	—	21.2	22.0	0.151	0.296	0.431	0.553	0.658	0.751	0.814	0.801	0.894	0.902	0.800
...do	do	Exposed cylinders	do	15.8	16.8	0.200	0.370	0.524	0.642	0.733	0.798	0.821	0.770	—	—	—	21.2	22.0	0.151	0.296	0.434	0.560	0.660	0.751	0.814	0.801	0.894	0.902	0.800
Small	do	do	do	15.8	16.8	0.195	0.368	0.513	0.630	0.728	0.780	0.816	0.767	—	—	—	21.1	22.0	0.145	0.285	0.419	0.546	0.660	0.747	0.800	0.844	0.866	0.880	0.780
do	do	Ring 10°	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	
do	do	Ring 5°	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	Ring 0°	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	Ring -5°	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	Ring -10°	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	Ring -15°	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
do	do	do	do	15.8	17.0	—																							

## THICK WING—VARIOUS RADIAL-ENGINE COWLINGSTANDARDS—TANDEM PROPELLERS

TABLE VIII

$$\text{PROPELLER OPERATING COEFFICIENT, } C_s = \sqrt[5]{\frac{\rho V^5}{P n_F^3}}$$

ANGLE OF ATTACK =  $-5^\circ$ 

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.	$\frac{V}{nD}$										Propeller pitch at 0.75 R.		$\frac{V}{nD}$																
					Front	Rear	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1			
		Front	Rear		Front	Rear	Front	Rear	17.0	17.0	16.8	16.8	16.6	16.6	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	16.8	16.8	16.6	16.6	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6				
2-A	do	do	do	15.9	17.1	16.6	16.6	16.3	16.3	16.0	16.0	15.7	15.7	15.5	15.5	15.3	15.3	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4	14.2	14.2	14.0	14.0				
2-A	do	do	Exposed cylinders	15.9	17.1	16.6	16.6	16.3	16.3	16.0	16.0	15.7	15.7	15.5	15.5	15.3	15.3	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4	14.2	14.2	14.0	14.0				
2-A	do	do	Exposed cylinders	15.9	17.1	16.6	16.6	16.3	16.3	16.0	16.0	15.7	15.7	15.5	15.5	15.3	15.3	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4	14.2	14.2	14.0	14.0				
2-A	Small	do	do	15.9	17.1	16.6	16.6	16.3	16.3	16.0	16.0	15.7	15.7	15.5	15.5	15.3	15.3	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4	14.2	14.2	14.0	14.0				
2-A	do	N.A.C.A. hood	Ring 5°	15.7	17.0	16.6	16.6	16.3	16.3	16.0	16.0	15.7	15.7	15.5	15.5	15.3	15.3	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4	14.2	14.2	14.0	14.0				
2-A	do	do	Ring 0°	15.8	16.8	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
3-A	Large	N.A.C.A. hood	do	15.9	17.8	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
4-A	do	do	do	15.9	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
4-A	do	do	Ring 0°	15.9	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
1-B	do	do	Ring 5°	10.5	17.0	16.5	16.5	16.3	16.3	16.0	16.0	15.7	15.7	15.5	15.5	15.3	15.3	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4	14.2	14.2	14.0	14.0				
2-B	do	do	Ring 0°	15.8	10.8	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 5°	15.8	10.8	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 10°	15.8	16.8	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Exposed cylinders	15.8	16.8	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring -5°	15.8	16.8	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring -10°	15.8	16.8	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring -15°	15.8	16.8	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	Small	do	Exposed cylinders	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 10°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 5°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 0°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 9°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring -6°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring -10°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 4°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 0°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 5°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring -5°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring -10°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 4°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
2-B	do	do	Ring 0°	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4				
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2	16.6	16.6	16.3	16.3	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4	14.2	14.2	14.0	14.0		
4-B	do	do	do	10.1	17.0	16.5	16.5	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4	14.2	14.2	14.0	14.0		
1-C	do	do	do	15.8	17.0	16.7	16.7	16.4	16.4	16.2	16.2	16.0	16.0	15.8	15.8	15.6	15.6	15.4	15.4	15.2	15.2	15.0	15.0	14.8	14.8	14.6	14.6	14.4	14.4	14.2	14.2	14.0	14.0
1-C	do	do	do	14.7	16.8	17.1	17.1	17.4	17.4	17.6	17.6	17.8	17.8	18.0	18.0	18.2	18.2	18.4	18.4	18.6	18.6	18.8	18.8	19.0	19.0	19.2	19.2	19.4	19.4	19.6			

TABLE VIII—Continued

$$\text{PROPELLER OPERATING COEFFICIENT, } C_s = \frac{5}{\sqrt{Pn_r^3}} \text{ Continued}$$

