

REPORT No. 434

LIFT AND DRAG CHARACTERISTICS AND GLIDING PERFORMANCE OF AN AUTOGIRO AS DETERMINED IN FLIGHT

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SUMMARY

The results of flight tests made by the National Advisory Committee for Aeronautics on a Pitcairn "PCA-2" autogiro are presented in this report. Lift and drag coefficients with the propeller stopped have been determined over approximately a 90° range of angles of attack. Based on the sum of fixed-wing and swept-disk areas, the maximum lift coefficient is 0.895, the minimum drag coefficient with propeller stopped is 0.015, and the maximum L/D with propeller stopped is 4.8. Lift coefficients were found also with the propeller delivering positive thrust and did not differ consistently from those found with propeller stopped. Curves of gliding performance included in this report show a minimum vertical velocity of 15 feet per second at an air speed of 36 miles per hour and a flight-path angle of -17°. In vertical descent the vertical velocity is 35 feet per second.

INTRODUCTION

Research on the autogiro has been undertaken by the National Advisory Committee for Aeronautics in connection with the study of the general problem of safety in flight. The essential characteristic of the autogiro that distinguishes it from conventional airplanes is that the velocity of the lifting surfaces with respect to the air is almost entirely independent of the velocity of the machine as a whole. The value of this attribute with respect to safety lies in the increase in the useful range of air speeds at which flight may be maintained.

The determination of lift and drag characteristics was decided upon as the initial step into an extensive program of research because of the lack of reliable full-scale information on the fundamental aerodynamic characteristics of the autogiro and the need to establish clearly a datum to which further work will be referred. The curves and data contained in the body of this report constitute, so far as is known, the first authentic full-scale information concerning autogiro characteristics that has been published. This report presents the results of a series of glide tests, made to determine the lift and drag characteristics of a Pitcairn PCA-2 autogiro over the full range of angles

of attack. The tests were performed by the National Advisory Committee for Aeronautics at Langley Field, Va.

APPARATUS AND METHODS

The tests were performed on a Pitcairn PCA-2 autogiro, shown in Figure 1. The essential physical characteristics of the autogiro are as follows:

Rotor		Symbol	
Number of blades.....	b	4	
Profile of section.....		Göttingen 429.	
Diameter.....	$2R$	45.0 ft.	
Blade chord (outer straight portion).....	c	1.833 ft.	
Disk area.....	S_D	1,588 sq. ft.	
Solidity.....	Total blade area/disk area.....	0.0976.	
Wing			
Profile.....		Modified N.A.C.A.-M3.	
Span.....		30 ft. 3 $\frac{3}{4}$ in.	
Chord—root.....		4 ft. 4 in.	
Area—projected.....	S_W	101 sq. ft.	
Aspect ratio.....		9.1.	
Incidence.....		1.7°.	
General			
Total area.....	$S = S_D + S_W$	1,689 sq. ft.	
Gross weight as flown.....	W	2,940 lb.	
Wing loading.....	W/S	1.74 lb./sq. ft.	
Engine.....		Wright R-975.	
Power—rated.....		300 hp	

The essential quantities necessary to a determination of lift and drag characteristics are dynamic pressure, flight-path angle, and attitude angle. Measurements of dynamic pressure and flight-path angle were obtained during a portion of the tests from an N. A. C. A. flight-path-angle and air-speed recorder suspended 80 feet below the aircraft. (Reference 1.) Subsequently it became necessary to alter the standard instrument so that it could record glides at an angle as great as 90°. The alteration consisted of the incorporation in the instrument of a yoke suspension and a 90° inclinometer unit, the yoke being shown in Figure 2. At low speeds, however, the instrument proved to be unstable and the inclinometer failed to function. An alternate method of obtaining flight-path angle was applied, in which the vertical velocity was calculated from a time history of altitude obtained by the observer with a sensitive altimeter and battery of stop watches. Flight-path angle followed directly

from the ratio between the vertical velocity and true air speed. The attitude of the autogiro was recorded

lack of reliable information on the propeller characteristics, no attempt was made to calculate thrust directly



FIGURE 1.—Three-quarter view of PCA-8 autogiro

by a pendulum-type inclinometer (reference 1) fixed in the fuselage.

Complementary quantities required during the glide tests included air density, control position, rotor speed, and, in a few cases, engine speed. Data from which air density was calculated were obtained by visual observations of a liquid-in-glass type thermometer placed in the air stream and a sensitive altimeter in the observer's cockpit. During a part of the tests atmospheric pressure was recorded by an aneroid-type recording altimeter, but the observations of pressure altitude proved to be a more desirable method. Rotor speeds were obtained visually by the pilot or observer from the indicating tachometer installed in the aircraft. In auxiliary tests made with positive thrust, the pilot also noted engine speed from the engine tachometer.

The flight tests consisted principally of steady 30-second glides at angles of attack ranging approximately from 0° to 90° with the propeller stopped in a vertical position by means of a brake. From the average values of dynamic pressure, attitude angle, and flight-path angle given by the continuous records obtained in each glide, the lift and drag characteristics were calculated as described in reference 2. A correction was made for the drag of the suspended instrument from data given in reference 2.

In order to determine the effect of the slipstream on the rotor characteristics, an auxiliary group of glide tests was made with the propeller rotating at sufficient speed to develop varied small amounts of positive thrust. Test procedure in this case was identical with that when the propeller was stopped. Owing to the

from engine speed and air speed. The magnitude of the thrust was closely approximated by a considera-

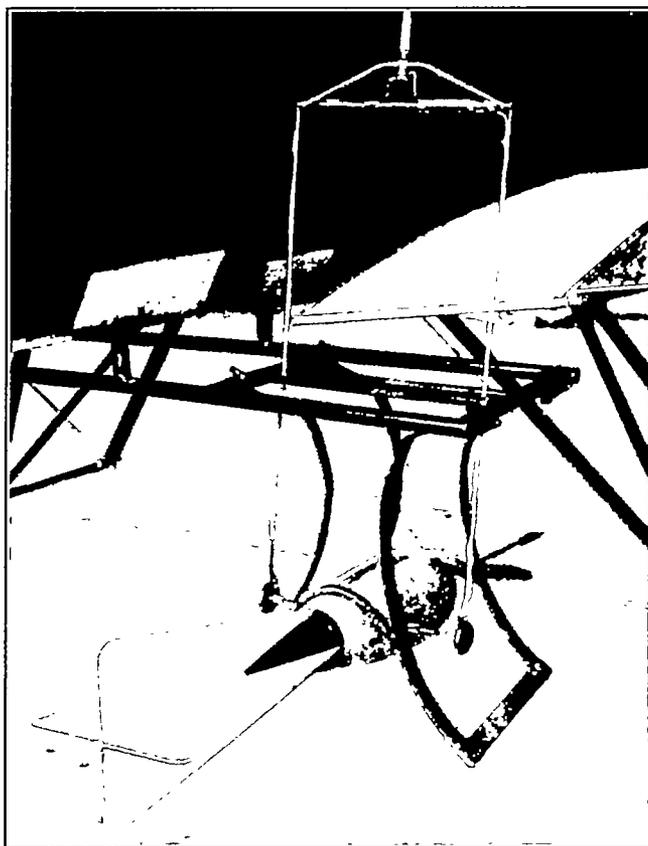


FIGURE 2.—Swivel suspension for flight-path-angle and air-speed recorder

tion of the change in flight-path angle from that at the same air speed with propeller stopped, using a pro-

propeller-drag coefficient calculated from the curves given in reference 3.

