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TECHNICAL NOTE

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STRESS-STRAIN AND ELONGATION GRAPHS FOR ALCLAD ALUMINUM-ALLOY 24S-T SHEET

By James A. Miller

National Bureau of Standards

Washington
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STRESS-STRAIN AND ELONGATION GRAPHS FOR ALCLAD ALUMINUM-ALLOY 24S-T SHEET

By James A. Miller

SUMMARY

The following properties were determined from tests on duplicate longitudinal and transverse specimens from Alclad aluminum-alloy 24S-T sheets with nominal thicknesses of 0.032, 0.064, and 0.125 inch:

Tensile and compressive stress-strain graphs and stress-deviation graphs to a strain of about 1 percent

Graphs of tangent modulus and of reduced modulus for a rectangular section against stress, in compression

Stress-strain graphs for tensile specimens tested to failure

Graphs of local elongation and elongation against gage length for tensile specimens tested to fracture

The stress-strain, stress-deviation, tangent modulus, and reduced modulus graphs are plotted on a dimensionless basis to make them applicable to material with yield strengths which differ from those of the test specimens.

INTRODUCTION

This report is the third of a series presenting data on high-strength aluminum-alloy sheet. The data are in the form of tables and graphs similar to those in the first report of the series on aluminum-alloy R301 sheet (reference 1), with the exception of the tangent modulus and reduced modulus graphs in which the modulus values are plotted against stress instead of strain. The graphs are presented in dimensionless form to make them applicable to sheets of these materials with yield strengths which differ from those of the test specimens. All data are given for duplicate specimens.

The report gives the results of tests on Alclad aluminum-alloy 24S-T sheet in thicknesses of 0.032, 0.064, and 0.125 inch, furnished by the Aluminum Company of America.

The author expresses his appreciation to Mr. P. L. Peach and Mrs. P. V. Jacobs, who assisted in the testing and in the preparation of the graphs.

This investigation was conducted at the National Bureau of Standards under the sponsorship and with the financial assistance of the National Advisory Committee for Aeronautics.

MATERIAL

The sheets were of Alclad aluminum alloy 24S in the "T" condition, as furnished by the manufacturer. The nominal thickness of the cladding on each side was 5 percent of the sheet thickness for the 0.032-inch sheet and 2.5 percent of the sheet thickness for the other two sheets.

DIMENSIONLESS DATA

Test Procedure

Tensile tests were made on two longitudinal (in direction of rolling) specimens and on two transverse (across direction of rolling) specimens from a sheet of each thickness. The specimens corresponded to specimens of type 5 described in reference 2. The specimens were tested in a beam-and-poise, screw-type testing machine of 50-kip capacity by using the 5-kip range. They were held in Templin grips. The strain was measured with a pair of Tuckerman 1-inch optical strain gages attached to opposite sheet faces of the reduced section. The rate of loading was about 2 ksi per minute.

Compressive tests were made on two longitudinal and two transverse specimens from each sheet. The specimens were rectangular strips 0.50 inch wide by 2.25 inches long. The compressive specimens were tested between hardened-steel bearing blocks in the subpress described in reference 3. The loads were applied by the testing machine used for the tensile tests. Lateral support against premature buckling was furnished by lubricated solid guides, as described in reference 4. The strain was measured with a pair of Tuckerman 1-inch optical strain gages attached to opposite edge faces of the specimen. The rate of loading was about 2 ksi per minute.

Test Results

The results of the tensile and compressive tests are given in table 1. Each value of Young's modulus in the table was taken as the slope of a least-square straight line fitted to the stress-strain curve at stresses below the point where the cladding started to yield. It was based on four times the number of points shown on the graphs for that portion of the curves. The yield strengths determined by the offset method were obtained from the stress-strain curves and the experimental values of Young's modulus. The yield strengths determined by the secant method were obtained from the stress-strain curves and values of secant modulus respectively 0.7 and 0.85 times the experimental values of Young's modulus.

Stress-Strain Graphs

The stress-strain graphs are plotted in dimensionless form in figures 1 to 6. The coordinates σ, ϵ in these graphs are defined by

$$\sigma = \frac{s}{s_1} \qquad \epsilon = \frac{Ee}{s_1}$$

where

s stress corresponding to strain e

s_1 secant yield strength (0.7E)

E Young's modulus

Composite dimensionless stress-strain graphs which show the bands within which lie the data for tests of a given kind and a given direction in the sheet are shown in figures 7 and 8. The maximum width of band in terms of σ is 0.025 in tension and 0.020 in compression. Each band represents data for six specimens; the widths might have been greater if tests had been made on a larger number of specimens. Part of the deviation of the curves from affinity may be attributed to experimental variation in the values of Young's modulus which were obtained from a relatively small region of each curve.

Stress-Deviation Graphs

Dimensionless stress-deviation graphs are shown in figures 9 to 14. The ordinates are the same as those used for the stress-strain graphs. The abscissas are the corresponding values of $\delta = \epsilon - \sigma$. All the curves intersect at the point $\sigma = 1$, $\delta = 3/7$, which corresponds to the secant yield strength (0.7E). This point is indicated on the graphs by a short vertical line.

The graphs were plotted on logarithmic paper to indicate that portion of the stress-strain curves which can be represented by the analytical expression given in reference 5

$$e = \frac{s}{E} + K\left(\frac{s}{E}\right)^n$$

This relation holds when the plot of deviation against stress on logarithmic paper is a straight line, because

$$\log\left(e - \frac{s}{E}\right) = \log K + n \log \frac{s}{E}$$

or

$$\log\ (\epsilon - \sigma) = \log K \left(\frac{s_1}{E}\right)^{n-1} + n \log \sigma$$

Each graph has a pronounced knee. It follows that the stress-strain graphs of the sheets, which have a cladding that yields at a comparatively low stress, cannot be accurately represented by a single analytical expression of the foregoing type. The graphs for longitudinal tension and compression can be approximated by two straight lines represented by two equations of the foregoing type with different sets of constants. The upper line fits the points for values of s/s_1 from somewhat below s_2/s_1 (where s_2 is the secant yield strength (0.85E)) up to 1. For these, the ratios s_1/s_2 given in table 1 can be used to obtain a value for the shape parameter n from figure 10 in reference 5. The graphs for transverse tension are curved above an approximately straight portion and the graphs for transverse compression are generally curved throughout. For these, the values of s_1/s_2 given in table 1 indicate the sharpness of the knee of the stress-strain curve and may be used for obtaining an average value of the parameter n from figure 10 of reference 5 for that portion of the graph having values of s/s_1 between s_2/s_1 and 1.

Tangent Modulus Graphs

Dimensionless graphs of tangent modulus against stress for the compressive specimens are shown in figures 15 to 20. The ordinates are the ratios of tangent modulus E_t to Young's modulus. Each value of tangent modulus was taken as the ratio of a stress increment to its strain increment for the successive pairs of points shown in the stress-strain graphs. The abscissas are the mean values of σ for the stress increments.

Most of the graphs do not show a well-defined region of constant "secondary" modulus. Nearly all the points above the knee of the curve are above the nominal values of secondary modulus based on the nominal percentage of core material in the sheet. These nominal values correspond to a value of 0.90 for E_t/E for the 0.032-inch sheet and 0.95 for the 0.064- and the 0.125-inch sheets.

The limits within which the tangent-modulus curves fall are shown in figure 21. The maximum spread in values of E_t/E is 0.06. Much of this spread can be attributed to the differences in percentage of cladding thickness of the 0.032-inch sheet and of the other sheets. An example of the use of these graphs is given in reference 6.

Reduced Modulus Graphs

Dimensionless graphs of reduced modulus against stress are shown in figures 22 to 24. The ordinates are the ratios of reduced modulus for a rectangular cross section E_r to Young's modulus, and the abscissas are the corresponding values of σ. The curves were derived from the corresponding curves of tangent modulus against stress by using the formula

$$\frac{E_r}{E} = \frac{4E_t/E}{\left(1 + \sqrt{E_t/E}\right)^2}$$

The limits of the dimensionless graphs of reduced modulus against stress are shown in figure 25. The maximum spread in values of E_r/E is 0.035.

TENSILE STRESS-STRAIN TESTS TO FAILURE

Procedure

Tensile tests to failure were made on two longitudinal and two transverse specimens from a sheet of each thickness. The specimens corresponded to specimens of type 5 described in reference 2. The tests were made in fluid-support, Bourdon-tube, hydraulic testing machines having Tate-Emery load indicators. The specimens were held in Templin grips. They were tested at a cross-head speed of about 0.1 inch per minute. Autographic load-extension curves were obtained with a Templin type stress-strain recorder by using a Peters averaging total-elongation extensometer with a 2-inch gage length and a

magnification factor of 25. Stresses based on the original cross section and corresponding strains based on the original gage length were determined from these curves. The data for the portion at and beyond the knee of each curve were combined with stress-strain data on duplicate specimens on which strain up to the knee of the curve had been measured with Tuckerman optical strain gages.

Stress-Strain Graphs

The resulting stress-strain curves are shown in figures 26 to 28. Values of tensile strength and elongation in 2 inches are given in the tables in each figure. The values of elongation usually corresponded to a strain of about 0.008 less than the maximum recorded strain under load.

LOCAL ELONGATION TESTS

Procedure

Photogrid measurements (reference 7) were made on two longitudinal and two transverse tensile specimens from a sheet of each thickness. The specimens corresponded to specimens of type 5 described in reference 2. The photogrid negative was made from the master grid described in reference 1. The specimens were coated with cold top enamel. This had been found to be less critical with respect to exposure time than the photoengraving glue mentioned in reference 7. The prints were also usually easier to measure near the fracture. The specimens were held in Templin grips and were fractured in a testing machine at a cross-head speed of about 0.1 inch per minute. Measurements of grid spacing were made by the technique described in reference 1, except that the magnification was about 100 diameters.

Graphs

The local elongation in percent of the original spacing, plotted against the distance before test from one end of the gage length, are shown in figures 29 to 34. The fracture in each case occurred in the grid spacing in which the greatest elongation took place.

The elongations in percent of the original gage length were computed for various gage lengths from the local-elongation data.

These values are plotted against gage length in figures 35 to 40. The gage lengths were plotted to a logarithmic scale to present a large range of values on a single graph.

National Bureau of Standards
Washington, D. C., June 17, 1947

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TABLE 1.- RESULTS OF TENSILE AND COMPRESSIVE TESTS ON ALCLAD ALUMINUM-ALLOY 24S-T SHEET

Specimen	Test	Direction	Sheet thickness (in.)	Young's modulus, E (ksi)	Yield strength: Offset method (offset = 0.2 percent) (ksi)	Yield strength: Secant method s_1 (0.7E) (ksi)	Yield strength: Secant method s_2 (0.85E) (ksi)	s_1/s_2	Tensile strength (ksi)	Elongation in 2 in. (percent)
032-T1L	Tensile	Longitudinal	0.0327	10,680	51.5	51.5	51.2	1.006	68.1	17.5
032-T2L	----do.----	-----do.----	.0327	10,610	51.4	51.5	51.2	1.005	68.3	19.0
032-T1T	----do.----	Transverse	.0325	10,570	44.8	44.4	39.3	1.131	66.2	18.5
032-T2T	----do.----	-----do.----	.0327	10,660	44.6	44.1	38.9	1.135	65.7	17.5
032-C1L	Compressive	Longitudinal	.0327	10,630	43.0	42.1	37.0	1.138	----	----
032-C2L	----do.----	-----do.----	.0327	10,610	43.2	42.3	37.3	1.134	----	----
032-C1T	----do.----	Transverse	.0325	10,680	47.8	47.6	43.3	1.100	----	----
032-C2T	----do.----	-----do.----	.0326	10,590	47.8	47.6	43.5	1.095	----	----
064-T1L	Tensile	Longitudinal	.0647	10,620	48.6	48.6	48.3	1.007	69.2	21.0
064-T2L	----do.----	-----do.----	.0648	10,660	48.6	48.6	48.2	1.007	68.9	21.0
064-T1T	----do.----	Transverse	.0648	10,650	42.9	42.2	37.6	1.121	66.5	20.0
064-T2T	----do.----	-----do.----	.0646	10,730	43.3	42.6	37.9	1.123	66.9	18.0
064-C1L	Compressive	Longitudinal	.0648	10,670	41.4	40.3	35.9	1.123	----	----
064-C2L	----do.----	-----do.----	.0646	10,670	41.5	40.3	36.0	1.121	----	----
064-C1T	----do.----	Transverse	.0648	10,670	46.2	45.9	42.2	1.088	----	----
064-C2T	----do.----	-----do.----	.0645	10,640	46.5	46.2	42.6	1.085	----	----
125-T1L	Tensile	Longitudinal	.1239	10,780	55.4	55.4	55.0	1.009	71.8	19.5
125-T2L	----do.----	-----do.----	.1239	10,680	55.3	55.4	54.9	1.010	71.7	19.0
125-T1T	----do.----	Transverse	.1237	10,650	46.9	46.5	40.6	1.147	69.7	19.5
125-T2T	----do.----	-----do.----	.1245	10,600	47.3	47.0	41.1	1.144	69.2	19.5
125-C1L	Compressive	Longitudinal	.1242	10,750	44.9	44.1	39.0	1.131	----	----
125-C2L	----do.----	-----do.----	.1240	10,770	45.0	44.2	39.0	1.134	----	----
125-C1T	----do.----	Transverse	.1244	10,640	50.8	50.9	46.0	1.106	----	----
125-C2T	----do.----	-----do.----	.1240	10,740	50.8	50.9	45.8	1.110	----	----

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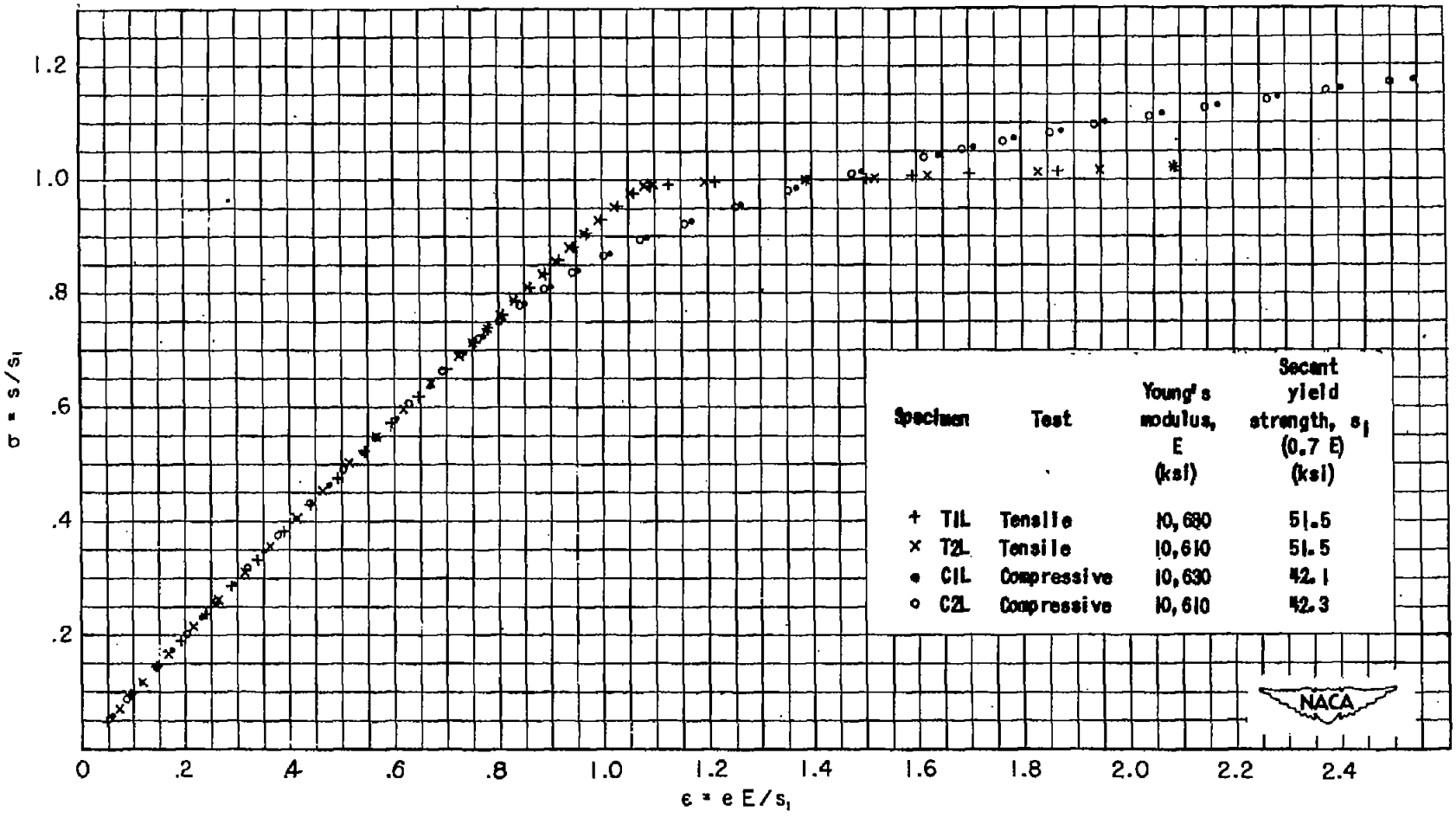

Figure 1.- Dimensionless stress-strain graphs. Alclad 24S-T sheet, longitudinal specimens 0.032 inch thick.