ANGLE OF ATTACK=0°

Front propeller: Right hand no. 4412—4-foot diameter. Rear propeller: Left hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.	$\frac{V}{nD}$									Propeller pitch at 0.75 R.	$\frac{V}{nD}$												
					0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9		Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1
		Front	Rear		Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	0.104	0.330	0.498	0.671	0.858	1.058	1.302	1.050	2.580	22.0	22.0	0.152	0.304	0.457	0.614	0.775	0.943	1.121	1.320	1.505	1.920	-----
2-A	do	do	do	15.9	17.1	.160	.334	.503	.676	.862	1.063	1.300	1.040	2.390	20.8	22.0	.152	.306	.462	.620	.780	.950	1.130	1.332	1.575	1.925	-----
2-A	do	do	Exposed cylinders	15.9	17.1	.160	.334	.504	.678	.862	1.065	1.308	1.030	2.360	20.8	22.0	.152	.306	.462	.621	.782	.950	1.130	1.334	1.608	1.930	2.760
2-A	Small	do	do	15.7	17.0	.167	.334	.506	.684	.872	1.083	1.318	1.078	2.780	20.8	22.0	.153	.307	.464	.622	.783	.958	1.143	1.347	1.600	1.960	-----
2-A	do	N.A.C.A. hood	Ring 5°	15.8	16.8	.160	.334	.503	.680	.867	1.073	1.318	1.080	2.420	21.2	22.0	.152	.306	.460	.617	.777	.944	1.125	1.330	1.575	1.905	2.580
2-A	do	do	Ring 0°	15.8	16.8	.160	.333	.503	.680	.866	1.070	1.312	1.082	2.463	21.2	22.0	.152	.306	.460	.617	.775	.946	1.124	1.324	1.576	1.940	2.920
3-A	Large	N.A.C.A. hood	do	15.9	17.8	.168	.331	.499	.670	.858	1.060	1.300	1.046	2.590	20.9	22.7	.153	.306	.461	.617	.775	.946	1.124	1.320	1.558	1.875	-----
4-A	do	do	do	15.9	17.0	.167	.334	.504	.678	.860	1.063	1.300	1.020	2.340	21.2	22.0	.152	.305	.459	.617	.778	.943	1.122	1.320	1.558	1.875	-----
1-B	do	do	Ring 5°	16.5	17.0	.165	.331	.500	.673	.850	1.051	1.280	1.573	2.080	21.8	22.0	.152	.304	.458	.614	.774	.938	1.112	1.304	1.520	1.810	2.385
2-B	do	do	Ring 0°	15.8	16.8	.167	.334	.504	.678	.863	1.061	1.280	1.574	2.060	21.2	22.0	.152	.306	.461	.617	.778	.940	1.118	1.305	1.530	1.812	2.340
2-B	do	do	Ring 5°	15.8	16.8	.167	.334	.505	.678	.862	1.065	1.292	1.586	2.080	21.2	22.0	.152	.306	.461	.617	.778	.940	1.118	1.305	1.530	1.812	2.340
2-B	do	do	Ring 10°	15.8	16.8	.167	.335	.504	.680	.862	1.064	1.292	1.580	2.080	21.2	22.0	.153	.305	.466	.614	.776	.944	1.118	1.308	1.524	1.800	2.182
2-B	do	do	Exposed cylinders	15.8	16.8	.167	.335	.505	.681	.862	1.062	1.292	1.583	2.080	21.2	22.0	.152	.304	.460	.617	.778	.943	1.118	1.308	1.518	1.782	2.160
2-B	do	do	Ring -5°	15.8	16.8	.167	.335	.506	.680	.864	1.065	1.291	1.576	2.060	21.2	22.0	.152	.304	.460	.617	.778	.943	1.118	1.308	1.518	1.782	2.160
2-B	do	do	Ring -10°	15.8	16.8	.167	.335	.506	.680	.862	1.063	1.293	1.580	2.030	21.2	22.0	.152	.304	.460	.617	.778	.943	1.118	1.308	1.518	1.782	2.160
2-B	do	do	Ring -15°	15.8	16.8	.167	.335	.506	.680	.866	1.062	1.284	1.578	2.060	21.2	22.0	.152	.304	.460	.617	.778	.943	1.118	1.308	1.518	1.782	2.160
2-B	do	do	Small	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	do	
2-B	do	do	Exposed cylinders	15.8	17.0	.167	.334	.506	.680	.860	1.070	1.300	1.500	2.070	21.1	22.0	.153	.306	.462	.620	.780	.947	1.125	1.318	1.540	1.825	2.260
2-B	do	do	Ring 10°	15.8	17.0	.167	.334	.504	.679	.861	1.060	1.287	1.570	2.035	21.1	22.0	.152	.304	.462	.620	.780	.947	1.125	1.318	1.540	1.825	2.260
2-B	do	do	Ring 5°	15.8	17.0	.167	.334	.504	.679	.861	1.059	1.282	1.578	2.063	21.1	22.0	.152	.304	.462	.620	.780	.947	1.125	1.318	1.540	1.825	2.260
2-B	do	do	Ring 0°	15.8	17.0	.167	.334	.504	.679	.862	1.063	1.283	1.583	2.030	21.1	22.0	.152	.304	.462	.620	.780	.947	1.125	1.318	1.540	1.825	2.260
2-B	do	do	Ring -5°	15.8	17.0	.167	.335	.502	.677	.862	1.063	1.292	1.580	2.020	21.1	22.0	.152	.304	.462	.620	.780	.947	1.125	1.318	1.540	1.825	2.260
2-B	do	do	Ring -10°	15.8	17.0	.167	.335	.502	.679	.863	1.063	1.290	1.575	2.020	21.1	22.0	.152	.304	.462	.620	.780	.947	1.125	1.318	1.540	1.825	2.260
2-B	do	do	Ring 4°	15.8	17.0	.167	.334	.504	.679	.860	1.060	1.287	1.573	2.020	21.1	22.0	.152	.304	.462	.620	.780	.947	1.125	1.318	1.540	1.825	2.260
2-B	do	do	Ring 0°	15.8	17.0	.167	.334	.505	.680	.860	1.070	1.300	1.500	2.070	21.1	22.0	.153	.306	.462	.620	.780	.947	1.125	1.318	1.540	1.825	2.260
2-B	do	do	Ring 5°	15.8	17.0	.167	.334	.504	.679	.861	1.060	1.287	1.570	2.035	21.1	22.0	.152	.304	.462	.620	.780	.947	1.125	1.318	1.540	1.825	2.260
2-B	do	do	Ring 10°	15.8	17.0	.167	.334	.504	.678	.862	1.061	1.288	1.578	2.030	21.1	22.0	.152	.304	.462	.620	.780	.947	1.125	1.318	1.540	1.825	2.260
2-B	do	do	Ring 0°	15.8	17.0	.167	.334	.504	.678	.860	1.060	1.290	1.552	2.030	21.1	22.0	.152	.304	.460	.619	.780	.944	1.120	1.315	1.530	1.808	2.260
2-B	do	do	Ring 10°	15.8	17.0	.166	.333	.501	.676	.861	1.062	1.290	1.550	2.000	21.1	22.0	.152	.304	.460	.619	.780	.944	1.120	1.315	1.530	1.808	2.260
2-B	do	do	Ring 5°	15.8	17.0	.167	.334	.504	.678	.860	1.060	1.290	1.552	2.030	21.1	22.0	.152	.304	.460	.619	.780	.944	1.120	1.315	1.530	1.808	2.260
3-B	Large	N.A.O.A. hood	Ring 5°	16.7	17.2	.167	.334	.504	.677	.861	1.060	1.290	1.550	2.150	20.8	22.0	.154	.308	.463	.620	.780	.949	1.120	1.312	1.562	1.803	2.340
4-B	do	do	do	16.1	17.0	.166	.333	.501	.674	.853	1.048	1.272	1.552	2.030	21.3	22.0	.152	.304	.459	.616	.775	.940	1.116	1.310	1.527	1.814	2.240
1-C	do	do	do	15.8	17.0	.166	.336	.503	.676	.858	1.050	1.272	1.553	2.005	21.0	22.0	.154	.308	.462	.620	.776	.941	1.113	1.304	1.520	1.793	2.190
1-C	Small	Exposed cylinders	do	14.7	15.6	.171	.342	.517	.696	.854	1.088	1.333	1.650	2.285	21.2	22.0	.152	.306	.460	.617	.777	.939	1.109	1.296	1.508	1.780	2.170
1-C	do	do	Exposed cylinders	14.7	15.6	.171	.342	.517	.695	.858	1.090	1.330	1.640	2.220	21.2	22.0	.153	.307	.462	.618	.777	.940	1.110	1.300	1.512	1.784	2.180
2-C	Large	N.A.C.A. hood	do	15.8	17.0	.166	.333	.502	.675	.855	1.048	1.263	1.528	1.922	21.0	22.0	.153	.307	.462	.618	.777	.940	1.110	1.300	1.512	1.784	2.180
3-C	do	do	do	15.8	17.0	.167	.334	.502	.676	.857	1.050	1.270	1.536	1.934	21.0	22.0	.153	.307	.462	.619	.778	.942	1.116	1.300	1.510	1.780	2.170

TABLE VIII—Continued

$$\text{PROPELLER OPERATING COEFFICIENT, } C_s = \sqrt{\frac{\rho V^5}{P n_p^3}} \text{—Continued}$$