RESULTS

The lift and drag characteristics of the autogiro are presented in Figures 3 and 4 and in Tables I and II. The area to which the force coefficients are referred is the sum of the swept-disk area and the fixed-wing

the state of operation of an autogiro rotor, is defined by the equation

$$\mu = \frac{V \cos \alpha}{\Omega R}$$

where V —true air speed, feet per second.

α —angle of attack, degrees.

Ω —rotor angular velocity, radians per second.

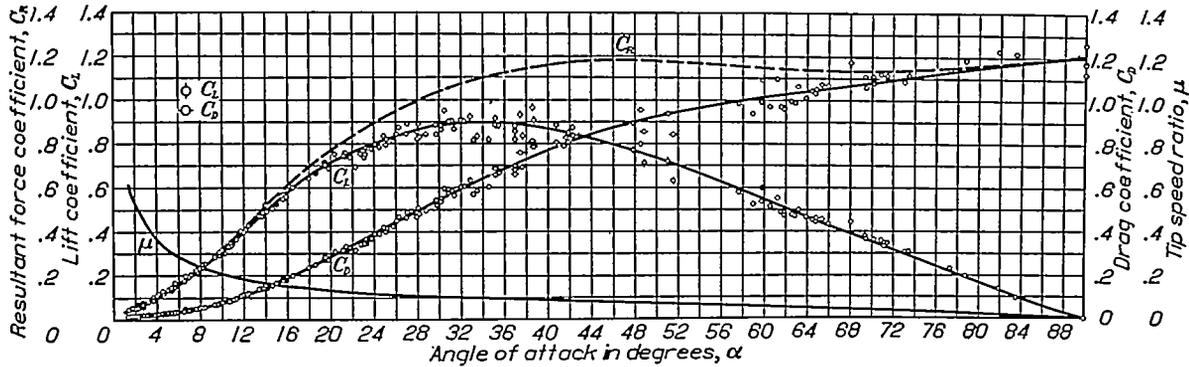


FIGURE 3.—Characteristic curves for PCA-3 autogiro

area, the wing being considered as extending through the fuselage. The use of the swept-disk area is arbitrary, but an arbitrary selection is necessary, inasmuch as the predominating velocity of the rotor blades is not the velocity of flight. The inclusion of the fixed-wing area follows by analogy with a biplane. With this choice of area the coefficients are of the same order of

The effect of the calculated propeller drag upon the drag coefficient and the L/D curve against angle of attack is shown in Figure 5. The propeller drag was estimated from the curves in reference 3 and was

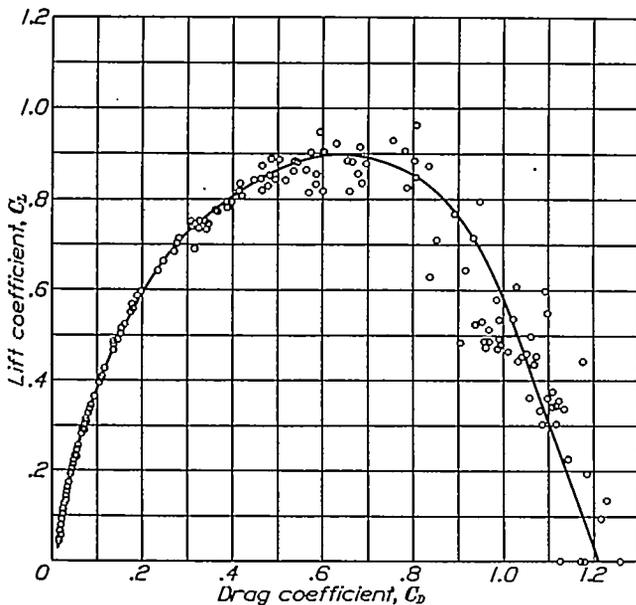


FIGURE 4.—Polar curve for PCA-3 autogiro

magnitude of those of a normal wing. The angle of attack given in the graphs and tables is the angle between the relative wind and a perpendicular to the rotor axis lying in the plane of symmetry. Drag coefficients, unless otherwise specified, have been calculated from the drag of the aircraft as flown less the drag of the suspended instrument.

The rotor parameter μ is plotted in Figure 3 against angle of attack. This parameter, which determines

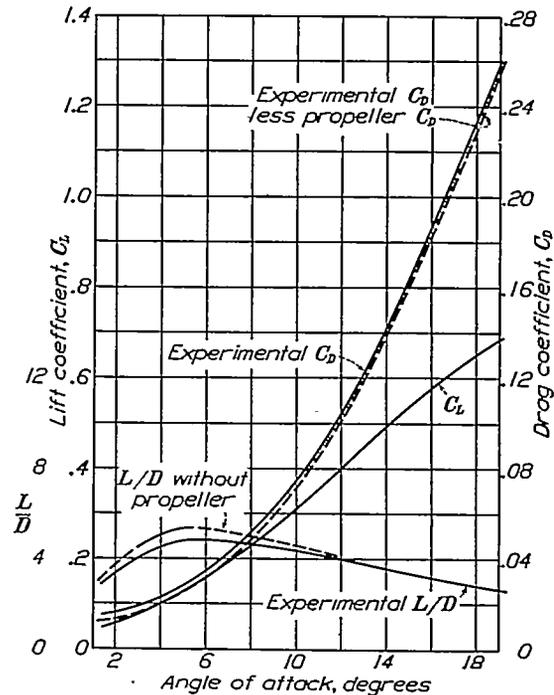


FIGURE 5.—Curves showing effect of propeller on PCA-3 autogiro characteristic curves. Estimated propeller $C_D=0.003$, propeller drag=4.98 g. (From reference 3.)

assumed constant over the range of angles of attack covered by Figure 5.

The gliding performance with stopped propeller is shown in Figures 6, 7, and 8. Figure 6 shows the variation in flight-path angle γ and indicated vertical velocity V_v , with indicated air speed. Figure 7 shows indicated vertical velocity as a function of flight-path angle. In Figure 8 vertical velocity has been plotted

against horizontal velocity, and lines of constant flight-path angle have been shown. The polar distance from the origin, indicated by the circular arcs drawn, represents the air speed along the flight path.