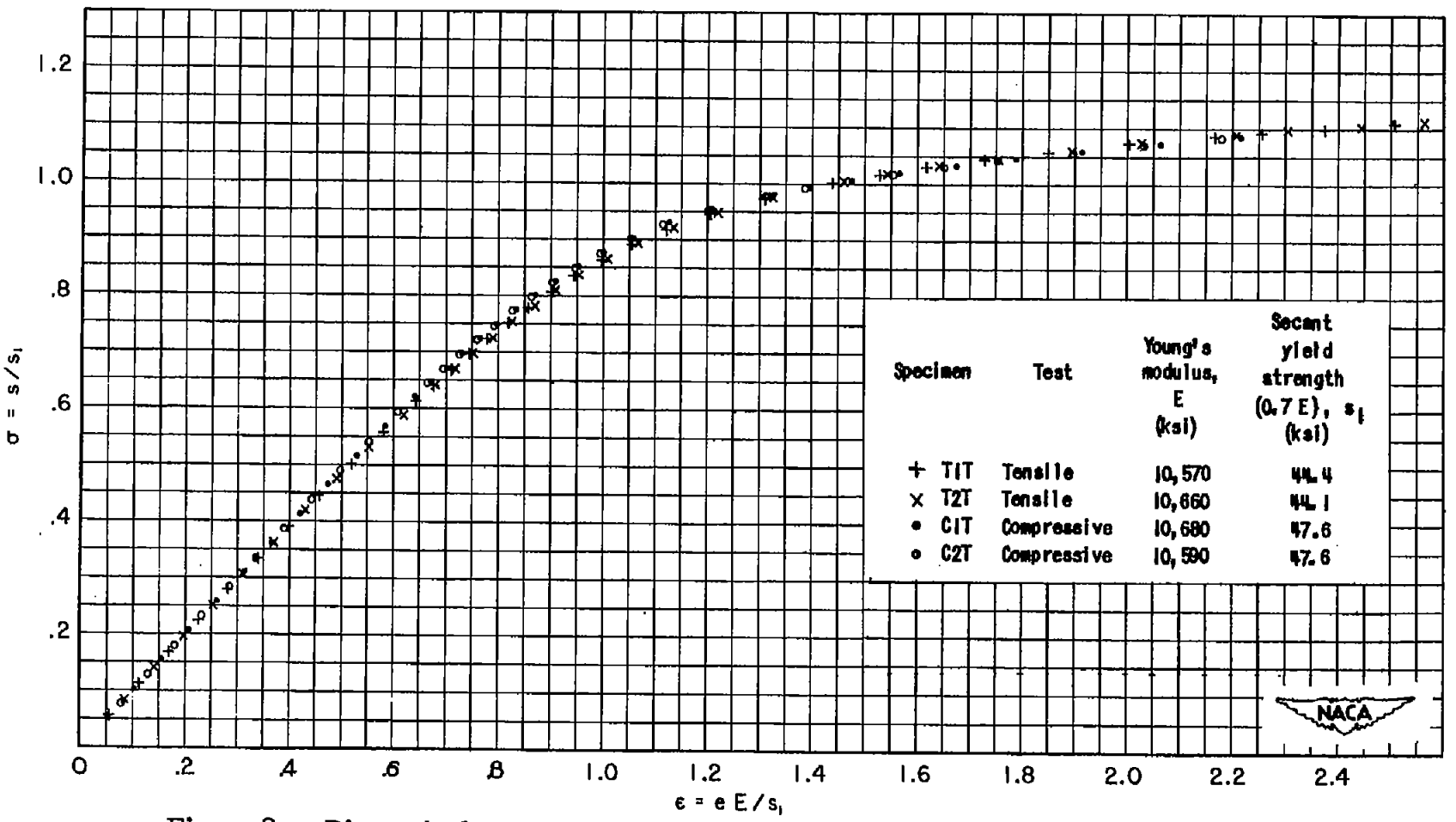

Figure 2.- Dimensionless stress-strain graphs. Alclad 24S-T sheet, transverse specimens 0.032 inch thick.

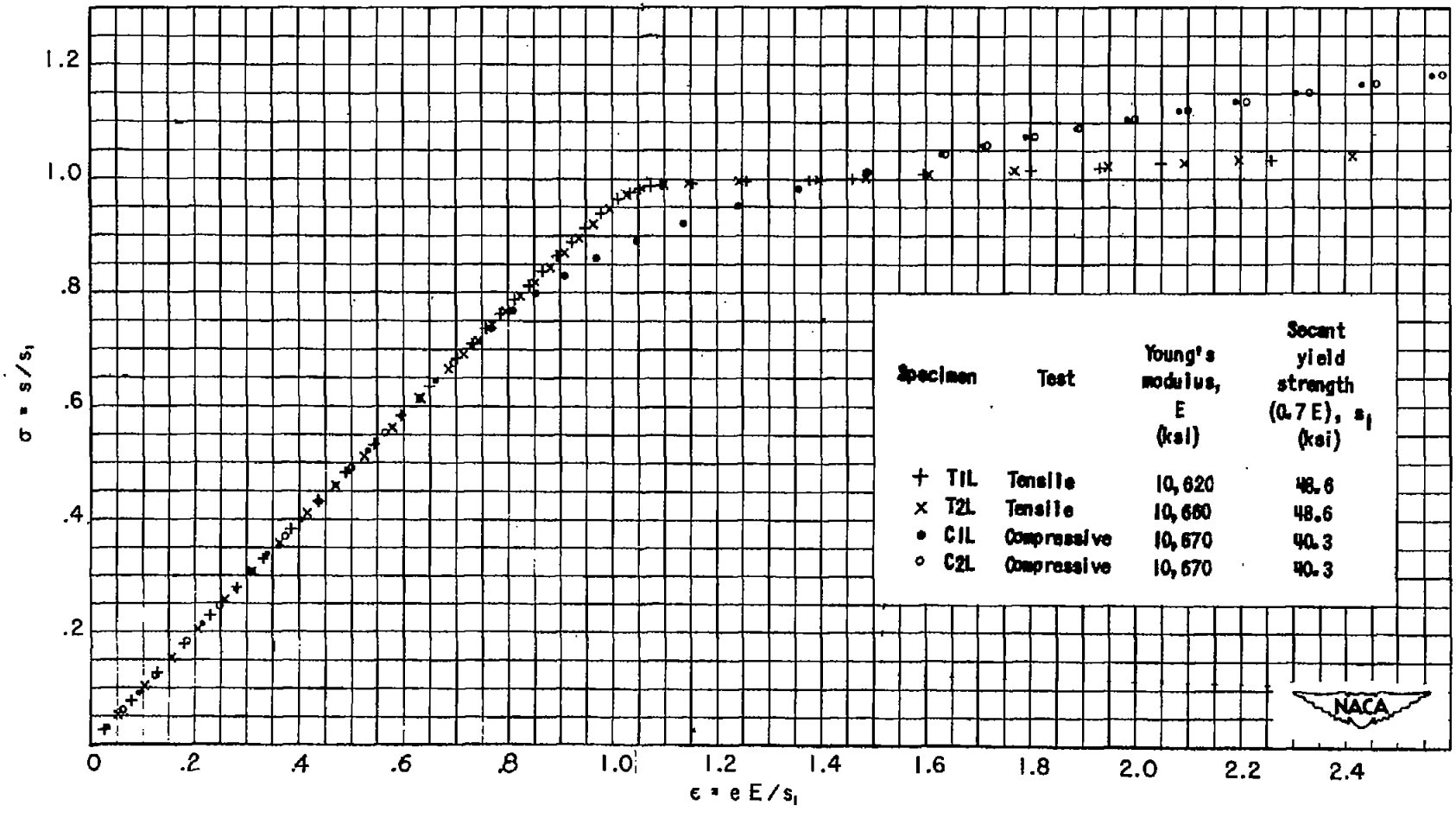

Figure 3.- Dimensionless stress-strain graphs. Alclad 24S-T sheet, longitudinal specimens 0.064 inch thick.

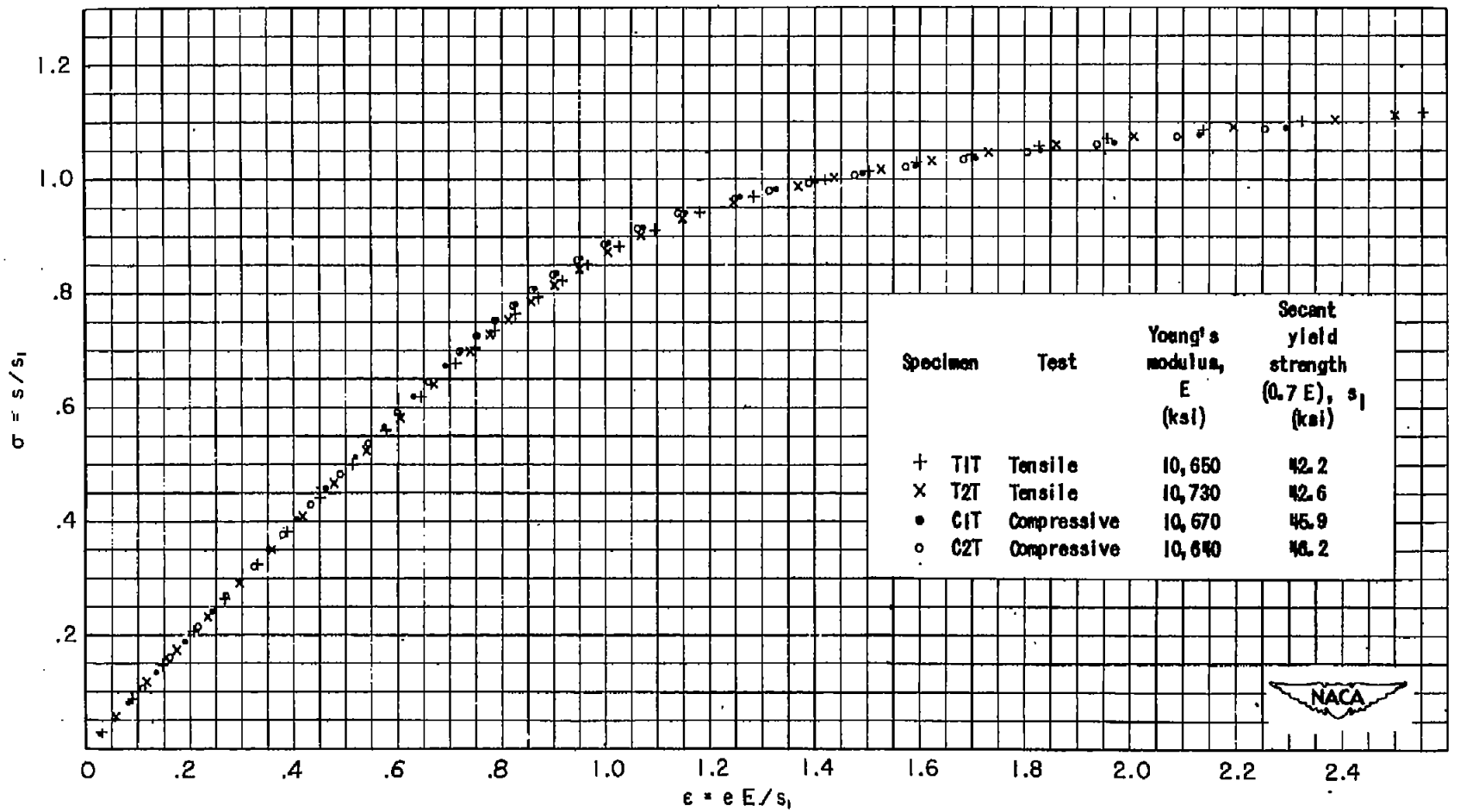

Figure 4.- Dimensionless stress-strain graphs. Alclad 24S-T sheet, transverse specimens 0.064 inch thick.

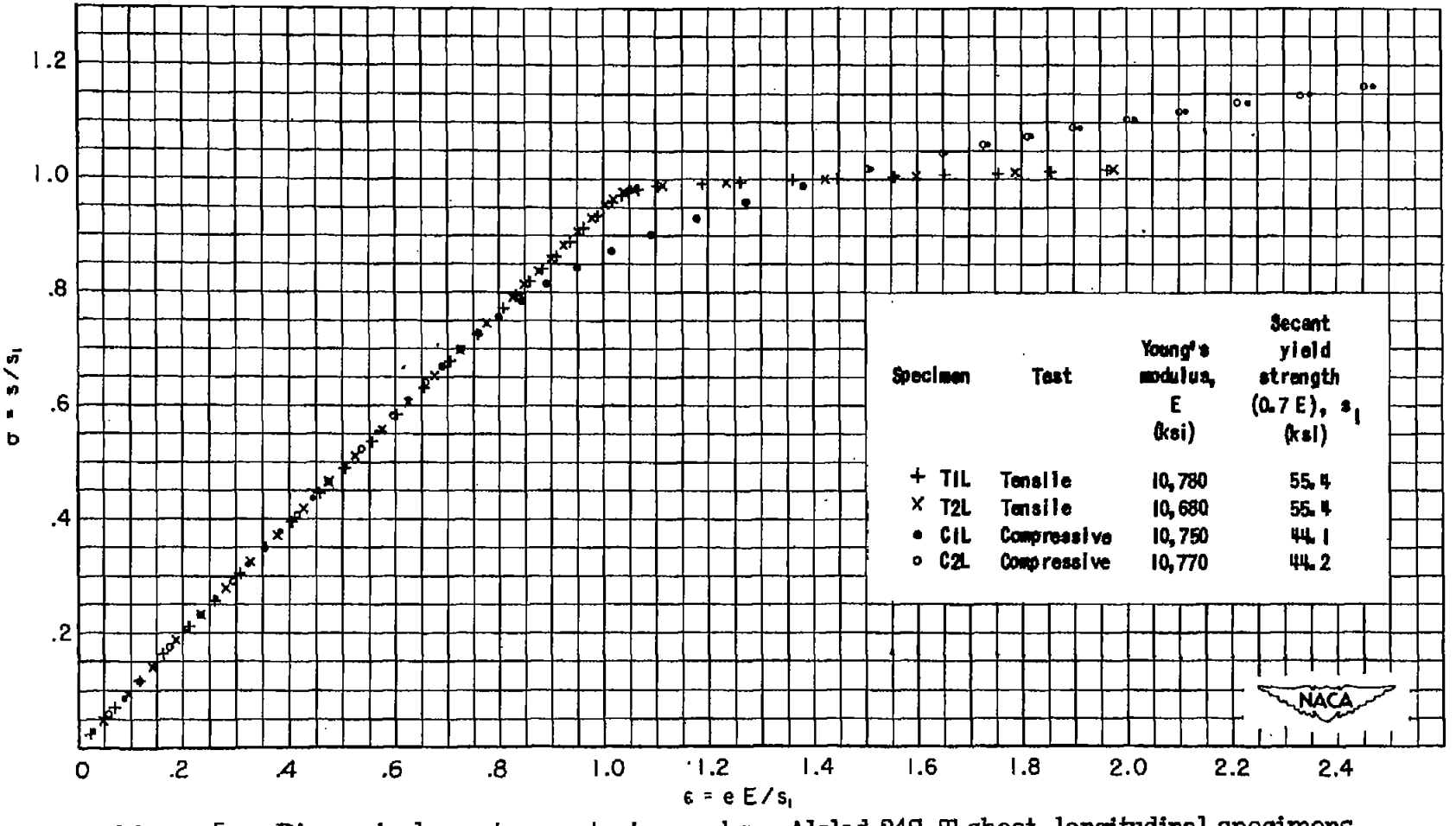

Figure 5.- Dimensionless stress-strain graphs. Alclad 24S-T sheet, longitudinal specimens 0.125 inch thick.