ANGLE OF ATTACK=5°

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.	$\frac{V}{nD}$									Propeller pitch at 0.75 R.		$\frac{V}{nD}$											
		Front	Rear		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9			0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	
		Front	Rear		.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	
1-A	Large	N.A.O.A. hood	Ring 5°	17.0	17.0	0.164	0.330	0.497	0.670	0.858	1.003	1.317	1.085	3.120	22.0	22.0	0.151	0.303	0.457	0.615	0.775	0.945	1.120	1.330	1.594	2.040	
2-A	do	do	do	15.9	17.1	.165	.332	.502	.676	.860	1.068	1.317	1.085	2.720	20.8	22.0	.156	.308	.462	.620	.781	.951	1.134	1.340	1.600	2.000	
2-A	do	do	Exposed cylinders	15.9	17.1	.166	.333	.502	.676	.861	1.069	1.314	1.073	2.900	20.8	22.0	.153	.306	.461	.618	.781	.950	1.130	1.340	1.695	1.998	3.740
2-A	do	do	Exposed cylinders	15.9	17.1	.166	.334	.504	.679	.862	1.068	1.309	1.051	3.116	20.8	22.0	.153	.306	.462	.620	.782	.954	1.130	1.340	1.695	1.970	3.056
2-A	Small	do	do	15.7	17.0	.170	.336	.506	.686	.876	1.090	1.343	1.718	2.920	20.8	22.0	.153	.306	.464	.623	.788	.960	1.145	1.352	1.608	2.008	
2-A	do	N.A.O.A. hood	Ring 5°	15.8	16.8	.167	.335	.504	.678	.867	1.076	1.320	1.063	2.460	21.2	22.0	.152	.306	.469	.617	.777	.945	1.128	1.330	1.575	1.930	2.720
2-A	do	do	Ring 0°	15.8	16.8	.167	.334	.504	.679	.868	1.073	1.325	1.680	2.630	21.2	22.0	.152	.306	.469	.617	.777	.945	1.128	1.330	1.575	1.930	2.720
3-A	Large	N.A.C.A. hood	do	15.9	17.8	.165	.332	.500	.676	.859	1.070	1.315	1.680	—	20.9	22.7	.152	.305	.458	.618	.776	.944	1.130	1.335	1.600	1.957	2.590
4-A	do	do	do	15.9	17.0	.167	.334	.503	.678	.863	1.068	1.308	1.628	2.330	21.2	22.0	.151	.305	.460	.618	.778	.945	1.123	1.322	1.568	1.920	2.720
1-B	do	do	Ring 0°	16.5	17.0	.166	.332	.499	.671	.851	1.047	1.205	1.537	1.940	21.8	22.0	.182	.304	.458	.614	.775	.936	1.108	1.295	1.511	1.780	2.175
2-B	do	do	Ring 0°	15.8	16.8	do	21.2	22.0	.153	.305	.466	.618	.774	.937	1.110	1.295	1.508	1.770	2.142								
2-B	do	do	Ring 5°	15.8	16.8	.167	.334	.504	.678	.860	1.060	1.280	1.560	2.000	21.2	22.0	.153	.305	.466	.618	.774	.937	1.110	1.295	1.508	1.770	2.142
2-B	do	do	Ring 10°	15.8	16.8	do	21.2	22.0	.153	.305	.466	.618	.774	.937	1.110	1.295	1.508	1.770	2.142								
2-B	do	do	Exposed cylinders	15.8	16.8	.167	.334	.505	.678	.858	1.057	1.270	1.562	1.986	21.2	22.0	.153	.305	.466	.618	.774	.941	1.112	1.300	1.515	1.785	2.180
2-B	do	do	Exposed cylinders	15.8	16.8	.167	.334	.504	.677	.860	1.060	1.280	1.560	1.958	21.2	22.0	.152	.306	.466	.616	.776	.941	1.111	1.300	1.510	1.773	2.110
2-B	do	do	Ring -5°	15.8	16.8	do	21.2	22.0	do																		
2-B	do	do	Ring -10°	15.8	16.8	do	21.2	22.0	do																		
2-B	do	do	Ring -15°	15.8	16.8	do	21.2	22.0	do																		
2-B	do	do	Ring 10°	15.8	17.0	do	21.1	22.0	.153	.306	.466	.618	.780	.948	1.120	1.310	1.525	1.800	2.208								
2-B	do	do	Ring 5°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring 0°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring 5°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring -5°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring -10°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring -15°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring 4°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring 0°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring -5°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring -8°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring -10°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring -10°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring 4°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring 5°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring 5°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring 0°	15.8	17.0	do	21.1	22.0	do																		
2-B	do	do	Ring 0°	15.8	17.0	do	21.1	22.0	do																		
3-B	Large	N.A.O.A. hood	Ring 5°	15.7	17.2	.167	.334	.504	.677	.859	1.059	1.282	1.568	2.040	20.8	22.0	.154	.308	.463	.620	.779	.944	1.123	1.318	1.540	1.816	2.260
4-B	do	do	do	16.1	17.0	.168	.332	.500	.671	.860	1.060	1.208	1.568	1.975	21.3	22.0	.152	.305	.460	.618	.774	.938	1.108	1.293	1.510	1.787	2.205
1-C	do	do	do	15.8	17.0	.167	.334	.503	.677	.858	1.054	1.280	1.552	1.990	21.0	22.0	.154	.306	.460	.617	.774	.940	1.112	1.300	1.514	1.783	2.182
1-C	Small	do	do	14.7	15.8	.171	.342	.515	.695	.882	1.088	1.325	1.600	2.140	21.2	22.0	.152	.304	.461	.618	.775	.937	1.105	1.290	1.408	1.745	2.090
2-C	Large	N.A.O.A. hood	do	15.8	17.0	.160	.333	.501	.673	.851	1.048	1.203	1.534	1.950	21.0	22.0	.152	.304	.460	.616	.775	.937	1.110	1.298	1.510	1.784	2.200
3-C	do	do	do	15.8	17.0	.167	.335	.503	.676	.856	1.052	1.270	1.538	1.945	21.0	22.0	.153	.305	.460	.615	.775	.940	1.110	1.296	1.508	1.770	2.101