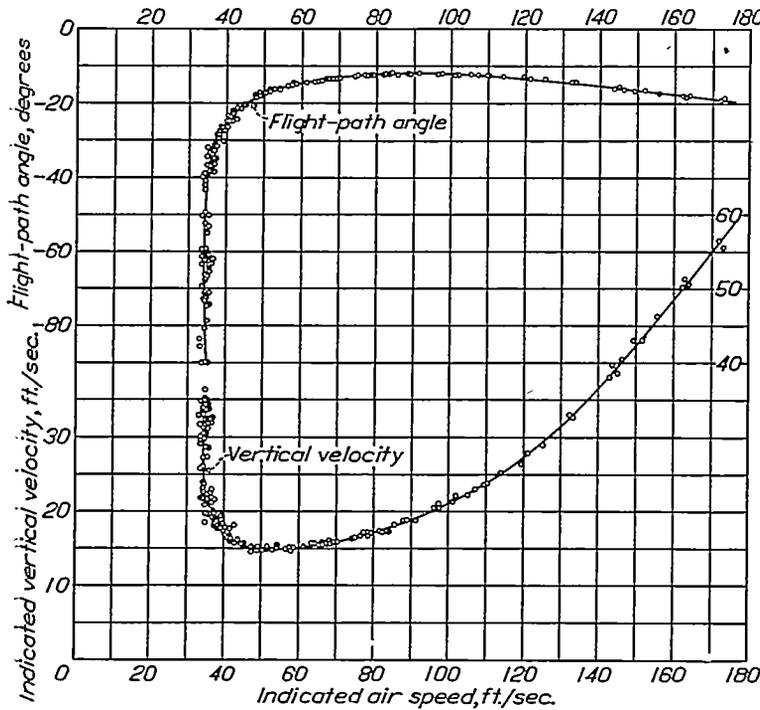


FIGURE 6.—Flight-path angle and vertical velocity as functions of air speed for PCA-2 autogiro gliding with stopped propeller

Results of the tests with positive thrust are shown in Figure 9, in which the lift coefficients obtained are plotted against angle of attack. The portion of the lift curve obtained with propeller stopped at corresponding angles of attack is shown in the same figure for comparison.

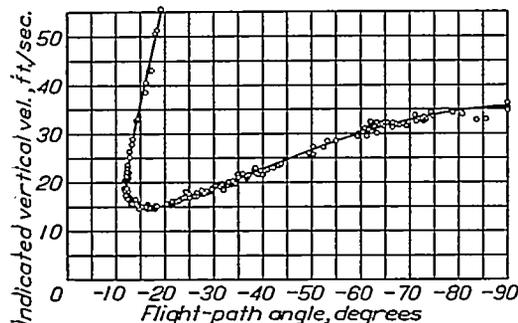


FIGURE 7.—Variation of vertical velocity with flight-path angle for PCA-2 autogiro gliding with stopped propeller

Table I presents the data obtained in glides with stopped propeller when the flight-path angle was directly measured, Table II shows the data obtained by indirect measurement of flight-path angle in glides with stopped propeller, and Table III contains the data obtained from glides with rotating propeller.

ACCURACY

The effect of accidental errors is reflected in the dispersion of experimental points on the curves. It will be noted that this dispersion increases rapidly above an angle of attack of 16°. This effect is probably a result of the errors introduced by the indirect method of determining flight-path angles at large angles of attack, augmented by the unsteadiness of the aircraft at low air speeds. The number of experimental points obtained is large enough, however, to reduce the resultant accidental errors in faired curves to a small value.

Errors consistent in sign are not indicated by the dispersion of points. The chief source of such errors is the effect of the rotor-induced flow on the magnitude and direction of the resultant air velocity in the vicinity of the suspended flight-path-angle and air-speed recorder. The effect of this flow on the alignment of the suspended instrument, as well as the effect of any inherent misalignment, was eliminated by a determination of the alignment in level flight at various speeds. The alignment thus established is believed precise to within $\pm 0.1^\circ$. The effect of the induced flow on the recorded dynamic pressure, however, was not eliminated. Calculations based on the usual wing theory indicate that the magnitude of the induced velocity at the suspended instrument is approximately $-0.013 C_R V$ where C_R is the coefficient of resultant force based on disk area. Owing to uncertainty concerning the justification for applying wing theory to this case, no correction to recorded results was applied. It is probable that at high angles of attack the error in dynamic pressure will be from -2 per cent to -3 per

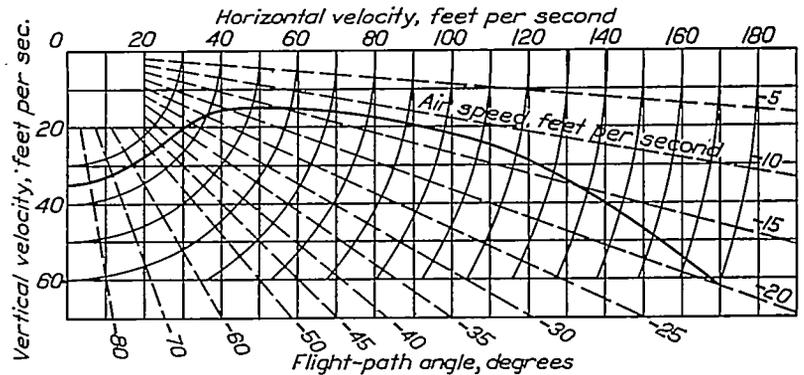


FIGURE 8.—Gliding performance curve of PCA-2 autogiro, with stopped propeller

cent, whereas at low angles of attack the correction may be safely neglected.

If the indeterminate effect of rotor-induced velocities on the suspended instrument is disregarded, it is believed that the values of the faired curves may be relied upon within the following limits:

Quantity	Angles of attack from 0° to 16°	Angles of attack from 16° to 90°
C_L	±2 per cent.....	±3 per cent.
C_D	do.....	Do.
α	±0.2°.....	±4°.
$\mu = \frac{V \cos \alpha}{\Omega R}$	±3 per cent.....	±4 per cent.
γ —flight-path angle.....	±0.1°.....	±4°.
V_s	±2 per cent.....	±2 per cent.
V	±1 per cent.....	Do.

DISCUSSION

The curves included in this report show clearly the general aerodynamic characteristics of the autogiro. The curve in Figure 3 illustrates the fact that the resultant force coefficient is almost constant at all angles of attack above that corresponding to maximum lift. The results in Figure 5 show a maximum L/D of 4.8 with propeller stopped, at a lift coefficient of 0.150, corresponding to an air speed of 67 miles per hour. By the subtraction of the estimated propeller drag, a maximum L/D of 5.3 is obtained. The curves of gliding performance (figs. 6, 7, and 8) illustrate the ability of the autogiro to descend steeply at a low air speed; when the vertical velocity is a minimum of 15 feet per second, the air speed is about 53 feet per second (36 miles per hour) and the flight-path angle is -17° . These curves also show the rapid increase in vertical velocity with any small decrease in air speed below 45 feet per second. The data in Figure 9 indicate that the presence of positive thrust has no consistent effect on the lift coefficient.