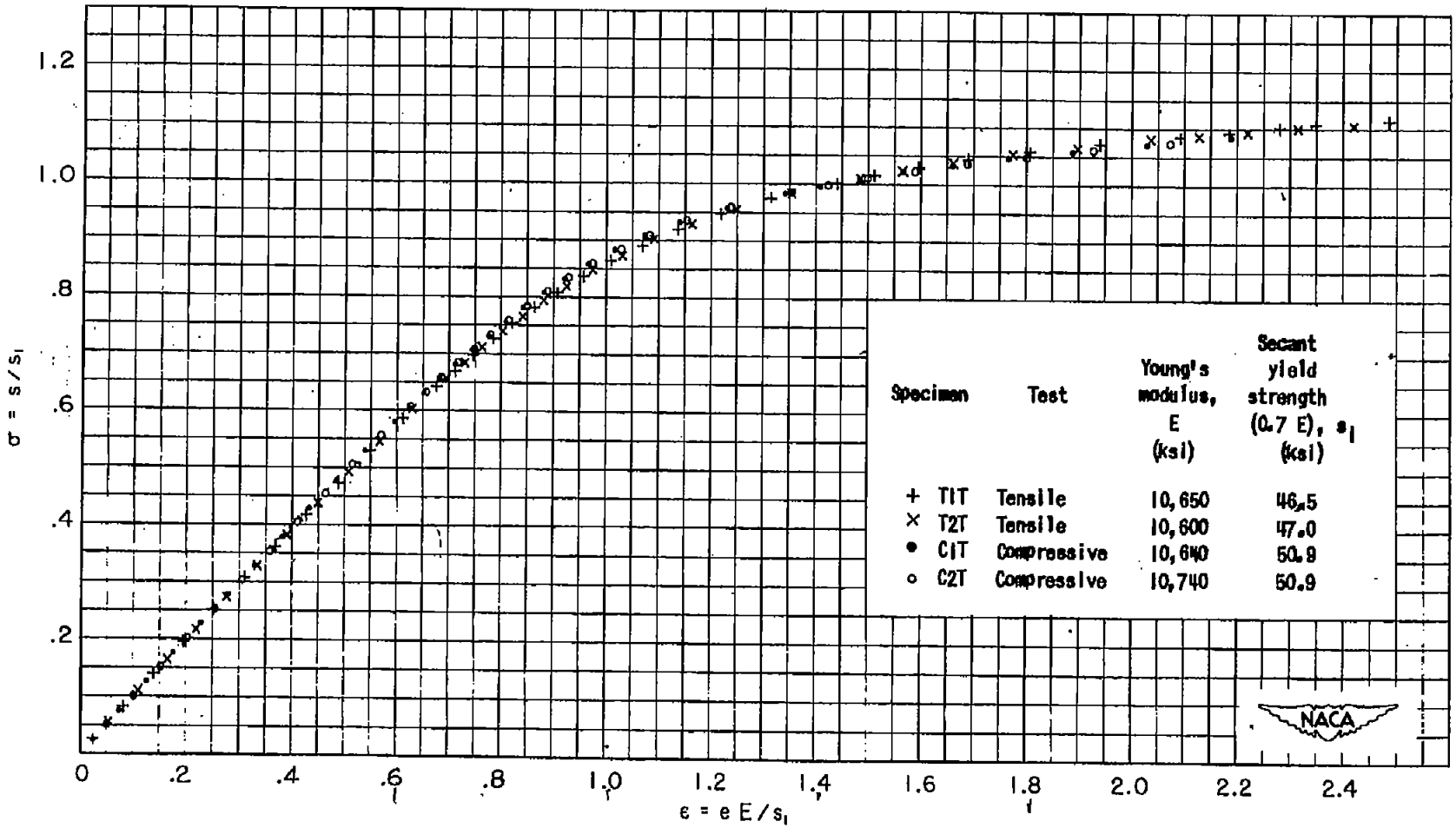

Figure 6.- Dimensionless stress-strain graphs. Alclad 24S-T sheet, transverse specimens 0.125 inch thick.

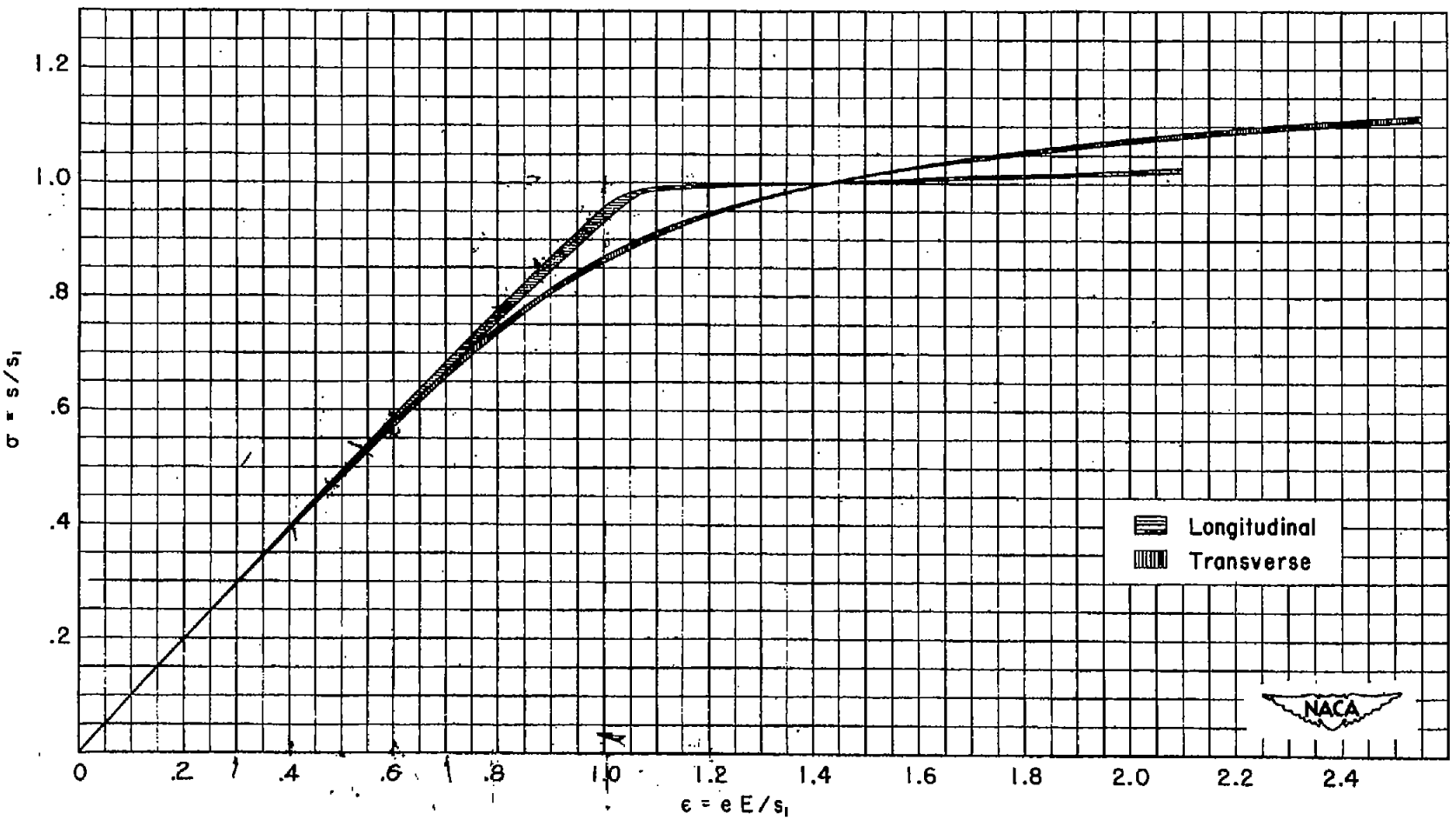

Figure 7.- Limits of dimensionless tensile stress-strain graphs. Alclad 24S-T sheets 0.032 0.064, and 0.125 inch thick.

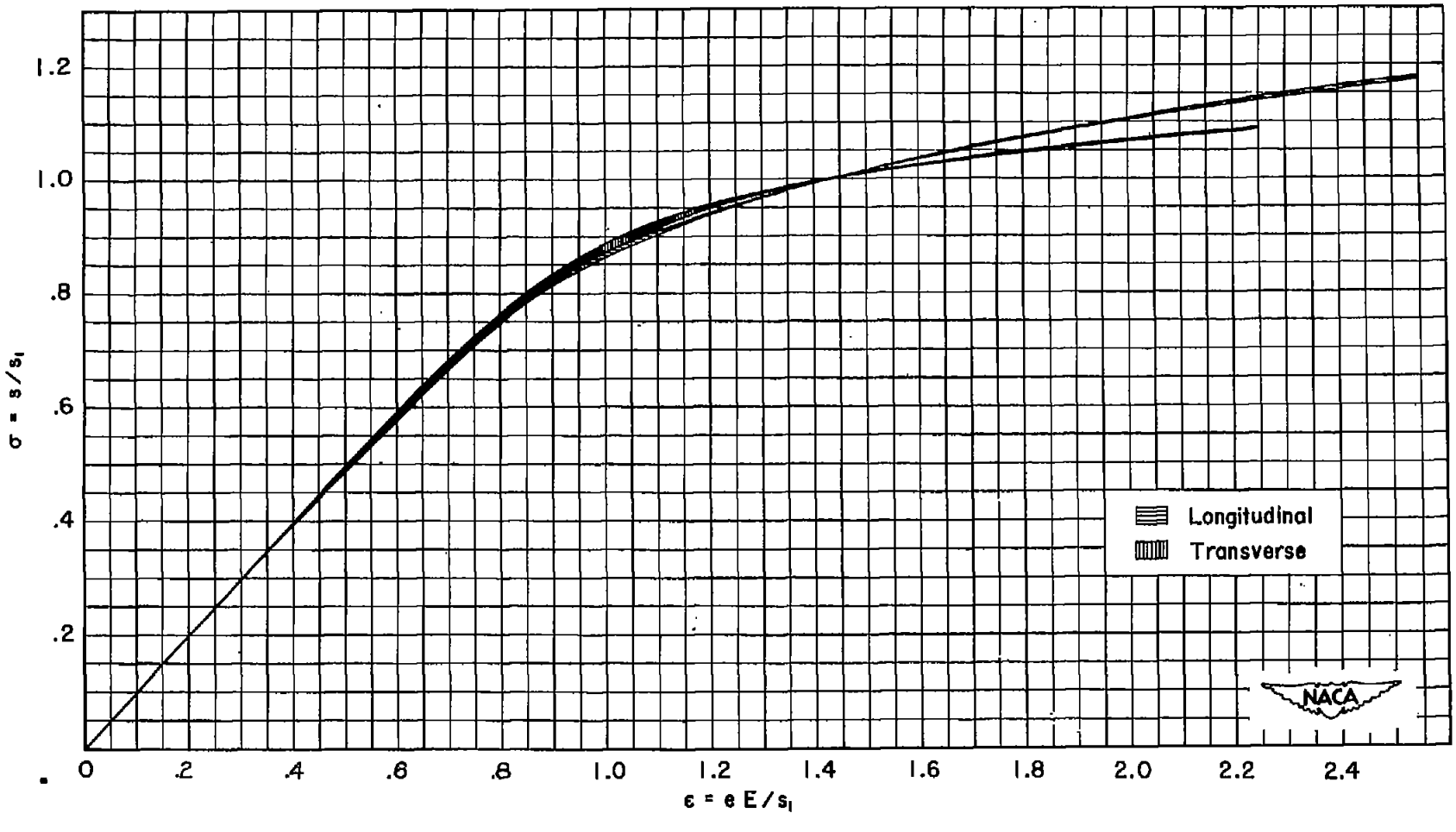

Figure 8.- Limits of dimensionless compressive stress-strain graphs. Alclad 24S-T sheets 0.032, 0.064, and 0.125 inch thick.

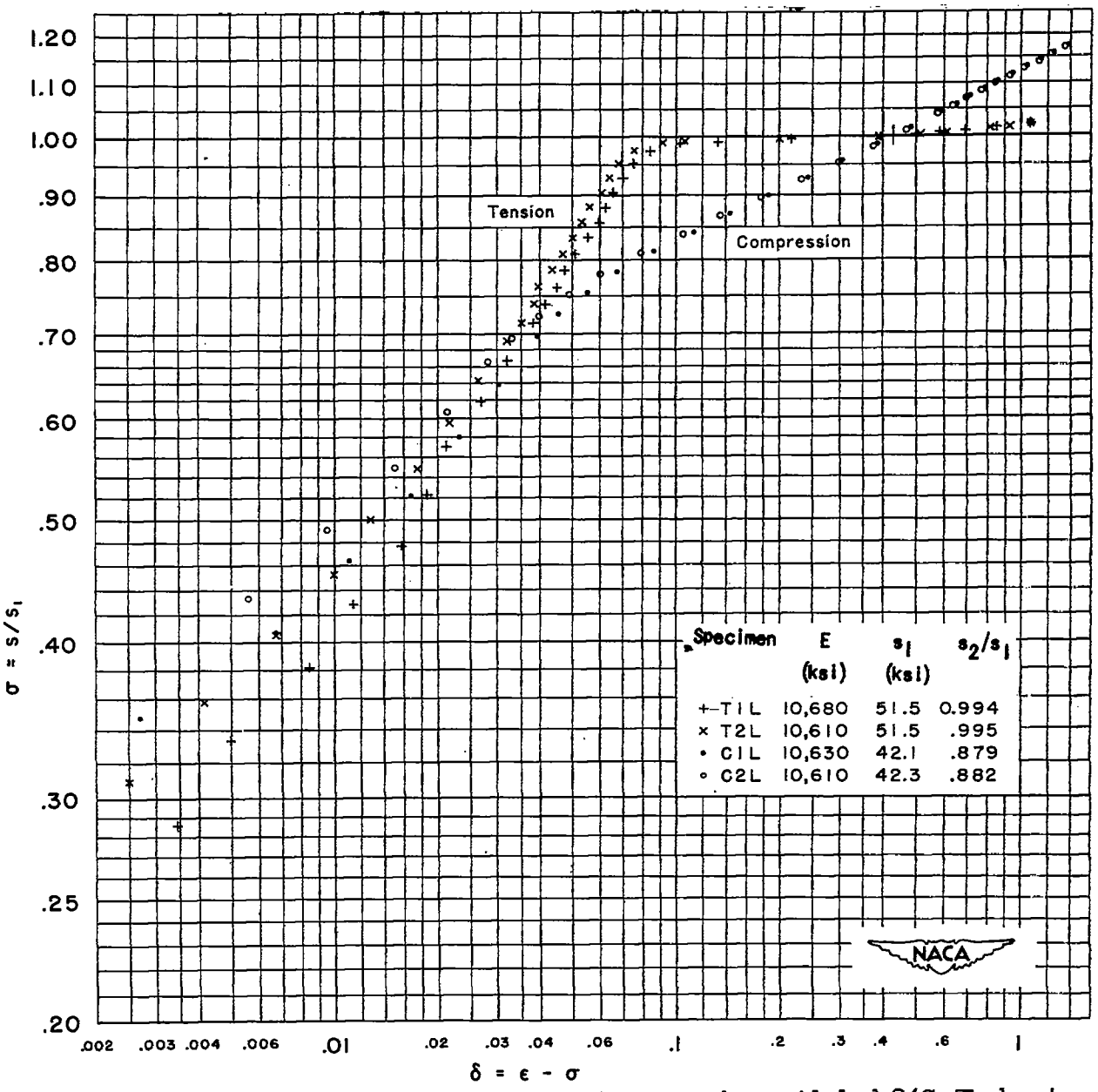

Figure 9.- Dimensionless stress-deviation graphs. Alclad 24S-T sheet, longitudinal specimens 0.032 inch thick. E, Young's modulus; s_1, secant yield strength (0.7 E); s_2, secant yield strength (0.85 E).