TABLE IX

LIFT COEFFICIENT WITH PROPELLER OPERATING,  $C_{LP} = \frac{L_P}{qS}$

ANGLE OF ATTACK = -5°

**Front propeller:** Right-hand no. 4412—4-foot diameter. **Rear propeller** Left-hand no. 4412—4-foot diameter.

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.		$\frac{V}{nD}$									Propeller pitch at 0.75 R.		$\frac{V}{nD}$										
		Front	Rear	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0				0.159	0.188	0.140	0.132	0.142	0.133	22.0	22.0					0.194	0.189	0.161	0.137	0.126	0.125	0.125
2-A	do	do	do	15.9	17.1				.205	.184	.170	.169	.151	.147	20.8	22.0					.204	.180	.160	.153	.147	.140	.139
	do	Exposed cylinders	Exposed cylinders	15.9	17.1				.180	.102	.163	.148	.145	.145	20.8	22.0					.206	.179	.160	.151	.146	.145	.145
Small			do	15.9	17.1				.223	.169	.151	.150	.160	.152	20.8	22.0					.200	.176	.160	.148	.140	.136	.134
do	N.A.C.A. hood	Ring 5°	15.7	17.0				.197	.172	.157	.148	.142	.140	20.8	22.0					.193	.175	.160	.149	.140	.134	.130	
do	Ring 0°	do	15.8	16.8				.188	.183	.170	.162	.155	.150	21.2	22.0					.181	.175	.168	.143	.137	.135	.130	
3-A	Large	N.A.C.A. hood	do	15.9	17.8				.204	.190	.167	.154	.143	.135	20.0	22.7					.179	.163	.155	.149	.149	.140	.149
4-A	do	do	do	15.9	17.0				.180	.165	.163	.143	.140	.140	21.2	22.0					.172	.160	.147	.139	.133	.130	.130
1-B	do	do	Ring 0°	15.9	17.0																						
2-B	do	do	Ring 5°	16.5	17.0				.056	.055	.003	.114	.122	.123	21.8	22.0					.074	.074	.090	.110	.122	.132	.140
	do	do	Ring 0°	15.8	16.8				.086	.103	.119	.130	.140	.150	21.2	22.0					.050	.098	.120	.125	.128	.134	.147
do	do	Ring 10°	15.8	16.8				.086	.103	.119	.130	.140	.150	21.2	22.0					.068	.094	.113	.130	.140	.146	.160	
do	do	Exposed cylinders	do	15.8	16.8				.040	.085	.114	.130	.143	.152	21.2	22.0					.095	.101	.104	.110	.125	.141	.151
do	do	Ring -5°	do	15.8	16.8				.060	.085	.110	.130	.141	.149	21.2	22.0					.068	.094	.113	.130	.140	.146	.160
do	do	Ring -10°	do	15.8	16.8				.056	.085	.110	.130	.141	.149	21.2	22.0					.068	.094	.113	.130	.140	.146	.160
do	do	Ring -15°	do	15.8	16.8				.056	.085	.110	.130	.141	.149	21.2	22.0					.068	.094	.113	.130	.140	.146	.160
Small		Exposed cylinders	do	15.8	17.0				.066	.066	.118	.134	.144	.150	21.1	22.0					.068	.115	.130	.140	.150	.155	.160
do	do	Ring 10°	15.8	17.0				.066	.066	.118	.134	.144	.150	21.1	22.0					.068	.115	.130	.140	.150	.155	.160	
do	do	Ring 5°	15.8	17.0																							
do	do	Ring 0°	15.8	17.0																							
do	do	Ring -5°	15.8	17.0																							
do	do	Ring -10°	15.8	17.0																							
do	do	Ring 4°	15.8	17.0																							
do	do	Exposed cylinders	15.8	17.0																							
do	do	Ring 0°	15.8	17.0																							
do	do	Ring -5°	15.8	17.0																							
do	do	Ring -8°	15.8	17.0																							
do	do	Ring -10°	15.8	17.0																							
do	do	Ring 4°	15.8	17.0																							
do	do	Ring -5°	15.8	17.0																							
do	do	Ring 0°	15.8	17.0																							
do	do	Ring 10°	15.8	17.0																							
do	do	Ring 0°	15.8	17.0																							
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2				.100	.100	.105	.112	.125	.140	20.8	22.0					.064	.081	.108	.120	.127	.132	.131
4-B	do	do	do	16.1	17.0				.044	.075	.090	.110	.120	.126	21.3	22.0					.079	.085	.100	.110	.118	.125	.130
1-O	do	do	do	15.8	17.0				.173	.143	.132	.128	.131	.135	21.0	22.0					.177	.164	.141	.138	.134	.138	.143
Small		Exposed cylinders	Exposed cylinders	14.7	15.6				.169	.157	.162	.143	.159	.158	21.2	22.0					.165	.153	.151	.148	.146	.143	.141
do	Ring 0°	Ring 5°	14.7	15.6				.173	.153	.141	.133	.133	.138														
2-O	Large	N.A.C.A. hood	do	15.8	17.0				.183	.169	.168	.153	.160	.148	21.0	22.0					.180	.163	.158	.158	.158	.158	.168
3-O	do	do	do	15.8	17.0				.151	.141	.135	.133	.135	.140	21.0	22.0					.131	.143	.143	.133	.128	.128	.127

TABLE IX—Continued  
 LIFT COEFFICIENT WITH PROPELLER OPERATING,  $C_{LP} = \frac{L_p}{qS}$ —Continued  
 ANGLE OF ATTACK =  $0^\circ$

**Front propeller:** Right-hand no. 4412—4-foot diameter. **Rear propeller:** Left-hand no. 4412—4-foot diameter.

TABLE IX—Continued

LIFT COEFFICIENT WITH PROPELLER OPERATING,  $C_{LP} = \frac{L_p}{qS}$ —Continued  
 ANGLE OF ATTACK =  $5^\circ$

Front propeller: Right hand no. 4412—4-foot diameter. Rear propeller: Left hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.	$\frac{V}{nD}$										Propeller pitch at 0.75 R.	$\frac{V}{nD}$													
		Front	Rear		Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	
1-A	Large	N.A.C.A. hood	Ring 5°	°	°											°	°												
2-A	do	do	do	17.0	17.0											0.033	0.605	0.041	0.611	0.603	0.611	22.0	22.0						
	do	do	Exposed cylinders	15.0	17.1											.040	.633	.026	.019	.015	.010	20.8	22.0						
	do	do	Exposed cylinders	15.0	17.1											.052	.631	.019	.007	.003	.598	20.8	22.0						
	Small	do	do	15.0	17.1											.035	.641	.020	.010	.004	.600	20.8	22.0						
	do	N.A.C.A. hood	Ring 5°	15.8	16.8											.070	.643	.025	.010	.590	.592	20.8	22.0						
	do	do	Ring 0°	15.8	16.8											.096	.660	.030	.025	.016	.010	21.2	22.0						
				15.8	16.8										.090	.639	.020	.600	.003	.597	21.2	22.0							
3-A	Large	N.A.C.A. hood	do	15.0	17.8											.670	.034	.018	.608	.003	.600	20.9	22.7						
4-A	do	do	do	15.0	17.0											.080	.645	.622	.608	.003	.002	21.2	22.0						
	do	do	Ring 0°	15.0	17.0											.572	.590	.588	.592	.505	.507	21.8	22.0						
1-B	do	do	Ring 5°	10.5	17.0											.560	.575	.582	.588	.590	.591	21.2	22.0						
2-B	do	do	Ring 0°	15.8	16.8											.560	.575	.582	.588	.590	.591	21.2	22.0						
	do	do	Ring 5°	15.8	16.8											.560	.575	.582	.588	.590	.591	21.2	22.0						
	do	do	Ring 10°	15.8	16.8											.583	.590	.588	.593	.593	.591	21.2	22.0						
	do	do	Exposed cylinders	15.8	16.8											.593	.590	.590	.590	.590	.590	21.2	22.0						
	do	do	Ring -5°	15.8	16.8											.560	.590	.590	.590	.590	.590	21.2	22.0						
	do	do	Ring -10°	15.8	16.8											.560	.590	.590	.590	.590	.590	21.2	22.0						
	do	do	Ring -15°	15.8	16.8											.560	.590	.590	.590	.590	.590	21.2	22.0						
	do	do	do	15.8	16.8											.604	.600	.602	.605	.010	.011	21.1	22.0						
	do	do	Ring 10°	15.8	17.0											.572	.585	.590	.590	.006	.010	21.1	22.0						
	do	do	Ring 5°	15.8	17.0											.560	.575	.582	.588	.590	.591	21.2	22.0						
	do	do	Ring 0°	15.8	17.0											.560	.575	.582	.588	.590	.591	21.2	22.0						
	do	do	Ring 4°	15.8	17.0											.581	.589	.590	.591	.013	.014	21.1	22.0						
	do	do	Ring 0°	15.8	17.0											.581	.589	.590	.591	.013	.014	21.1	22.0						
	do	do	Ring 5°	15.8	17.0											.581	.589	.590	.591	.013	.014	21.1	22.0						
	do	do	Ring 10°	15.8	17.0											.581	.589	.590	.591	.013	.014	21.1	22.0						
	do	do	Ring 0°	15.8	17.0											.581	.589	.590	.591	.013	.014	21.1	22.0						
	do	do	Ring 4°	15.8	17.0											.581	.589	.590	.591	.013	.014	21.1	22.0						
	do	do	Ring -5°	15.8	17.0											.581	.589	.590	.591	.013	.014	21.1	22.0						
	do	do	Ring -8°	15.8	17.0											.588	.599	.603	.612	.018	.021	21.1	22.0						
	do	do	Ring -10°	15.8	17.0											.588	.599	.603	.612	.018	.021	21.1	22.0						
	do	do	Ring 4°	15.8	17.0											.580	.590	.593	.603	.010	.014	21.1	22.0						
	do	do	Ring -5°	15.8	17.0											.580	.590	.593	.603	.010	.014	21.1	22.0						
	do	do	Ring 0°	15.8	17.0											.573	.585	.595	.601	.006	.010	21.1	22.0						
	do	do	Ring 10°	15.8	17.0											.573	.585	.595	.601	.006	.010	21.1	22.0						
	do	do	Ring 0°	15.8	17.0											.573	.585	.595	.601	.006	.010	21.1	22.0						
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2											.595	.579	.573	.575	.590	.593	20.8	22.0						
4-B	do	do	do	16.1	17.0											.580	.589	.584	.593	.608	.607	21.3	22.0						
1-C	do	do	do	15.8	17.0											.633	.648	.626	.614	.611	.603	21.0	22.0						
	Small	Exposed cylinders	Exposed cylinders	14.7	15.6											.634	.656	.628	.603	.583	.569	21.2	22.0						
	do	do	Ring 0°	14.7	15.6											.633	.633	.601	.598	.578	.573								
2-C	Large	N.A.C.A. hood	do	15.8	17.0											.693	.665	.645	.633	.623	.618	21.0	22.0						
3-C	do	do	do	15.8	17.0											.686	.646	.613	.604	.603	.684	21.0	22.0						