The large speed range possible for the autogiro is indicated by the ratio between C_{Lmax} and C_{Dmin} in Figure 3, the experimental value of $\frac{0.895}{0.015} = 60$ being unusually high. Comparable values for a conventional airplane would be $\frac{1.40}{0.050} = 28$. Level flight at low speeds proved difficult, however, owing to decreasing control effectiveness as air speed approached its minimum. At air speeds corresponding to the region of C_{Lmax} the aileron moments were insufficient to overcome the required engine torque. The practical speed range is then less than that indicated by the force coefficients.

The problem of control at the low air speeds and high angles of attack attainable in the autogiro demands attention. During glides at air speeds near the minimum value, corresponding to angles of attack from about 35° to 90° , lateral control was inadequate and the aircraft was unsteady. Elevator control, although sluggish, remained positive at all times, but the ailerons and rudder often proved unable to check or delay a tendency of the autogiro to roll or yaw.

CONCLUSIONS

The tests on the *PCA-2* autogiro as presented in this report lead to the following conclusions:

1. The maximum lift coefficient, based on the sum of wing and swept-disk area, is 0.895, the minimum drag coefficient with propeller stopped is 0.015, the maximum L/D with propeller stopped is 4.8, and the maximum resultant force coefficient is 1.208.
2. The resultant force coefficient is approximately constant for all angles of attack greater than that corresponding to maximum lift.
3. The minimum vertical velocity when gliding with stopped propeller is 15 feet per second, at an air speed of 36 miles per hour, and a flight-path angle of -17° .

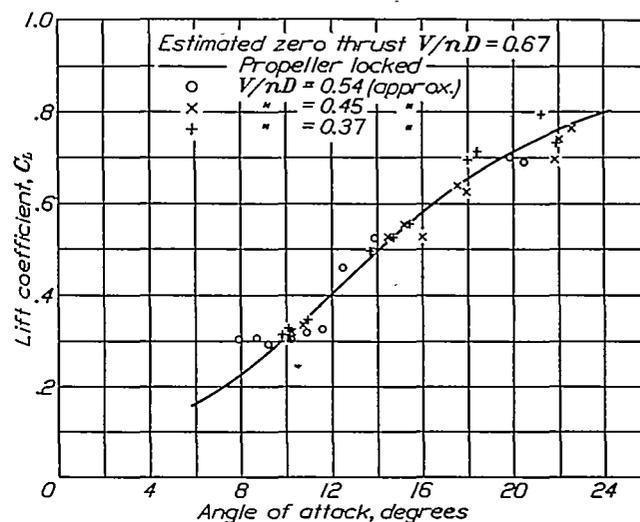


FIGURE 9.—Lift coefficient against angle of attack with varying thrust

4. The vertical velocity in a vertical descent is 35 feet per second.
5. The presence of positive thrust has no consistent influence on lift coefficient.

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NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS,
LANGLEY FIELD, VA., May 2, 1932.