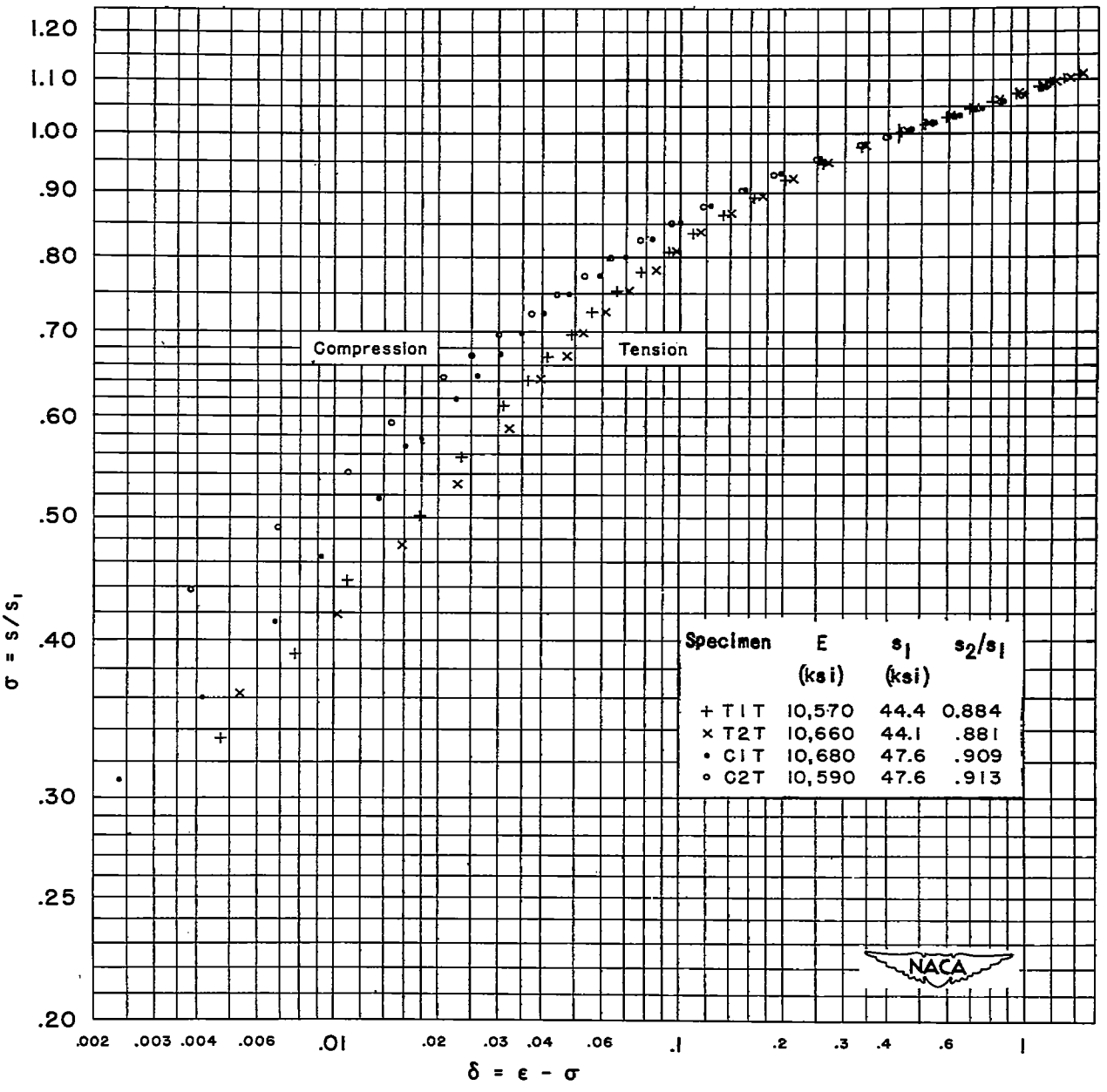

Figure 10.- Dimensionless stress-deviation graphs. Alclad 24S-T sheet, transverse specimens 0.032 inch thick. E, Young's modulus; s_1, secant yield strength (0.7 E); s_2, secant yield strength (0.85 E).

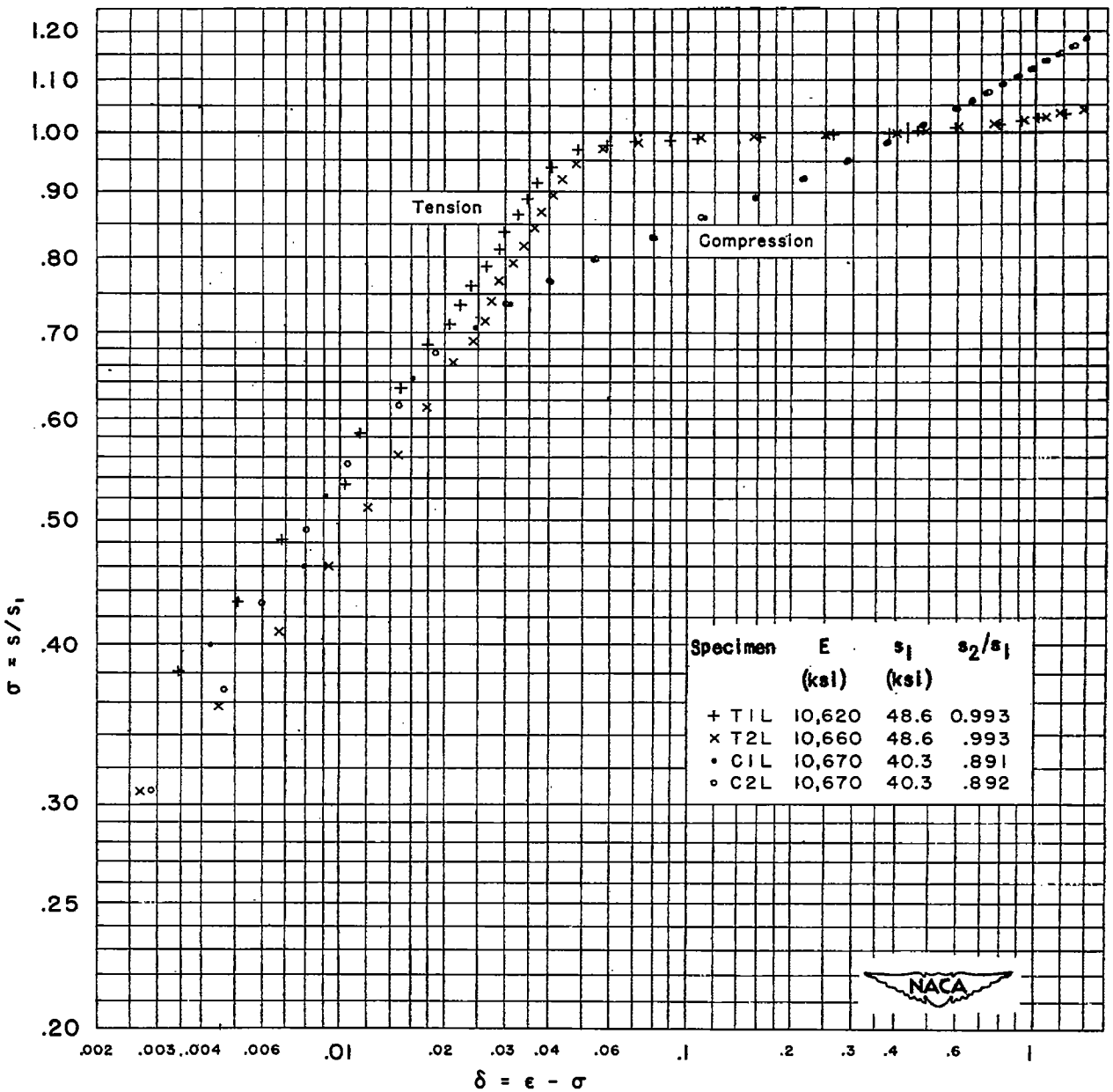

Figure 11.- Dimensionless stress-deviation graphs. Alclad 24S-T sheet, longitudinal specimens 0.064 inch thick. E, Young's modulus; s_1, secant yield strength (0.7 E); s_2, secant yield strength (0.85 E).

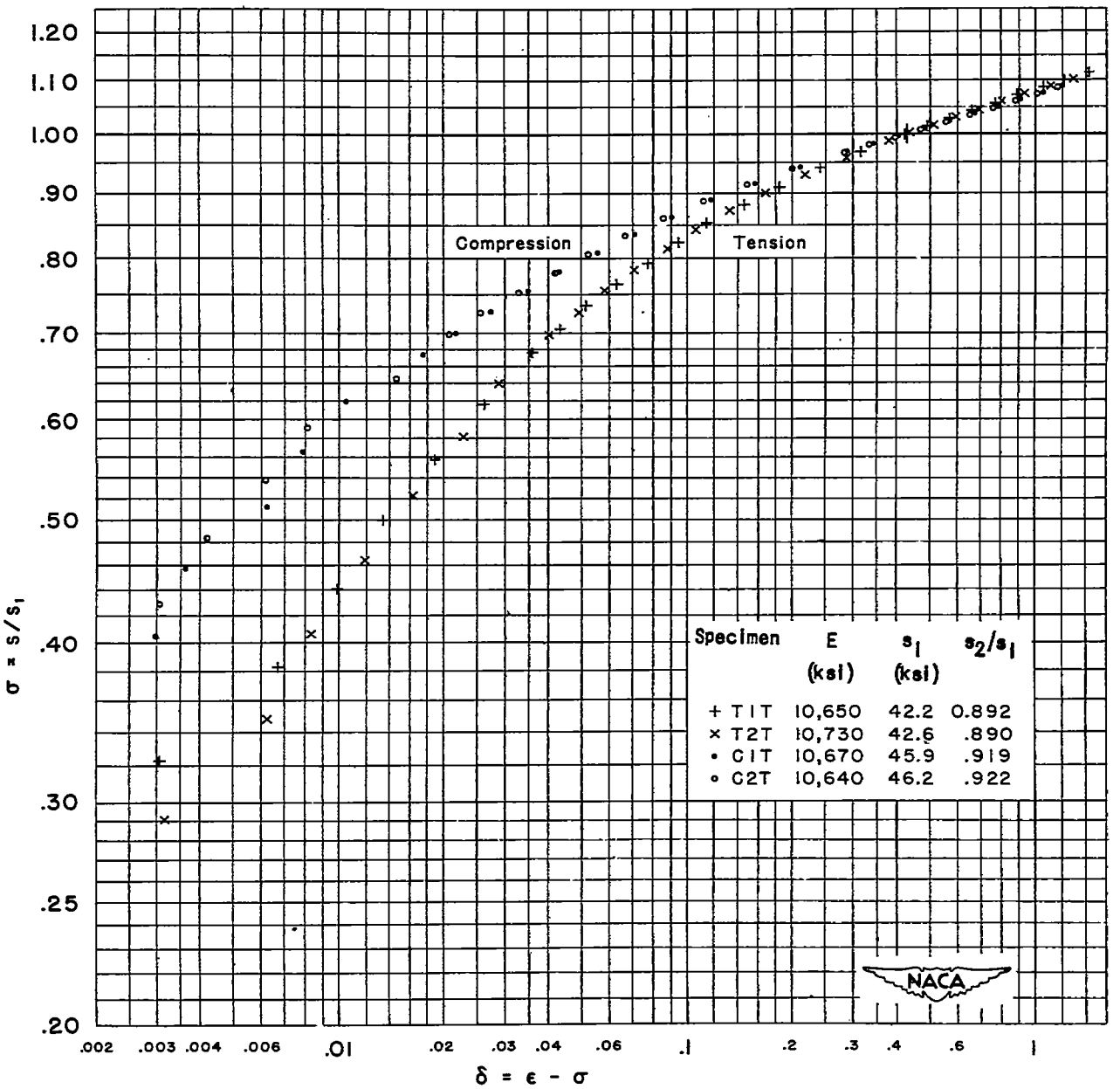

Figure 12.- Dimensionless stress-deviation graphs. Alclad 24S-T sheet, transverse specimens 0.064 inch thick. E, Young's modulus; s_1, secant yield strength (0.7 E); s_2, secant yield strength (0.85 E).

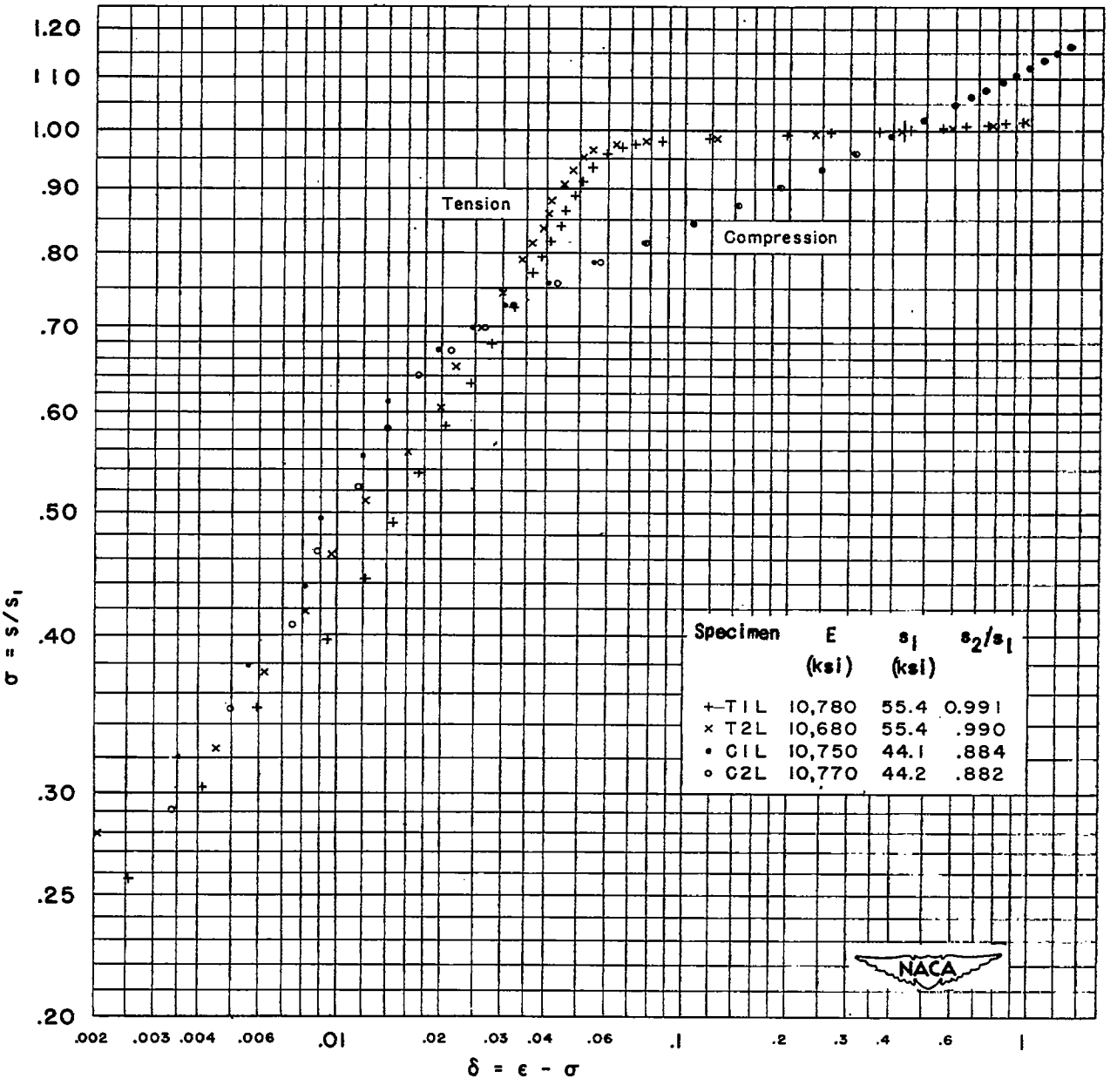

Figure 13.- Dimensionless stress-deviation graphs. Alclad 24S-T sheet, longitudinal specimens 0.125 inch thick. E, Young's modulus; s_1, secant yield strength (0.7 E); s_2, secant yield strength (0.85 E).