TABLE X

MOMENT COEFFICIENT WITH PROPELLER OPERATING,  $C_{M_P} = \frac{M_P}{q S c}$

ANGLE OF ATTACK =  $-6^\circ$   
Front propeller: Right-hand no. 4412—4-foot diameter.  
Rear propeller: Left-hand no. 4412—4-foot diameter

THICK WING—VARIOUS RADIAL-ENGINE COWLING—TANDEM PROPELLERS

Nacelle position	Type of nacelle	Engine cowling		$\frac{V}{nD}$									$\frac{V}{nD}$									
		Front	Rear	Front	Rear	Propeller pitch at 0.75 R.	Front	Rear	Front	Rear	Propeller pitch at 0.75 R.	Front	Rear	Front	Rear	Propeller pitch at 0.75 R.	Front	Rear	Front	Rear		
1-A	Large	N.A.O.A. hood	Ring 5°	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	○	
2-A	do	do	do	17.0	17.0	-0.233	-0.165	-0.120	-0.083	-0.074	-0.061	22.0	22.0	22.0	22.0	-0.220	-0.167	-0.122	-0.100	-0.085	-0.075	-0.065
2-A	do	do	do	16.9	17.1	-2.23	-1.18	-0.89	-0.72	-0.66	-0.56	20.8	22.0	22.0	22.0	-2.15	-1.15	-0.88	-0.70	-0.62	-0.54	-0.48
2-A	do	do	do	16.9	17.1	-2.48	-1.62	-1.03	-0.72	-0.66	-0.56	20.8	22.0	22.0	22.0	-2.13	-1.10	-0.80	-0.63	-0.56	-0.48	-0.42
2-A	do	do	do	16.9	17.1	-2.95	-1.83	-1.16	-0.88	-0.70	-0.63	20.8	22.0	22.0	22.0	-2.20	-1.18	-0.93	-0.78	-0.67	-0.59	-0.50
2-A	do	do	do	16.7	17.0	-2.90	-1.50	-1.10	-0.85	-0.65	-0.56	20.8	22.0	22.0	22.0	-2.07	-1.12	-0.96	-0.81	-0.71	-0.65	-0.56
2-A	do	do	do	16.8	16.8	-2.25	-1.12	-0.85	-0.65	-0.56	-0.46	21.2	22.0	22.0	22.0	-2.00	-1.14	-0.94	-0.79	-0.71	-0.65	-0.56
2-A	do	do	do	16.8	16.8	-2.43	-1.63	-1.12	-0.85	-0.67	-0.56	21.2	22.0	22.0	22.0	-2.02	-1.18	-0.93	-0.78	-0.68	-0.62	-0.53
2-A	do	do	do	16.9	17.8	-2.46	-1.69	-1.13	-0.87	-0.70	-0.58	20.9	22.7	22.7	22.7	-2.04	-1.10	-0.93	-0.78	-0.68	-0.62	-0.53
2-A	do	do	do	15.9	17.0	-2.24	-1.60	-1.17	-0.89	-0.70	-0.55	21.8	22.0	22.0	22.0	-2.02	-1.13	-0.96	-0.80	-0.68	-0.62	-0.53
1-B	do	do	do	15.9	17.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
2-B	do	do	do	10.5	17.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
2-B	do	do	do	15.8	16.8	-0.04	-0.03	-0.03	-0.04	-0.08	-0.08	21.8	22.0	22.0	22.0	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04
2-B	do	do	do	15.8	16.8	-0.05	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.07	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05
2-B	do	do	do	15.8	16.8	-0.06	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.08	-0.06	-0.06	-0.06	-0.06	-0.06	-0.06
2-B	do	do	do	15.8	16.8	-0.07	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.09	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07
2-B	do	do	do	15.8	16.8	-0.08	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.10	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08
2-B	do	do	do	15.8	16.8	-0.09	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.11	-0.09	-0.09	-0.09	-0.09	-0.09	-0.09
2-B	do	do	do	15.8	16.8	-0.10	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.12	-0.10	-0.10	-0.10	-0.10	-0.10	-0.10
2-B	do	do	do	15.8	16.8	-0.11	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.13	-0.11	-0.11	-0.11	-0.11	-0.11	-0.11
2-B	do	do	do	15.8	16.8	-0.12	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.14	-0.12	-0.12	-0.12	-0.12	-0.12	-0.12
2-B	do	do	do	15.8	16.8	-0.13	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.15	-0.13	-0.13	-0.13	-0.13	-0.13	-0.13
2-B	do	do	do	15.8	16.8	-0.14	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.16	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14
2-B	do	do	do	15.8	16.8	-0.15	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.17	-0.15	-0.15	-0.15	-0.15	-0.15	-0.15
2-B	do	do	do	15.8	16.8	-0.16	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.18	-0.16	-0.16	-0.16	-0.16	-0.16	-0.16
2-B	do	do	do	15.8	16.8	-0.17	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.19	-0.17	-0.17	-0.17	-0.17	-0.17	-0.17
2-B	do	do	do	15.8	16.8	-0.18	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.20	-0.18	-0.18	-0.18	-0.18	-0.18	-0.18
2-B	do	do	do	15.8	16.8	-0.19	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.21	-0.19	-0.19	-0.19	-0.19	-0.19	-0.19
2-B	do	do	do	15.8	16.8	-0.20	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.22	-0.20	-0.20	-0.20	-0.20	-0.20	-0.20
2-B	do	do	do	15.8	16.8	-0.21	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.23	-0.21	-0.21	-0.21	-0.21	-0.21	-0.21
2-B	do	do	do	15.8	16.8	-0.22	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.24	-0.22	-0.22	-0.22	-0.22	-0.22	-0.22
2-B	do	do	do	15.8	16.8	-0.23	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.25	-0.23	-0.23	-0.23	-0.23	-0.23	-0.23
2-B	do	do	do	15.8	16.8	-0.24	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.26	-0.24	-0.24	-0.24	-0.24	-0.24	-0.24
2-B	do	do	do	15.8	16.8	-0.25	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.27	-0.25	-0.25	-0.25	-0.25	-0.25	-0.25
2-B	do	do	do	15.8	16.8	-0.26	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.28	-0.26	-0.26	-0.26	-0.26	-0.26	-0.26
2-B	do	do	do	15.8	16.8	-0.27	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.29	-0.27	-0.27	-0.27	-0.27	-0.27	-0.27
2-B	do	do	do	15.8	16.8	-0.28	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.30	-0.28	-0.28	-0.28	-0.28	-0.28	-0.28
2-B	do	do	do	15.8	16.8	-0.29	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.31	-0.29	-0.29	-0.29	-0.29	-0.29	-0.29
2-B	do	do	do	15.8	16.8	-0.30	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.32	-0.30	-0.30	-0.30	-0.30	-0.30	-0.30
2-B	do	do	do	15.8	16.8	-0.31	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.33	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31
2-B	do	do	do	15.8	16.8	-0.32	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.34	-0.32	-0.32	-0.32	-0.32	-0.32	-0.32
2-B	do	do	do	15.8	16.8	-0.33	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.35	-0.33	-0.33	-0.33	-0.33	-0.33	-0.33
2-B	do	do	do	15.8	16.8	-0.34	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.36	-0.34	-0.34	-0.34	-0.34	-0.34	-0.34
2-B	do	do	do	15.8	16.8	-0.35	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.37	-0.35	-0.35	-0.35	-0.35	-0.35	-0.35
2-B	do	do	do	15.8	16.8	-0.36	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.38	-0.36	-0.36	-0.36	-0.36	-0.36	-0.36
2-B	do	do	do	15.8	16.8	-0.37	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.39	-0.37	-0.37	-0.37	-0.37	-0.37	-0.37
2-B	do	do	do	15.8	16.8	-0.38	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.40	-0.38	-0.38	-0.38	-0.38	-0.38	-0.38
2-B	do	do	do	15.8	16.8	-0.39	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.41	-0.39	-0.39	-0.39	-0.39	-0.39	-0.39
2-B	do	do	do	15.8	16.8	-0.40	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.42	-0.40	-0.40	-0.40	-0.40	-0.40	-0.40
2-B	do	do	do	15.8	16.8	-0.41	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.43	-0.41	-0.41	-0.41	-0.41	-0.41	-0.41
2-B	do	do	do	15.8	16.8	-0.42	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.44	-0.42	-0.42	-0.42	-0.42	-0.42	-0.42
2-B	do	do	do	15.8	16.8	-0.43	-0.03	-0.03	-0.03	-0.08	-0.08	21.2	22.0	22.0	22.0	-0.45	-0.43	-0.43	-0.43</td			