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TABLE I
AUTOGIRO GLIDE TESTS—PROPELLER STOPPED

Flight No.	Run No.	Flight-path angle, γ deg.	Attitude angle, λ deg.	Angle of attack, α deg.	Weight, W lb.	Lift, L lb.	Apparent drag, D_a lb.	Bomb drag, D_b lb.	True drag, D lb.	Dynamic pressure, q lb./ft. ²	Lift coefficient, C_L	Drag coefficient, C_D	Rotor speed, Ω rad./sec.	Density, ρ slug/ft. ³	True air speed, V_T ft./sec.	μ $V \cos \alpha / \Omega R$
A-5	1	-15.4	-13.1	2.3	2,904	2,800	771	16	755	23.0	0.087	0.018				
	2	-16.5	-14.1	2.4	2,868	2,750	815	16	799	27.4	.060	.017				
	3	-18.0	-15.8	2.2	2,832	2,690	875	16	859	31.9	.050	.016				
	4	-18.7	-17.3	1.4	2,796	2,650	898	16	882	35.6	.044	.015				
	5	-16.0	-13.3	2.7	2,899	2,790	800	16	784	24.6	.067	.019	14.3	2.05×10^{-4}	155.0	0.478
	6	-17.3	-15.0	2.3	2,858	2,730	849	16	833	28.9	.056	.017	13.8	2.05	168.0	.535
	7	-18.0	-16.0	2.0	2,817	2,680	871	16	855	31.2	.051	.016	13.5	2.08	173.4	.569
	8	-19.2	-17.7	1.5	2,776	2,620	914	16	898	36.1	.044	.015	13.2	2.08	184.0	.618
A-6	1	-14.5	-11.3	3.2	2,912	2,820	728	15	713	20.8	.081	.020	14.3	2.04	143.0	.440
	2	-16.1	-13.8	2.3	2,884	2,770	799	16	783	25.5	.065	.018	14.3	2.03	163.6	.489
	3	-18.4	-16.7	1.7	2,856	2,710	802	16	886	31.5	.051	.017	13.6	2.05	175.6	.571
	6	-16.8	-14.1	2.7	2,772	2,650	802	16	786	26.4	.060	.018	14.1	2.08	169.7	.500
A-12	1	-12.3	-5.4	6.9	2,904	2,840	619	10	609	8.7	.193	.042	15.6	2.02	93.0	.262
	2	-12.3	-6.5	5.8	2,904	2,840	619	12	607	11.0	.152	.033	15.4	2.09	102.7	.294
	3	-12.3	-7.7	4.5	2,904	2,840	613	13	600	13.1	.123	.027	15.1	2.15	110.8	.324
	4	-12.4	-8.3	4.1	2,868	2,800	617	14	603	14.3	.116	.025	15.4	2.02	119.1	.342
	5	-13.3	-9.5	3.8	2,868	2,790	660	15	645	17.4	.094	.022	14.9	2.12	128.3	.382
	6	-14.2	-11.1	3.1	2,868	2,730	703	15	688	21.1	.077	.019	14.6	2.20	138.8	.419
	7	-12.2	-5.7	6.5	2,832	2,770	598	10	588	9.4	.174	.037	15.3	2.01	96.8	.270
	8	-12.4	-6.8	5.6	2,832	2,770	609	12	597	11.3	.145	.031	15.1	2.10	104.0	.304
	9	-12.4	-7.8	4.6	2,796	2,730	601	13	588	13.6	.119	.026	15.2	2.08	114.6	.333
	10	-12.8	-8.8	4.0	2,796	2,730	618	14	604	15.4	.104	.023	14.9	2.16	119.7	.356
A-13	1	-12.5	-7.2	5.3	2,904	2,830	627	13	614	12.4	.135	.030	15.5	2.02	110.9	.316
	2	-12.4	-8.3	4.1	2,904	2,840	625	14	611	14.5	.116	.025	15.2	2.08	118.0	.343
	3	-12.8	-9.1	3.7	2,868	2,800	634	14	620	17.0	.097	.022	15.2	2.02	129.8	.378
	4	-13.4	-9.7	3.7	2,868	2,790	666	15	651	18.6	.083	.021	15.1	2.10	133.3	.390
	5	-12.2	-6.9	5.3	2,832	2,770	598	12	586	11.3	.145	.031	14.9	2.00	106.3	.310
	6	-13.3	-3.7	9.6	2,832	2,750	651	8	645	5.6	.282	.068	15.0	2.05	73.7	.216
	7	-12.3	-4.7	7.6	2,832	2,770	605	8	595	7.3	.223	.043	15.2	2.10	83.6	.242
	8	-12.0	-5.4	6.6	2,796	2,730	581	9	572	8.3	.198	.041	15.2	2.02	90.5	.262
	9	-12.0	-5.4	6.6	2,796	2,730	581	10	571	9.3	.176	.037	15.2	2.08	94.8	.282
	10	-13.7	-3.7	10.0	2,796	2,710	663	6	657	5.1	.315	.076	15.4	2.10	69.7	.200
A-14	1	-13.1	-3.8	9.3	2,892	2,810	657	7	650	5.9	.293	.066	15.4	1.99	76.3	.218
	2	-12.6	-4.4	8.2	2,892	2,820	630	8	622	6.7	.248	.055	15.2	2.05	80.8	.233
	3	-12.1	-4.4	8.2	2,892	2,830	607	9	598	8.1	.206	.044	15.1	2.10	88.0	.253
	4	-11.9	-4.4	8.2	2,892	2,830	596	9	587	8.4	.199	.047	15.0	2.15	88.5	.253
	5	-12.1	-6.5	5.6	2,850	2,780	599	12	587	11.3	.148	.031	15.3	2.05	105.1	.303
	6	-12.4	-4.7	7.7	2,850	2,780	613	9	604	7.5	.219	.048	15.2	2.12	84.0	.243
	7	-12.4	-4.8	7.6	2,850	2,780	613	8	605	7.3	.224	.049	14.9	2.16	82.4	.243
	8	-12.3	-5.2	7.1	2,808	2,740	598	9	589	8.0	.204	.044	15.2	2.02	88.6	.267
	9	-11.9	-6.2	5.7	2,808	2,750	579	11	568	9.9	.184	.034	15.1	2.07	97.9	.286
	10	-12.2	-7.2	5.0	2,808	2,740	593	13	581	12.2	.133	.028	14.9	2.14	106.0	.316
A-19	1	-14.1	-3.3	10.8	2,886	2,800	705	6	699	4.9	.336	.083	15.5	1.99	70.4	.198
	2	-13.3	-3.7	9.6	2,886	2,810	664	7	657	5.7	.291	.068	15.3	2.02	75.2	.215
	3	-12.8	-4.4	8.4	2,886	2,810	638	8	630	6.6	.254	.067	15.2	2.06	79.8	.230
	4	-12.7	-4.8	7.9	2,886	2,810	635	8	627	7.2	.231	.054	15.0	2.11	82.5	.242
	5	-14.4	-3.1	11.3	2,850	2,760	710	5	705	4.5	.364	.093	15.3	2.00	66.8	.190
	6	-13.5	-3.8	9.7	2,850	2,770	665	6	659	5.4	.305	.072	15.2	2.03	73.0	.210
	7	-12.6	-4.4	8.2	2,850	2,780	621	8	613	7.0	.234	.052	15.0	2.09	81.9	.240
	8	-12.5	-4.8	7.7	2,850	2,780	616	8	608	7.5	.219	.048	14.9	2.14	83.6	.247
	9	-14.0	-3.4	10.6	2,832	2,750	685	6	679	4.9	.330	.081	15.2	2.00	70.2	.201
	10	-13.5	-3.8	9.7	2,832	2,750	660	7	653	5.6	.292	.069	15.0	2.04	73.7	.215
A-20	1	-16.1	-2.7	13.4	2,886	2,770	800	4	796	3.5	.471	.135	15.3	1.99	59.2	.167
	2	-14.3	-3.3	11.0	2,886	2,800	713	6	707	4.8	.345	.087	15.2	2.03	68.6	.190
	3	-13.5	-3.5	10.0	2,886	2,800	673	6	666	5.2	.316	.075	15.2	2.08	71.0	.200
	4	-16.5	-2.5	14.0	2,886	2,770	820	4	816	3.2	.516	.152	15.2	2.12	54.7	.150
	5	-14.1	-3.3	10.8	2,844	2,760	694	6	688	4.8	.342	.085	15.1	1.99	69.5	.190
	6	-13.5	-3.8	9.7	2,844	2,730	711	6	705	5.6	.390	.074	15.2	2.03	74.0	.200
	7	-15.4	-3.0	12.4	2,844	2,740	757	5	752	3.8	.427	.117	15.2	2.10	60.1	.160
	8	-14.0	-3.4	10.6	2,844	2,760	689	6	683	5.1	.320	.079	15.2	2.14	68.9	.190
	9	-14.7	-3.0	11.7	2,814	2,720	715	5	710	4.0	.402	.105	15.2	1.96	63.9	.170
	10	-13.7	-3.7	10.0	2,814	2,730	667	6	661	5.2	.308	.074	15.4	2.00	72.4	.205
A-21	2	-18.4	-1.9	16.5	2,880	2,730	910	3	907	2.7	.597	.196				
	4	-18.0	-2.0	16.0	2,832	2,690	875	3	872	2.7	.588	.188				
	6	-18.0	-2.1	15.9	2,832	2,690	875	3	872	2.9	.556	.178				
	8	-17.6	-2.0	15.6	2,796	2,660	844	3	841	2.9	.560	.174				
	10	-17.1	-2.1	15.0	2,796	2,670	821	4	817	3.0	.523	.160				
A-22	2	-16.5	-2.4	14.1	2,880	2,760	818	4	814	3.5	.490	.145				
	3	-17.7	-2.1	15.6	2,880	2,740	875	3	872	2.9	.568	.178				
	4	-16.2	-2.6	13.6	2,880	2,760	804	4	800	3.5	.468	.136				
	5	-17.6	-2.1	15.5	2,844	2,710	859	3	856	2.9	.560	.177				
	6	-14.9	-2.9	12.0	2,844	2,750	731	5	726	4.1	.396	.104				
	7	-10.2	-2.4	13.8	2,844	2,730	794	4	790	3.3	.485	.140				
	8	-14.8	-2.9	11.9	2,844	2,750	725	5	720	4.1	.396	.103				
	9	-16.9	-2.3	14.6	2,808	2,700	820	4	816	3.2	.503	.152				
	10	-15.2	-3.0	12.2	2,808	2,720	739	5	734	4.0	.407	.110				