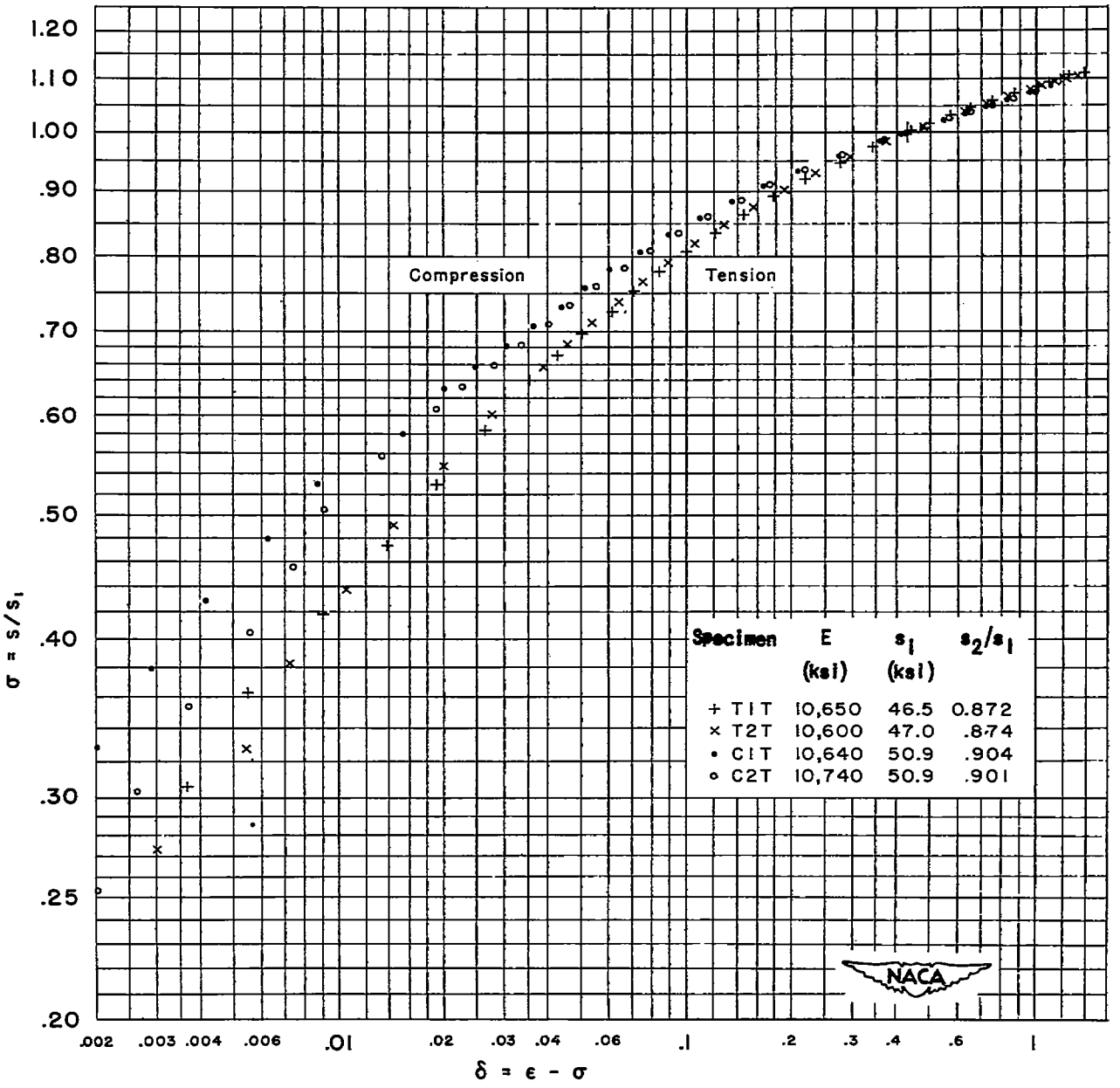

Figure 14.- Dimensionless stress-deviation graphs. Alclad 24S-T sheet, transverse specimens 0.125 inch thick. E, Young's modulus, s_1, secant yield strength (0.7 E); s_2, secant yield strength (0.85 E).

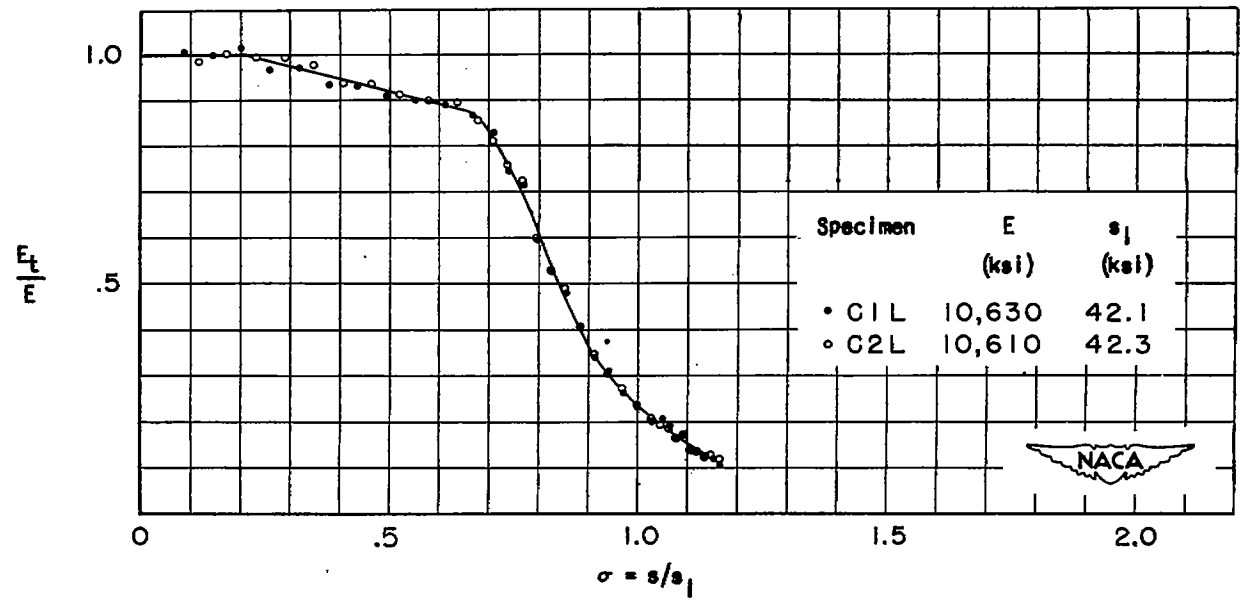

Figure 15.- Dimensionless compressive tangent modulus grapns. Alclad 24S-T sheet, longitudinal specimens 0.032 inch thick.

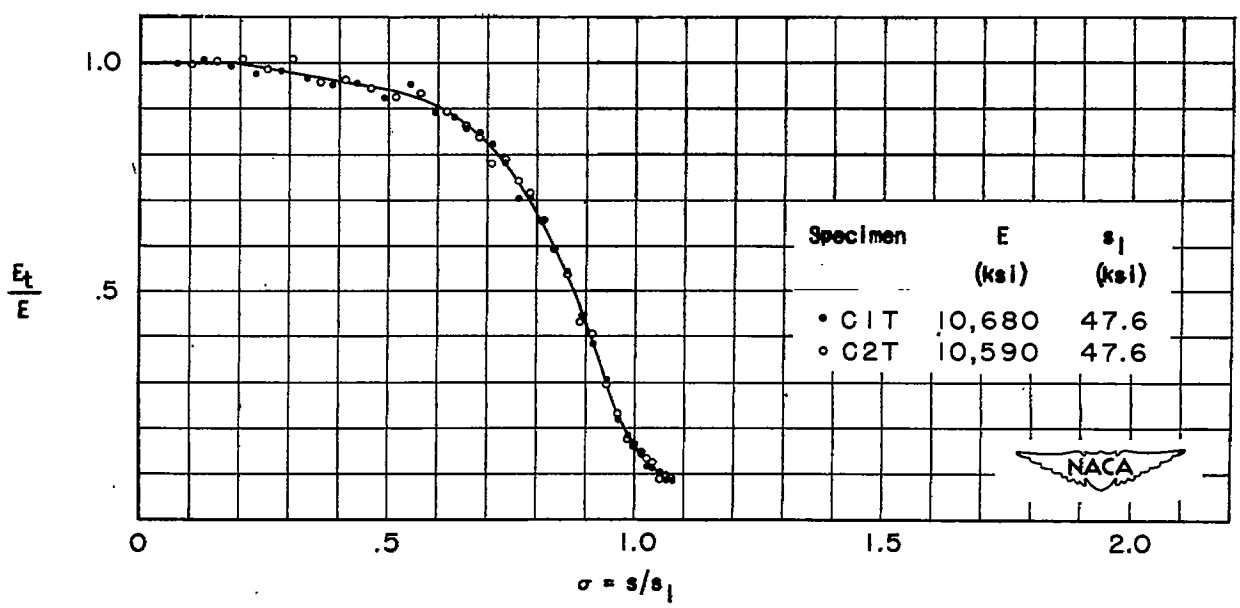

Figure 16.- Dimensionless compressive tangent modulus graphs. Alclad 24S-T sheet, transverse specimens 0.032 inch thick.

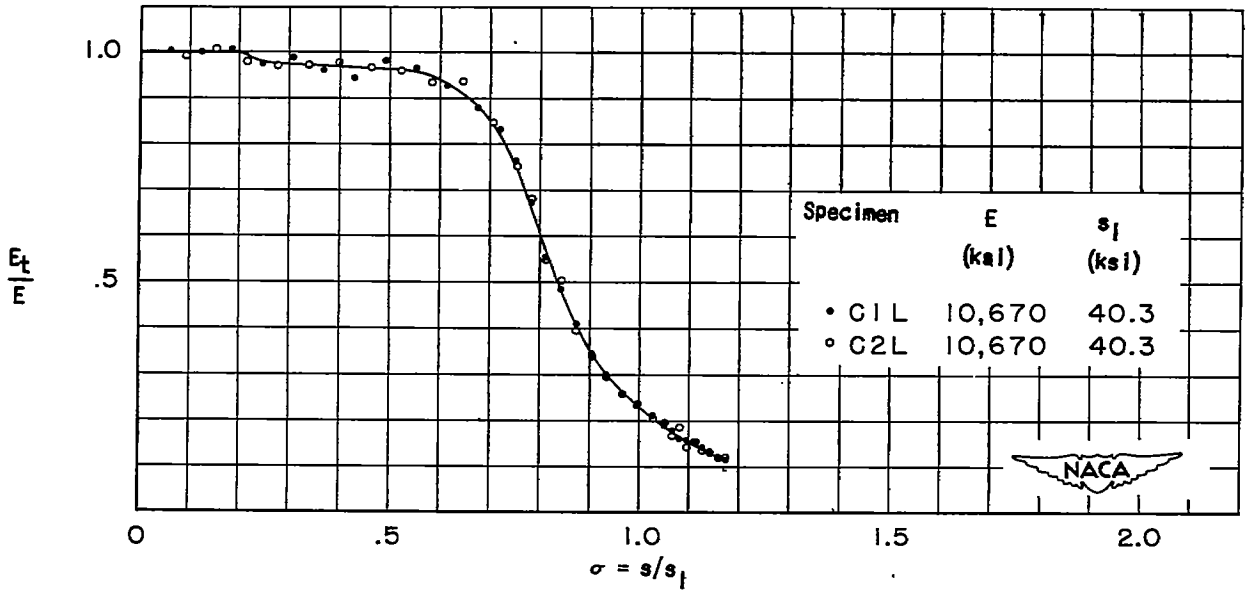

Figure 17.- Dimensionless compressive tangent modulus graphs. Alclad 24S-T sheet, longitudinal specimens 0.064 inch thick.

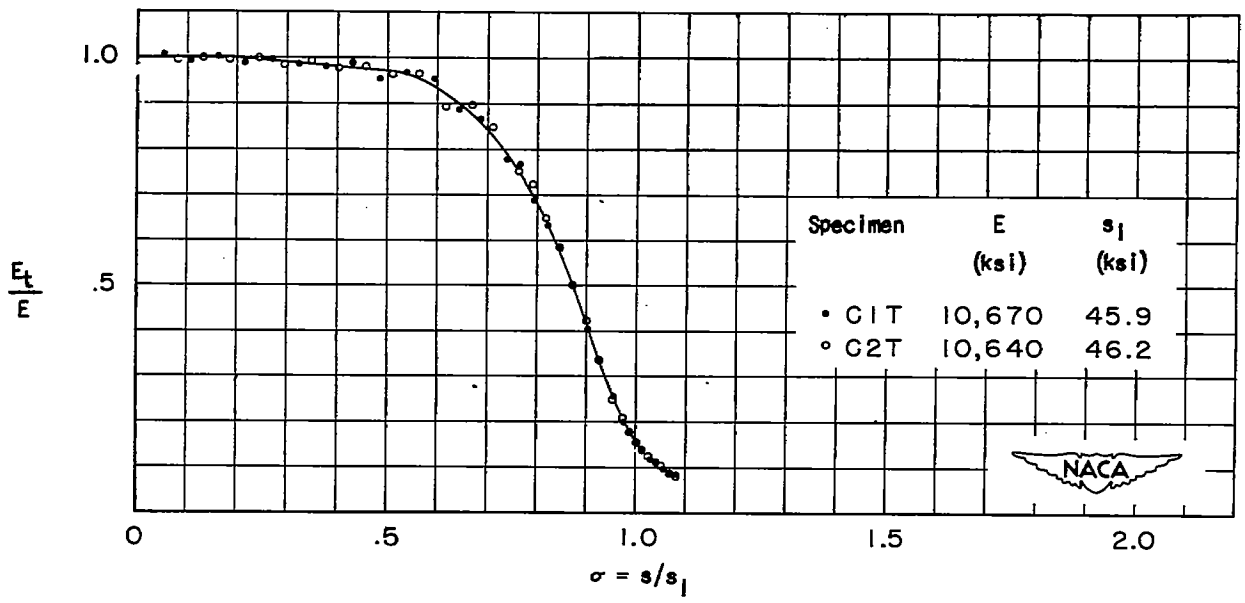

Figure 18.- Dimensionless compressive tangent modulus graphs. Alclad 24S-T sheet, transverse specimens 0.064 inch thick.

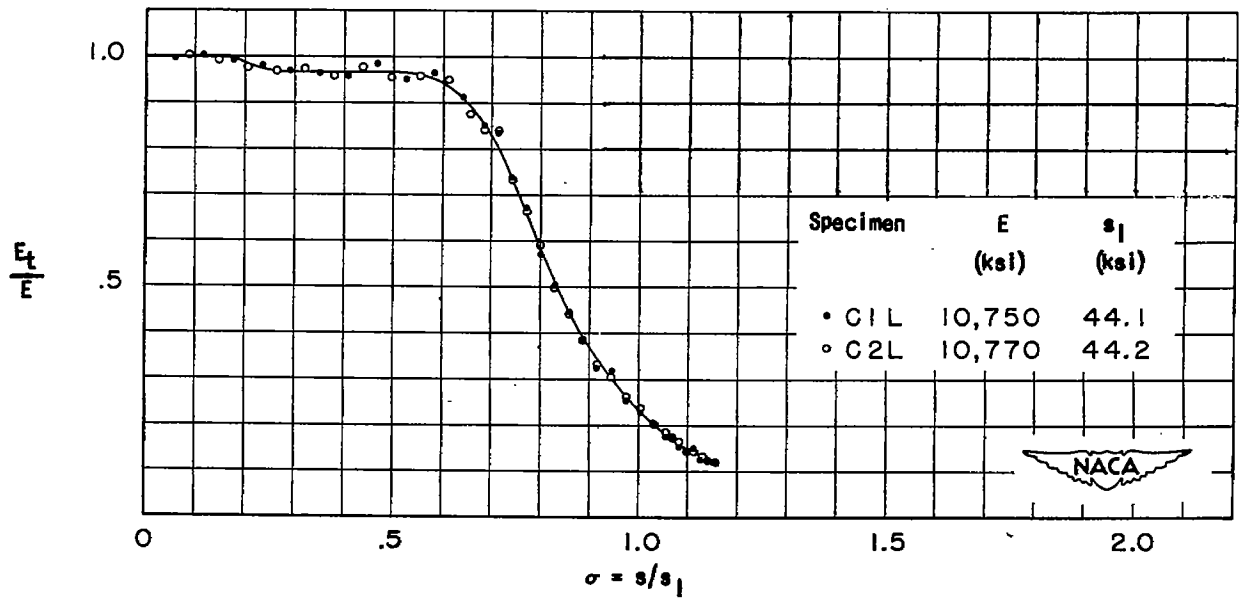

Figure 19.- Dimensionless compressive tangent modulus graphs. Alclad 24S-T sheet, longitudinal specimens 0.125 inch thick.

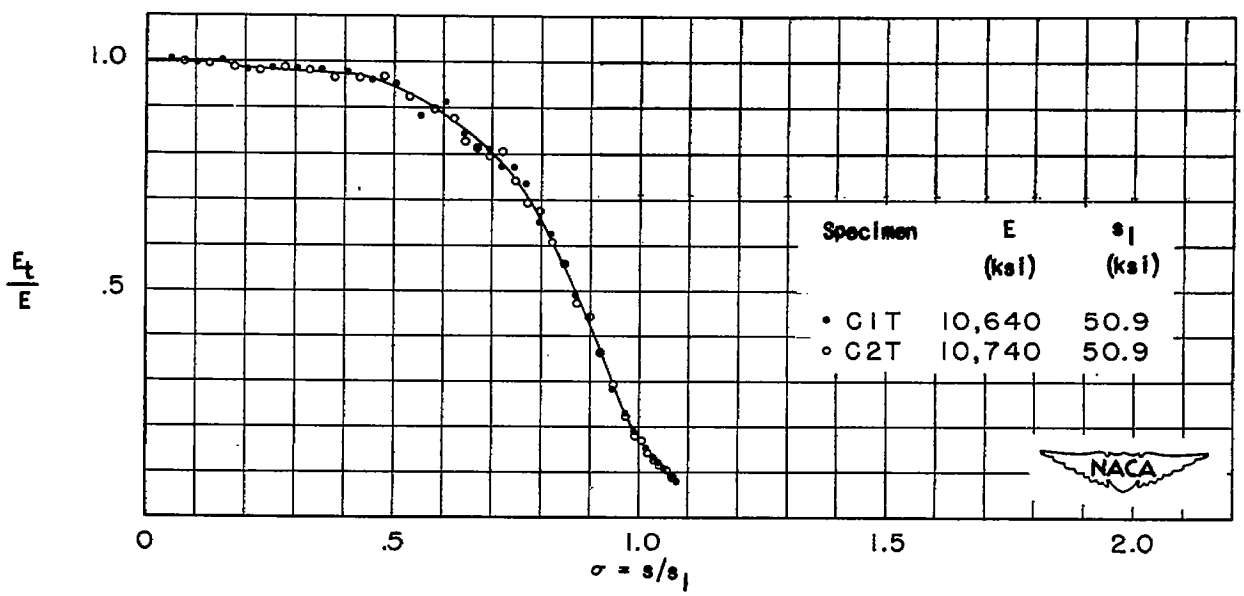

Figure 20.- Dimensionless compressive tangent modulus graphs. Alclad 24S-T sheet, transverse specimens 0.125 inch thick.