TABLE X—Continued  
MOMENT COEFFICIENT WITH PROPELLER OPERATING,  $C_{m_p} = \frac{M_p}{qSC}$ —Continued

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

TABLE X—Continued

MOMENT COEFFICIENT WITH PROPELLER OPERATING,  $C_{mP} = \frac{M_P}{qSc}$  Continued  
ANGLE OF ATTACK=5°

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 R.										Propeller pitch at 0.75 R.													
				$\frac{V}{nD}$										$\frac{V}{nD}$													
		Front		Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	.....	.....	.....	-0.240	-0.160	-0.117	-0.090	-0.072	-0.060	17.0	17.0	.....	.....	.....	.....	-0.213	-0.152	-0.120	-0.095	-0.080	-0.070	-0.060
2-A	do	do	do	15.9	17.1	.....	.....	.....	-0.246	-0.154	-0.110	-0.081	-0.063	-0.052	15.9	17.1	.....	.....	.....	.....	-0.208	-0.148	-0.112	-0.091	-0.077	-0.066	-0.057
	do	do	Exposed cylinders	15.9	17.1	.....	.....	.....	-0.246	-0.153	-0.107	-0.080	-0.062	-0.049	15.9	17.1	.....	.....	.....	.....	-0.201	-0.143	-0.110	-0.088	-0.072	-0.061	-0.053
	do	Exposed cylinders	do	15.9	17.1	.....	.....	.....	-0.237	-0.153	-0.107	-0.078	-0.060	-0.048	15.9	17.1	.....	.....	.....	.....	-0.198	-0.137	-0.108	-0.087	-0.072	-0.061	-0.052
	Small	do	do	15.7	17.0	.....	.....	.....	-0.230	-0.148	-0.100	-0.078	-0.062	-0.050	15.8	17.0	.....	.....	.....	.....	-0.202	-0.140	-0.105	-0.083	-0.068	-0.050	-0.054
	do	N.A.C.A. hood	Ring 5°	15.8	16.8	.....	.....	.....	-0.223	-0.143	-0.099	-0.077	-0.060	-0.049	15.8	16.8	.....	.....	.....	.....	-0.200	-0.140	-0.100	-0.080	-0.068	-0.053	-0.050
	do	Ring 0°	do	15.8	16.8	.....	.....	.....	-0.220	-0.142	-0.098	-0.072	-0.055	-0.044	15.8	16.8	.....	.....	.....	.....	-0.200	-0.140	-0.100	-0.080	-0.068	-0.053	-0.050
3-A	Large	N.A.O.A. hood	do	15.0	17.8	.....	.....	.....	-0.234	-0.140	-0.097	-0.070	-0.055	-0.045	15.0	17.8	.....	.....	.....	.....	-0.207	-0.142	-0.103	-0.080	-0.065	-0.057	-0.052
4-A	do	do	do	15.9	17.0	.....	.....	.....	-0.238	-0.150	-0.104	-0.078	-0.060	-0.047	15.9	17.0	.....	.....	.....	.....	-0.198	-0.140	-0.108	-0.085	-0.070	-0.058	-0.050
1-B	do	do	Ring 5°	16.5	17.0	.....	.....	.....	.081	-.016	-.022	-.041	-.053	-.003	16.5	17.0	.....	.....	.....	.....	.058	.010	-.020	-.038	-.050	-.058	-.064
2-B	do	do	Ring 0°	15.8	16.8	.....	.....	.....	.070	.007	-.028	-.048	-.059	-.068	15.8	16.8	.....	.....	.....	.....	.062	.007	-.020	-.040	-.052	-.057	-.062
	do	do	Ring 5°	15.8	16.8	.....	.....	.....	.070	.007	-.028	-.048	-.059	-.068	15.8	16.8	.....	.....	.....	.....	.062	.007	-.028	-.044	-.055	-.061	-.067
	do	do	Ring 10°	15.8	16.8	.....	.....	.....	.065	.004	-.029	-.050	-.063	-.070	15.8	16.8	.....	.....	.....	.....	.042	.002	-.028	-.044	-.055	-.061	-.067
	do	do	Exposed cylinders	15.8	16.8	.....	.....	.....	.065	.010	-.026	-.048	-.060	-.068	15.8	16.8	.....	.....	.....	.....	.050	.000	-.026	-.042	-.051	-.060	-.065
	do	do	Exposed cylinders	15.8	16.8	.....	.....	.....	.065	.010	-.026	-.048	-.060	-.068	15.8	16.8	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring -5°	15.8	16.8	.....	.....	.....	.065	.010	-.026	-.048	-.060	-.068	15.8	16.8	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring -10°	15.8	16.8	.....	.....	.....	.065	.010	-.026	-.048	-.060	-.068	15.8	16.8	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring -15°	15.8	16.8	.....	.....	.....	.065	.010	-.026	-.048	-.060	-.068	15.8	16.8	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring 4°	15.8	17.0	.....	.....	.....	.063	.000	-.033	-.053	-.065	-.072	15.8	17.0	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring 10°	15.8	17.0	.....	.....	.....	.063	.000	-.033	-.053	-.065	-.072	15.8	17.0	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring 5°	15.8	17.0	.....	.....	.....	.063	.000	-.033	-.053	-.065	-.072	15.8	17.0	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring 0°	15.8	17.0	.....	.....	.....	.067	.002	-.032	-.052	-.063	-.072	15.8	17.0	.....	.....	.....	.....	.062	-.002	-.030	-.047	-.057	-.063	-.067
	do	do	Ring -5°	15.8	17.0	.....	.....	.....	.082	.001	-.032	-.050	-.063	-.072	15.8	17.0	.....	.....	.....	.....	.062	-.002	-.028	-.046	-.059	-.067	-.071
	do	do	Ring -8°	15.8	17.0	.....	.....	.....	.086	.001	-.030	-.050	-.062	-.070	15.8	17.0	.....	.....	.....	.....	.062	-.002	-.028	-.046	-.059	-.067	-.070
	do	do	Ring -10°	15.8	17.0	.....	.....	.....	.057	.000	-.030	-.050	-.063	-.072	15.8	17.0	.....	.....	.....	.....	.042	-.004	-.028	-.045	-.058	-.064	-.070
	do	do	Ring 4°	15.8	17.0	.....	.....	.....	.065	.000	-.030	-.050	-.063	-.072	15.8	17.0	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring 5°	15.8	17.0	.....	.....	.....	.065	.000	-.030	-.050	-.063	-.072	15.8	17.0	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring 0°	15.8	17.0	.....	.....	.....	.062	.003	-.030	-.049	-.060	-.068	15.8	17.0	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring 10°	15.8	17.0	.....	.....	.....	.062	.003	-.030	-.049	-.060	-.068	15.8	17.0	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
	do	do	Ring 0°	15.8	17.0	.....	.....	.....	.062	.003	-.030	-.049	-.060	-.068	15.8	17.0	.....	.....	.....	.....	.062	-.007	-.031	-.043	-.053	-.060	-.067