TABLE II
AUTOGIRO GLIDE TESTS—PROPELLER STOPPED

Flight No.	Run No.	Vert. velocity V, ft./sec.	Flight-path angle, γ deg.	Attitude angle, λ deg.	Angle of attack, α deg.	Weight, W lb.	Lift, L lb.	Apparent drag, D_a lb.	Bomb drag, D_b lb.	True drag, D lb.	Dynamic pressure, q lb./ft. ²	Lift coefficient, C_L	Drag coefficient, C_D	Rotor speed, Ω rad./sec.	Density, ρ slug/ft. ³	True airspeed, V_T ft./sec.	μ $V \cos \alpha / MR$
A-26	1	19.0	-24.9	-1.3	23.1	2,850	2,570	1,200	2	1,193	2.1	0.734	0.341	-----	2.04x10 ⁻³	45.1	-----
	2	20.0	-23.6	-1.6	23.0	2,840	2,480	1,401	2	1,399	1.7	.851	.481	-----	2.08	40.7	-----
A-26A	1	19.5	-27.5	-1.7	25.8	2,886	2,560	1,331	2	1,329	1.9	.803	.420	-----	2.11	42.2	-----
	2	19.6	-29.6	-1.5	23.1	2,968	2,600	1,418	2	1,418	1.7	.887	.503	-----	2.10	39.7	-----
	3	22.9	-39.0	-1.5	37.5	2,850	2,210	1,794	2	1,792	1.4	.929	.754	-----	2.13	36.4	-----
	4	17.4	-22.9	-1.7	21.2	2,832	2,610	1,103	2	1,101	2.1	.741	.313	-----	2.08	44.6	-----
	5	20.9	-32.4	-1.5	30.9	2,814	2,380	1,510	2	1,503	1.6	.801	.572	-----	2.05	39.0	-----
	6	19.5	-23.6	-1.6	27.0	2,798	2,450	1,339	2	1,337	1.7	.844	.461	-----	2.07	40.7	-----
	7	18.6	-25.5	-1.7	23.8	2,778	2,510	1,195	2	1,193	1.9	.771	.366	-----	2.05	43.3	-----
	8	18.3	-24.8	-1.6	23.2	2,760	2,500	1,168	2	1,166	2.0	.747	.346	-----	2.09	43.5	-----
	9	20.4	-30.4	-1.6	23.8	2,742	2,670	1,388	2	1,386	1.7	.841	.493	-----	2.05	40.3	-----
A-27	1	18.9	-23.0	-1.7	26.3	2,868	2,530	1,350	2	1,348	1.7	.872	.464	15.0	2.12	40.2	0.103
	2	17.4	-21.5	-1.7	19.8	2,856	2,650	1,048	2	1,046	2.3	.635	.370	15.2	2.04	47.4	.123
	3	19.3	-23.7	-1.6	27.1	2,844	2,600	1,367	2	1,365	1.7	.888	.484	15.2	2.06	40.2	.109
	4	17.4	-22.9	-1.6	21.3	2,832	2,610	1,102	2	1,100	2.1	.741	.313	15.0	2.09	44.7	.122
	5	19.1	-26.8	-1.6	25.2	2,820	2,620	1,272	2	1,270	1.8	.819	.412	15.0	2.04	42.3	.111
	6	21.7	-33.0	-1.6	31.4	2,803	2,630	1,530	2	1,528	1.6	.865	.561	15.2	2.04	39.8	.098
	7	18.2	-25.0	-1.7	23.3	2,796	2,560	1,180	2	1,178	1.9	.778	.361	14.9	2.06	43.1	.117
	8	18.5	-23.5	-1.6	24.9	2,784	2,490	1,245	2	1,243	1.8	.834	.416	15.0	2.06	41.4	.110
A-28	1	16.9	-20.4	-1.8	18.6	2,860	2,690	993	3	995	2.4	.663	.246	15.4	2.04	48.4	.133
	2	17.8	-23.2	-1.7	21.5	2,843	2,613	1,120	3	1,117	2.1	.745	.318	15.4	2.03	45.2	.121
	3	18.3	-24.3	-1.5	22.8	2,826	2,676	1,164	3	1,161	2.0	.760	.339	15.2	2.06	44.4	.119
	5	18.9	-23.7	-1.6	25.1	2,804	2,603	1,269	2	1,257	1.9	.792	.397	15.1	2.11	42.1	.112
	6	20.4	-29.9	-1.7	28.2	2,787	2,417	1,391	2	1,389	1.7	.820	.478	15.2	2.06	40.9	.108
	7	19.1	-27.8	-1.7	23.1	2,770	2,450	1,294	2	1,292	1.7	.841	.446	15.1	2.06	40.9	.108
	8	19.1	-27.8	-1.7	23.1	2,770	2,450	1,294	2	1,292	1.7	.841	.446	15.1	2.06	40.9	.108
A-30	2	20.3	-29.5	-1.5	28.0	2,900	2,520	1,430	2	1,428	1.8	.819	.464	15.0	2.15	41.2	.106
	3	24.2	-38.5	-1.5	37.0	2,890	2,260	1,800	2	1,798	1.6	.817	.659	15.0	2.14	38.8	.092
	4	23.7	-33.4	-1.4	37.0	2,880	2,280	1,790	2	1,788	1.6	.855	.678	14.9	2.14	38.2	.091
	5	23.0	-40.0	-1.4	36.6	2,870	2,200	1,847	2	1,845	1.4	.962	.807	15.1	2.11	35.8	.082
	6	23.4	-38.5	-1.5	37.0	2,860	2,240	1,775	2	1,773	1.5	.873	.695	15.0	2.14	37.6	.089
	7	24.3	-42.3	-1.5	40.8	2,840	2,100	1,910	2	1,903	1.4	.883	.801	14.9	2.15	36.1	.082
	8	20.2	-31.3	-1.6	29.7	2,830	2,410	1,471	2	1,469	1.6	.884	.539	14.9	2.15	38.8	.100
	9	20.3	-31.7	-1.5	30.2	2,820	2,400	1,482	2	1,480	1.6	.880	.543	14.8	2.16	38.6	.100
	A-31	1	21.0	-33.8	-1.5	32.3	2,860	2,376	1,590	2	1,588	1.6	.901	.602	14.8	2.18	37.8
2		20.5	-31.7	-1.5	30.2	2,845	2,420	1,493	2	1,494	1.7	.862	.535	14.8	2.18	39.0	.099
3		23.0	-40.3	-1.4	43.9	2,830	1,908	2,177	2	2,175	1.5	.709	.832	14.8	2.18	37.2	.071
4		22.4	-37.0	-1.5	35.5	2,815	2,249	1,695	2	1,693	1.5	.881	.665	14.8	2.18	37.2	.089
5		22.3	-33.7	-1.5	35.2	2,800	2,245	1,674	2	1,672	1.5	.883	.655	14.8	2.16	37.3	.090
6		24.7	-43.3	-1.4	41.9	2,785	2,027	1,910	2	1,908	1.4	.847	.803	14.8	2.17	36.0	.079
7		23.3	-32.4	-1.3	31.1	2,770	2,194	1,590	2	1,588	1.4	.713	.933	14.8	2.20	35.7	.065
8		19.5	-32.0	-1.5	30.5	2,765	2,396	1,460	2	1,458	1.5	.949	.693	14.8	2.16	36.8	.094
A-32	1	25.0	-43.6	-1.3	42.3	2,870	2,078	1,980	2	1,978	1.4	.872	.833	14.8	2.15	36.2	.079
	2	31.3	-61.2	-1.3	59.9	2,855	1,375	2,489	2	2,487	1.4	.699	1.092	15.1	2.13	35.7	.051
	3	20.6	-32.8	-1.6	31.2	2,840	2,385	1,539	2	1,537	1.6	.904	.653	14.9	2.16	38.0	.095
	4	27.2	-50.2	-1.6	48.6	2,825	1,810	2,170	2	2,168	1.4	.794	.949	14.9	2.15	35.4	.063
	5	22.0	-36.7	-1.5	35.2	2,810	2,233	1,630	2	1,628	1.5	.815	.681	14.9	2.15	36.8	.088
	6	27.5	-49.4	-1.5	47.9	2,795	1,520	2,121	2	2,119	1.4	.767	.891	15.0	2.14	36.2	.070
	7	20.8	-33.5	-1.5	32.0	2,780	2,318	1,535	2	1,533	1.5	.905	.600	14.8	2.13	37.7	.094
	8	22.2	-35.0	-1.5	33.5	2,765	2,294	1,587	2	1,585	1.5	.831	.682	14.8	2.15	38.7	.095
	9	20.8	-34.4	-1.5	32.9	2,760	2,269	1,554	2	1,552	1.5	.821	.690	14.8	2.15	36.8	.091
A-33	1	33.4	-60.4	-1.3	63.1	2,870	1,010	2,686	2	2,684	1.4	.442	1.175	15.2	2.12	35.7	.037
	2	35.7	-74.8	-1.3	73.5	2,855	748	2,760	2	2,748	1.5	.304	1.116	15.1	2.12	37.0	.028
	3	34.1	-63.2	-1.3	61.9	2,840	1,260	2,530	2	2,528	1.6	.485	.958	15.1	2.14	38.2	.031
	4	32.6	-63.6	-1.3	61.9	2,825	1,257	2,530	2	2,528	1.6	.493	.990	15.0	2.14	37.5	.049
	5	34.9	-73.3	-1.3	73.0	2,810	805	2,692	2	2,690	1.4	.338	1.134	15.0	2.13	36.4	.031
	6	34.0	-62.0	-1.3	62.0	2,795	1,310	2,468	2	2,466	1.5	.481	.994	14.9	2.17	38.5	.034
	7	32.7	-60.9	-1.3	60.9	2,780	1,350	2,430	2	2,428	1.5	.530	.951	14.9	2.15	37.4	.034
	8	30.3	-55.0	-1.3	55.0	2,765	1,385	2,390	2	2,388	1.5	.643	.917	14.7	2.13	37.0	.034
	9	32.4	-62.3	-1.3	62.3	2,750	1,278	2,430	2	2,428	1.4	.637	1.022	14.7	2.11	36.6	.031
	10	31.1	-59.4	-1.3	59.4	2,735	1,391	2,350	2	2,348	1.4	.608	1.029	14.9	2.08	36.1	.035
A-34	1	34.4	-62.1	-1.5	60.6	2,895	1,352	2,550	2	2,548	1.6	.512	.967	15.3	2.06	38.9	.056
	2	34.3	-63.3	-1.7	61.6	2,880	1,289	2,560	2	2,558	1.6	.487	.989	15.1	2.12	38.4	.054
	3	34.3	-65.4	-1.5	63.9	2,843	1,280	2,580	2	2,578	1.5	.463	1.010	15.2	2.12	37.7	.048
	4	33.9	-64.2	-1.6	62.6	2,817	1,294	2,530	2	2,528	1.5	.479	.992	15.2	2.12	37.7	.051
	5	22.8	-35.0	-1.8	33.2	2,791	2,290	1,600	2	1,600	1.7	.813	.689	15.0	2.11	39.7	.093
	6	23.0	-36.4	-1.8	34.6	2,785	2,230	1,642	2	1,638	1.6	.817	.600	14.9	2.14	38.8	.095
	7	20.5	-31.6	-1.8	29.8	2,739	2,330	1,435	2	1,433	1.6	.841	.517	14.9	2.14	39.1	.101
	8	30.2	-53.2	-1.6	51.6	2,687	1,608	2,150	2	2,148	1.5	.629	.838	14.7	2.12	37.7	.070
	9	30.2	-53.2	-1.6	51.6	2,687	1,608	2,150	2								