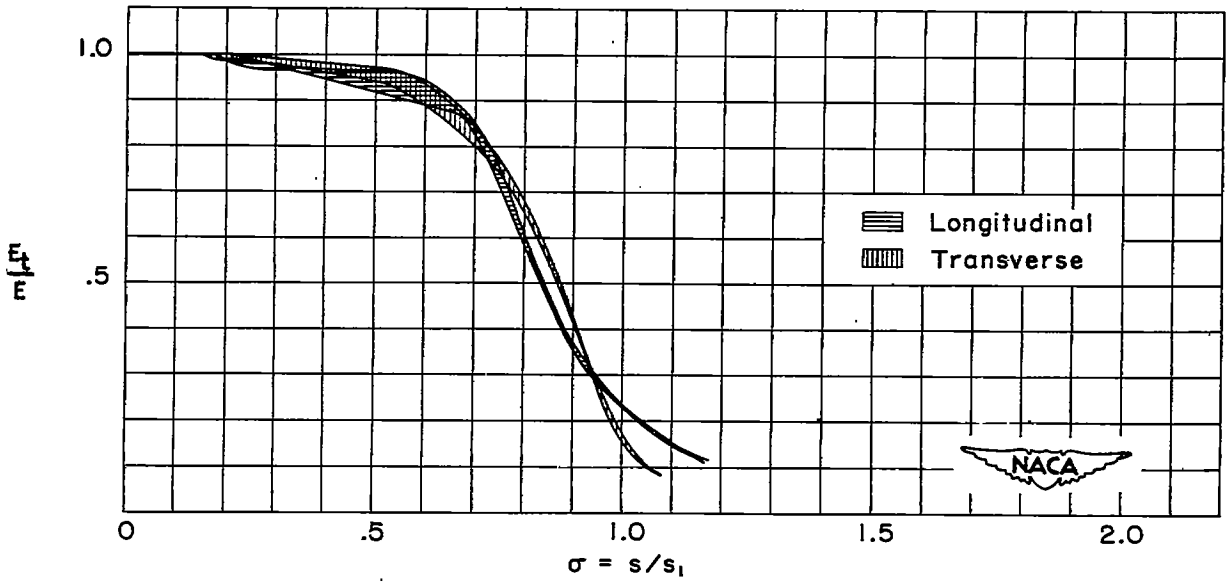

Figure 21.- Limits of dimensionless compressive tangent modulus graphs. Alclad 24S-T sheets 0.032, 0.064, and 0.125 inch thick.

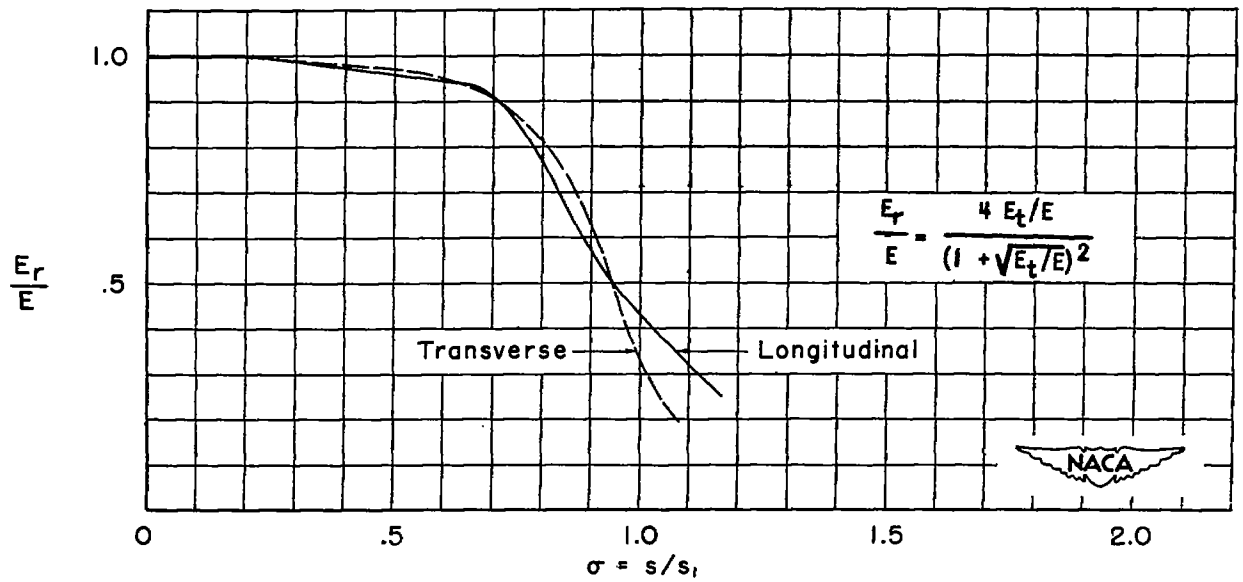

Figure 22.- Dimensionless compressive reduced modulus graphs, rectangular sections. Alclad 24S-T sheet 0.032 inch thick.

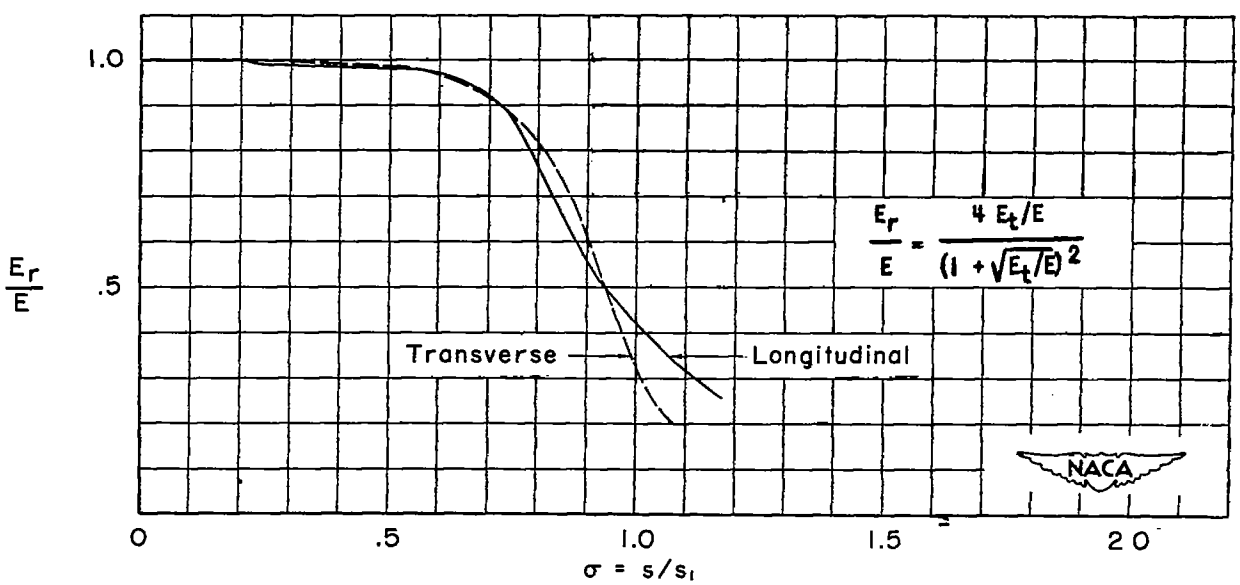

Figure 23.- Dimensionless compressive reduced modulus graphs, rectangular sections. Alclad 24S-T sheet 0.064 inch thick.

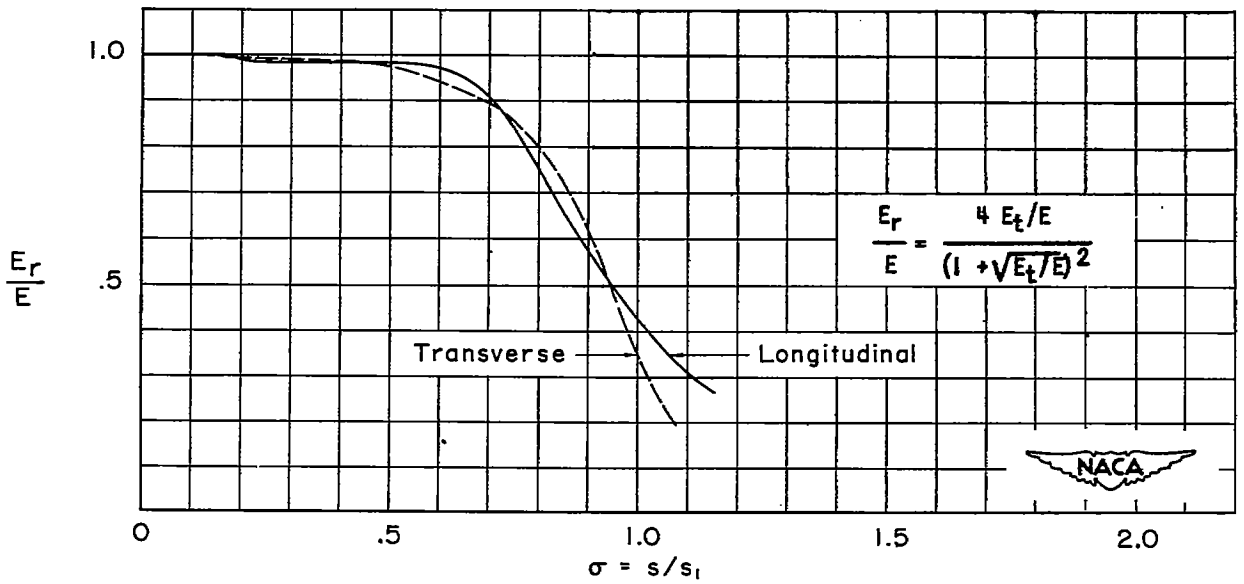

Figure 24.- Dimensionless compressive reduced modulus graphs, rectangular sections. Alclad 24S-T sheet 0.125 inch thick.

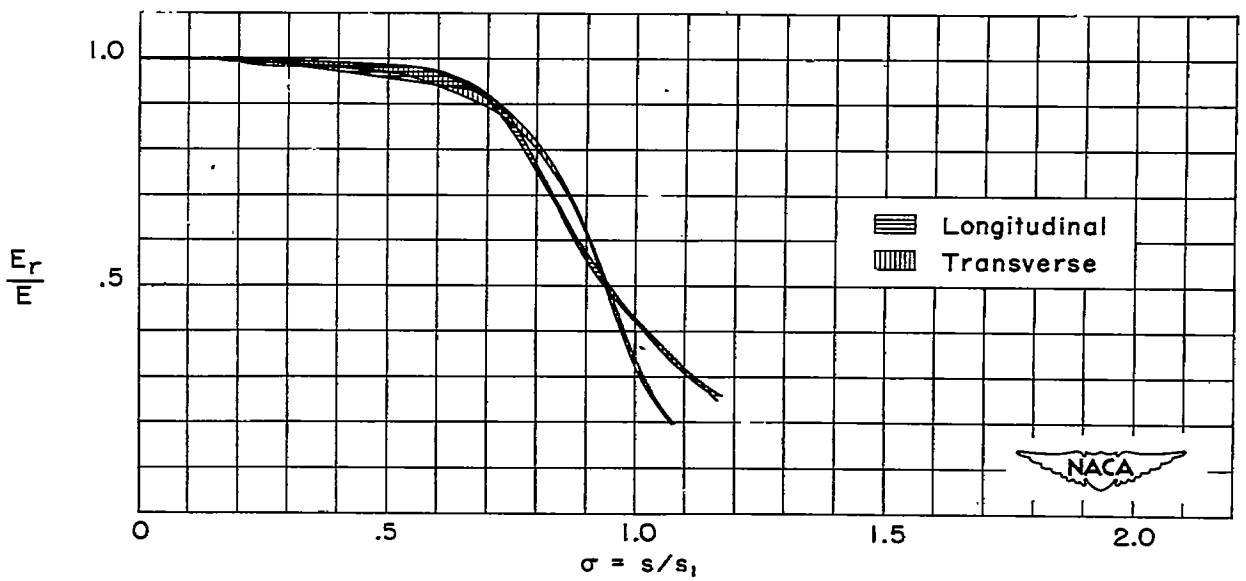

Figure 25.- Limits of dimensionless reduced modulus graphs for rectangular sections. Alclad 24S-T sheets 0.032, 0.064, and 0.125 inch thick.

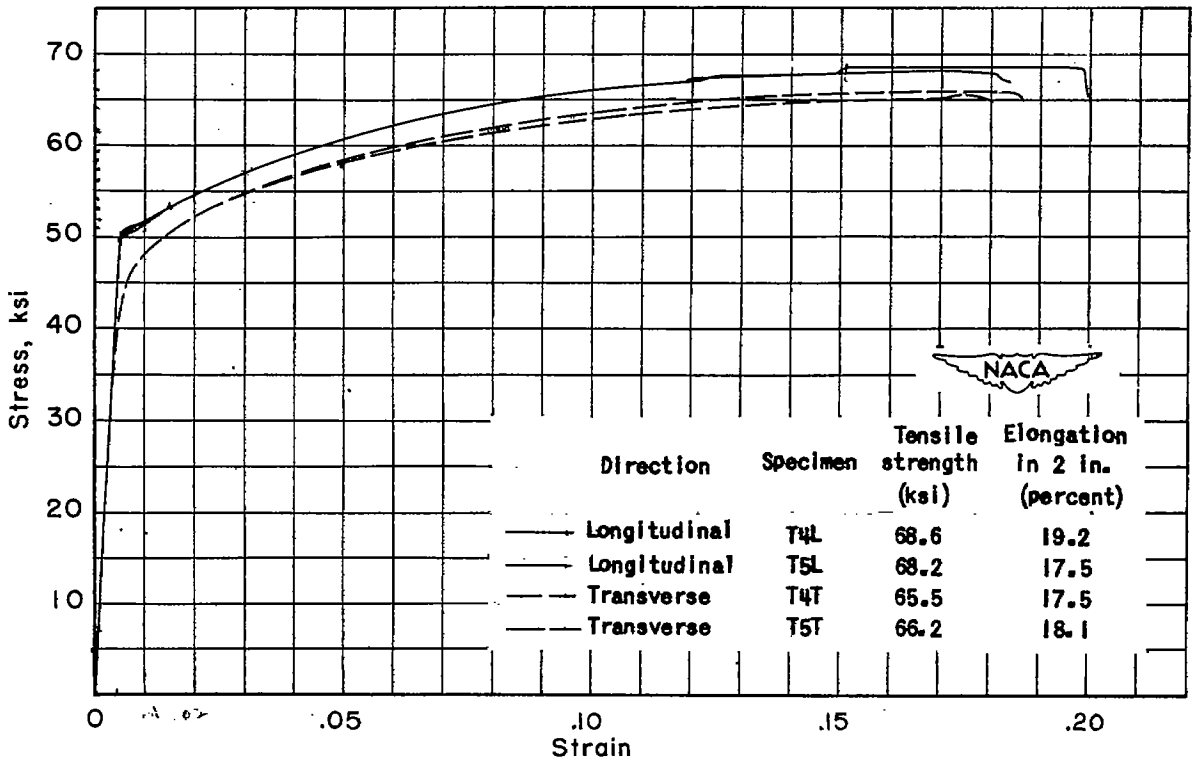

Figure 26.- Curves of tensile stress-strain tests to failure. Alclad 24S-T sheet 0.032 inch thick.