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2	.....	.....	.....	.055	.002	-.034	-.053	-.062	-.065	15.7	17.2	.....	.....	.....	.....	.038	-.003	-.028	-.045	-.056	-.062	-.065
4-B	do	do	do	16.1	17.0	.....	.....	.....	.071	.011	-.025	-.047	-.059	-.065	16.1	17.0	.....	.....	.....	.....	.057	.007	-.020	-.044	-.054	-.060	-.063
1-C	do	do	do	15.8	17.0	.....	.....	.....	.043	.028	-.018	-.012	-.008	-.007	15.8	17.0	.....	.....	.....	.....	.080	-.073	-.068	-.063	-.060	-.057	-.055
	do	do	do	14.7	15.6	.....	.....	.....	.048	.038	-.020	-.021	-.015	-.014	14.7	15.6	.....	.....	.....	.....	.097	-.086	-.078	-.074	-.073	-.069	-.065
	do	do	Ring 5°	14.7	15.6	.....	.....	.....	.100	.070	-.070	-.004	-.050	-.055	14.7	15.6	.....	.....	.....	.....	.058	-.057	-.057	-.056	-.056	-.056	-.054
2-C	Large	N.A.C.A. hood	do	15.8	17.0	.....	.....	.....	.063	.059	-.057	-.055	-.056	-.055	15.8	17.0	.....	.....	.....	.....	.070	-.068	-.068	-.060	-.060	-.056	-.054
3-C	do	do	do	15.8	17.0	.....	.....	.....	.068	.069	-.069	-.068	-.065	-.063	15.8	17.0	.....	.....	.....	.....	.070	-.068	-.068	-.060	-.060	-.056	-.054

THICK WING—VARIOUS RADIAL-ENGINE COWLING TANDEM PROPELLERS

TABLE XI  
PROPELLER COEFFICIENTS—NACELLE-ALONE TESTS

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter. Angle of attack=0°

Type of nacelle	Engine cowling			Propeller pitch at 0.75 $R_s$		$\frac{V}{nD}$									
	Front	Rear	Front	Rear	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	
Propeller spacing 1 diameter															
Thrust coefficient $C_T = \frac{T - \Delta D}{\rho n_p^2 D^3}$	Large	N.A.C.A. hood	Ring 5°	°	16.6	17.0	0.1555	0.1454	0.1326	0.1163	0.0973	0.0760	0.0517	0.0238	-0.0060
	Small	Ring 0°	do	°	16.4	17.0	.1561	.1453	.1322	.1165	.0987	.0763	.0579	.0323	-.0045
	Do	Exposed cylinders	Exposed cylinders	°	16.4	17.0	.1558	.1452	.1318	.1168	.0969	.0761	.0536	.0201	-0.0010
Propeller spacing 1½ diameters															
Front propeller power coefficient $C_{P_F} = \frac{P_F}{\rho n_p^2 D^3}$	Large	N.A.C.A. hood	Ring 5°	16.4	17.0	0.1572	0.1458	0.1317	0.1148	0.0953	0.0741	0.0509	0.0243	-0.0065	
	Small	Ring 0°	do	16.4	17.0	.1580	.1460	.1327	.1157	.0967	.0755	.0570	.0327	-.0045	
	Do	Exposed cylinders	Exposed cylinders	16.4	17.0	.1587	.1465	.1332	.1168	.0975	.0764	.0581	.0330	-.0010	
Propeller spacing 1 diameter															
Front propeller power coefficient $C_{P_F} = \frac{P_F}{\rho n_p^2 D^3}$	Large	N.A.C.A. hood	Ring 5°	16.6	17.0	0.0384	0.0384	0.0332	0.0390	0.0352	0.0307	0.0245	0.0160	0.0045	
	Small	Ring 0°	do	16.4	17.0	.0380	.0380	.0380	.0387	.0387	.0393	.0233	.0160	.0040	
	Do	Exposed cylinders	Exposed cylinders	16.4	17.0	.0387	.0385	.0382	.0375	.0340	.0295	.0230	.0145	.0040	
Propeller spacing 1½ diameters															
Rear propeller power coefficient $C_{P_R} = \frac{P_R}{\rho n_p^2 D^3}$	Large	N.A.C.A. hood	Ring 5°	16.4	17.0	0.0376	0.0375	0.0374	0.0372	0.0342	0.0298	0.0235	0.0162	0.0047	
	Small	Ring 0°	do	16.4	17.0	.0401	.0400	.0370	.0355	.0321	.0294	.0239	.0165	.0080	
	Do	Exposed cylinders	Exposed cylinders	16.4	17.0	.0404	.0400	.0385	.0353	.0320	.0278	.0233	.0166	.0088	
Propeller spacing 1 diameter															
Rear propeller power coefficient $C_{P_R} = \frac{P_R}{\rho n_p^2 D^3}$	Large	N.A.C.A. hood	Ring 5°	16.4	17.0	0.0410	0.0405	0.0389	0.0380	0.0329	0.0285	0.0233	0.0168	0.0088	
	Small	Ring 0°	do	16.4	17.0	.0412	.0400	.0370	.0355	.0321	.0294	.0239	.0165	.0080	
	Do	Exposed cylinders	Exposed cylinders	16.4	17.0	.0404	.0400	.0385	.0353	.0320	.0278	.0233	.0166	.0088	
Propeller spacing 1 diameter															
Propulsive efficiency $\eta = \frac{(T - \Delta D)}{P}$	Large	N.A.C.A. hood	Ring 5°	16.6	17.0	0.194	0.194	0.167	0.151	0.126	0.114	0.086	0.070	0.058	
	Small	Ring 0°	do	16.4	17.0	.197	.197	.173	.152	.146	.130	.102	.087	.071	
	Do	Exposed cylinders	Exposed cylinders	16.4	17.0	.197	.197	.169	.151	.138	.125	.099	.072	.054	
Propeller spacing 1½ diameters															
Propeller operating coefficient $C_B = \sqrt{\frac{P}{(T - \Delta D) V}}$	Large	N.A.C.A. hood	Ring 5°	16.4	17.0	0.200	0.374	0.518	0.627	0.712	0.762	0.762	0.607	-----	
	Small	Ring 0°	do	16.4	17.0	.197	.373	.522	.646	.750	.825	.872	.821	.345	
	Do	Exposed cylinders	Exposed cylinders	16.4	17.0	.197	.369	.516	.638	.735	.798	.809	.672	-----	
Propeller spacing 1 diameter															
Propeller operating coefficient $C_B = \sqrt{\frac{P}{(T - \Delta D) V}}$	Large	N.A.C.A. hood	Ring 5°	16.6	17.0	0.166	0.332	0.501	0.673	0.855	1.054	1.284	1.587	2.130	
	Small	Ring 0°	do	16.4	17.0	.166	.333	.503	.676	.861	1.062	1.293	1.597	2.180	
	Do	Exposed cylinders	Exposed cylinders	16.4	17.0	.166	.333	.502	.675	.860	1.063	1.293	1.603	2.185	
Propeller spacing 1½ diameters															
Propeller operating coefficient $C_B = \sqrt{\frac{P}{(T - \Delta D) V}}$	Large	N.A.C.A. hood	Ring 5°	16.4	17.0	0.166	0.333	0.502	0.674	0.857	1.060	1.290	1.603	2.130	
	Small	Ring 0°	do	16.4	17.0	.166	.333	.502	.674	.857	1.060	1.290	1.603	2.130	
	Do	Exposed cylinders	Exposed cylinders	16.4	17.0	.166	.333	.502	.674	.857	1.060	1.290	1.603	2.130	