TABLE II—Continued

AUTOGIRO GLIDE TESTS—PROPELLER STOPPED—Continued

Flight No.	Run No.	Vert. velocity V_v , ft./sec.	Flight-path angle, γ deg.	Attitude angle, λ deg.	Angle of attack, α deg.	Weight, W lb.	Lift, L lb.	Apparent drag, D_a lb.	Bomb drag, D_b lb.	True drag, D lb.	Dynamic pressure, q lb./ft. ²	Lift coefficient, C_L	Drag coefficient, C_D	Rotor speed, Ω rad./sec.	Density, ρ slug/ft. ³	True airspeed, V_T ft./sec.	μ $V \cos \alpha / \Omega R$	
A-40	2	36.0	-74.4	-1.3	73.1	2,880	775	2,770	2	2,768	1.5	.304	1.085	14.9	2.17x10 ⁻³	37.4	.032	
	3	37.0	-90.0	-1.4	90.0	2,860	0	2,860	2	2,838	1.4	0	1.179	15.0	2.13	36.7	0	
	5	35.4	-71.1	-1.6	69.5	2,850	923	2,700	2	2,698	1.5	.362	1.057	14.9	2.17	37.4	.039	
	6	33.3	-66.5	-1.6	64.9	2,830	1,128	2,590	2	2,588	1.5	.459	1.050	14.8	2.21	36.3	.047	
	8	33.5	-64.6	-1.7	62.9	2,790	1,197	2,520	2	2,518	1.6	.470	.987	14.6	2.20	37.1	.051	
	9	32.3	-61.6	-1.8	59.8	2,770	1,318	2,440	2	2,433	1.5	.535	.990	14.7	2.17	36.7	.056	
	10	31.3	-59.5	-1.8	57.7	2,760	1,400	2,380	2	2,378	1.4	.579	.982	14.6	2.17	36.3	.059	
	A-41	2	33.8	-67.1	-1.7	65.4	2,820	1,068	2,600	2	2,598	1.4	.453	1.072	15.1	2.13	36.7	.042
		3	33.9	-71.3	-1.9	69.4	2,780	896	2,640	2	2,633	1.4	.377	1.109	14.9	2.19	35.8	.034
		4	37.0	-90.0	-1.8	90.0	2,770	0	2,770	2	2,768	1.5	0	1.124	14.9	2.15	36.8	0
5		33.5	-67.8	-1.8	66.0	2,740	1,035	2,540	2	2,538	1.4	.436	1.067	14.9	2.15	36.2	.041	
6		34.1	-63.7	-1.8	61.9	2,720	299	2,700	2	2,698	1.3	.136	1.227	14.6	2.21	34.3	.012	
7		33.2	-66.5	-2.0	64.5	2,690	1,072	2,470	2	2,468	1.4	.432	1.040	14.8	2.14	36.2	.043	
A-42		1	36.8	-90.0	-1.9	90.0	2,880	0	2,880	2	2,878	1.4	0	1.238	14.9	2.14	35.5	0
	2	36.1	-80.8	-2.0	78.8	2,860	460	2,820	2	2,818	1.4	.194	1.184	15.2	2.10	36.6	.021	
	3	24.2	-41.0	-2.3	38.7	2,839	2,130	1,860	2	1,858	1.4	.906	.781	15.1	2.07	36.0	.085	
	4	32.2	-63.4	-2.1	61.3	2,810	1,233	2,610	2	2,508	1.4	.550	1.097	15.0	2.08	36.0	.031	
	8	25.2	-43.8	-2.1	41.7	2,710	1,956	1,874	2	1,872	1.4	.824	.787	14.9	2.12	36.4	.031	
	9	34.9	-85.6	-2.1	83.5	2,680	210	2,670	2	2,668	1.3	.065	1.214	14.7	2.12	35.0	.012	
	10	23.6	-39.6	-1.9	37.7	2,660	2,050	1,697	2	1,695	1.5	.832	.688	14.8	2.13	37.0	.038	