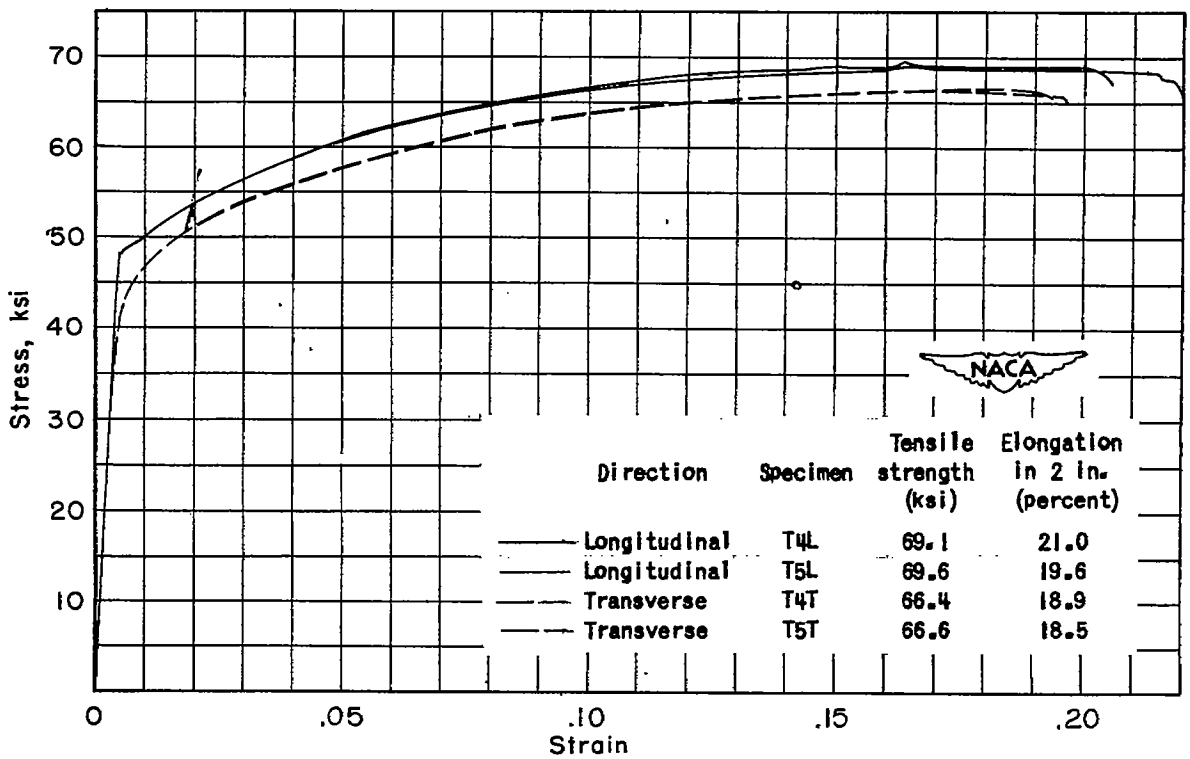

Figure 27.- Curves of tensile stress-strain tests to failure. Alclad 24S-T sheet 0.064 inch thick.

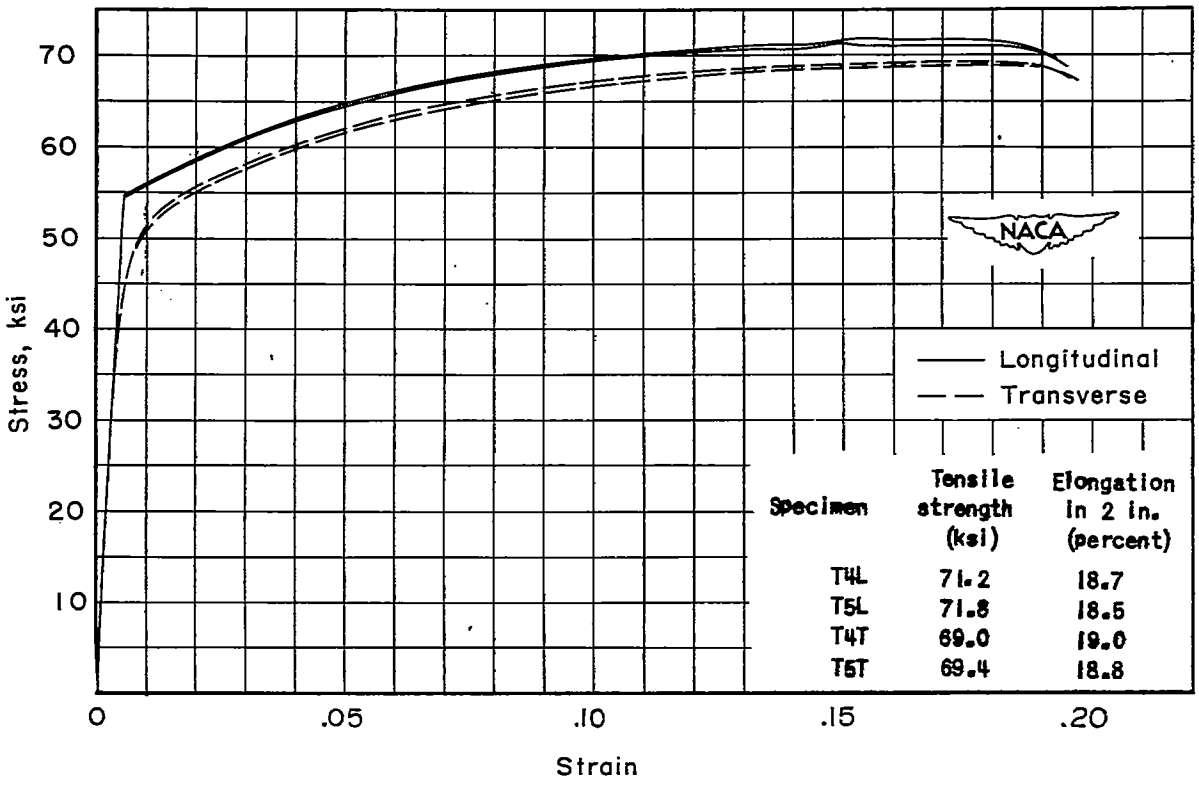

Figure 28.- Curves of tensile stress-strain tests to failure. Alclad 24S-T sheet 0.125 inch thick.

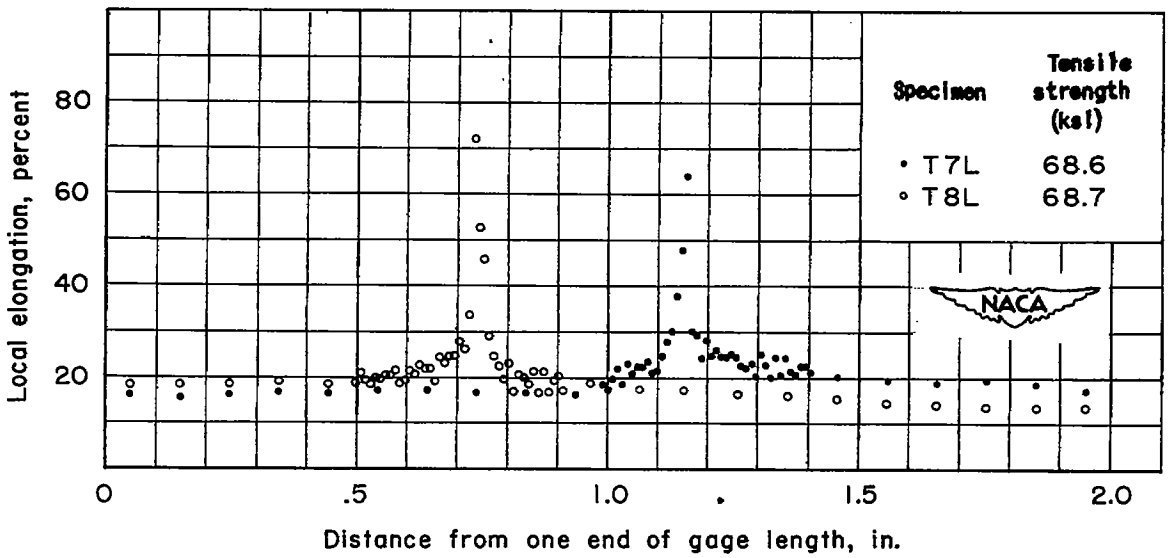

Figure 29.- Local elongation. Alclad 24S-T sheet, longitudinal specimens 0.032 inch thick.

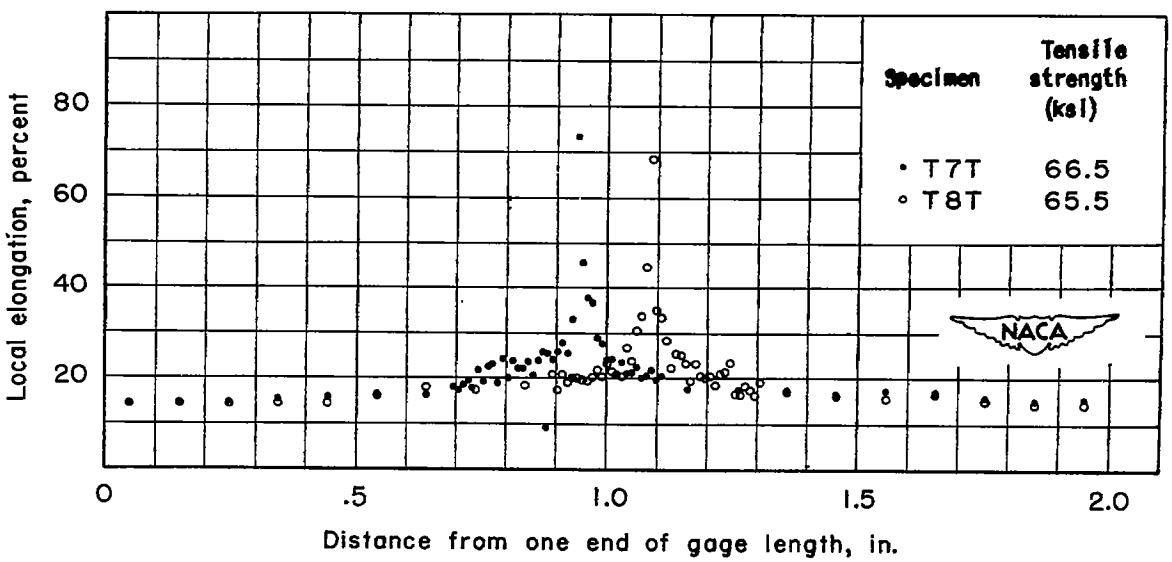

Figure 30.- Local elongation. Alclad 24S-T sheet, transverse specimens 0.032 inch thick.

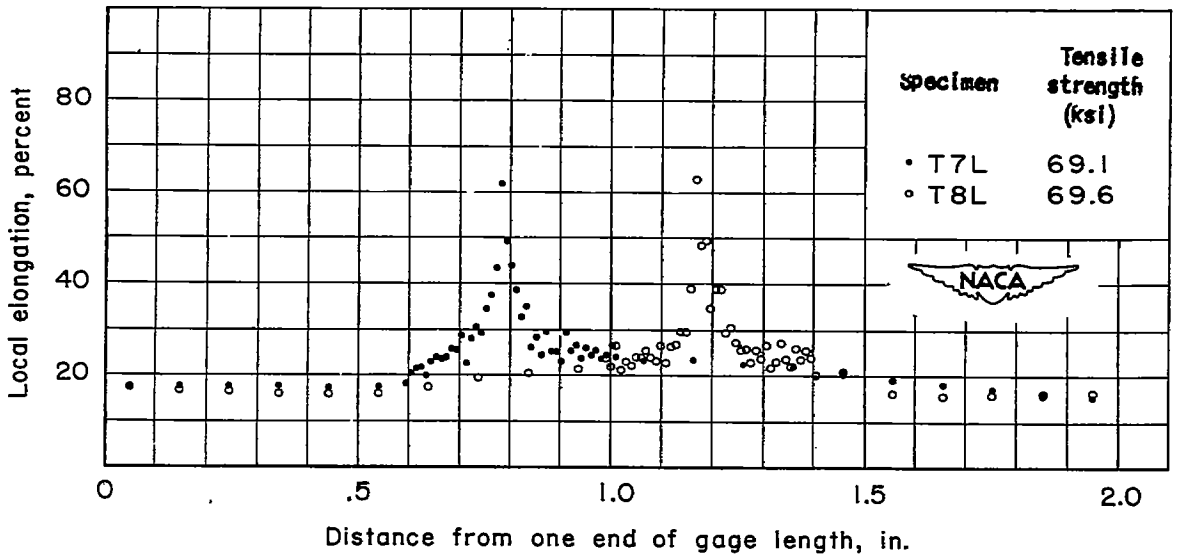

Figure 31.- Local elongation. Alclad 24S-T sheet, longitudinal specimens 0.064 inch thick.

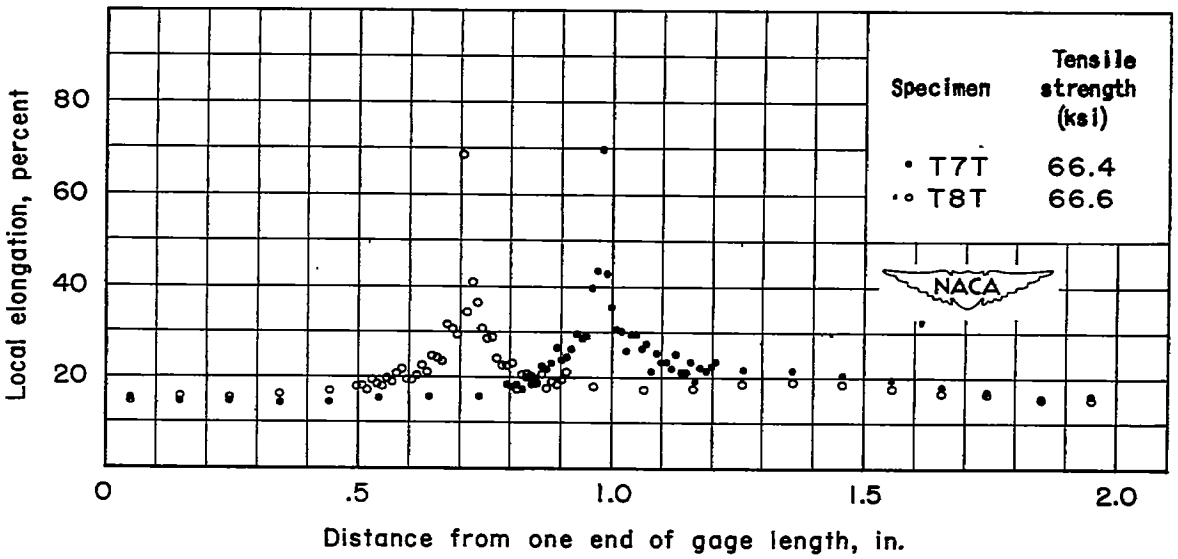

Figure 32.- Local elongation. Alclad 24S-T sheet, transverse specimens 0.064 inch thick.

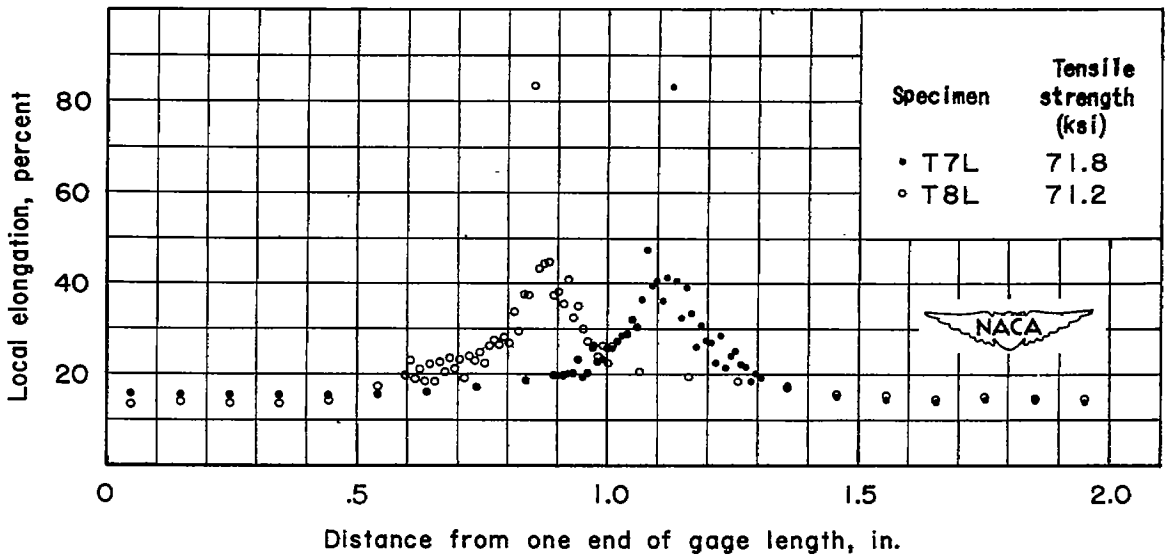

Figure 33.- Local elongation. Alclad 24S-T sheet, longitudinal specimens 0.125 inch thick.