TABLE XII  
RELATIVE MERITS OF TANDEM WING-NACELLE-PROPELLER COMBINATIONS

Front propeller: Right-hand no. 4412—4-foot diameter. Rear propeller: Left-hand no. 4412—4-foot diameter

Nacelle position	Type of nacelle	Engine cowling		Propeller pitch at 0.75 $R_e$		High-speed and cruising condition $V/nD = 0.65$ $C_L = 0.409$			Climbing condition $V/nD = 0.42$ $C_L = 0.652$		
		Front	Rear	Front	Rear	Propulsive efficiency ( $\eta$ )	Nacelle drag efficiency factor (N.D.F.)	Net efficiency ( $\eta$ )	Propulsive efficiency ( $\eta$ )	Nacelle drag efficiency factor (N.D.F.)	Net efficiency ( $\eta$ )
1-A	Large	N.A.C.A. hood	Ring 5°	17.0	17.0	0.742	0.220	0.522	0.620	0.020	0.600
2-A	do	do	do	15.9	17.1	.760	.220	.540	.622	.042	.580
	do	Exposed cylinders	do	15.9	17.1	.748	.247	.501	.626	.043	.583
	Small	do	do	15.9	17.1	.780	.307	.473	.638	.043	.595
	do	N.A.C.A. hood	Ring 5°	15.7	17.0	.788	.402	.386	.640	.061	.579
	do	Ring 0°	do	15.8	16.8	.780	.333	.447	.638	.032	.584
3-A	Large	N.A.C.A. hood	do	15.9	17.8	.744	.241	.503	.612	.039	.573
4-A	do	do	do	15.9	17.0	.748	.266	.482	.629	.028	.601
1-B	do	do	Ring 5°	15.9	17.0	.742	.281	.461	—	—	—
2-B	do	do	Ring 0°	16.5	17.0	.787	.181	.606	.652	.049	.603
	do	do	Ring 5°	15.8	16.8	.790	.205	.585	—	—	—
	do	do	Ring 10°	15.8	16.8	.800	.189	.611	.667	.031	.636
	do	do	Exposed cylinders	15.8	16.8	.788	.202	.598	—	—	—
	do	Ring -5°	do	15.8	16.8	.824	.256	.576	.653	.050	.603
	do	Ring -10°	do	15.8	16.8	.810	.268	.542	—	—	—
	do	Ring -15°	do	15.8	16.8	.790	.249	.541	—	—	—
	Small	Exposed cylinders	do	15.8	16.8	.814	.270	.544	—	—	—
	do	do	Ring 10°	15.8	17.0	.810	.288	.534	.660	.064	.586
	do	do	Ring 5°	15.8	17.0	.860	.304	.546	—	—	—
	do	do	Ring 0°	15.8	17.0	.835	.277	.558	—	—	—
	do	do	Ring -5°	15.8	17.0	.830	.306	.524	—	—	—
	do	do	Ring -10°	15.8	17.0	.820	.297	.523	—	—	—
	do	do	Ring -15°	15.8	17.0	.800	.322	.478	—	—	—
	do	do	Exposed cylinders	15.8	17.0	.855	.303	.492	—	—	—
	do	Ring 0°	do	15.8	17.0	.860	.312	.538	.670	.071	.599
	do	Ring -5°	do	15.8	17.0	.800	.254	.536	.670	.057	.613
	do	Ring -10°	do	15.8	17.0	.780	.261	.529	.680	.045	.615
	do	Ring 4°	Ring 5°	15.8	17.0	.805	.275	.530	.653	.038	.587
	do	Ring -5°	do	15.8	17.0	.880	.344	.536	—	—	—
	do	Ring 0°	do	15.8	17.0	.814	.288	.548	—	—	—
	do	do	Ring 10°	15.8	17.0	.870	.287	.573	.680	.072	.588
	do	do	Ring 0°	15.8	17.0	.840	.308	.534	—	—	—
3-B	Large	N.A.C.A. hood	Ring 5°	15.7	17.2	.790	.211	.579	.645	.041	.604
4-B	do	do	do	16.1	17.0	.758	.170	.588	.630	.013	.587
1-C	do	do	do	15.8	17.0	.710	.121	.589	.590	.001	.589
	Small	Exposed cylinders	Exposed cylinders	14.7	15.6	.723	.200	.523	.610	.018	.592
	do	Ring 0°	Ring 5°	14.7	15.6	.775	.271	.504	.605	.015	.590
2-C	Large	N.A.C.A. hood	do	15.8	17.0	.720	.108	.614	.605	.004	.601
3-C	do	do	do	15.8	17.0	.725	.131	.594	.605	—.002	.607