TABLE III

AUTOGIRO GLIDE TESTS—PROPELLER ROTATING

Flight No.	Run No.	Vertical velocity, V_v , ft./sec.	Dyn-amic pres-sure, q lb./ft. ²	Density, ρ slug/ft. ³	True air speed V_T ft./sec.	Flight-path angle, γ deg.	Attitude angle deg. λ	Angle of attack, α deg.	Weight, W lb.	Lift, L lb.	Lift coefficient, C_L	Normal flight path angle, γ deg.	Thrust, T lb.	Engine speed, N r. p. m.	$V/\Omega D$
A-44	1	15.4	5.5	2.16x10 ⁻³	71.0	-12.5	-2.3	10.2	2,880	2,810	0.305	-13.4	18	830	0.570
	4	15.6	5.2	2.15	69.1	-13.0	-2.1	10.9	2,840	2,770	.319	-13.7	10	820	.562
	6	17.2	2.2	2.17	45.4	-22.3	-1.8	20.5	2,820	2,610	.690	-22.1	-21	500	.005
	7	16.1	4.9	2.16	67.6	-13.8	-2.2	11.6	2,810	2,730	.327	-14.0	-14	830	.543
	9	16.5	2.2	2.16	44.9	-21.5	-1.6	18.9	2,780	2,590	.701	-22.1	19	510	.583
A-45	1	13.6	5.5	2.16	71.0	-11.0	-9	10.1	2,880	2,830	.307	-13.4	94	1,020	.405
	2	13.7	3.1	2.15	53.9	-14.7	-2	14.5	2,870	2,780	.527	-16.8	90	810	.444
	3	17.7	2.2	2.18	45.3	-23.0	-1.1	21.9	2,890	2,630	.696	-22.1	-46	610	.493
	4	13.2	4.9	2.16	67.6	-11.2	-6	10.7	2,840	2,790	.335	-14.0	115	1,010	.447
	5	13.8	2.9	2.15	52.0	-15.3	-1	15.2	2,830	2,730	.554	-17.5	95	815	.420
	6	17.0	2.1	2.16	43.6	-22.9	-9	22.0	2,820	2,600	.740	-23.3	10	610	.477
	7	12.9	5.1	2.17	68.5	-10.8	-6	10.2	2,810	2,760	.321	-13.8	122	1,020	.448
	8	14.8	3.0	2.15	52.9	-16.2	-2	16.0	2,800	2,690	.527	-17.2	34	815	.433
	9	17.2	2.0	2.15	42.8	-23.7	-1.1	22.6	2,780	2,550	.763	-24.8	43	610	.469
A-46	1	9.6	4.9	2.14	67.5	-8.2	2.7	10.9	2,880	2,850	.345	-14.0	267	1,290	.349
	2	12.3	3.0	2.13	52.8	-13.5	1.9	15.4	2,870	2,790	.557	-17.2	171	1,040	.339
	3	15.7	2.0	2.14	42.9	-21.5	-3	21.2	2,860	2,660	.795	-24.8	165	760	.377
	4	9.4	5.3	2.13	70.5	-7.6	2.2	9.8	2,840	2,810	.314	-13.6	271	1,280	.368
	5	11.6	3.3	2.14	55.3	-12.1	1.6	13.7	2,830	2,760	.498	-16.3	193	1,020	.362
	6	14.5	2.3	2.14	46.2	-18.2	-2	18.0	2,820	2,680	.693	-21.1	131	760	.400
	7	9.1	5.0	2.13	68.9	-7.6	2.5	10.1	2,810	2,790	.327	-13.9	284	1,290	.357
	8	12.0	3.0	2.13	53.7	-12.9	1.8	14.7	2,800	2,730	.526	-17.2	195	1,020	.352
	9	14.1	2.2	2.14	45.1	-18.2	.2	18.4	2,780	2,640	.716	-22.1	178	770	.391
A-51	1	15.5	2.6	2.10	49.7	-13.2	-3	17.9	2,890	2,750	.625	-18.9	22	760	.437
	2	14.4	3.1	2.11	54.4	-15.4	-1.5	13.9	2,870	2,770	.525	-16.3	44	660	.550
	3	13.2	5.5	2.11	71.9	-10.6	-2.7	7.9	2,890	2,800	.303	-13.4	91	815	.589
	4	14.8	2.5	2.12	48.5	-17.8	-3	17.5	2,890	2,690	.637	-19.5	72	750	.432
	5	14.2	3.2	2.16	54.6	-15.1	-1.3	13.8	2,810	2,710	.497	-16.6	58	670	.544
	6	14.2	5.3	2.11	70.9	-11.5	-2.8	8.7	2,790	2,730	.305	-13.6	76	820	.570
	7	16.4	2.1	2.16	43.9	-21.9	0	21.9	2,770	2,570	.731	-23.3	47	750	.390
	8	13.9	3.4	2.08	57.4	-14.0	-1.5	12.5	2,750	2,670	.460	-16.1	83	660	.580
	9	15.0	5.4	2.06	72.4	-11.9	-2.7	9.2	2,730	2,670	.292	-13.5	46	820	.589