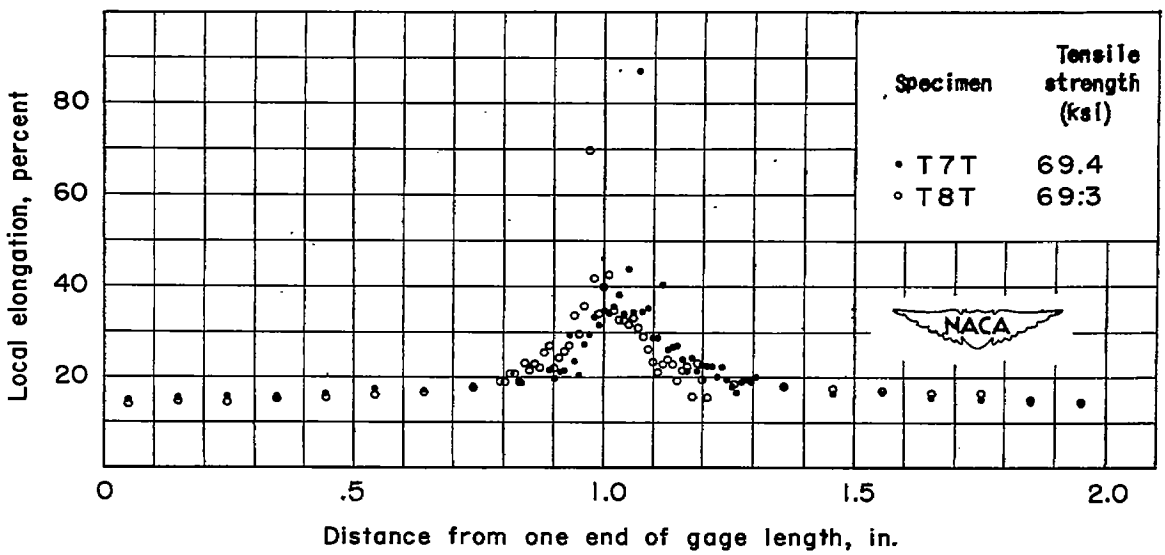

Figure 34.- Local elongation. Alclad 24S-T sheet, transverse specimens 0.125 inch thick.

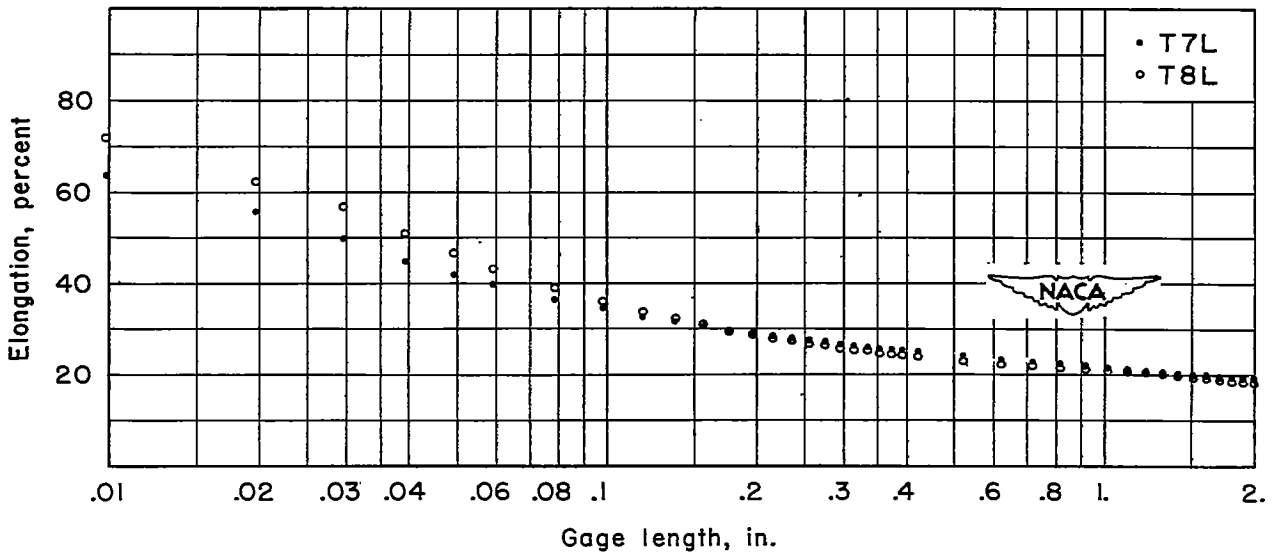

Figure 35.- Graphs of elongation against gage length. Alclad 24S-T sheet, longitudinal specimens 0.032 inch thick.

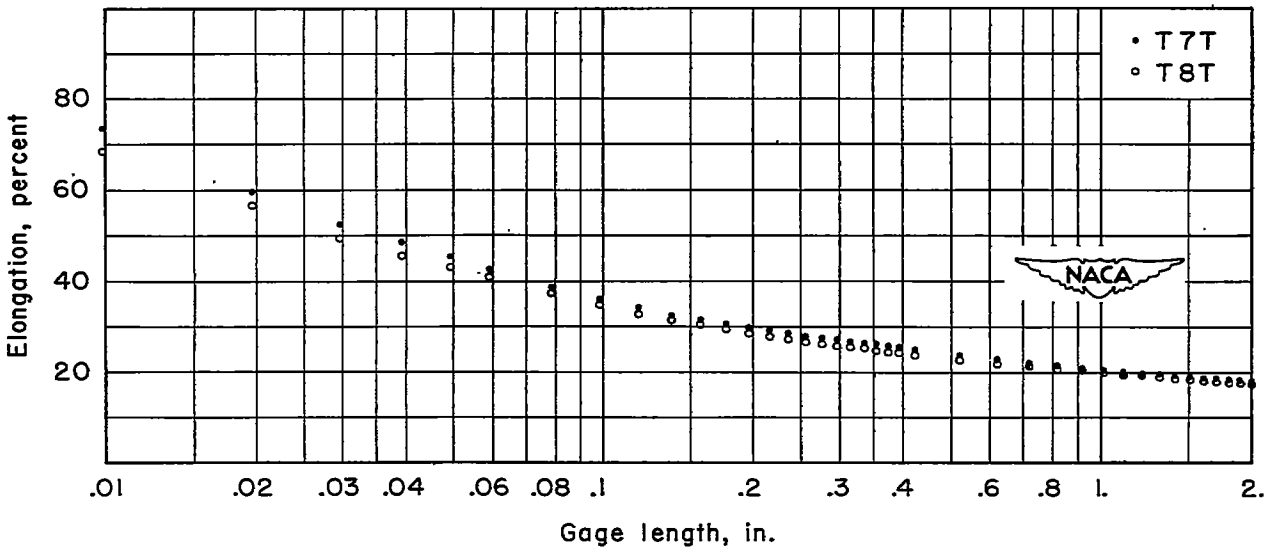

Figure 36.- Graphs of elongation against gage length. Alclad 24S-T sheet, transverse specimens 0.032 inch thick.

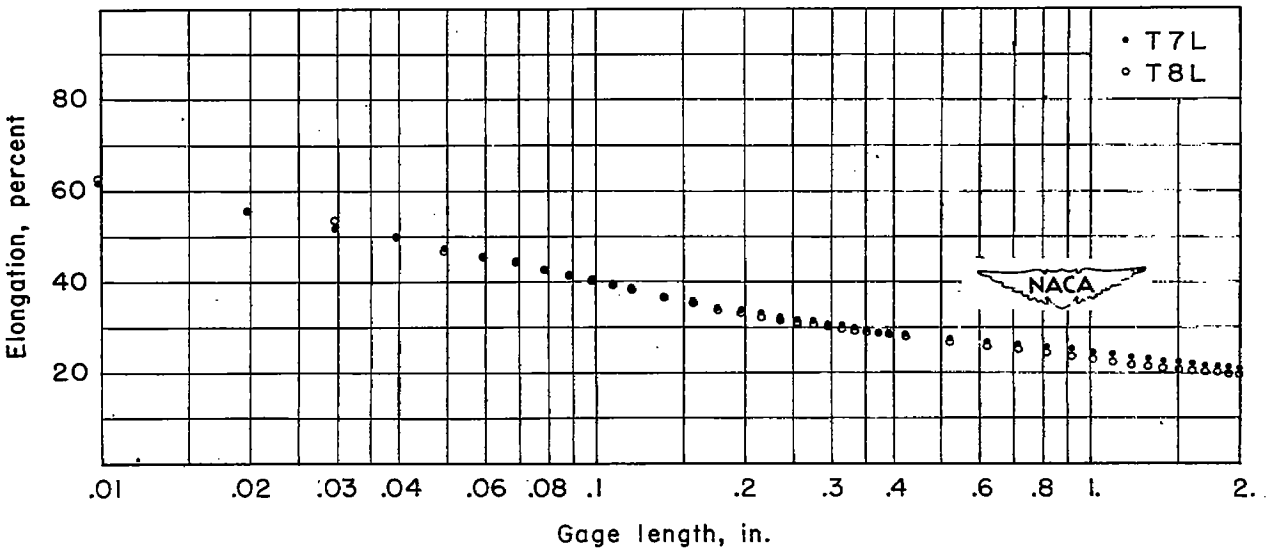

Figure 37.- Graphs of elongation against gage length. Alclad 24S-T sheet, longitudinal specimens 0.064 inch thick.

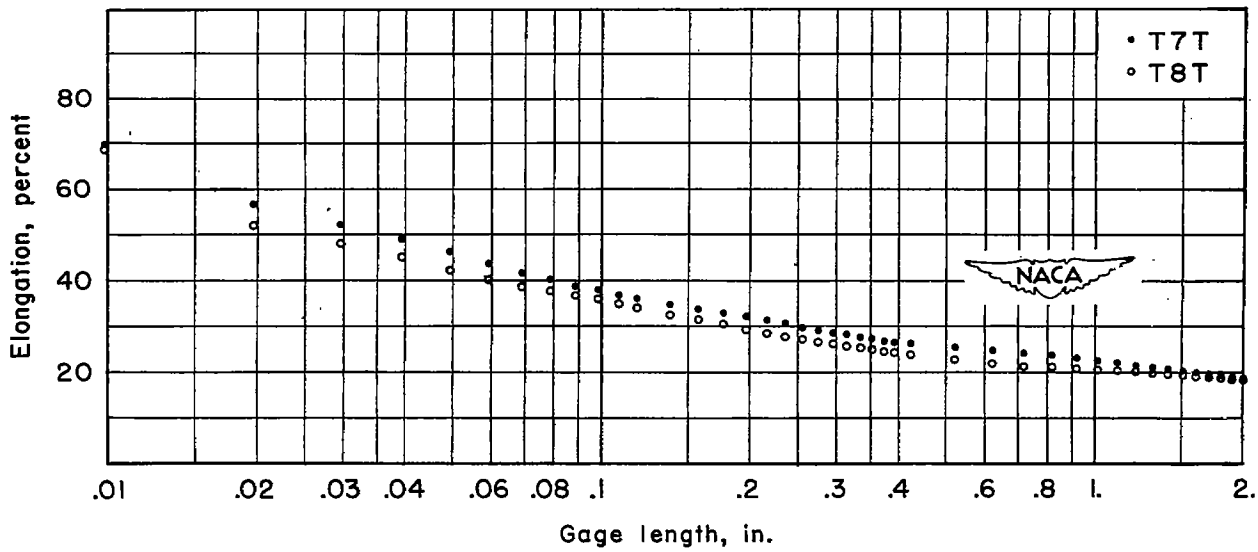

Figure 38.- Graphs of elongation against gage length. Alclad 24S-T sheet, transverse specimens 0.064 inch thick.

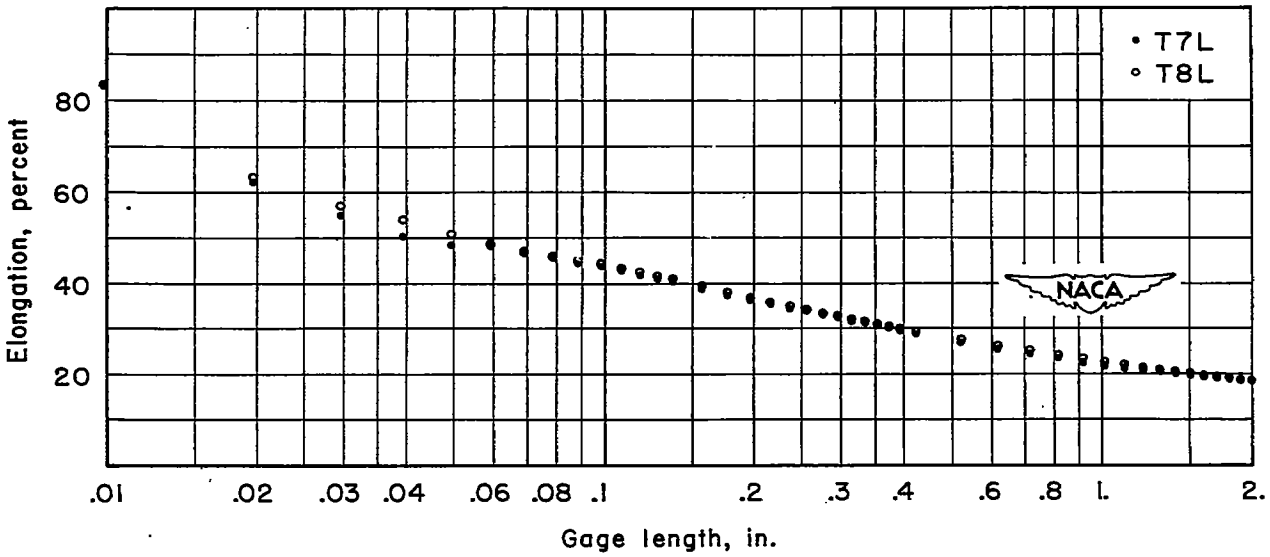

Figure 39.- Graphs of elongation against gage length. Alclad 24S-T sheet, longitudinal specimens 0.125 inch thick.

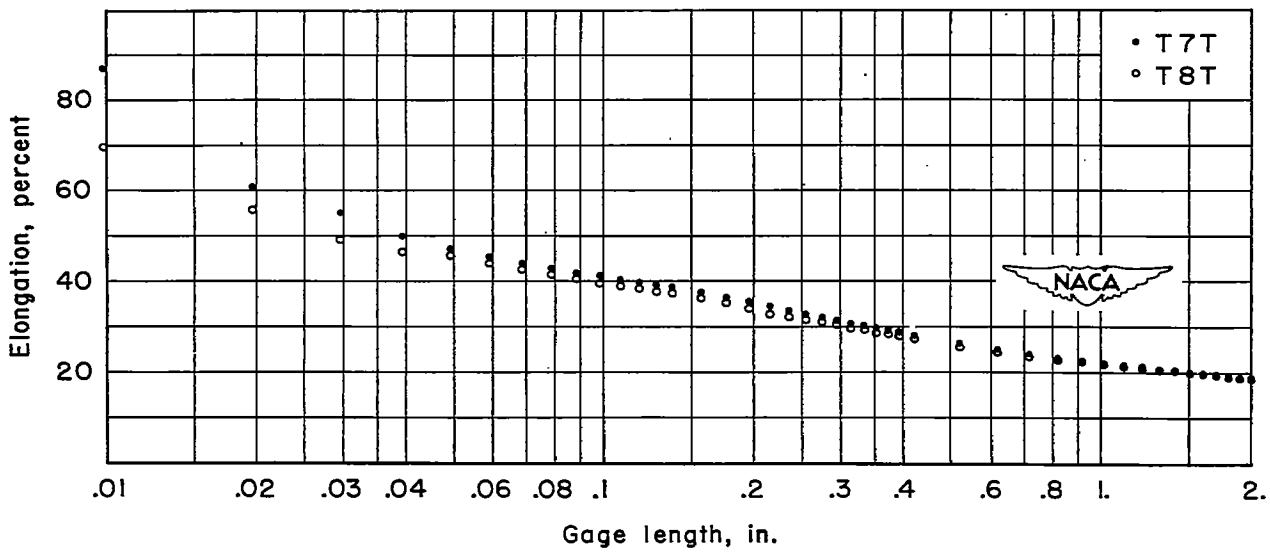

Figure 40.- Graphs of elongation against gage length. Alclad 24S-T sheet, transverse specimens 0.125 inch thick.